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Comune di Ponzano Veneto

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**Servizio di redazione del progetto definitivo,
AMPLIAMENTO E DEMOLIZIONE DELLA SCUOLA
SECONDARIA DI PRIMO GRADO GALILEO GALILEI - 1°
LOTTO FUNZIONALE -AMPLIAMENTO.**

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**SERVIZIO DI REDAZIONE DEL PROGETTO DEFINITIVO, AMPLIAMENTO
E DEMOLIZIONE DELLA SCUOLA SECONDARIA DI PRIMO GRADO
GALILEO GALILEI**

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Titolo elaborato/documenttitle

RELAZIONE DI CALCOLO DELLE STRUTTURE

RELAZIONE SULLE FONDAZIONI

VALIDAZIONE DEI RISULTATI

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1 INTRODUZIONE

La presente relazione riguarda il dimensionamento delle strutture per l'edificazione di un edificio scolastico nel Comune di Ponzano Veneto (TV), elenca la normativa di riferimento utilizzata, riporta i carichi permanenti ed accidentali, specifica le caratteristiche dei materiali, descrive le ipotesi di calcolo assunte nelle operazioni di progetto e dimostra le calcolazioni e le verifiche strutturali condotte. Le verifiche strutturali sono descritte, attraverso la rappresentazione degli schemi statici di calcolo e la verifica delle sezioni caratteristiche.

1.1 *Descrizione Generale dell'opera*

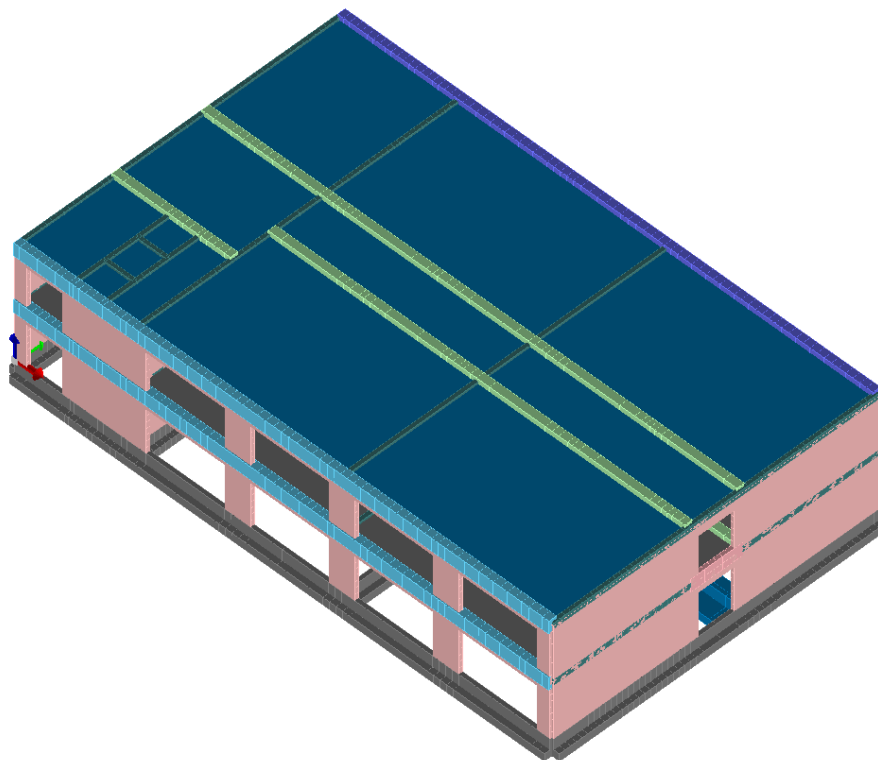
Il progetto architettonico prevede la nuova edificazione di un complesso scolastico composto dalla scuola di dimensioni 36,20 x 22,10 m, disposta su due piani con altezza pari a 7.94 m, e dalla palestra di dimensioni 32,15 x 33,50 m di altezza complessiva 9,30 m.

1.1 *Descrizione Strutturale*

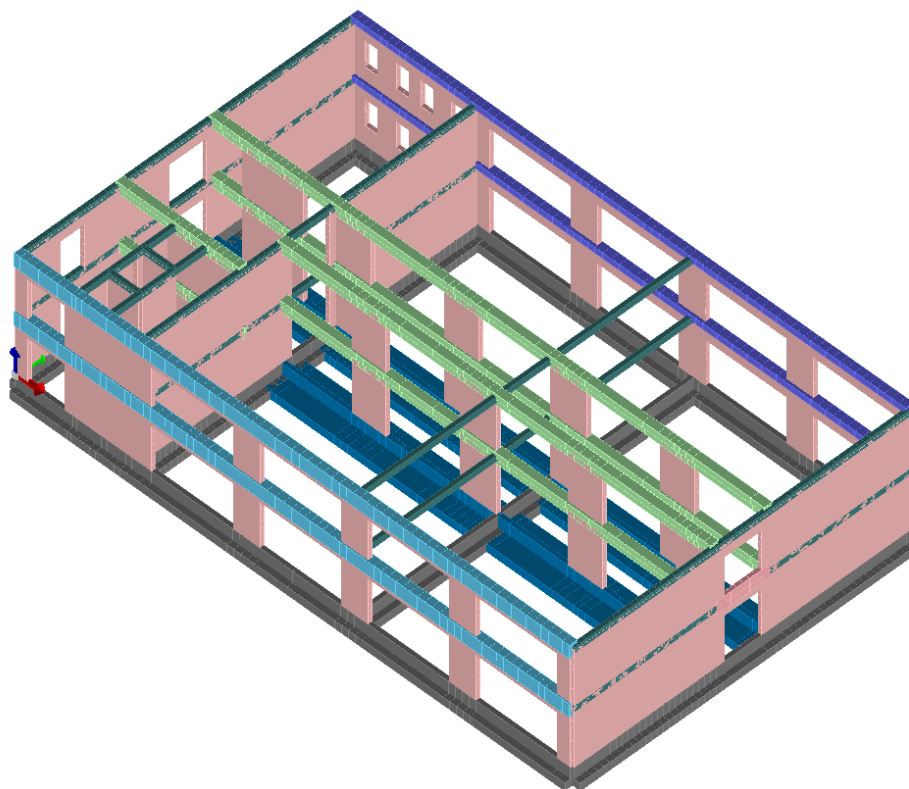
Il progetto strutturale prevede:

- fondazioni superficiali in c.a. a trave rovescia di base 100x50+25x75 cm, 150x50+25x75 cm ed 250x50+25x75 cm. Il copriferro delle strutture di fondazione è pari a 4 cm. *L'armatura delle travi rispetto il minimo previsto dalla NTC2018, §7.2.5 pari allo 0.2% ($100 \times 26 \times 0.001 = 2.6 \text{ cm}^2/\text{m}$);*
- setti in c.a. di spessore 25 cm a di altezza massima 930 cm (EC.2, §5.3.1, $h/b \geq 4$). *L'armatura dei setti rispettano la minima prevista dalla NTC2018, §7.4.6.2.2 pari allo 1%;*
- solai di piano in c.a. tipo Predalles di spessore 5+25+6 cm ad interasse 120 cm con alleggerimento in polistirolo;
- travi/cordolo del solaio di piano di sezione rettangolare 25x36 cm sopra i setti in c.a. e sezione a T di 25x50+50x36 cm e ad L 25x50+50x36 cm nelle zone senza setti di spina e perimetrali;
- solaio di copertura in c.a. tipo Predalles di spessore 5+25+6 cm ad interasse 120 cm con alleggerimento in polistirolo;
- travi/cordolo del solaio di copertura di sezione rettangolare 25x36 cm sopra i setti in c.a. e sezione a T di 25x50+50x36 cm e ad L 25x50+50x36 cm nelle zone senza setti di spina e perimetrali
- Copertura lignea della palestra realizzata con travi principali a doppia rastremazione di base 24 cm e altezza variabile da 160 a 200 cm ad interasse 700 cm, le travi secondarie lignee

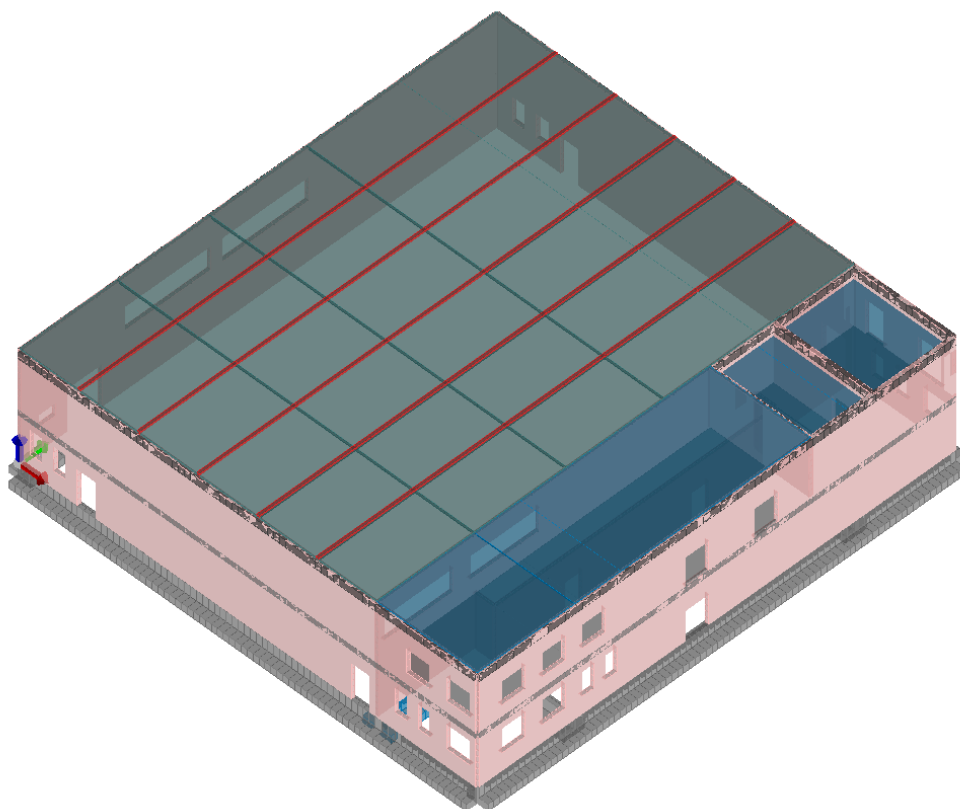
hanno sezione 20x40 cm ad interasse 350 cm. Soprastante le travi è presente un pannello sandwich isolante di spessore 20 cm;



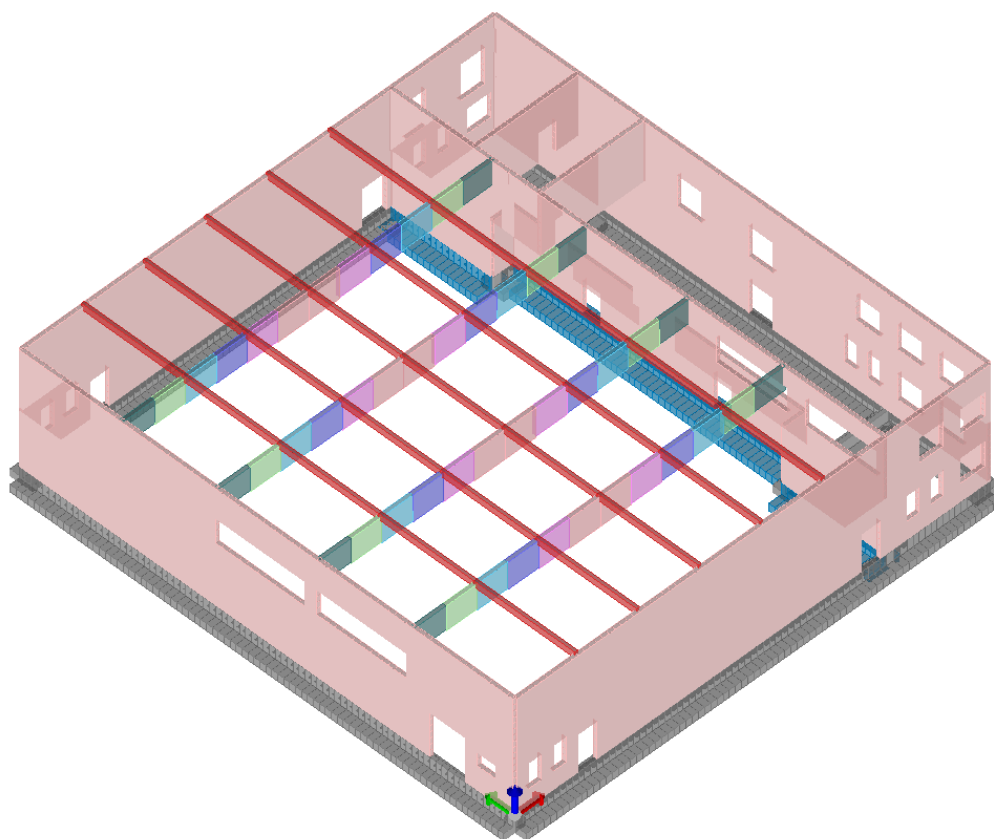
Vista 3D della scuola



Vista 3D della scuola senza impalcati



Vista 3D della palestra



Vista 3D della palestra senza impalcati

2 **NORMATIVA DI RIFERIMENTO**

Il progetto è stato redatto in osservanza delle **nuove norme tecniche per le costruzioni emanate con il Decreto Ministeriale del 17 gennaio 2018**. Per quanto non compiutamente descritto nella suddetta, si è fatto riferimento alle seguenti normative (di comprovata affidabilità):

PROGETTAZIONE STRUTTURALE

- L. 05.11.1971 n° 1086: "Norme per la disciplina delle opere in conglomerato cementizio armato, normale e precompresso ed a struttura metallica".
- L. 02.02.1974 n° 64: "Provvedimenti per le costruzioni con particolari prescrizioni per le zone sismiche".
- C.M. 21.01.2019 n° 7: "Istruzioni per l'applicazione delle Norme tecniche per le costruzioni di cui al decreto ministeriale 17 gennaio 2018".
- UNI ENV 1992-1-1 "Eurocodice 2 – Progettazione delle strutture di calcestruzzo – part.1-1"
- UNI ENV 1992-1-1 "Eurocodice 5 – Progettazione delle strutture in legno – part.1-1"

MATERIALI

- Decreto del Presidente della Repubblica 21.04.1993 n° 246: "Regolamento di attuazione della direttiva 89/106/CEE relativa ai prodotti da costruzione".
- C.M. 21.01.2019 n° 7: "Istruzioni per l'applicazione delle Norme tecniche per le costruzioni di cui al decreto ministeriale 17 gennaio 2018".
- UNI EN 206-1 "Specificazione, prestazione, produzione e conformità del calcestruzzo"
- UNI EN 1194 "Strutture di legno – Legno lamellare incollato"

3 GENERALITÀ SUL METODO DI CALCOLO E ANALISI

Le calcolazioni sono state condotte adottando il metodo semiprobabilistico agli stati limite; sono stati soddisfatti i requisiti per la sicurezza allo stato limite ultimo (*anche sotto l'azione sismica*) e allo stato limite di esercizio.

La schematizzazione della procedura progettuale adottata può essere così sinteticamente riassunta:

- individuazione della classe d'uso dell'opera e della sua vita utile;
- definizione delle azioni agenti in condizioni statiche e dinamiche attraverso l'individuazione delle condizioni di carico;
- predisposizione delle combinazioni di carico (*con i relativi coefficienti di combinazione*);
- predimensionamento delle membrature strutturali;
- applicazione dei criteri della gerarchia delle resistenze e scelta delle soluzioni strutturali che impediscono rotture fragili (*nel caso di $q > 1$*);
- verifica della funzionalità allo stato limite di danno delle strutture progettate (*nel caso di tamponamenti rigidi*).

La sicurezza e le prestazioni saranno garantite verificando gli stati limite sopra definiti in funzione dell'utilizzo della struttura, della sua vita nominale e di quanto stabilito dalle norme; in particolare si è verificata:

- la sicurezza nei riguardi degli stati limite ultimi (SLU e SLV) che possono provocare eccessive deformazioni permanenti, crolli parziali o globali, dissesti, che possono compromettere l'incolumità delle persone e/o la perdita di beni, provocare danni ambientali e sociali, mettere fuori servizio l'opera. Per le verifiche sono stati utilizzati i coefficienti parziali relativi alle azioni ed alle resistenze dei materiali in accordo a quanto previsto dalle NTC per i vari tipi di materiale. I valori utilizzati sono riportati nel seguito;
- la sicurezza nei riguardi degli stati limite di esercizio (SLE) che possono limitare nell'uso e nella durata l'utilizzo della struttura per le azioni di esercizio. In particolare di concerto con il committente e coerentemente alle norme tecniche si sono definiti i limiti riportati nel seguito;
- la sicurezza nei riguardi dello stato limite del danno (SLD) causato da azioni sismiche con opportuni periodi di ritorno definiti di concerto al committente ed alle norme vigenti per le costruzioni in zona sismica;
- la robustezza nei confronti di opportune azioni accidentali in modo da evitare danni sproporzionati in caso di incendi, urti, esplosioni, errori umani.

4 DURABILITA'

Particolare cura è stata posta per garantire la durabilità della struttura, con la consapevolezza che tutte le prestazioni attese potranno essere garantite solo mediante opportune procedure da seguire non solo in fase di progettazione, ma anche di costruzione, manutenzione e gestione dell'opera; si dovranno, inoltre, utilizzare tutti gli accorgimenti utili alla conservazione delle caratteristiche fisiche e dinamiche dei materiali e delle strutture.

La qualità dei materiali e le dimensioni degli elementi sono coerenti con tali obiettivi.

Per garantire la durabilità della struttura sono stati presi in considerazione opportuni stati limite di esercizio (SLE) in funzione dell'uso e dell'ambiente in cui la struttura dovrà vivere limitando sia gli stati tensionali sia, nel caso delle opere in calcestruzzo, l'ampiezza delle fessure. La definizione quantitativa delle prestazioni, la classe di esposizione e le verifiche sono riportati nel seguito e negli allegati di calcolo.

Per strutture in c.a.: il copriferro minimo da adottare in funzione delle esigenze di protezione dell'armatura e per garantire la corretta trasmissione delle forze di aderenza è stato determinato in base alle prescrizioni delle NTC §4.1.6.1.3 (C4.1.6.1.3 della Circolare) e dell'Eurocodice 2 prospetti 4.2, 4.3N e 4.4N.

Per strutture in acciaio: è vietato l'uso di profilati con spessore $t < 4$ mm. Una deroga a tale norma, fino ad uno spessore $t=3$ mm, è consentita per opere sicuramente protette contro la corrosione, quali per esempio tubi chiusi alle estremità e profili zincati, od opere non esposte agli agenti atmosferici (NTC, §4.2.9.1). Le limitazioni di cui sopra non riguardano elementi e profili sagomati a freddo. E' proibito l'impiego di acciaio incrudito in ogni caso in cui si preveda la plasticizzazione del materiale (NTC, §4.2.9.2).

Per strutture in legno: in relazione alla classe di servizio della struttura e alle condizioni di carico, dovrà essere un programma delle operazioni di manutenzione e di controllo da effettuare durante l'esercizio della struttura (NTC, §4.4.13). La durabilità delle strutture lignee deve essere sempre assicurata, prevedendo particolari costruttivi ed opportuni accorgimenti di protezione dagli agenti atmosferici e dagli attacchi biologici di funghi e/o insetti xilofaghi, utilizzando specie legnose più idonee per durabilità naturale e per possibilità d'impregnazione, in relazione alle condizioni ambientali di esercizio (C4.4.13).

5 RELAZIONE SUI MATERIALI

5.1 Calcestruzzo per fondazioni

Calcestruzzo per opere in Cemento armato normale c.a.n.

Classe di esposizione	UNI EN 206-1		XC2	
Classe di consistenza	UNI EN 206-1		S4	
Tipo cemento	UNI EN 197-1		CEM I 32,5	
Classe di resistenza	UNI EN 206-1		C25/30	
Acqua d'impasto	UNI EN 1008			
Rapporto acqua/cemento	UNI EN 206-1	a/c	0,6	
Contenuto minimo cemento	UNI EN 206-1		280 kg	
Copriferro minimo	EC2-1-1	c_{min}	15 mm	
Aggregati	UNI EN 12620			
Dimensione massima aggregato	EC2-1-1	D_{max}	11 mm	$D_{max} = 3/4 * c_{min}$
Additivi	UNI EN 934-2			
Resistenza cubica caratteristica	DM2018	R_{ck}	30 MPa	
Coefficiente parziale di sicurezza	DM2018	γ_c	1,5	
Coefficiente riduttivo per carichi durata	DM2018	α_c	0,85	
Resistenza cilindrica caratteristica	DM2018	f_{ck}	24,90 MPa	$f_{ck} = 0.83 * R_{ck}$
Resistenza di calcolo di compressione	DM2018	f_{cd}	14,11 MPa	$f_{cd} = \alpha_{cc} * f_{ck} / \gamma_c$
Resistenza trazione media	DM2018	f_{ctm}	2,56 MPa	$f_{ctm} = 0.3 * f_{ck}^{2/3}$
Resistenza trazione 5%-ile	DM2018	$f_{ctk,5}$	1,79 MPa	$f_{ctk,5} = 0.7 * f_{ctm}$
Resistenza di calcolo di taglio	DM2018	f_{ctd}	1,19 MPa	$f_{ctd} = f_{ctk,5} / \gamma_c$
Resistenza trazione 95%-ile	DM2018	$f_{ctk,95}$	3,33 MPa	$f_{ctk,95} = 1.3 * f_{ctm}$
Resistenza trazione per flessione	DM2018	f_{cfm}	3,07 MPa	$f_{cfm} = 1.2 * f_{ctm}$
Modulo elastico istantaneo	DM2018	E_{cm}	31447 MPa	$E_{cm} = 22000 * ((f_{ck} + 8) / 10)^{0.3}$
Coefficiente di Poisson	DM2018	ν	0,2	
Modulo elastico tangenziale	DM2018	G	13103 MPa	$G = E_{cm} / (2 * (1 + \nu))$
coefficiente di dilatazione termica	DM2018	α	0,00001 °C ⁻¹	
Controllo di accettazione	DM2018		tipo A	
Resistenza minima dei provini	DM2018	R_1	26,5 MPa	$R_1 \geq R_{ck} - 3.5$
Resistenza media dei provini	DM2018	R_m	33,5 MPa	$R_m \geq R_{ck} + 3.5$

1.1 Calcestruzzo per setti

Calcestruzzo per opere in Cemento armato normale c.a.n.

Classe di esposizione	UNI EN 206-1		XC1	
Classe di consistenza	UNI EN 206-1		S4	
Tipo cemento	UNI EN 197-1		CEM I 32,5	
Classe di resistenza	UNI EN 206-1		C25/30	
Acqua d'impasto	UNI EN 1008			
Rapporto acqua/cemento	UNI EN 206-1	a/c	0,65	
Contenuto minimo cemento	UNI EN 206-1		280 kg	
Copriferro minimo	EC2-1-1	C_{min}	10 mm	
Aggregati	UNI EN 12620			
Dimensione massima aggregato	EC2-1-1	D_{max}	7 mm	$D_{max} = 3/4 * C_{min}$
Additivi	UNI EN 934-2			
Resistenza cubica caratteristica	DM2018	R_{ck}	30 MPa	
Coefficiente parziale di sicurezza	DM2018	γ_c	1,5	
Coefficiente riduttivo per carichi durati	DM2018	α_c	0,85	
Resistenza cilindrica caratteristica	DM2018	f_{ck}	24,90 MPa	$f_{ck} = 0.83 * R_{ck}$
Resistenza di calcolo di compressione	DM2018	f_{cd}	14,11 MPa	$f_{cd} = \alpha_{cc} * f_{ck} / \gamma_c$
Resistenza trazione media	DM2018	f_{ctm}	2,56 MPa	$f_{ctm} = 0.3 * f_{ck}^{2/3}$
Resistenza trazione 5%-ile	DM2018	$f_{ctk,5}$	1,79 MPa	$f_{ctk,5} = 0.7 * f_{ctm}$
Resistenza di calcolo di taglio	DM2018	f_{ctd}	1,19 MPa	$f_{ctd} = f_{ctk,5} / \gamma_c$
Resistenza trazione 95%-ile	DM2018	$f_{ctk,95}$	3,33 MPa	$f_{ctk,95} = 1.3 * f_{ctm}$
Resistenza trazione per flessione	DM2018	f_{cfm}	3,07 MPa	$f_{cfm} = 1.2 * f_{ctm}$
Modulo elastico istantaneo	DM2018	E_{cm}	31447 MPa	$E_{cm} = 22000 * ((f_{ck} + 8) / 10)^{0.3}$
Coefficiente di Poisson	DM2018	ν	0,2	
Modulo elastico tangenziale	DM2018	G	13103 MPa	$G = E_{cm} / (2 * (1 + \nu))$
coefficiente di dilatazione termica	DM2018	α	0,00001 °C ⁻¹	
Controllo di accettazione	DM2018		tipo A	
Resistenza minima dei provini	DM2018	R_1	26,5 MPa	$R_1 \geq R_{ck} - 3.5$
Resistenza media dei provini	DM2018	R_m	33,5 MPa	$R_m \geq R_{ck} + 3.5$

1.2 Acciaio per Cemento Armato

Acciaio per opere in Cemento armato normale c.a.n. B450C e B450A

Tensione caratteristica di rottura	DM2018	f_t	540 MPa	
Tensione caratteristica di snervamento	DM2018	$f_{y,k}$	450 MPa	
Coefficiente parziale di sicurezza	DM2018	γ_s	1,15	
Tensione di calcolo	DM2018	$f_{y,d}$	391 MPa	$f_{yd} = f_{yk} / \gamma_s$
Diametro mandrino piegamenti 90°	DM2018	$\phi < 12 \text{ mm}$	4 ϕ	
Diametro mandrino piegamenti 90°	DM2018	$12 < \phi < 16$	5 ϕ	
Diametro mandrino piegamenti 90°	DM2018	$16 < \phi < 25$	8 ϕ	
Controllo di accettazione	DM2018	B450C		
Tensione di snervamento minima	DM2018	$f_{y,min}$	425 MPa	
Tensione di snervamento massima	DM2018	$f_{y,max}$	572 MPa	
rapporto tensione rottura/snervamento	DM2018	$f_t/f_y \geq$	1,13	
rapporto tensione rottura/snervamento	DM2018	$f_t/f_y <$	1,37	
Allungamento massimo	DM2018	A_{gt}	6,0 %	
Controllo di accettazione	DM2018	B450A		
Tensione di snervamento minima	DM2018	$f_{y,min}$	425 MPa	
Tensione di snervamento massima	DM2018	$f_{y,max}$	572 MPa	
rapporto tensione rottura/snervamento	DM2018	$f_t/f_y \geq$	1,03	
Allungamento massimo	DM2018	A_{gt}	2,0 %	

5.1 Legno

legno Lamellare

Classe	GL28h	GL28h	
Flessione	GL28h	f_{mk}	28,0 MPa
Trazione parallela alla fibratura	GL28h	$f_{t,0,k}$	22,5 MPa
Trazione perpendicolare alla fibratura	GL28h	$f_{t,90,k}$	0,5 MPa
Compressione parallela alla fibratura	GL28h	$f_{c,0,k}$	26,5 MPa
Compressione perpendicolare alla fibratura	GL28h	$f_{c,90,k}$	3,0 MPa
Taglio	GL28h	f_{vk}	3,2 MPa
Modulo elastico medio parallelo alle fibre	GL28h	$E_{0,mean}$	12600 MPa
Modulo elastico caratteristico parallelo alle fibre	GL28h	$E_{0,05}$	10200 MPa
Modulo elastico medio	GL28h	$E_{90,mean}$	420 MPa
Modulo di taglio medio	GL28h	G_{mean}	780 MPa
Massa volumica caratteristica	GL28h	ρ_k	410 kg/m ³
Massa volumica media	GL28h	ρ_m	410 kg/m ³
Coefficiente parziale di sicurezza	DM2018	γ_M	1,45

2 CARATTERISTICHE DEL SOTTOSUOLO

2.1 Categoria del sottosuolo

Dalla relazione Geologica redatta dal Geol. Alberto Coral il 07.05.2019, si desume una stratigrafia costituita prevalentemente da ghiaie. Dalle informazioni, si classifica il terreno, in base alla tabella 3.2.II del D.M. 2018, di categoria **B**.

2.2 Caratteristiche meccaniche del sottosuolo

La valutazione del carico a rottura del terreno è pari a $R_t = 2.00$ MPa. Questo valore è stato ottenuto adottando:

- angolo di attrito interno $\phi=40^\circ$;
- fondazione con $B=2.00$ m;
- coesione del terreno $c_u=0.00$ MPa;
- peso di volume del terreno di $\gamma=20.00$ kN/m³;
- profondità pari a 1.50 m dal p.d.c..

Adottando l'approccio 2 del D.M. 2018 si considerano i seguenti parametri ai fini della valutazione della capacità portante di progetto del sottosuolo:

- le azioni della struttura sono amplificate con i coefficienti [A1] *tab.6.2.I*, $\gamma_G=1.30/1.00$ per azioni permanenti e $\gamma_Q=1.50/0.00$ per azioni variabili, corrispondenti alle azioni allo stato limite ultimo;
- i parametri caratteristici di resistenza del terreno sono divisi per il coefficiente [M1] *tab.6.2.II*, $\gamma_M=1.0$;
- la resistenza di progetto del terreno è determinata dividendo la resistenza ultima per il coefficiente [R3] *tab.6.4.I*, $\gamma_R=2.3$.

La resistenza di progetto del terreno risulta pari a:

$$R_d = R_t / (\gamma_M * \gamma_R) = 2.00 / (1.0 * 2.3) = 0.87 \text{ Mpa}$$

Il geologo raccomanda comunque di non superare la resistenza di progetto di 0.25 Mpa.

3 AZIONI DI PROGETTO

3.1 Azioni Permanenti

Analisi dei carichi copertura LIGNEA palestra

PERMANENTE

fotovoltaico	= 0,30 kN/mq
pannello	= 0,20 kN/mq
	0,50 kN/mq

ACCIDENTALE

neve	1,20 kN/mq
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Analisi dei carichi copertura SOLAIO palestra

PERMANENTE

macchine termiche	= 2,00 kN/mq
fotovoltaico	= 0,30 kN/mq
guaina	0,02 m * 20,00 kN/mc = 0,40 kN/mq
isolamento	0,15 m * 2,00 kN/mc = 0,30 kN/mq
Solaio Predalles 5+25+6	5,00 kN/mq
	8,00 kN/mq

ACCIDENTALE

accessibilità e manutenzione	2,00 kN/mq
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Analisi dei carichi copertura SOLAIO scuola

PERMANENTE

fotovoltaico	= 0,30 kN/mq
guaina	0,02 m * 20,00 kN/mc = 0,40 kN/mq
isolamento	0,15 m * 2,00 kN/mc = 0,30 kN/mq
Solaio Predalles 5+25+6	5,00 kN/mq
	6,00 kN/mq

ACCIDENTALE

accessibilità e manutenzione	2,00 kN/mq
------------------------------	-------------------

Analisi dei carichi SOLAIO di piano scuola/palestra

PERMANENTE

resina	0,01 m * 20,00 kN/mc = 0,10 kN/mq
massetto riscaldamento	0,10 m * 20,00 kN/mc = 2,00 kN/mq
isolamento	0,10 m * 2,00 kN/mc = 0,20 kN/mq
isocall	0,10 m * 5,00 kN/mc = 0,50 kN/mq
Solaio Predalles 5+25+6	5,00 kN/mq
	7,80 kN/mq

ACCIDENTALE

scuola	3,00 kN/mq
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3.2 Azioni Variabile da neve

Azione della Neve - NTC 2008

zona	II	zona di appartenenza	NTC2018, §3.4.2
$a_s =$	1,00 mslm	altitudine sul livello del mare	NTC2018, §3.4.2
$q_{sk} =$	1,00 kN/m ²	valore caratteristico di riferimento	NTC2018, §3.4.2
$\alpha =$	23 °	angolo inclinazione falda	NTC2018, §3.4.3
$\mu =$	0,80	coefficiente di forma della copertura	NTC2018, Tab.3.4.11
$C_E =$	1,0	coefficiente di esposizione	NTC2018, Tab.3.4.1
$C_t =$	1,0	coefficiente termico	NTC2018, §3.4.5
$q_s =$	0,80 kN/m ²	carico da neve	NTC2018, [3.4.1]

Zona I - Alpina

Aosta, Belluno, Bergamo, Biella, Bolzano, Brescia, Como, Cuneo, Lecco, Pordenone, Sondrio, Torino, Trento, Udine, Verbanco-Cusio-Ossola, Vercelli, Vicenza:

$$q_{sk} = 1,50 \text{ kN/m}^2 \quad a_s \leq 200 \text{ m} \quad [3.4.2]$$

$$q_{sk} = 1,39 [1 + (a_s/725)] \text{ kN/m}^2 \quad a_s > 200 \text{ m}$$

Zona I - Mediterranea

Alessandria, Ancona, Asti, Bologna, Cremona, Forlì-Cesena, Lodi, Milano, Modena, Monza Brianza, Novara, Parma, Pavia, Pesaro e Urbino, Piacenza, Ravenna, Reggio Emilia, Rimini, Treviso, Varese:

$$q_{sk} = 1,50 \text{ kN/m}^2 \quad a_s \leq 200 \text{ m} \quad [3.4.3]$$

$$q_{sk} = 1,35 [1 + (a_s/602)] \text{ kN/m}^2 \quad a_s > 200 \text{ m}$$

Zona II

Arezzo, Ascoli Piceno, Avellino, Bari, Barletta-Andria-Trani, Benevento, Campobasso, Chieti, Fermo, Ferrara, Firenze, Foggia, Grosseto, Genova, Gorizia, Imperia, Isernia, L'Aquila, La Spezia, Lucca, Macerata, Mantova, Massa Carrara, Padova, Perugia, Pescara, Pistoia, Prato, Rieti, Rovigo, Savona, Teramo, Trieste, Venezia, Verona:

$$q_{sk} = 1,00 \text{ kN/m}^2 \quad a_s \leq 200 \text{ m} \quad [3.4.4]$$

$$q_{sk} = 0,85 [1 + (a_s/481)] \text{ kN/m}^2 \quad a_s > 200 \text{ m}$$

Zona III

Agrigento, Brindisi, Cagliari, Caltanissetta, Carbonia-Iglesias, Caserta, Catania, Catanzaro, Cosenza, Crotone, Enna, Grosseto, Latina, Lecce, Livorno, Matera, Medio Campidano, Messina, Napoli, Nuoro, Olbia-Tempio, Oristano, Palermo, Pisa, Potenza, Ragusa, Reggio Calabria, Roma, Salerno, Sassari, Siena, Siracusa, Taranto, Terni, Trapani, Vibo Valentia, Viterbo:

$$q_{sk} = 0,60 \text{ kN/m}^2 \quad a_s \leq 200 \text{ m} \quad [3.4.5]$$

$$q_{sk} = 0,51 [1 + (a_s/481)] \text{ kN/m}^2 \quad a_s > 200 \text{ m}$$

Per altitudini superiori a 1500 m sul livello del mare si deve fare riferimento alle condizioni locali di clima e di esposizione utilizzando comunque valori di carico neve non inferiori a quelli previsti per 1500 m.

Per un'opera di nuova realizzazione in fase di costruzione o per le fasi transitorie relative ad interventi sulle costruzioni esistenti, il periodo di ritorno dell'azione può essere ridotto come di seguito specificato:

- per fasi di costruzione o fasi transitorie con durata prevista in sede di progetto non superiore a tre mesi, si assumerà $T_r \geq 5$ anni;
- per fasi di costruzione o fasi transitorie con durata prevista in sede di progetto compresa fra tre mesi e un anno, si assumerà $T_r \geq 10$ anni.

Tab. 3.4.11 - Valori del coefficiente di forma

Coefficiente di forma	$0^\circ \leq \alpha \leq 30^\circ$	$30^\circ < \alpha < 60^\circ$	$\alpha \geq 60^\circ$
μ_1	0,8	$0,8 \frac{(60 - \alpha)}{30}$	0,0

Tab. 3.4.1 - Valori di C_E per diverse classi di esposizione

Topografia	Descrizione	C_E
Battuta dai venti	Aree pianeggianti non ostruite esposte su tutti i lati, senza costruzioni o alberi più alti	0,9
Normale	Aree in cui non è presente una significativa rimozione di neve sulla costruzione prodotta dal vento, a causa del terreno, altre costruzioni o alberi	1,0
Riparata	Aree in cui la costruzione considerata è sensibilmente più bassa del circostante terreno o circondata da costruzioni o alberi più alti	1,1

3.4.3.2 COPERTURA AD UNA FALDA

Nel caso delle coperture ad una falda, si deve considerare la condizione di carico riportata in Fig. 3.4.2.



Fig. 3.4.2 - Condizioni di carico per coperture ad una falda

3.4.3.3 COPERTURA A DUE FALDE

Nel caso delle coperture a due falde, si devono considerare le tre condizioni di carico alternative, denominate Caso I, Caso II e Caso III in Fig. 3.4.3.

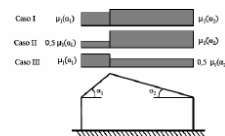


Fig. 3.4.3 - Condizioni di carico per coperture a due falde

3.3 Azioni Variabile da vento

Azione del Vento - NTC 2018		
zona	1 #	zonizzazione italiana per la determinazione di v_{ref} NTC08, Tab.3.3.1
a_s	30 m	altitudine (s.m.m) del sito ove sorge la costruzione NTC08, §3.3.1
$V_{h,0}$	25 m/s	velocità in funzione della zona NTC08, §3.3.1
a_0	1000 m	coefficiente caratteristico del sito ove sorge la costruzione NTC08, Tab.3.3.1
k_0	0,400 1/s	coefficiente caratteristico del sito ove sorge la costruzione NTC08, Tab.3.3.1
C_s	1,000	coefficiente di altitudine NTC08, Tab.3.3.1
V_0	25 m/s	velocità base di riferimento al livello del mare NTC08, §3.3.1
T_R	50 anni	periodo di ritorno NTC08, §3.3.2
C_R	1,00	coefficiente di ritorno NTC08, §3.3.2
V_r	25 m/s	velocità di riferimento NTC08, §3.3.2
ρ	1,25 kg/m ³	densità dell'aria assunta convenzionalmente costante NTC08, §3.3.6
q_r	0,39 kN/m ²	pressione cinetica di riferimento NTC08, §3.3.6
Classe	C #	classe di rugosità del terreno NTC08, §3.3.7
Categoria	II #	categoria di esposizione del sito ove sorge la costruzione NTC08, §3.3.7
z	7 m	altezza dell'edificio NTC08, §3.3.7
C_t	1,00 #	coefficiente di topografia c_t NTC08, §3.3.7
k_0	0,19	NTC08, Tab.3.3.8
Z_0	0,05 m	NTC08, Tab.3.3.8
Z_{min}	4,00 m	NTC08, Tab.3.3.8
C_e	2,130 #	coefficiente di esposizione valutato per $z = h$ NTC08, §3.3.7
C_d	1,000 #	coefficiente dinamico C_d NTC08, §3.3.9
q_p	0,83 kN/m ²	pressione cinetica di picco (a meno di C_d) NTC08, §3.3.4
C_p	0,80	
i	1 m	
q_0	0,67 kN/m	
C_p	0,40	
i	1 m	
q_0	0,33 kN/m	

La pressione del vento è data dall'espressione:

$$P = q_r C_s C_p C_d \quad [3.3.4]$$

dove
 q_r è la pressione cinetica di riferimento di cui al § 3.3.6;
 C_s è il coefficiente di esposizione di cui al § 3.3.7;
 C_p è il coefficiente di pressione di cui al § 3.3.8;
 C_d è il coefficiente dinamico di cui al § 3.3.9.

In mancanza di specifiche ed adeguate indagini statistiche, v_r è data dall'espressione:

v_{ref} è la velocità base di riferimento al livello del mare, assegnata nella Tab. 3.3.1 in funzione della zona in cui sorge la costruzione (Fig. 3.3.1);
 C_s è il coefficiente di altitudine fornito dalla relazione:

$$C_s = 1 \quad \text{per } a_s \leq a_0$$

$$C_s = 1 + k_s \left(\frac{a_s}{a_0} - 1 \right) \quad \text{per } a_s > a_0, \leq 1500 \text{ m} \quad [3.3.1a]$$

dove:
 a_s, k_s sono parametri forniti nella Tab. 3.3.1 in funzione della zona in cui sorge la costruzione (Fig. 3.3.1);
 a_0 è l'altitudine sul livello del mare del sito ove sorge la costruzione.

Zona	Descrizione	v_{ref} [m/s]	a_0 [m]	k_s
1	Valle d'Aosta, Piemonte, Lombardia, Trentino Alto Adige, Veneto, Friuli Venezia Giulia (con l'eccezione della provincia di Trieste)	25	1000	0,40
2	Emilia Romagna	25	750	0,45
3	Toscana, Marche, Umbria, Lazio, Abruzzo, Molise, Puglia, Campania, Basilicata, Calabria (eccezione la provincia di Reggio Calabria)	27	500	0,37
4	Sicilia e provincia di Reggio Calabria	28	500	0,36
5	Sardegna (zona a oriente della retta congiungente Capo Testada con l'Isola di Maddalena)	28	750	0,40
6	Sardegna (zona a occidente della retta congiungente Capo Testada con l'Isola di Maddalena)	28	500	0,36
7	Liguria	28	1000	0,54
8	Provincia di Trieste	30	1500	0,50
9	Isole (con l'eccezione di Sicilia e Sardegna) e mare aperto	31	500	0,32

La velocità di riferimento v_r è il valore medio su 10 minuti, a 10 m di altezza dal suolo su un terreno pianeggiante e omogeneo di categoria di esposizione II (vedi Tab. 3.3.2), rilevato al periodo di ritorno di progetto T_R . Tale velocità è definita dalla relazione:

$$v_r = v_r \cdot C_r \quad [3.3.2]$$

dove:
 v_r è la velocità base di riferimento, di cui al § 3.3.1;

C_r è il coefficiente di ritorno, funzione del periodo di ritorno di progetto T_R .

In mancanza di specifiche ed adeguate indagini statistiche, il coefficiente di ritorno è fornito dalla relazione:

$$C_r = 0,75 \sqrt{1,02 + \ln \left[\frac{a_r}{T_R} \left(1 + \frac{1}{T_R} \right) \right]} \quad [3.3.3]$$

	2 km	10 km	20 km	500m	750m
A	--	IV	IV	V	V
B	--	III	III	IV	IV
C	--	*	III	III	IV
D	--	II	II	II	**

* Categoria II in zona 1,2,3,4
 * Categoria III in zona 5
 ** Categoria II in zona 2,3,4,5

	2 km	10 km	20 km	500m	750m
A	--	I	I	I	I
B	--	I	I	I	I
C	--	I	I	I	I
D	--	I	I	I	I

* Categoria II in zona 1,2,3,4
 * Categoria III in zona 5
 ** Categoria II in zona 2,3,4,5

Map of ZONA 6 showing a coastal profile. The profile starts at the 'mare' (sea) on the left, rises to a peak labeled 'costa' (coast), and then descends. Distance markers are indicated: 2 km from the sea, 10 km from the sea, and 30 km from the sea. A 500m scale bar is shown above the profile.

A	--	III	IV	V	V
B	--	III	IV	IV	V
C	--	II	III	IV	IV
D	I	I	II	III	IV

* Categoria II in zona 6

Map of ZONE 7,8 showing a coastal profile. The profile starts at the 'mare' (sea) on the left, rises to a peak labeled 'costa' (coast), and then descends. Distance markers are indicated: 1,5 km from the sea and 0,5 km from the sea. A 500m scale bar is shown above the profile.

A	--	--	IV	IV
B	--	--	IV	IV
C	--	--	IV	IV
D	I	I	II	*

* Categoria II in zona 8

* Categoria III in zona 7

La pressione cinetica di riferimento q_r è data dall'espressione:

$$q_r = \frac{1}{2} \rho v_r^2 \quad [3.3.6]$$

dove

v_r è la velocità di riferimento del vento di cui al § 3.3.2;

ρ è la densità dell'aria assunta convenzionalmente costante e pari a 1,25 kg/m³.

Esprimendo p in kg/m² e v_r in m/s, q_r risulta espresso in N/m².

Il coefficiente di esposizione C_s dipende dall'altezza z ed esposto del punto considerato, dalla topografia del terreno e dalla categoria di esposizione del sito ove sorge la costruzione. In assenza di analisi specifiche che tengano in conto la direzione di provenienza del vento e l'effetto di valenza e topografia del terreno che ricomprende la costruzione, per altezze sul suolo non maggiori di $z = 200$ m, sono da usare le seguenti relazioni:

$$C_s(z) = k_s \left[\ln \left(\frac{z}{Z_0} \right) \right] \quad \text{per } z \geq Z_{min}$$

$$C_s(z) = C_s(Z_{min}) \quad \text{per } z < Z_{min} \quad [3.3.7]$$

dove:
 k_s, Z_{min} sono assegnati in Tab. 3.3.1 in funzione della categoria di esposizione del sito ove sorge la costruzione;

C_s è il coefficiente di topografia.

Categoria di esposizione del sito	k_s	Z_{min} [m]	C_s [m]
I	0,17	0,05	1
II	0,18	0,05	1
III	0,19	0,05	1
IV	0,22	0,05	1
V	0,23	0,05	1

Tab. 3.3.III - Classi di rugosità del terreno

Classe di rugosità del terreno	Descrizione
A	Aree urbane in cui almeno il 10% della superficie sia coperta da edifici la cui altezza media superi i 15 m
B	Aree urbane (non di classe A), suburbane, industriali e boschive
C	Aree con ostacoli diffusi (alberi, case, muri, recinzioni...); aree con rugosità non riconducibile alle classi A, B, D
D	a) Mare e relativa fascia costiera (entro 2 km dalla costa); b) Lago (con larghezza massima pari ad almeno 1 km) e relativa fascia costiera (entro 1 km dalla costa); c) Aree prive di ostacoli o con al più rari ostacoli isolati (aperta campagna, aeroporti, aree agricole, pascoli, zone paludose o sabbiose, superfici innevate o ghiacciate, ...)

L'assegnazione della classe di rugosità non dipende dalla conformazione orografica e topografica del terreno. Si può assumere che il sito appartenga alla Classe A o B, purché la costruzione si trovi nell'area relativa per non meno di 1 km e comunque per non meno di 20 volte l'altezza della costruzione, per tutti i settori di provenienza del vento angoli almeno 30°. Si deve assumere che il sito appartenga alla Classe D, qualora la costruzione sorge nelle aree indicate con la lettera a) o b), oppure entro un raggio di 1 km da una via su un settore angolare 30°, dove il 90% del terreno sia del tipo indicato con la lettera c). Laddove sussistono dubbi sulla scelta della classe di rugosità, si deve assegnare la classe più sfavorevole (l'azione del vento è in genere massima in Classe A e massima in Classe D).

3.4 Azione Variabile da Sisma

Le azioni sismiche di progetto, in base alle quali valutare il rispetto dei diversi limiti considerati, si definiscono a partire dalla “pericolosità sismica di base” del sito di costruzione.

La pericolosità sismica è definita in termini di accelerazione orizzontale massima attesa a_g in condizioni di campo libero su sito di riferimento rigido con superficie topografica orizzontale (di categoria A quale definita al § 3.2.2), nonché di ordinate dello spettro di risposta elastico in accelerazione ad essa corrispondente $S_e(T)$, con riferimento a prefissate probabilità di eccedenza P_{VR} , come definito al § 3.2.1, nel periodo di riferimento V_R , come definito al § 2.4.

Determinazione del periodo di riferimento

Secondo il § 2.4.3 le azioni sismiche sulle costruzioni sono valutate in relazione ad un periodo di riferimento V_R che si ricava moltiplicando la vita nominale V_N per il coefficiente d'uso C_U :

$$V_R = V_N \cdot C_U$$

La vita nominale dell'opera V_N è intesa come il numero di anni nel quale la struttura purché soggetta alla manutenzione ordinaria, deve potere essere usata per lo scopo al quale è destinata. La vita nominale dei diversi tipi di opere è riportata nella seguente tabella (§ 2.4.1 tabella 2.4.I).

TIPO DI COSTRUZIONE			Vita Nominale V_N (in anni)
☐	1	Opere provvisorie – Opere provvisionali – Strutture in fase costruttiva	≤ 10
☐	2	Opere ordinarie, ponti, opere infrastrutturali e dighe di dimensioni contenute o di importanza normale	≥ 50
☒	3	Grandi opere, ponti, opere infrastrutturali e dighe di grandi dimensioni o di importanza strategica	≥ 100

In presenza di azioni sismiche, con riferimento alle conseguenze di un'interruzione di operatività o di un eventuale collasso, le costruzioni sono suddivise in classi d'uso così definite:

Classe I: Costruzioni con presenza solo occasionale di persone, edifici agricoli.

Classe II: Costruzioni il cui uso prevede normali affollamenti, senza contenuti pericolosi per l'ambiente e senza funzioni pubbliche e sociali essenziali. Industrie con attività non pericolose per l'ambiente. Ponti, opere infrastrutturali, reti viarie non ricadenti in Classe d'uso III o in Classe d'uso IV, reti ferroviarie la cui interruzione non provochi situazioni di emergenza. Dighe il cui collasso non provochi conseguenze rilevanti.

Classe III: Costruzioni il cui uso prevede affollamenti significativi. Industrie con attività pericolose per l'ambiente. Reti viarie extraurbane non ricadenti in Classe d'uso IV. Ponti e reti ferroviarie la cui interruzione provochi situazioni di emergenza. Dighe rilevanti per le conseguenze di un loro eventuale collasso.

Classe IV: Costruzioni con funzioni pubbliche o strategiche importanti, anche in riferimento alla gestione della protezione civile in caso di calamità. Industrie con attività particolarmente pericolose per l'ambiente. Reti viarie di tipo A o B, di cui al D.M. 5 novembre 2001, n. 6792, "Norme funzionali e geometriche per la costruzione delle strade", e di tipo C quando appartenenti ad itinerari di collegamento tra capoluoghi di provincia non altresì serviti da strade di tipo A o B. Ponti e reti ferroviarie di importanza critica per il mantenimento delle vie di comunicazione, particolarmente dopo un evento sismico. Dighe connesse al funzionamento di acquedotti e a impianti di produzione di energia elettrica.

Il valore del coefficiente d'uso C_U è definito, al variare della Classe d'uso, come mostrato in § 2.4.3 tabella 2.4.II.

CLASSE D'USO	I	II	III	IV
COEFFICIENTE C_U	0.7	1.0	1.5	2.0
	☐	☐	☒	☐

Se $V_R \leq 35$ anni si pone $V_R = 35$ anni.

Il periodo di riferimento è pari a $V_R = 100 * 1.5 = 150$ anni

Stato limite di superamento

Nei confronti delle azioni sismiche gli stati limite, sia di esercizio che ultimi, sono individuati riferendosi alle prestazioni della costruzione nel suo complesso, includendo gli elementi strutturali, quelli non strutturali e gli impianti.

Gli stati limite d'esercizio sono:

- **Stato limite di Operatività (SLO):** a seguito del terremoto la costruzione nel suo complesso, includendo gli elementi strutturali, quelli non strutturali, le apparecchiature rilevanti alla sua funzione, non deve subire danni ed interruzioni d'uso significativi;
- **Stato limite di danno (SLD):** a seguito del terremoto la costruzione nel suo complesso, includendo gli elementi strutturali, quelli non strutturali, le apparecchiature rilevanti alla sua funzione, subisce danni tali da non mettere a rischio gli utenti e da non compromettere significativamente la capacità di resistenza e di rigidezza nei confronti delle azioni verticali ed orizzontali, mantenendosi immediatamente utilizzabile pur nell'interruzione d'uso di parte delle apparecchiature.

Gli stati limite ultimi sono:

- **Stato Limite di salvaguardia della Vita (SLV):** a seguito del terremoto la costruzione subisce rotture e crolli dei componenti non strutturali ed impiantistici e significativi danni dei componenti strutturali cui si associa una perdita significativa di rigidezza nei confronti delle azioni orizzontali; la costruzione conserva invece una parte della resistenza e rigidezza per azioni verticali e un margine di sicurezza nei confronti del collasso per azioni sismiche orizzontali;
- **Stato Limite di prevenzione del Collasso (SLC):** a seguito del terremoto la costruzione subisce gravi rotture e crolli dei componenti non strutturali ed impiantistici e danni molto gravi dei componenti strutturali; la costruzione conserva ancora un margine di sicurezza per azioni verticali ed un esiguo margine di sicurezza nei confronti del collasso per azioni orizzontali.

Le probabilità di superamento nel periodo di riferimento P_{VR} , cui riferirsi per individuare l'azione sismica agente in ciascuno degli stati limite considerati, sono riportate nella successiva tabella 3.2.1.

Stati Limite		P_{VR} : Probabilità di superamento nel periodo di riferimento V_R
Stati limite di esercizio	SLO	81%
	SLD	63%
Stati limite ultimi	SLV	10%
	SLC	5%

Il periodo di ritorno dell'azione sismica corrispondente a ciascun stato limite vale:

$$T_R = -V_R / \ln(1 - P_{VR}) \quad (DM 2018 - Allegato A - [1])$$

I valori del **periodo di ritorno** per ogni stato limite di verifica sono riportati nella seguente tabella.

<i>Stati Limite</i>		<i>T_R (anni)</i>
<i>Stati limite di esercizio</i>	<i>SLO</i>	90
	<i>SLD</i>	151
<i>Stati limite ultimi</i>	<i>SLV</i>	1424
	<i>SLC</i>	2475

Categoria del sottosuolo

Si seguono le indicazioni contenute nel § 3.2.2 del D.M. 17.01.2018 relative alla classificazione del sottosuolo e all'individuazione delle condizioni topografiche della superficie del sito oggetto dell'intervento.

Ai fini della definizione dell'azione sismica di progetto, si rende necessario valutare l'effetto della risposta sismica locale mediante analisi del sottosuolo, come indicato al § 7.11.3. Da conoscenze dirette si evince che il sottosuolo rientra nella categoria **B**.

Condizioni topografiche

La risposta sismica riferita ad un sottosuolo rigido di categoria A deve quindi essere amplificata da opportuni coefficienti d'amplificazione che tengono conto della diversa stratigrafia del sito; essi sono: S_s , coefficiente stratigrafico e C_C , coefficiente che modifica il periodo, T_C corrispondente all'inizio del tratto a velocità costante dello spettro di risposta elastico.

Allo scopo di individuare le condizioni topografiche della superficie del sito e valutare i corrispondenti coefficienti amplificativi topografici, S_T della risposta sismica finale la Normativa mette a disposizione la seguente classificazione:

<i>Categoria</i>		<i>Classificazione della superficie topografica</i>	<i>S_r</i>
☒	T1	Superficie pianeggiante, pendii e rilevati isolati con inclinazione media $i \leq 15^\circ$	1.0
☐	T2	Pendii con inclinazione media $i > 15^\circ$	1.2
☐	T3	Rilievi con larghezza in cresta molto minore che alla base e inclinazione media $15^\circ \leq i < 30^\circ$	1.2
☐	T4	Rilievi con larghezza in cresta molto minore che alla base e inclinazione media $i > 30^\circ$	1.4

Metodo di analisi sismica

Il progetto previsto propone una struttura a setti sismo resistenti in c.a.. La struttura, rispecchia i criteri del §7.3.3.2, è cioè pressoché simmetrica e regolare in altezza. L'analisi della sicurezza in condizioni sismiche è svolta secondo l'analisi statica / dinamica di cui al § 7.3.2 del D.M. del 17/01/2018.

Spettro di risposta lineare

Il progetto dell'ampliamento è condotto per lo stato limite: (§3.2.1)

SLV, la struttura deve conservare una resistenza e una rigidezza per azioni verticali e orizzontali

SLD, la struttura subisce danni tali da non compromettere la sua capacità di resistenza e rigidezza

A partire dalle coordinate del sito della costruzione (**longitudine: 12.2065°; latitudine: 45.7192°**) e dai valori dei parametri sismici relativi ai nodi di un reticolo di riferimento fornito dalla Normativa, si sono determinati, utilizzando il programma in Excel "Spettri di Risposta ver. 1.0.3, i valori caratteristici per ogni stato limite di verifica.

FASE 1. INDIVIDUAZIONE DELLA PERICOLOSITÀ DEL SITO

☒ Ricerca per coordinate

LONGITUDINE

LATITUDINE

☐ Ricerca per comune

REGIONE

PROVINCIA

COMUNE

Elaborazioni grafiche

Grafici spettri di risposta

Variabilità dei parametri

Elaborazioni numeriche

Tabella parametri

Nodi del reticolo intorno al sito

Reticolo di riferimento

Controllo sul reticolo
☒ Sito esterno al reticolo
☐ Interpolazione su 3 nodi
☒ Interpolazione corretta

Interpolazione

La "Ricerca per comune" utilizza le coordinate ISTAT del comune per identificare il sito. Si sottolinea che all'interno del territorio comunale le azioni sismiche possono essere significativamente diverse da quelle così individuate e si consiglia, quindi, la "Ricerca per coordinate".

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FASE 2

FASE 3

FASE 2. SCELTA DELLA STRATEGIA DI PROGETTAZIONE

Vita nominale della costruzione (in anni) - V_N info

Coefficiente d'uso della costruzione - c_U info

Valori di progetto

Periodo di riferimento per la costruzione (in anni) - V_R info

Periodi di ritorno per la definizione dell'azione sismica (in anni) - T_R info

Stati limite di esercizio - SLE {

SLO - $P_{VR} = 81\%$	90
SLD - $P_{VR} = 63\%$	151

Stati limite ultimi - SLU {

SLV - $P_{VR} = 10\%$	1424
SLC - $P_{VR} = 5\%$	2475

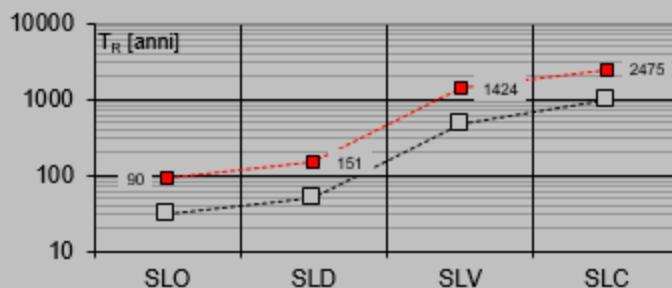
Elaborazioni

Grafici parametri azione

Grafici spettri di risposta

Tabella parametri azione

Strategia di progettazione



LEGENDA GRAFICO

---□--- Strategia per costruzioni ordinarie
 ---■--- Strategia scelta

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Valori dei parametri a_g , F_o , T_C^* per i periodi di ritorno T_R associati a ciascun

SLATO LIMITE	T_R [anni]	a_g [g]	F_o [-]	T_C^* [s]
SLO	90	0,080	2,440	0,276
SLD	151	0,103	2,424	0,291
SLV	1424	0,265	2,479	0,350
SLC	2475	0,330	2,476	0,363

Il fattore di struttura, è determinato da:

- la struttura è considerata pareti non accoppiate in c.a. $q_0 = 3.0$

Tab. 7.3.II – Valori massimi del valore di base q_0 del fattore di comportamento allo SLV per diverse tecniche costruttive ed in funzione della tipologia strutturale e della classe di duttilità CD

Tipologia strutturale	q_0	
	CD "A"	CD "B"
Costruzioni di calcestruzzo (§ 7.4.3.2)		
Strutture a telaio, a pareti accoppiate, miste (v. § 7.4.3.1)	$4,5 \alpha_u / \alpha_1$	$3,0 \alpha_u / \alpha_1$
Strutture a pareti non accoppiate (v. § 7.4.3.1)	$4,0 \alpha_u / \alpha_1$	3,0
Strutture deformabili torsionalmente (v. § 7.4.3.1)	3,0	2,0
Strutture a pendolo inverso (v. § 7.4.3.1)	2,0	1,5
Strutture a pendolo inverso intelaiate monopiano (v. § 7.4.3.1)	3,5	2,5

- la struttura è considerata regolare in altezza.

$$K_R = 1.0$$

$$q = 3.00 * 1.00 * 1.00 = 3.00$$

FASE 3. DETERMINAZIONE DELL'AZIONE DI PROGETTO

Stato Limite

Stato Limite considerato: **SLV** info

Risposta sismica locale

Categoria di sottosuolo: **B** info $S_s = 1,137$ $C_D = 1,357$ info

Categoria topografica: **T1** info $h/H = 1,000$ $S_T = 1,000$ info

(h=quota sito, H=altezza rilievo topografico)

Compon. orizzontale

☐ Spettro di progetto elastico (SLE) Smorzamento ξ (%): **5** $\eta = 1,000$ info

☒ Spettro di progetto inelastico (SLU) Fattore q_0 : **3** Regol. in altezza: **sì** info

Compon. verticale

Spettro di progetto Fattore q : **1,5** $\eta = 0,667$ info

Elaborazioni

Grafici spettri di risposta →

Parametri e punti spettri di risposta →

Spettri di risposta

$S_{d,o}$ [g]
 $S_{d,v}$ [g]
 S_e [g]

— Spettro di progetto - componente orizzontale
 — Spettro di progetto - componente verticale
 — Spettro elastico di riferimento (Cat. A-T1, $\xi = 5\%$)

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Parametri e punti dello spettro di risposta orizzontale per lo stato lir8LV**Parametri indipendenti**

STATO LIMITE	SLV
a_g	0,265 g
F_a	2,479
T_c	0,350 s
S_g	1,137
C_c	1,357
S_T	1,000
q	3,000

Parametri dipendenti

S	1,137
η	0,333
T_B	0,158 s
T_C	0,475 s
T_D	2,661 s

Espressioni dei parametri dipendenti

$$S = S_g \cdot S_T \quad (\text{NTC-08 Eq. 3.2.5})$$

$$\eta = \sqrt{10(5+\xi)} \geq 0,55 \quad \eta = 1/q \quad (\text{NTC-08 Eq. 3.2.6; § 3.2.3.5})$$

$$T_B = T_c / 3 \quad (\text{NTC-07 Eq. 3.2.8})$$

$$T_C = C_c \cdot T_c \quad (\text{NTC-07 Eq. 3.2.7})$$

$$T_D = 4,0 \cdot a_g / g + 1,6 \quad (\text{NTC-07 Eq. 3.2.9})$$

Espressioni dello spettro di risposta (NTC-08 Eq. 3.2.4)

$$\begin{aligned} 0 \leq T < T_B & \quad S_d(T) = a_g \cdot S \cdot \eta \cdot F_a \cdot \left[\frac{T}{T_B} + \frac{1}{\eta \cdot F_a} \left(1 - \frac{T}{T_B} \right) \right] \\ T_B \leq T < T_C & \quad S_d(T) = a_g \cdot S \cdot \eta \cdot F_a \\ T_C \leq T < T_D & \quad S_d(T) = a_g \cdot S \cdot \eta \cdot F_a \cdot \left(\frac{T_C}{T} \right) \\ T_D \leq T & \quad S_d(T) = a_g \cdot S \cdot \eta \cdot F_a \cdot \left(\frac{T_C \cdot T_D}{T^2} \right) \end{aligned}$$

La ppetra di progetto $S_d(T)$ per le verifiche agli Stati Limite Ultimi è ottenuta dalle espressioni della ppetra elastica $S_e(T)$ moltiplicandola con $1/q$, dove q è il fattore di struttura. (NTC-08 § 3.2.3.5)

Punti dello spettro di risposta

	T [s]	Se [g]
	0,000	0,302
$T_B \leftarrow$	0,158	0,249
$T_C \leftarrow$	0,475	0,249
	0,579	0,204
	0,683	0,173
	0,787	0,150
	0,891	0,133
	0,995	0,119
	1,100	0,108
	1,204	0,098
	1,308	0,091
	1,412	0,084
	1,516	0,078
	1,620	0,073
	1,724	0,069
	1,828	0,065
	1,932	0,061
	2,036	0,058
	2,141	0,055
	2,245	0,053
	2,349	0,053
	2,453	0,053
	2,557	0,053
$T_D \leftarrow$	2,661	0,053
	2,725	0,053
	2,789	0,053
	2,852	0,053
	2,916	0,053
	2,980	0,053
	3,044	0,053
	3,107	0,053
	3,171	0,053
	3,235	0,053
	3,299	0,053
	3,362	0,053
	3,426	0,053
	3,490	0,053
	3,554	0,053
	3,617	0,053
	3,681	0,053
	3,745	0,053
	3,809	0,053
	3,872	0,053
	3,936	0,053
	4,000	0,053

4 COMBINAZIONE DELLE AZIONI

Ai fini delle verifiche degli stati limite si definiscono le seguenti combinazioni delle azioni.

- Combinazione fondamentale, generalmente impiegata per gli stati limite ultimi (SLU):

$$\gamma_{G1} \cdot G_1 + \gamma_{G2} \cdot G_2 + \gamma_P \cdot P + \gamma_{Q1} \cdot Q_{k1} + \gamma_{Q2} \cdot \psi_{02} \cdot Q_{k2} + \gamma_{Q3} \cdot \psi_{03} \cdot Q_{k3} + \dots \quad (2.5.1)$$

- Combinazione caratteristica rara, generalmente impiegata per gli stati limite di esercizio (SLE) irreversibili, da utilizzarsi nelle verifiche alle tensioni ammissibili di cui al § 2.7:

$$G_1 + G_2 + P + Q_{k1} + \psi_{02} \cdot Q_{k2} + \psi_{03} \cdot Q_{k3} + \dots \quad (2.5.2)$$

- Combinazione frequente, generalmente impiegata per gli stati limite di esercizio (SLE) reversibili:

$$G_1 + G_2 + P + \psi_{11} \cdot Q_{k1} + \psi_{22} \cdot Q_{k2} + \psi_{23} \cdot Q_{k3} + \dots \quad (2.5.3)$$

- Combinazione quasi permanente (SLE), generalmente impiegata per gli effetti a lungo termine:

$$G_1 + G_2 + P + \psi_{21} \cdot Q_{k1} + \psi_{22} \cdot Q_{k2} + \psi_{23} \cdot Q_{k3} + \dots \quad (2.5.4)$$

- Combinazione sismica, impiegata per gli stati limite ultimi e di esercizio connessi all'azione sismica E:

$$E + G_1 + G_2 + P + \psi_{21} \cdot Q_{k1} + \psi_{22} \cdot Q_{k2} + \dots \quad (2.5.5)$$

Nelle combinazioni per SLE, si intende che vengono omessi i carichi Q_{kj} che danno un contributo favorevole ai fini delle verifiche e, se del caso, i carichi G_2 .

I valori dei coefficienti parziali di sicurezza γ_{Gi} e γ_{Qj} sono:

Categoria/Azione variabile	ψ_{0j}	ψ_{1j}	ψ_{2j}
Categoria A Ambienti ad uso residenziale	0,7	0,5	0,3
Categoria B Uffici	0,7	0,5	0,3
Categoria C Ambienti suscettibili di affollamento	0,7	0,7	0,6
Categoria D Ambienti ad uso commerciale	0,7	0,7	0,6
Categoria E Biblioteche, archivi, magazzini e ambienti ad uso industriale	1,0	0,9	0,8
Categoria F Rimesse e parcheggi (per autoveicoli di peso ≤ 30 kN)	0,7	0,7	0,6
Categoria G Rimesse e parcheggi (per autoveicoli di peso > 30 kN)	0,7	0,5	0,3
Categoria H Coperture	0,0	0,0	0,0
Vento	0,6	0,2	0,0
Neve (a quota ≤ 1000 m s.l.m.)	0,5	0,2	0,0
Neve (a quota > 1000 m s.l.m.)	0,7	0,5	0,2
Variazioni termiche	0,6	0,5	0,0

5 AZIONI NELLE VERIFICHE AGLI STATI LIMITE

Le verifiche agli stati limite sono eseguite per tutte le più gravose condizioni di carico che possono agire sulla struttura, valutando gli effetti delle combinazioni definite sopra.

5.1 Stati Limite Ultimi

Nelle verifiche agli stati limite ultimi si distinguono:

- lo stato limite di equilibrio come corpo rigido: EQU
- lo stato limite di resistenza della struttura compresi gli elementi di fondazione: STR
- lo stato limite di resistenza del terreno: GEO

Di seguito si riportano i valori dei coefficienti parziali delle azioni da assumere per la determinazione degli effetti delle azioni nelle verifiche agli stati limite ultimi.

		Coefficiente γ_F	EQU	A1 STR	A2 GEO
Carichi permanenti	favorevoli	γ_{G1}	0,9	1,0	1,0
	sfavorevoli		1,1	1,3	1,0
Carichi permanenti non strutturali (1)	favorevoli	γ_{G2}	0,0	0,0	0,0
	sfavorevoli		1,5	1,5	1,3
Carichi variabili	sfavorevoli	γ_{Qi}	0,0	0,0	0,0
	sfavorevoli		1,5	1,5	1,3

⁽¹⁾Nel caso in cui i carichi permanenti non strutturali (ad es. carichi permanenti portati) siano compiutamente definiti si potranno adottare per essi gli stessi coefficienti validi per le azioni permanenti

dove:

γ_{G1} coefficiente parziale del peso proprio della struttura, nonché del peso proprio del terreno e

dell'acqua, quando pertinenti;

γ_{G2} coefficiente parziale dei pesi propri degli elementi non strutturali;

γ_{Qi} coefficiente parziale delle azioni variabili.

Nelle verifiche nei confronti degli stati limite ultimi strutturali si è seguito l'approccio 2 previsto dalla normativa, ossia si è impiegata un'unica combinazione dei gruppi di coefficienti parziali definiti per le Azioni (A), per la resistenza dei materiali (M) e per la resistenza globale (R). In tale approccio, per le azioni si impiegano i coefficienti γ_F riportati nella colonna A1.

5.2 Stati Limite di Esercizio

Le verifiche da farsi per la tipologia di opera in esame sono (§4.1.2.2 DM2018):

Verifica di deformabilità

Per assicurare limiti di deformabilità accettabili, si deve confrontare la congruenza delle deformazioni in relazione alla destinazione d'uso e alle esigenze estetiche.

Verifica di fessurazione

Per assicurare la funzionalità e la durata delle opere si deve assicurare che:

- sia garantito un sufficiente ricoprimento delle armature con calcestruzzo di buona qualità e compattezza, bassa porosità e bassa permeabilità;
- non sia superato lo stato limite di fessurazione adeguato alle condizioni ambientali, alle sollecitazioni ed alla sensibilità delle armature alla corrosione;

In base alle condizioni ambientali e al tipo di armatura specifica del caso considerato:

- ambiente molto aggressivo
- armatura poco sensibile alla corrosione

E' assunto il valore limite di apertura delle fessure $w_1=0.2$ mm, come da tabelle seguenti:

Tabella 4.1.III

CONDIZIONI AMBIENTALI	CLASSE DI ESPOSIZIONE
Ordinarie	X0, XC1, XC2, XC3, XF1
Aggressive	XC4, XD1, XS1, XA1, XA2, XF2, XF3
Molto aggressive	XD2, XD3, XS2, XS3, XA3, XF4

Tabella 4.1.IV ($w_1=0.2$ mm; $w_2=0.3$ mm; $w_3=0.4$ mm)

Gruppi di esigenze	Condizioni ambientali	Combinazione di azioni	Armatura			
			Sensibile		Poco sensibile	
			Stato limite	w_d	Stato limite	w_d
a	Ordinarie	frequente	ap. fessure	$\leq w_2$	ap. fessure	$\leq w_3$
		quasi permanente	ap. fessure	$\leq w_1$	ap. fessure	$\leq w_2$
b	Aggressive	frequente	ap. fessure	$\leq w_1$	ap. fessure	$\leq w_2$
		quasi permanente	decompressione	-	ap. fessure	$\leq w_1$
c	Molto aggressive	frequente	formazione fessure	-	ap. fessure	$\leq w_1$
		quasi permanente	decompressione	-	ap. fessure	$\leq w_1$

Verifica delle tensioni di esercizio

Si deve verificare che la tensione massima di esercizio del calcestruzzo sia limitata secondo

$$\sigma_c < 0,60 f_{ck} \quad \text{per combinazione caratteristica (rara)} \quad (4.1.40)$$

$$\sigma_c < 0,45 f_{ck} \quad \text{per combinazione quasi permanente.} \quad (4.1.41)$$

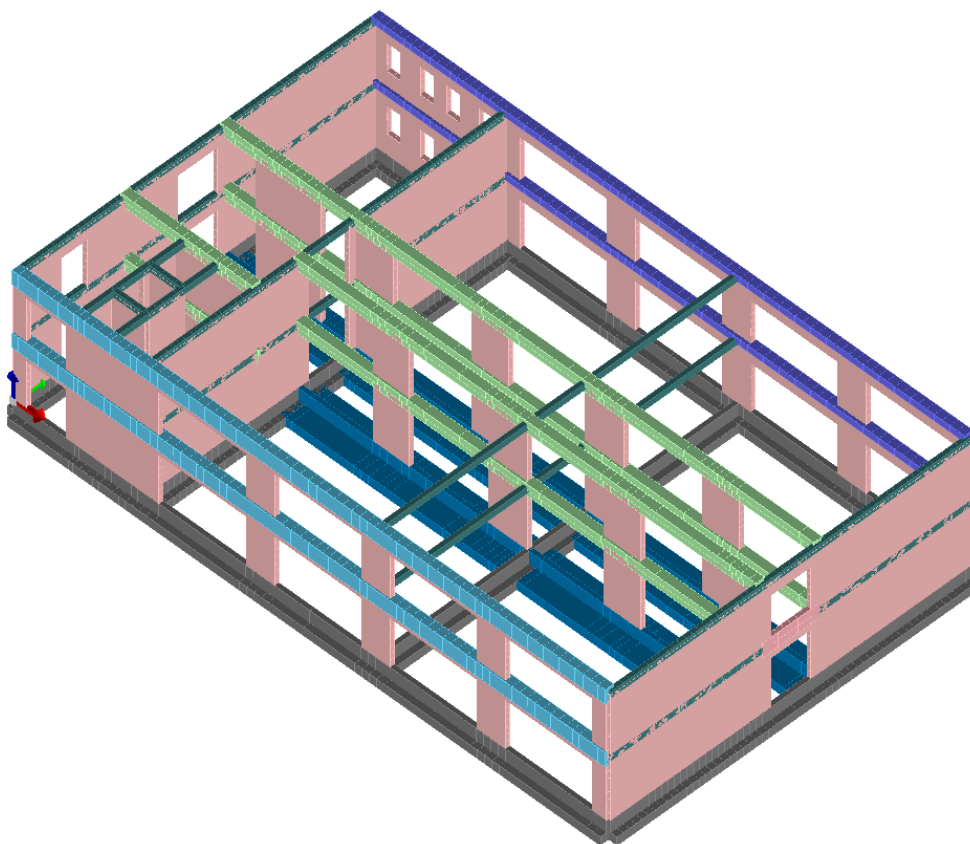
e che la tensione massima di esercizio dell'acciaio sia limitata secondo

$$\sigma_s < 0,8 f_{yk} \quad \text{per combinazione caratteristica (rara)} \quad (4.1.42)$$

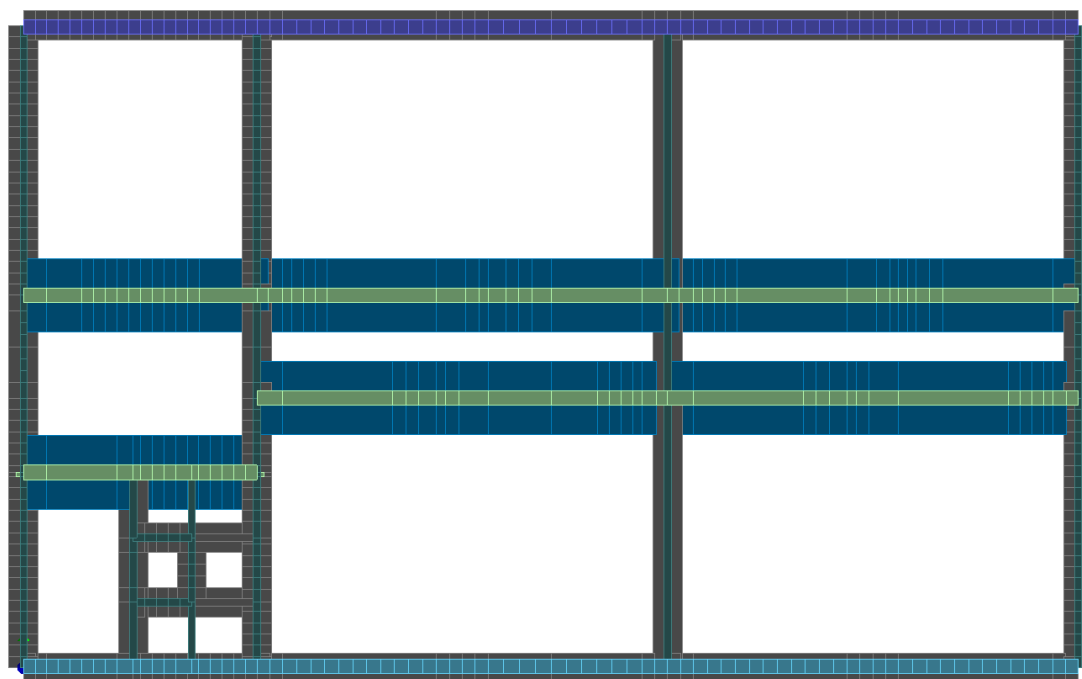
Le verifiche sono svolte, utilizzando le seguenti condizioni:

- si adottano le proprietà geometriche della sezione corrispondente alla condizione fessurata (il cls è considerato elastico in compressione, ma incapace di sostenere la trazione);
- in via semplificata, si assume il comportamento elastico-lineare e per le armature il coefficiente di omogeneizzazione con il valore convenzionale $n=15$;

6 VERIFICA DELLE STRUTTURE DELLA SCUOLA



Vista tridimensionale dello scheletro delle strutture



Vista dall'alto dello scheletro delle strutture

CARATTERISTICHE MATERIALI UTILIZZATI

Il programma consente l'uso di materiali diversi. Sono previsti i seguenti tipi di materiale:

1	materiale tipo cemento armato
2	materiale tipo acciaio
3	materiale tipo muratura
4	materiale tipo legno
5	materiale tipo generico

I materiali utilizzati nella modellazione sono individuati da una sigla identificativa ed un codice numerico (gli elementi strutturali richiamano quest'ultimo nella propria descrizione). Per ogni materiale vengono riportati in tabella i seguenti dati:

Young	modulo di elasticità normale
Poisson	coefficiente di contrazione trasversale
G	modulo di elasticità tangenziale
Gamma	peso specifico
Alfa	coefficiente di dilatazione termica

I dati soprariportati vengono utilizzati per la modellazione dello schema statico e per la determinazione dei carichi inerziali e termici. In relazione al tipo di materiale vengono riportati inoltre:

1	cemento armato	Rck Fctm	resistenza caratteristica cubica resistenza media a trazione semplice
2	acciaio	Ft Fy Fd Fdt Sadm Sadmt	tensione di rottura a trazione tensione di snervamento resistenza di calcolo resistenza di calcolo per spess. $t > 40$ mm tensione ammissibile tensione ammissibile per spess. $t > 40$ mm
3	muratura	Resist. Fk Resist. Fvko	resistenza caratteristica a compressione resistenza caratteristica a taglio
4	legno	Resist. fc0k Resist. ft0k Resist. fmk Resist. fvk Modulo E0,05 Lamellare	Resistenza caratteristica (tensione amm. per REGLES) per compressione Resistenza caratteristica (tensione amm. per REGLES) per trazione Resistenza caratteristica (tensione amm. per REGLES) per flessione Resistenza caratteristica (tensione amm. per REGLES) per taglio Modulo elastico parallelo caratteristico lamellare o massiccio

Vengono inoltre riportate le tabelle contenenti il riassunto delle informazioni assegnate nei criteri di progetto in uso.

Id	Tipo / Note	V. caratt.	V. medio	Young	Poisson	G	Gamma	Alfa	Altri
		daN/cm2	daN/cm2	daN/cm2		daN/cm2	daN/cm3		
1	Calcestruzzo Classe C25/30			3.145e+05	0.20	1.310e+05	2.50e-03	1.00e-05	
	Resistenza Rc	300.0							
	Resistenza fctm		25.6						
	Rapporto Rfessurata								1.00
	Coefficiente ksb								0.85
	Rapporto HRDb								1.00e-05
	Rapporto HRDv								1.00e-05

MODELLAZIONE DELLE SEZIONI

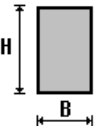
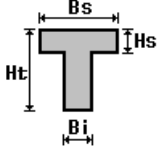
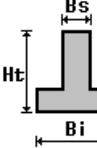
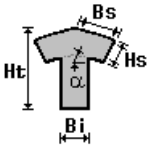
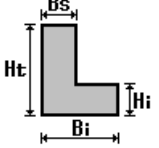
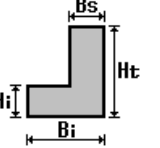
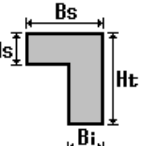
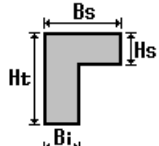
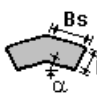
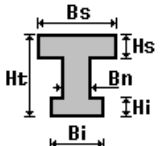
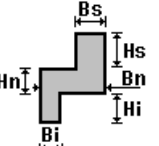
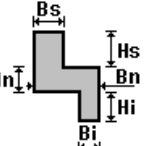
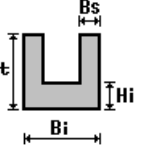
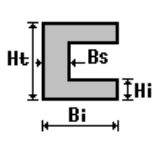
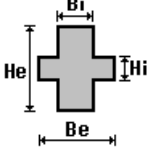
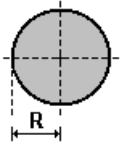
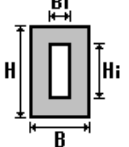
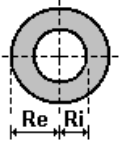
Il programma consente l'uso di sezioni diverse. Sono previsti i seguenti tipi di sezione:

1. sezione di tipo generico
2. profilati semplici
3. profilati accoppiati e speciali

Le sezioni utilizzate nella modellazione sono individuate da una sigla identificativa ed un codice numerico (gli elementi strutturali richiamano quest'ultimo nella propria descrizione). Per ogni sezione vengono riportati in tabella i seguenti dati:

Area	area della sezione
A V2	area della sezione/fattore di taglio (per il taglio in direzione 2)
A V3	area della sezione/fattore di taglio (per il taglio in direzione 3)
Jt	fattore torsionale di rigidezza
J2-2	momento d'inerzia della sezione riferito all'asse 2
J3-3	momento d'inerzia della sezione riferito all'asse 3
W2-2	modulo di resistenza della sezione riferito all'asse 2
W3-3	modulo di resistenza della sezione riferito all'asse 3
Wp2-2	modulo di resistenza plastico della sezione riferito all'asse 2
Wp3-3	modulo di resistenza plastico della sezione riferito all'asse 3

I dati sopra riportati vengono utilizzati per la determinazione dei carichi inerziali e per la definizione delle rigidezze degli elementi strutturali; qualora il valore di Area V2 (e/o Area V3) sia nullo la deformabilità per taglio V2 (e/o V3) è trascurata. La valutazione delle caratteristiche inerziali delle sezioni è condotta nel riferimento 2-3 dell'elemento.

					
rettangolare	a T	a T rovescia	a T di colmo	a L	a L specchiata
					
a L specchiata rovescia	a L rovescia	a L di colmo	a doppio T	a quattro specchiata	a quattro
					
a U	a C	a croce	circolare	rettangolare cava	circolare cava

Per quanto concerne i profilati semplici ed accoppiati l'asse 2 del riferimento coincide con l'asse x riportato nei più diffusi profilati.

Per quanto concerne le sezioni di tipo generico (tipo 1.):

i valori dimensionali con prefisso B sono riferiti all'asse 2

i valori dimensionali con prefisso H sono riferiti all'asse 3

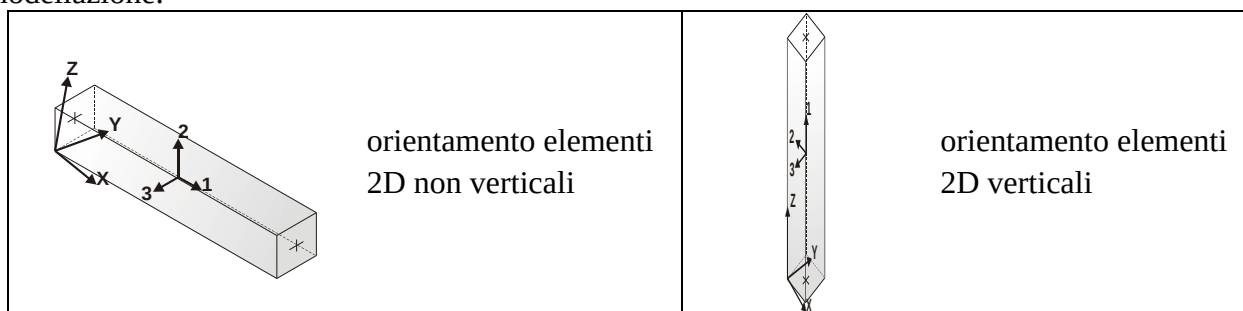
Id	Tipo	Area	A V2	A V3	Jt	J 2-2	J 3-3	W 2-2	W 3-3	Wp 2-2	Wp 3-3
		cm2	cm2	cm2	cm4	cm4	cm4	cm3	cm3	cm3	cm3
1	T rovescia: bi=100 ht=125 bs=25 hi=50	6875.00	0.0	0.0	3.423e+06	4.264e+06	7.247e+06	8.529e+04	8.736e+04	1.367e+05	1.709e+05
2	T rovescia: bi=250 ht=125 bs=25 hi=50	1.438e+04	0.0	0.0	9.673e+06	6.520e+07	9.852e+06	5.216e+05	1.073e+05	7.930e+05	2.699e+05
3	Rettangolare: b=25 h=36	900.00	750.00	750.00	1.071e+05	4.688e+04	9.720e+04	3750.00	5400.00	5625.00	8100.00
4	T ribassata: bi=25 ht=86 bs=50 hs=36	3050.00	0.0	0.0	7.992e+05	4.401e+05	1.819e+06	1.760e+04	3.610e+04	3.031e+04	6.214e+04
5	L inv.ribas.: bi=25 ht=86 bs=50 hs=36	3050.00	0.0	0.0	7.992e+05	5.554e+05	1.819e+06	1.844e+04	3.610e+04	3.358e+04	6.214e+04
6	T rovescia: bi=25 ht=86 bs=50 hs=36	3050.00	0.0	0.0	7.992e+05	5.554e+05	1.819e+06	1.844e+04	3.610e+04	3.358e+04	6.214e+04
8	Rettangolare: b=25 h=86	2150.00	1791.67	1791.67	3.659e+05	1.120e+05	1.325e+06	8958.33	3.082e+04	1.344e+04	4.623e+04

MODELLAZIONE STRUTTURA: ELEMENTI TRAVE

Il programma utilizza per la modellazione elementi a due nodi denominati in generale travi.

Ogni elemento trave è individuato dal nodo iniziale e dal nodo finale.

Ogni elemento è caratterizzato da un insieme di proprietà riportate in tabella che ne completano la modellazione.



In particolare per ogni elemento viene indicato in tabella:

Elem.	numero dell'elemento
Note	codice di comportamento: trave, trave di fondazione, pilastro, asta, asta tesa, asta compressa,
Nodo I (J)	numero del nodo iniziale (finale)
Mat.	codice del materiale assegnato all'elemento
Sez.	codice della sezione assegnata all'elemento
Rotaz.	valore della rotazione dell'elemento, attorno al proprio asse, nel caso in cui l'orientamento di default non sia adottabile; l'orientamento di default prevede per gli elementi non verticali l'asse 2 contenuto nel piano verticale e l'asse 3 orizzontale, per gli elementi verticali l'asse 2 diretto secondo X negativo e l'asse 3 diretto secondo Y negativo
Svincolo I (J)	codici di svincolo per le azioni interne; i primi sei codici si riferiscono al nodo iniziale, i restanti sei al nodo finale (il valore 1 indica che la relativa azione interna non è attiva)
Wink V	costante di sottofondo (coefficiente di Winkler) per la modellazione della trave su suolo elastico
Wink O	costante di sottofondo (coefficiente di Winkler) per la modellazione del suolo elastico orizzontale

Elem.	Note	Nodo I	Nodo J	Mat.	Sez.	Rotaz.	Svincolo I gradi	Svincolo J	Wink V	Wink O daN/cm3	daN/cm3
1	Trave f.		1	1787	1	1				4.00	1.00
2	Trave f.		37	988	1	1				4.00	1.00

3	Trave f.	12	472	1	1	4.00	1.00
4	Trave f.	1	156	1	1	4.00	1.00
5	Trave f.	64	14	1	2	4.00	1.00
6	Trave f.	25	26	1	2	4.00	1.00
7	Trave f.	4	1295	1	1	4.00	1.00
8	Trave f.	53	2272	1	1	4.00	1.00
9	Trave f.	54	43	1	1	4.00	1.00
10	Trave f.	55	67	1	1	4.00	1.00
11	Trave f.	56	7	1	1	4.00	1.00
12	Trave f.	57	2773	1	2	4.00	1.00
13	Trave f.	58	31	1	2	4.00	1.00
14	Trave f.	59	69	1	1	4.00	1.00
15	Trave f.	13	2273	1	1	4.00	1.00
16	Trave f.	38	2938	1	1	4.00	1.00
17	Trave f.	24	66	1	1	4.00	1.00
18	Trave f.	2	3	1	1	4.00	1.00
19	Trave f.	14	15	1	2	4.00	1.00
20	Trave f.	26	2299	1	2	4.00	1.00
21	Trave f.	16	68	1	1	4.00	1.00
22	Trave f.	25	2254	1	1	4.00	1.00
23	Trave f.	43	1189	1	1	4.00	1.00
24	Trave f.	36	946	1	1	4.00	1.00
25	Trave f.	7	357	1	1	4.00	1.00
26	Trave f.	19	2824	1	2	4.00	1.00
27	Trave f.	31	63	1	2	4.00	1.00
28	Trave f.	28	1762	1	1	4.00	1.00
29	Trave f.	39	999	1	1	4.00	1.00
30	Trave f.	3	167	1	1	4.00	1.00
31	Trave f.	15	3130	1	2	4.00	1.00
32	Trave f.	27	2342	1	2	4.00	1.00
33	Trave f.	44	45	1	1	4.00	1.00
34	Trave f.	8	9	1	1	4.00	1.00
35	Trave f.	20	2717	1	2	4.00	1.00
36	Trave f.	32	2554	1	2	4.00	1.00
37	Trave f.	40	1124	1	1	4.00	1.00
38	Trave f.	4	292	1	1	4.00	1.00
39	Trave f.	16	50	1	2	4.00	1.00
40	Trave f.	28	2460	1	2	4.00	1.00
41	Trave f.	45	1233	1	1	4.00	1.00
42	Trave f.	9	401	1	1	4.00	1.00
43	Trave f.	21	2721	1	2	4.00	1.00
44	Trave f.	33	2589	1	2	4.00	1.00
45	Trave f.	41	1143	1	1	4.00	1.00
46	Trave f.	5	311	1	1	4.00	1.00
47	Trave f.	17	2882	1	2	4.00	1.00
48	Trave f.	29	2465	1	2	4.00	1.00
49	Trave f.	46	47	1	1	4.00	1.00
50	Trave f.	10	11	1	1	4.00	1.00
51	Trave f.	22	2617	1	2	4.00	1.00
52	Trave f.	34	2677	1	2	4.00	1.00
53	Trave f.	52	41	1	1	4.00	1.00
54	Trave f.	49	5	1	1	4.00	1.00
55	Trave f.	50	2841	1	2	4.00	1.00
56	Trave f.	51	2440	1	2	4.00	1.00
57	Trave f.	42	54	1	1	4.00	1.00
58	Trave f.	6	56	1	1	4.00	1.00
59	Trave f.	18	57	1	2	4.00	1.00
60	Trave f.	30	2498	1	2	4.00	1.00
61	Trave f.	47	1279	1	1	4.00	1.00
62	Trave f.	11	447	1	1	4.00	1.00
63	Trave f.	23	2676	1	2	4.00	1.00
64	Trave f.	35	36	1	2	4.00	1.00
65	Trave f.	60	1214	1	1	4.00	1.00
66	Trave f.	61	382	1	1	4.00	1.00
67	Trave f.	61	62	1	1	4.00	1.00
68	Trave f.	62	20	1	2	4.00	1.00
69	Trave f.	63	2574	1	2	4.00	1.00
70	Trave f.	62	63	1	1	4.00	1.00
71	Trave f.	63	60	1	1	4.00	1.00
72	Trave f.	64	1957	1	1	4.00	1.00
73	Trave f.	65	1465	1	1	4.00	1.00
74	Trave f.	67	36	1	1	4.00	1.00
75	Trave f.	69	28	1	1	4.00	1.00
76	Trave f.	66	55	1	1	4.00	1.00
77	Trave f.	68	59	1	1	4.00	1.00
78	Trave f.	1787	1797	1	1	4.00	1.00
79	Trave f.	988	38	1	1	4.00	1.00
80	Trave f.	472	482	1	1	4.00	1.00
81	Trave f.	156	2	1	1	4.00	1.00
82	Trave f.	1295	1305	1	1	4.00	1.00
83	Trave f.	2272	25	1	1	4.00	1.00
84	Trave f.	2273	53	1	1	4.00	1.00
85	Trave f.	2034	37	1	1	4.00	1.00
86	Trave f.	1189	60	1	1	4.00	1.00
87	Trave f.	726	48	1	1	4.00	1.00
88	Trave f.	357	61	1	1	4.00	1.00
89	Trave f.	1542	40	1	1	4.00	1.00
90	Trave f.	999	1016	1	1	4.00	1.00
91	Trave f.	167	184	1	1	4.00	1.00
92	Trave f.	1124	52	1	1	4.00	1.00
93	Trave f.	292	49	1	1	4.00	1.00
94	Trave f.	1233	1250	1	1	4.00	1.00
95	Trave f.	401	418	1	1	4.00	1.00
96	Trave f.	1143	1160	1	1	4.00	1.00
97	Trave f.	311	328	1	1	4.00	1.00
98	Trave f.	1279	48	1	1	4.00	1.00
99	Trave f.	447	12	1	1	4.00	1.00
100	Trave f.	1214	44	1	1	4.00	1.00
101	Trave f.	382	8	1	1	4.00	1.00
102	Trave f.	1957	1967	1	1	4.00	1.00
103	Trave f.	1465	1475	1	1	4.00	1.00

104	Trave f.	2044	2034	1	1	4.00	1.00
105	Trave f.	736	726	1	1	4.00	1.00
106	Trave f.	1552	1542	1	1	4.00	1.00
107	Trave f.	1797	1807	1	1	4.00	1.00
108	Trave f.	482	492	1	1	4.00	1.00
109	Trave f.	1305	1315	1	1	4.00	1.00
110	Trave f.	1016	1026	1	1	4.00	1.00
111	Trave f.	184	194	1	1	4.00	1.00
112	Trave f.	1250	1260	1	1	4.00	1.00
113	Trave f.	418	428	1	1	4.00	1.00
114	Trave f.	1160	1170	1	1	4.00	1.00
115	Trave f.	328	338	1	1	4.00	1.00
116	Trave f.	1967	1977	1	1	4.00	1.00
117	Trave f.	1475	1485	1	1	4.00	1.00
118	Trave f.	2054	2044	1	1	4.00	1.00
119	Trave f.	746	736	1	1	4.00	1.00
120	Trave f.	1562	1552	1	1	4.00	1.00
121	Trave f.	1807	1817	1	1	4.00	1.00
122	Trave f.	492	502	1	1	4.00	1.00
123	Trave f.	1315	1325	1	1	4.00	1.00
124	Trave f.	1026	1036	1	1	4.00	1.00
125	Trave f.	194	204	1	1	4.00	1.00
126	Trave f.	1260	46	1	1	4.00	1.00
127	Trave f.	428	10	1	1	4.00	1.00
128	Trave f.	1170	42	1	1	4.00	1.00
129	Trave f.	338	6	1	1	4.00	1.00
130	Trave f.	1977	1987	1	1	4.00	1.00
131	Trave f.	1485	1495	1	1	4.00	1.00
132	Trave f.	2064	2054	1	1	4.00	1.00
133	Trave f.	756	746	1	1	4.00	1.00
134	Trave f.	1572	1562	1	1	4.00	1.00
135	Trave f.	1817	1827	1	1	4.00	1.00
136	Trave f.	502	512	1	1	4.00	1.00
137	Trave f.	1325	1335	1	1	4.00	1.00
138	Trave f.	1036	1046	1	1	4.00	1.00
139	Trave f.	204	214	1	1	4.00	1.00
140	Trave f.	1987	1997	1	1	4.00	1.00
141	Trave f.	1495	1505	1	1	4.00	1.00
142	Trave f.	2074	2064	1	1	4.00	1.00
143	Trave f.	766	756	1	1	4.00	1.00
144	Trave f.	1582	1572	1	1	4.00	1.00
145	Trave f.	1827	1837	1	1	4.00	1.00
146	Trave f.	512	522	1	1	4.00	1.00
147	Trave f.	1335	1345	1	1	4.00	1.00
148	Trave f.	1046	1056	1	1	4.00	1.00
149	Trave f.	214	224	1	1	4.00	1.00
150	Trave f.	1997	2007	1	1	4.00	1.00
151	Trave f.	1505	1515	1	1	4.00	1.00
152	Trave f.	2084	2074	1	1	4.00	1.00
153	Trave f.	776	766	1	1	4.00	1.00
154	Trave f.	1592	1582	1	1	4.00	1.00
155	Trave f.	1837	1847	1	1	4.00	1.00
156	Trave f.	522	532	1	1	4.00	1.00
157	Trave f.	1345	1355	1	1	4.00	1.00
158	Trave f.	1056	1066	1	1	4.00	1.00
159	Trave f.	224	234	1	1	4.00	1.00
160	Trave f.	2007	13	1	1	4.00	1.00
161	Trave f.	1515	16	1	1	4.00	1.00
162	Trave f.	2094	2084	1	1	4.00	1.00
163	Trave f.	786	776	1	1	4.00	1.00
164	Trave f.	1602	1592	1	1	4.00	1.00
165	Trave f.	1847	1857	1	1	4.00	1.00
166	Trave f.	532	542	1	1	4.00	1.00
167	Trave f.	1355	1365	1	1	4.00	1.00
168	Trave f.	1066	1076	1	1	4.00	1.00
169	Trave f.	234	244	1	1	4.00	1.00
170	Trave f.	2104	2094	1	1	4.00	1.00
171	Trave f.	796	786	1	1	4.00	1.00
172	Trave f.	1612	1602	1	1	4.00	1.00
173	Trave f.	1857	1867	1	1	4.00	1.00
174	Trave f.	542	552	1	1	4.00	1.00
175	Trave f.	1365	1375	1	1	4.00	1.00
176	Trave f.	1076	1086	1	1	4.00	1.00
177	Trave f.	244	254	1	1	4.00	1.00
178	Trave f.	2114	2104	1	1	4.00	1.00
179	Trave f.	806	796	1	1	4.00	1.00
180	Trave f.	1622	1612	1	1	4.00	1.00
181	Trave f.	1867	1877	1	1	4.00	1.00
182	Trave f.	552	562	1	1	4.00	1.00
183	Trave f.	1375	1385	1	1	4.00	1.00
184	Trave f.	1086	1096	1	1	4.00	1.00
185	Trave f.	254	264	1	1	4.00	1.00
186	Trave f.	2124	2114	1	1	4.00	1.00
187	Trave f.	816	806	1	1	4.00	1.00
188	Trave f.	1632	1622	1	1	4.00	1.00
189	Trave f.	1877	1887	1	1	4.00	1.00
190	Trave f.	562	572	1	1	4.00	1.00
191	Trave f.	1385	1395	1	1	4.00	1.00
192	Trave f.	1096	1106	1	1	4.00	1.00
193	Trave f.	264	274	1	1	4.00	1.00
194	Trave f.	2134	2124	1	1	4.00	1.00
195	Trave f.	826	816	1	1	4.00	1.00
196	Trave f.	1642	1632	1	1	4.00	1.00
197	Trave f.	1887	1897	1	1	4.00	1.00
198	Trave f.	572	582	1	1	4.00	1.00
199	Trave f.	1395	1405	1	1	4.00	1.00
200	Trave f.	1106	40	1	1	4.00	1.00
201	Trave f.	274	4	1	1	4.00	1.00
202	Trave f.	2144	2134	1	1	4.00	1.00
203	Trave f.	836	826	1	1	4.00	1.00
204	Trave f.	1652	1642	1	1	4.00	1.00

205	Trave f.	1897	1907	1	1	4.00	1.00
206	Trave f.	582	592	1	1	4.00	1.00
207	Trave f.	1405	1415	1	1	4.00	1.00
208	Trave f.	2154	2144	1	1	4.00	1.00
209	Trave f.	846	836	1	1	4.00	1.00
210	Trave f.	1662	1652	1	1	4.00	1.00
211	Trave f.	1907	1917	1	1	4.00	1.00
212	Trave f.	592	602	1	1	4.00	1.00
213	Trave f.	1415	1425	1	1	4.00	1.00
214	Trave f.	2164	2154	1	1	4.00	1.00
215	Trave f.	856	846	1	1	4.00	1.00
216	Trave f.	1672	1662	1	1	4.00	1.00
217	Trave f.	1917	1927	1	1	4.00	1.00
218	Trave f.	602	612	1	1	4.00	1.00
219	Trave f.	1425	1435	1	1	4.00	1.00
220	Trave f.	2174	2164	1	1	4.00	1.00
221	Trave f.	866	856	1	1	4.00	1.00
222	Trave f.	1682	1672	1	1	4.00	1.00
223	Trave f.	1927	1937	1	1	4.00	1.00
224	Trave f.	612	622	1	1	4.00	1.00
225	Trave f.	1435	1445	1	1	4.00	1.00
226	Trave f.	2184	2174	1	1	4.00	1.00
227	Trave f.	876	866	1	1	4.00	1.00
228	Trave f.	1692	1682	1	1	4.00	1.00
229	Trave f.	1937	1947	1	1	4.00	1.00
230	Trave f.	622	632	1	1	4.00	1.00
231	Trave f.	1445	1455	1	1	4.00	1.00
232	Trave f.	2194	2184	1	1	4.00	1.00
233	Trave f.	886	876	1	1	4.00	1.00
234	Trave f.	1702	1692	1	1	4.00	1.00
235	Trave f.	1947	64	1	1	4.00	1.00
236	Trave f.	632	642	1	1	4.00	1.00
237	Trave f.	1455	65	1	1	4.00	1.00
238	Trave f.	2204	2194	1	1	4.00	1.00
239	Trave f.	896	886	1	1	4.00	1.00
240	Trave f.	1712	1702	1	1	4.00	1.00
241	Trave f.	642	652	1	1	4.00	1.00
242	Trave f.	2214	2204	1	1	4.00	1.00
243	Trave f.	906	896	1	1	4.00	1.00
244	Trave f.	1722	1712	1	1	4.00	1.00
245	Trave f.	652	662	1	1	4.00	1.00
246	Trave f.	2224	2214	1	1	4.00	1.00
247	Trave f.	916	906	1	1	4.00	1.00
248	Trave f.	1732	1722	1	1	4.00	1.00
249	Trave f.	662	672	1	1	4.00	1.00
250	Trave f.	2234	2224	1	1	4.00	1.00
251	Trave f.	926	916	1	1	4.00	1.00
252	Trave f.	1742	1732	1	1	4.00	1.00
253	Trave f.	672	682	1	1	4.00	1.00
254	Trave f.	2244	2234	1	1	4.00	1.00
255	Trave f.	936	926	1	1	4.00	1.00
256	Trave f.	1752	1742	1	1	4.00	1.00
257	Trave f.	682	692	1	1	4.00	1.00
258	Trave f.	2254	2244	1	1	4.00	1.00
259	Trave f.	946	936	1	1	4.00	1.00
260	Trave f.	1762	1752	1	1	4.00	1.00
261	Trave f.	692	24	1	1	4.00	1.00
262	Trave f.	2299	2304	1	2	4.00	1.00
263	Trave f.	2300	28	1	2	4.00	1.00
264	Trave f.	2460	51	1	2	4.00	1.00
265	Trave f.	2409	29	1	2	4.00	1.00
266	Trave f.	2342	2352	1	2	4.00	1.00
267	Trave f.	2412	2409	1	2	4.00	1.00
268	Trave f.	2304	2322	1	2	4.00	1.00
269	Trave f.	2430	2412	1	2	4.00	1.00
270	Trave f.	2352	2362	1	2	4.00	1.00
271	Trave f.	2322	27	1	2	4.00	1.00
272	Trave f.	2440	2430	1	2	4.00	1.00
273	Trave f.	2362	2372	1	2	4.00	1.00
274	Trave f.	2372	2382	1	2	4.00	1.00
275	Trave f.	2382	2392	1	2	4.00	1.00
276	Trave f.	2392	2300	1	2	4.00	1.00
277	Trave f.	2465	2470	1	2	4.00	1.00
278	Trave f.	2466	58	1	2	4.00	1.00
279	Trave f.	2498	2508	1	2	4.00	1.00
280	Trave f.	2470	30	1	2	4.00	1.00
281	Trave f.	2508	2466	1	2	4.00	1.00
282	Trave f.	2523	33	1	2	4.00	1.00
283	Trave f.	2574	32	1	2	4.00	1.00
284	Trave f.	2526	2523	1	2	4.00	1.00
285	Trave f.	2544	2526	1	2	4.00	1.00
286	Trave f.	2554	2544	1	2	4.00	1.00
287	Trave f.	2589	2600	1	2	4.00	1.00
288	Trave f.	2591	35	1	2	4.00	1.00
289	Trave f.	2610	2615	1	2	4.00	1.00
290	Trave f.	2600	34	1	2	4.00	1.00
291	Trave f.	2615	2591	1	2	4.00	1.00
292	Trave f.	2677	2610	1	2	4.00	1.00
293	Trave f.	2617	2636	1	2	4.00	1.00
294	Trave f.	2676	24	1	2	4.00	1.00
295	Trave f.	2636	2646	1	2	4.00	1.00
296	Trave f.	2646	2656	1	2	4.00	1.00
297	Trave f.	2656	23	1	2	4.00	1.00
298	Trave f.	2717	2758	1	2	4.00	1.00
299	Trave f.	2715	22	1	2	4.00	1.00
300	Trave f.	2721	2715	1	2	4.00	1.00
301	Trave f.	2748	21	1	2	4.00	1.00
302	Trave f.	2758	2748	1	2	4.00	1.00
303	Trave f.	2773	2776	1	2	4.00	1.00
304	Trave f.	2824	62	1	2	4.00	1.00
305	Trave f.	2776	2794	1	2	4.00	1.00

306	Trave f.	2794	2804	1	2	4.00	1.00
307	Trave f.	2804	19	1	2	4.00	1.00
308	Trave f.	2839	18	1	2	4.00	1.00
309	Trave f.	2841	2845	1	2	4.00	1.00
310	Trave f.	2882	2839	1	2	4.00	1.00
311	Trave f.	2845	2862	1	2	4.00	1.00
312	Trave f.	2862	17	1	2	4.00	1.00
313	Trave f.	2898	39	1	1	4.00	1.00
314	Trave f.	2908	2898	1	1	4.00	1.00
315	Trave f.	2918	2908	1	1	4.00	1.00
316	Trave f.	2928	2918	1	1	4.00	1.00
317	Trave f.	2938	2928	1	1	4.00	1.00
318	Trave f.	2947	3034	1	1	4.00	1.00
319	Trave f.	2949	2953	1	1	4.00	1.00
320	Trave f.	2959	3082	1	1	4.00	1.00
321	Trave f.	2947	2951	1	1	4.00	1.00
322	Trave f.	2949	1345	1	1	4.00	1.00
323	Trave f.	2961	1405	1	1	4.00	1.00
324	Trave f.	167	2947	1	1	4.00	1.00
325	Trave f.	2997	2949	1	1	4.00	1.00
326	Trave f.	2953	3118	1	1	4.00	1.00
327	Trave f.	3045	2961	1	1	4.00	1.00
328	Trave f.	2951	2955	1	1	4.00	1.00
329	Trave f.	3014	2997	1	1	4.00	1.00
330	Trave f.	3062	3045	1	1	4.00	1.00
331	Trave f.	2957	2961	1	1	4.00	1.00
332	Trave f.	2955	2959	1	1	4.00	1.00
333	Trave f.	3024	3014	1	1	4.00	1.00
334	Trave f.	3072	3062	1	1	4.00	1.00
335	Trave f.	3108	2957	1	1	4.00	1.00
336	Trave f.	3034	3024	1	1	4.00	1.00
337	Trave f.	3082	3072	1	1	4.00	1.00
338	Trave f.	3118	3108	1	1	4.00	1.00
339	Trave	5042	5052	1	3		
340	Trave	70	1796	1	3		
341	Trave	5002	5012	1	3		
342	Trave	81	480	1	3		
343	Trave	133	83	1	4		
344	Trave	182	2948	1	3		
345	Trave	2948	2952	1	3		
346	Trave	2960	3127	1	3		
347	Trave	2960	3090	1	3		
348	Trave	2950	2954	1	3		
349	Trave	2948	3042	1	3		
350	Trave	73	1304	1	3		
351	Trave	94	95	1	4		
352	Trave	85	119	1	4		
353	Trave	97	2340	1	4		
354	Trave	2791	2792	1	4		
355	Trave	4550	4560	1	3		
356	Trave	82	2282	1	3		
357	Trave	4510	4520	1	3		
358	Trave	93	135	1	8		
359	Trave	83	84	1	4		
360	Trave	2952	2956	1	3		
361	Trave	3060	2962	1	3		
362	Trave	2954	3126	1	3		
363	Trave	3012	2950	1	3		
364	Trave	85	137	1	3		
365	Trave	95	2319	1	4		
366	Trave	86	2890	1	4		
367	Trave	98	2485	1	4		
368	Trave	88	2832	1	4		
369	Trave	3736	3746	1	3		
370	Trave	133	1966	1	3		
371	Trave	3696	3706	1	3		
372	Trave	480	490	1	3		
373	Trave	3070	3060	1	3		
374	Trave	3022	3012	1	3		
375	Trave	134	1474	1	3		
376	Trave	119	2842	1	4		
377	Trave	120	2448	1	4		
378	Trave	2792	2802	1	4		
379	Trave	4034	4024	1	3		
380	Trave	94	2246	1	3		
381	Trave	5242	5232	1	3		
382	Trave	105	938	1	3		
383	Trave	84	3127	1	4		
384	Trave	2956	2960	1	3		
385	Trave	2958	2962	1	3		
386	Trave	97	1754	1	3		
387	Trave	96	2350	1	4		
388	Trave	87	126	1	4		
389	Trave	99	2506	1	4		
390	Trave	89	2718	1	4		
391	Trave	1796	1806	1	3		
392	Trave	3080	3070	1	3		
393	Trave	3032	3022	1	3		
394	Trave	1304	1314	1	3		
395	Trave	2340	120	1	4		
396	Trave	5282	5272	1	3		
397	Trave f.	2959	3130	1	1	4.00	1.00
398	Trave	124	6387	1	8		
399	Trave	3116	2958	1	3		
400	Trave	128	138	1	3		
401	Trave	2319	2320	1	4		
402	Trave	2840	87	1	4		
403	Trave	2485	2486	1	4		
404	Trave	131	89	1	4		
405	Trave	1966	1976	1	3		
406	Trave	490	500	1	3		

407	Trave	1474	1484	1	3
408	Trave	2842	2860	1	4
409	Trave	2427	98	1	4
410	Trave	2802	2812	1	4
411	Trave	4850	4840	1	3
412	Trave	2026	106	1	3
413	Trave	3934	3924	1	3
414	Trave	711	117	1	3
415	Trave	3127	3154	1	4
416	Trave	1534	109	1	3
417	Trave	2301	97	1	4
418	Trave	126	2791	1	4
419	Trave	100	132	1	4
420	Trave	90	2736	1	4
421	Trave	3090	3080	1	3
422	Trave	3042	3032	1	3
423	Trave	3806	5983	1	3
424	Trave	2282	6119	1	3
425	Trave	135	6389	1	8
426	Trave	3126	3116	1	3
427	Trave	137	128	1	3
428	Trave	2890	2840	1	4
429	Trave	2832	131	1	4
430	Trave	2428	2427	1	4
431	Trave	5352	5342	1	3
432	Trave	2036	2026	1	3
433	Trave	4750	4740	1	3
434	Trave	728	711	1	3
435	Trave	1544	1534	1	3
436	Trave	2350	2360	1	4
437	Trave	127	100	1	4
438	Trave	2718	2766	1	4
439	Trave	1806	1816	1	3
440	Trave	1314	1324	1	3
441	Trave	122	94	1	3
442	Trave	136	105	1	8
443	Trave	138	97	1	3
444	Trave	2320	2330	1	4
445	Trave	2486	99	1	4
446	Trave	1976	1986	1	3
447	Trave	500	510	1	3
448	Trave	1484	1494	1	3
449	Trave	2860	2870	1	4
450	Trave	2812	88	1	4
451	Trave	3974	3964	1	3
452	Trave	3776	3786	1	3
453	Trave	101	2562	1	4
454	Trave	91	2618	1	4
455	Trave	4044	4034	1	3
456	Trave	2438	2428	1	4
457	Trave	2046	2036	1	3
458	Trave	738	728	1	3
459	Trave	1554	1544	1	3
460	Trave	2467	127	1	4
461	Trave	4860	4850	1	3
462	Trave	5322	5312	1	3
463	Trave	132	2582	1	4
464	Trave	2716	91	1	4
465	Trave	6011	6046	1	4
466	Trave	4220	6009	1	6
467	Trave	2360	2370	1	4
468	Trave	2756	90	1	4
469	Trave	1816	1826	1	3
470	Trave	1324	1334	1	3
471	Trave	2330	96	1	4
472	Trave	1986	1996	1	3
473	Trave	510	520	1	3
474	Trave	1494	1504	1	3
475	Trave	2870	86	1	4
476	Trave	6046	6047	1	4
477	Trave	3388	5973	1	5
478	Trave	102	2666	1	4
479	Trave	92	2668	1	4
480	Trave	6047	6048	1	4
481	Trave	2448	2438	1	4
482	Trave	2056	2046	1	3
483	Trave	748	738	1	3
484	Trave	1564	1554	1	3
485	Trave	2506	2516	1	4
486	Trave	4790	4780	1	3
487	Trave	5012	5022	1	3
488	Trave	2736	2716	1	4
489	Trave	2766	2756	1	4
490	Trave	5052	5062	1	3
491	Trave	4014	4004	1	3
492	Trave	2541	102	1	4
493	Trave	2618	2621	1	4
494	Trave	2582	101	1	4
495	Trave	6048	6049	1	4
496	Trave	4520	4530	1	3
497	Trave	2370	2380	1	4
498	Trave	1826	1836	1	3
499	Trave	1334	1344	1	3
500	Trave	1996	2006	1	3
501	Trave	520	530	1	3
502	Trave	1504	1514	1	3
503	Trave	4560	4570	1	3
504	Trave	3706	3716	1	3
505	Trave	103	2680	1	4
506	Trave	2668	93	1	4
507	Trave	3746	3756	1	3

508	Trave	2066	2056	1	3
509	Trave	758	748	1	3
510	Trave	1574	1564	1	3
511	Trave	2542	2541	1	4
512	Trave	5292	5282	1	3
513	Trave	4830	4820	1	3
514	Trave	2666	2707	1	4
515	Trave	2516	2467	1	4
516	Trave	6049	6050	1	4
517	Trave	5252	5242	1	3
518	Trave	2621	2638	1	4
519	Trave	6050	6051	1	4
520	Trave	3944	3934	1	3
521	Trave	2380	2390	1	4
522	Trave	1836	1846	1	3
523	Trave	1344	1354	1	3
524	Trave	2006	2016	1	3
525	Trave	530	540	1	3
526	Trave	1514	1524	1	3
527	Trave	6051	6052	1	4
528	Trave	3786	3796	1	3
529	Trave	104	105	1	4
530	Trave	2076	2066	1	3
531	Trave	768	758	1	3
532	Trave	1584	1574	1	3
533	Trave	2552	2542	1	4
534	Trave	6052	6053	1	4
535	Trave	4760	4750	1	3
536	Trave	2603	104	1	4
537	Trave	2707	103	1	4
538	Trave	6053	6054	1	4
539	Trave	5022	5032	1	3
540	Trave	2638	2648	1	4
541	Trave	3984	3974	1	3
542	Trave	4530	4540	1	3
543	Trave	2390	2400	1	4
544	Trave	1846	1856	1	3
545	Trave	1354	1364	1	3
546	Trave	2016	82	1	3
547	Trave	540	550	1	3
548	Trave	1524	85	1	3
549	Trave	4800	4790	1	3
550	Trave	5332	5322	1	3
551	Trave	2086	2076	1	3
552	Trave	778	768	1	3
553	Trave	1594	1584	1	3
554	Trave	2562	2552	1	4
555	Trave	5062	5965	1	3
556	Trave	4024	4014	1	3
557	Trave	2604	2603	1	4
558	Trave	4570	5992	1	3
559	Trave	3716	3726	1	3
560	Trave	2648	92	1	4
561	Trave	3756	3766	1	3
562	Trave	5262	5252	1	3
563	Trave	2400	2301	1	4
564	Trave	1856	1866	1	3
565	Trave	1364	1374	1	3
566	Trave	550	560	1	3
567	Trave	6054	5992	1	4
568	Trave	4840	4830	1	3
569	Trave	2096	2086	1	3
570	Trave	788	778	1	3
571	Trave	1604	1594	1	3
572	Trave	2607	2604	1	4
573	Trave	5302	5292	1	3
574	Trave	3796	3806	1	3
575	Trave	6041	6008	1	3
576	Trave	3954	3944	1	3
577	Trave	1866	1876	1	3
578	Trave	1374	1384	1	3
579	Trave	560	570	1	3
580	Trave	3994	3984	1	3
581	Trave	4770	4760	1	3
582	Trave	2106	2096	1	3
583	Trave	798	788	1	3
584	Trave	1614	1604	1	3
585	Trave	2680	2607	1	4
586	Trave	6008	6014	1	3
587	Trave	5032	5042	1	3
588	Trave	4810	4800	1	3
589	Trave	4540	4550	1	3
590	Trave	1876	1886	1	3
591	Trave	1384	1394	1	3
592	Trave	570	580	1	3
593	Trave	3766	3776	1	3
594	Trave	5342	5332	1	3
595	Trave	2116	2106	1	3
596	Trave	808	798	1	3
597	Trave	1624	1614	1	3
598	Trave	6014	6040	1	3
599	Trave	3726	3736	1	3
600	Trave	5312	5302	1	3
601	Trave	5272	5262	1	3
602	Trave	1886	1896	1	3
603	Trave	1394	1404	1	3
604	Trave	580	590	1	3
605	Trave	2126	2116	1	3
606	Trave	818	808	1	3
607	Trave	1634	1624	1	3
608	Trave	4004	3994	1	3

609	Trave	3964	3954	1	3		
610	Trave	1896	1906	1	3		
611	Trave	1404	1414	1	3		
612	Trave	590	600	1	3		
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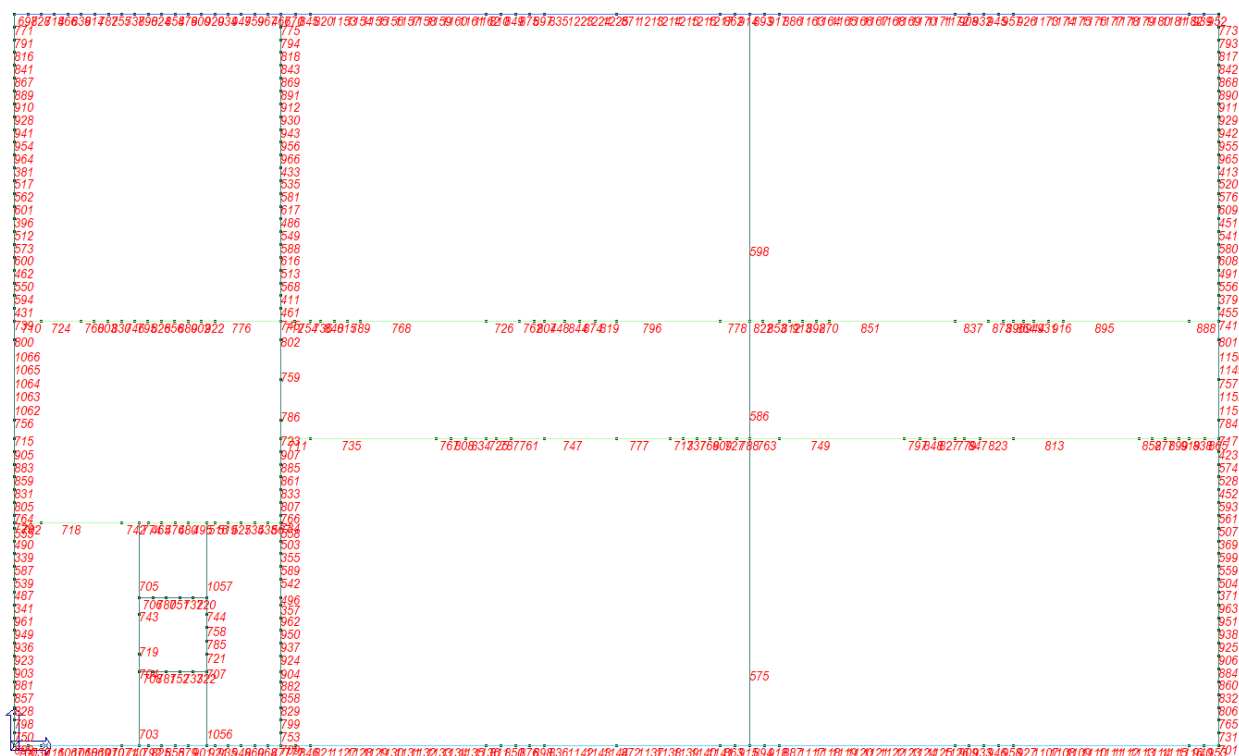
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1100	Trave	6222	6223	1	5
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1102	Trave	6224	6225	1	5
1103	Trave	6225	6226	1	5
1104	Trave	6226	6227	1	5
1105	Trave	6227	6228	1	5
1106	Trave	6228	2942	1	5
1107	Trave	6271	6272	1	5
1108	Trave	6272	6273	1	5
1109	Trave	6273	6274	1	5
1110	Trave	6274	6275	1	5
1111	Trave	6275	6276	1	5
1112	Trave	6276	6277	1	5
1113	Trave	6277	6278	1	5

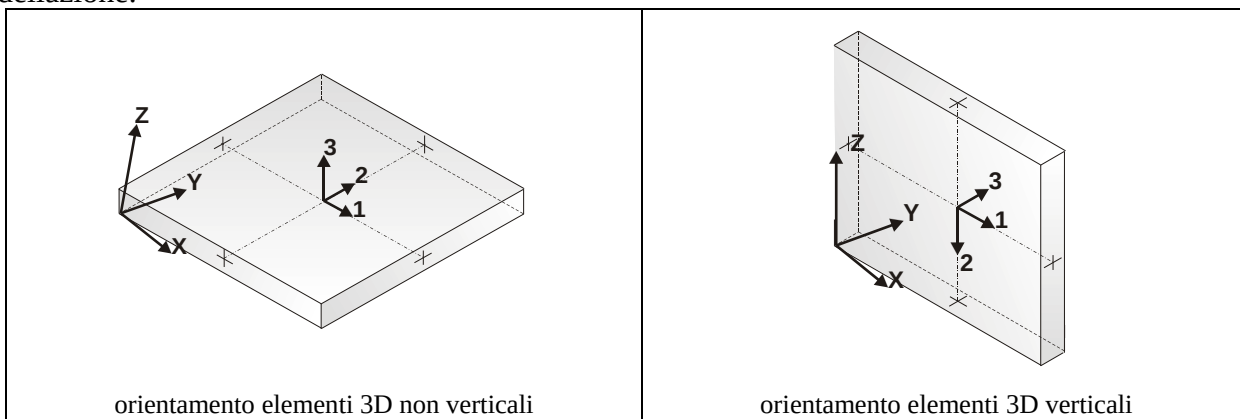
1114	Trave	6278	6279	1	5
1115	Trave	6279	6280	1	5
1116	Trave	6280	6045	1	5
1117	Trave	6301	6302	1	5
1118	Trave	6302	6303	1	5
1119	Trave	6303	6304	1	5
1120	Trave	6304	6305	1	5
1121	Trave	6305	6306	1	5
1122	Trave	6306	6307	1	5
1123	Trave	6307	6308	1	5
1124	Trave	6308	6309	1	5
1125	Trave	6309	6310	1	5
1126	Trave	6310	6038	1	5
1127	Trave	6331	6332	1	5
1128	Trave	6332	6333	1	5
1129	Trave	6333	6334	1	5
1130	Trave	6334	6335	1	5
1131	Trave	6335	6336	1	5
1132	Trave	6336	6337	1	5
1133	Trave	6337	6338	1	5
1134	Trave	6338	6339	1	5
1135	Trave	6339	6340	1	5
1136	Trave	6340	6018	1	5
1137	Trave	6361	6362	1	5
1138	Trave	6362	6363	1	5
1139	Trave	6363	6364	1	5
1140	Trave	6364	6365	1	5
1141	Trave	6365	6033	1	5
1142	Trave	6366	6367	1	5
1143	Trave	6367	6368	1	5
1144	Trave	6368	6029	1	5
1145	Trave	6387	6388	1	8
1146	Trave	6388	136	1	8
1147	Trave	6389	6390	1	8
1148	Trave	6390	124	1	8
1149	Trave	6391	6392	1	3
1150	Trave	6392	6005	1	3
1151	Trave	6393	6394	1	3
1152	Trave	6394	6004	1	3
1153	Trave	6415	6416	1	6
1154	Trave	6416	6417	1	6
1155	Trave	6417	6418	1	6
1156	Trave	6418	6419	1	6
1157	Trave	6419	6420	1	6
1158	Trave	6420	6421	1	6
1159	Trave	6421	6422	1	6
1160	Trave	6422	6423	1	6
1161	Trave	6423	6424	1	6
1162	Trave	6424	6017	1	6
1163	Trave	6425	6426	1	6
1164	Trave	6426	6427	1	6
1165	Trave	6427	6428	1	6
1166	Trave	6428	6429	1	6
1167	Trave	6429	6430	1	6
1168	Trave	6430	6431	1	6
1169	Trave	6431	6432	1	6
1170	Trave	6432	6433	1	6
1171	Trave	6433	6434	1	6
1172	Trave	6434	6036	1	6
1173	Trave	6435	6436	1	6
1174	Trave	6436	6437	1	6
1175	Trave	6437	6438	1	6
1176	Trave	6438	6439	1	6
1177	Trave	6439	6440	1	6
1178	Trave	6440	6441	1	6
1179	Trave	6441	6442	1	6
1180	Trave	6442	6443	1	6
1181	Trave	6443	6444	1	6
1182	Trave	6444	6043	1	6
1183	Trave	6445	6446	1	6
1184	Trave	6446	6447	1	6
1185	Trave	6447	6448	1	6
1186	Trave	6448	6449	1	6
1187	Trave	6449	6450	1	6
1188	Trave	6450	6451	1	6
1189	Trave	6451	6452	1	6
1190	Trave	6452	6453	1	6
1191	Trave	6453	6454	1	6
1192	Trave	6454	110	1	6
1193	Trave	6455	6456	1	6
1194	Trave	6456	6457	1	6
1195	Trave	6457	6458	1	6
1196	Trave	6458	6459	1	6
1197	Trave	6459	6460	1	6
1198	Trave	6460	6461	1	6
1199	Trave	6461	6462	1	6
1200	Trave	6462	6463	1	6
1201	Trave	6463	6464	1	6
1202	Trave	6464	114	1	6
1203	Trave	6465	6466	1	6
1204	Trave	6466	6467	1	6
1205	Trave	6467	6468	1	6
1206	Trave	6468	6469	1	6
1207	Trave	6469	6470	1	6
1208	Trave	6470	6471	1	6
1209	Trave	6471	6472	1	6
1210	Trave	6472	6473	1	6
1211	Trave	6473	6474	1	6
1212	Trave	6474	116	1	6
1213	Trave	6475	6476	1	6
1214	Trave	6476	6477	1	6



Copertura

MODELLAZIONE STRUTTURA: ELEMENTI SHELL

Il programma utilizza per la modellazione elementi a tre o quattro nodi denominati in generale shell. Ogni elemento shell è individuato dai nodi I, J, K, L (L=I per gli elementi a tre nodi). Ogni elemento è caratterizzato da un insieme di proprietà riportate in tabella che ne completano la modellazione.



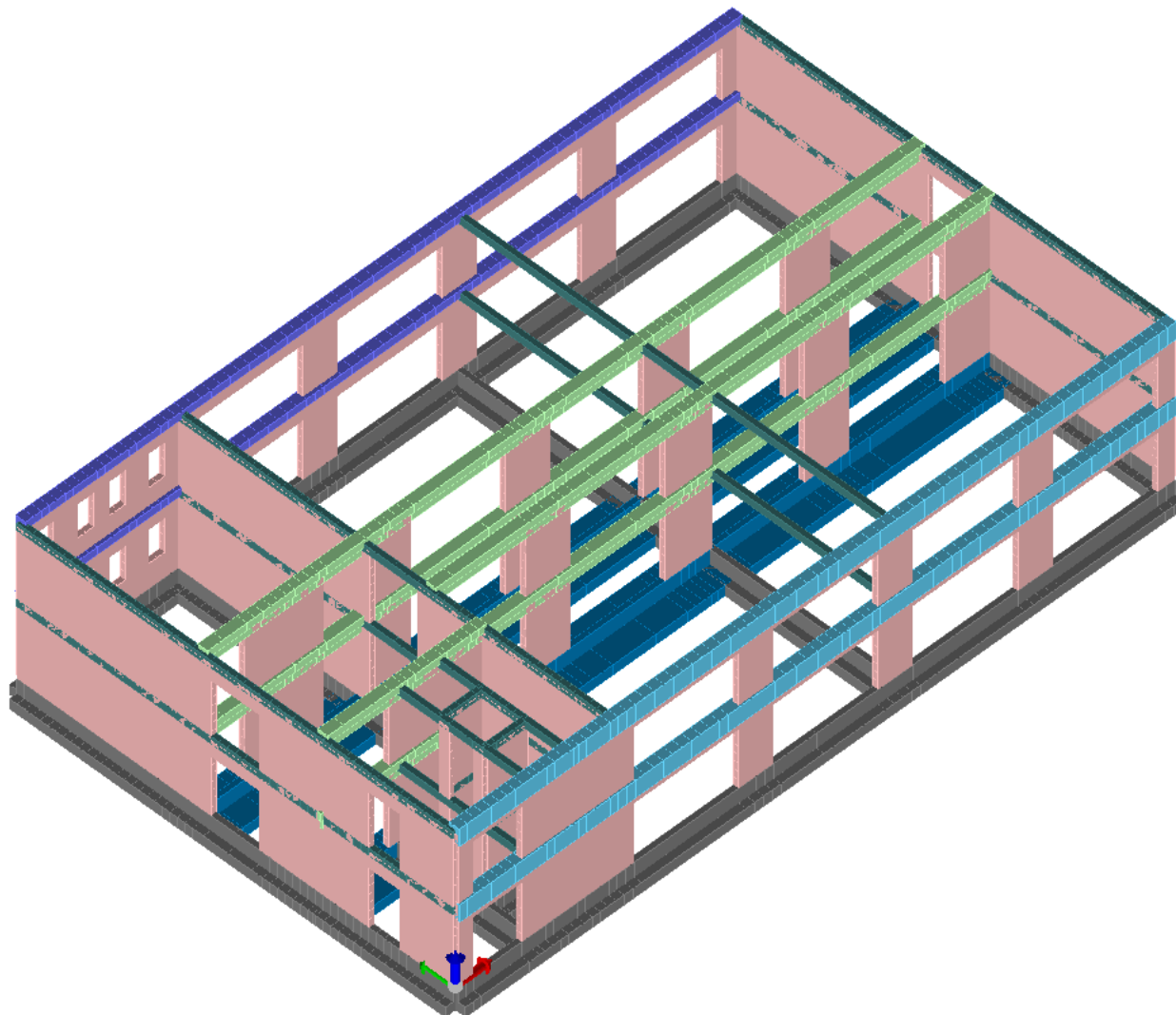
orientamento elementi 3D non verticali

orientamento elementi 3D verticali

In particolare per ogni elemento viene indicato in tabella:

Elem.	numero dell'elemento
Note	codice di comportamento: Guscio (elemento guscio in elevazione non verticale) Guscio fond. (elemento guscio su suolo elastico) Setto (elemento guscio in elevazione verticale) Membrana (elemento guscio con comportamento membranale)
Nodo I (J, K, L)	numero del nodo I (J, K, L)
Mat.	codice del materiale assegnato all'elemento
Spessore	spessore dell'elemento (costante)

Wink V	costante di sottofondo (coefficiente di Winkler) per la modellazione del suolo elastico verticale
Wink O	costante di sottofondo (coefficiente di Winkler) per la modellazione del suolo elastico orizzontale



MODELLAZIONE DELLA STRUTTURA: ELEMENTI SOLAIO-PANNELLO

Il programma utilizza per la modellazione elementi a tre o più nodi denominati in generale solaio o pannello.

Ogni elemento solaio-pannello è individuato da una poligonale di nodi 1,2, ..., N.

L'elemento solaio è utilizzato in primo luogo per la modellazione dei carichi agenti sugli elementi strutturali. In secondo luogo può essere utilizzato per la corretta ripartizione delle forze orizzontali agenti nel proprio piano. L'elemento balcone è derivato dall'elemento solaio.

I carichi agenti sugli elementi solaio, raccolti in un archivio, sono direttamente assegnati agli elementi utilizzando le informazioni raccolte nell'archivio (es. i coefficienti combinatori). La tabella seguente riporta i dati utilizzati per la definizione dei carichi e delle masse.

L'elemento pannello è utilizzato solo per l'applicazione dei carichi, quali pesi delle tamponature o spinte dovute al vento o terre. In questo caso i carichi sono applicati in analogia agli altri elementi strutturali (si veda il cap. SCHEMATIZZAZIONE DEI CASI DI CARICO).

Id.Arch.	Identificativo dell'archivio
Tipo	Tipo di carico Variab. Carico variabile generico Var. rid. Carico variabile generico con riduzione in funzione dell'area (c.5.5. ...) Neve Carico
G1k	carico permanente (comprensivo del peso proprio)
G2k	carico permanente non strutturale e non compiutamente definito
Qk	carico variabile
Fatt. A	fattore di riduzione del carico variabile (0.5 o 0.75) per tipo "Var.rid."
S sis.	fattore di riduzione del carico variabile per la definizione delle masse sismiche per D.M. 96 (vedi NOTA sul capitolo "normativa di riferimento")
Psi 0	Coefficiente combinatorio dei valori caratteristici delle azioni variabili: per valore raro
Psi 1	Coefficiente combinatorio dei valori caratteristici delle azioni variabili: per valore frequente
Psi 2	Coefficiente combinatorio dei valori caratteristici delle azioni variabili: per valore quasi permanente
Psi S 2	Coefficiente di combinazione che fornisce il valore quasi-permanente dell'azione variabile: per la definizione delle masse sismiche
Fatt. Fi	Coefficiente di correlazione dei carichi per edifici

Ogni elemento è caratterizzato da un insieme di proprietà riportate in tabella che ne completano la modellazione. In particolare per ogni elemento viene indicato in tabella:

Elem	numero dell'elemento
Tipo	codice di comportamento S elemento utilizzato solo per scarico C elemento utilizzato per scarico e per modellazione piano rigido P elemento utilizzato come pannello M scarico monodirezionale B scarico bidirezionale
Id.Arch.	Identificativo dell'archivio
Mat	codice del materiale assegnato all'elemento
Spessore	spessore dell'elemento (costante)
Orditura	angolo (rispetto all'asse X) della direzione dei travetti principali
Gk	carico permanente solaio (comprensivo del peso proprio)
Qk	carico variabile solaio
Nodi	numero dei nodi che definiscono l'elemento (5 per riga)

Nel caso in cui si sia proceduto alla progettazione dei solai con le tensioni ammissibili vengono riportate le massime tensioni nell'elemento (massima compressione nel calcestruzzo, massima tensione nell'acciaio, massima tensione tangenziale); nel caso in cui si sia proceduto alla

progettazione con il metodo degli stati limite vengono riportati il rapporto x/d e le verifiche per sollecitazioni proporzionali nonché le verifiche in esercizio.

In particolare i simboli utilizzati in tabella assumono il seguente significato:

Elem.	numero identificativo dell'elemento
Stato	Codici di verifica relativi alle tensioni normali e alle tensioni tangenziali
Note	Viene riportato il codice relativo alla sezione(s) e relativo al materiale(m);
Pos.	Ascissa del punto di verifica
F ist, F infi	Frecce istantanee e a tempo infinito
Momento	Momento flettente
Taglio	Sollecitazione di taglio
Af inf.	Area di armatura longitudinale posta all'intradosso della trave
Af sup.	Area di armatura longitudinale posta all'estradosso della trave
AfV	Area dell'armatura atta ad assorbire le azioni di taglio
Beff	Base della sezione di cls per l'assorbimento del taglio
simboli utilizzati con il metodo delle tensioni ammissibili:	
sc max	Massima tensione di compressione del calcestruzzo
sf max	Massima tensione nell'acciaio
tau max	Massima tensione tangenziale nel cls
simboli utilizzati con il metodo degli stati limite:	
x/d	rapporto tra posizione dell'asse neutro e altezza utile alla rottura della sezione (per sola flessione)
verif.	rapporto S_d/S_u con sollecitazioni ultime proporzionali: valore minore o uguale a 1 per verifica positiva
Verif.V	rapporto S_d/S_u con sollecitazioni taglianti proporzionali: valore minore o uguale a 1 per verifica positiva
rRfck	rapporto tra la massima compressione nel calcestruzzo e la tensione f_{ck} in combinazioni rare [normalizzato a 1]
rFfck	rapporto tra la massima compressione nel calcestruzzo e la tensione f_{ck} in combinazioni frequenti [normalizzato a 1]
rPfck	rapporto tra la massima compressione nel calcestruzzo e la tensione f_{ck} in combinazioni quasi permanenti [normalizzato a 1]
rRfyk	rapporto tra la massima tensione nell'acciaio e la tensione f_{yk} in combinazioni frequenti [normalizzato a 1]
rFyk	rapporto tra la massima tensione nell'acciaio e la tensione f_{yk} in combinazioni rare [normalizzato a 1]
rPfyk	rapporto tra la massima tensione nell'acciaio e la tensione f_{yk} in combinazioni quasi permanenti [normalizzato a 1]
wR	apertura caratteristica delle fessure in combinazioni rare
wF	apertura caratteristica delle fessure in combinazioni frequenti [mm]
wP	apertura caratteristica delle fessure in combinazioni quasi permanenti [mm]

Nel caso in cui si sia proceduto alla verifica delle tamponature secondo il D.M. 17.01.2018 - §7.2.3 viene riportata una tabella riassuntiva delle verifiche degli elementi pannello. La verifica confronta i momenti sollecitanti indotti dal sisma con i momenti resistenti, secondo tre ipotesi, due basate sulla resistenza a pressoflessione della tamponatura ed una basata sul cinematismo a seguito della formazione di tre cerniere plastiche sulla tamponatura (rif. Ufficio di Vigilanza sulle Costruzioni, Provincia di Terni).

Qualora la tamponatura sia di tipo antiespulsione (nelle due possibili varianti ordinaria o armata) viene condotta una verifica con meccanismo ad arco con degrado di resistenza. La verifica confronta le pressioni sollecitanti indotte dal sisma con le pressioni resistenti che la tamponatura

sviluppa attraverso il meccanismo ad arco. La verifica considera anche il degrado di resistenza dovuto al danneggiamento nel piano della tamponatura.

Per quest'ultima tamponatura sono disponibili, in funzione del materiale impiegato (materiale [52] o materiale [53]):

- **Tamponatura Antiespulsione ordinaria Poroton® Cis Edil** sp.30 cm; con metodo di verifica per meccanismo ad arco con degrado di resistenza, sviluppato attraverso i risultati di un progetto di ricerca sperimentale condotto dall'Università degli Studi di Padova.
Utilizzabile per il materiale [52].
- **Tamponatura Antiespulsione armata Poroton® Cis Edil** sp.30 cm; con metodo di verifica per meccanismo ad arco con degrado di resistenza, sviluppato attraverso i risultati di un progetto di ricerca sperimentale condotto dall'Università degli Studi di Padova.
Utilizzabile per il materiale [53].

La verifica è stata calibrata sulla base di prove sperimentali sul sistema di Tamponatura Antiespulsione anche in presenza di aperture.

(rif. Rapporti di Prova redatti dal Dipartimento ICEA - Università degli Studi di Padova di test sperimentali condotti sul sistema Tamponatura Antiespulsione di Cis Edil)

In particolare i simboli utilizzati in tabella assumono il seguente significato:

Elem.	Numero identificativo dell'elemento
Stato	Codice di verifica
Ver. c.c.	Verifica nell'ipotesi di trave appoggiata con carico concentrato in mezzzeria
Ver. c.d.	Verifica nell'ipotesi di trave appoggiata con carico distribuito
Ver. c.cin.	Verifica nell'ipotesi di cinematismo con formazione di cerniere plastiche in appoggio e mezzzeria
Ver. CIS	Rapporto pa/pr (valore minore o uguale a 1 per verifica positiva)
Z	Quota del baricentro dell'elemento
T1	Periodo proprio dell'edificio nella direzione di interesse (ortogonale al pannello)
Ta	Periodo proprio della parete
Sa	Accelerazione massima, adimensionalizzata allo SLV
pa	Pressione sulla parete causata dall'azione sismica
pr	Pressione resistente del meccanismo ad arco
Drift	Spostamento relativo interpiano allo SLV valutato secondo il D.M. 14.01.2018 - § 7.3.3.3
Beta a	Coef. riduttivo per tener conto del danneggiamento del piano dipendente dallo spostamento, ottenuto sperimentalmente

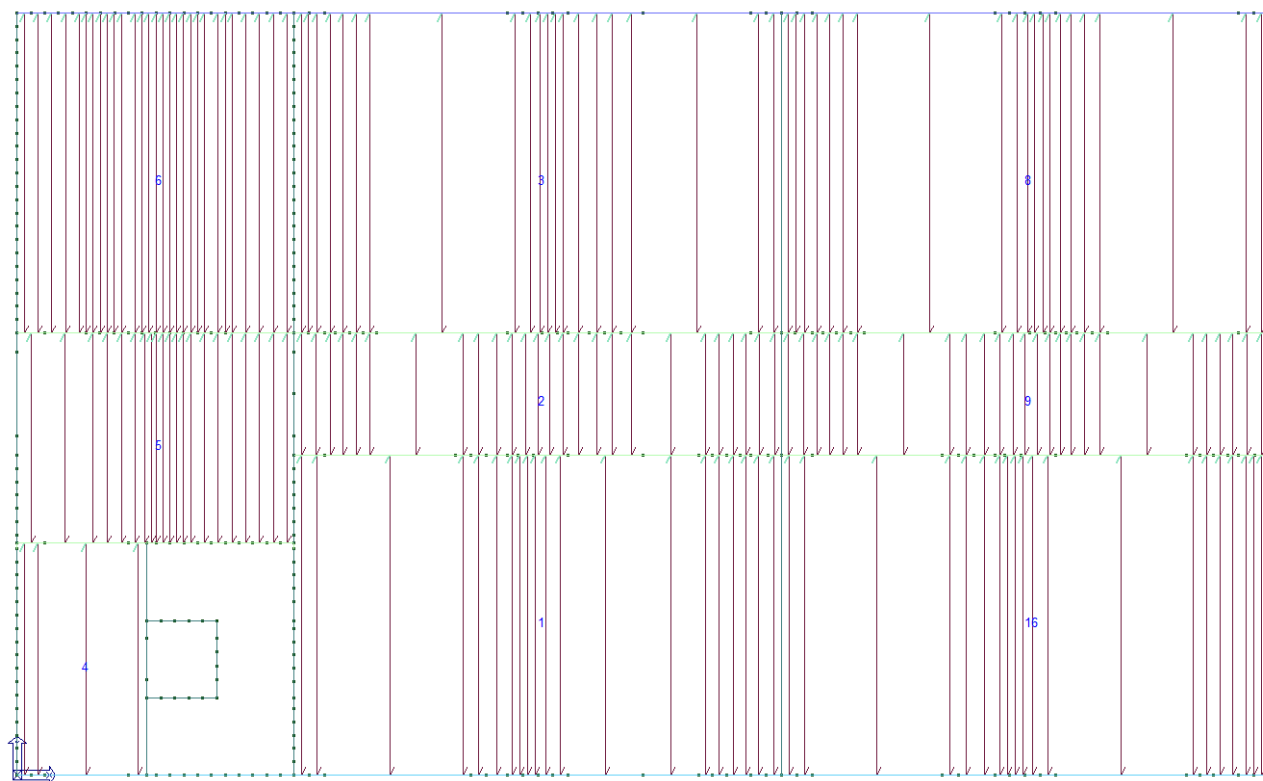
ID Arch.	Tipo	G1k daN/cm2	G2k daN/cm2	Qk daN/cm2	Fatt. A	s sis.	Psi 0	Psi 1	Psi 2	Psi S 2	Fatt. Fi
1	Variab.	5.00e-02	2.80e-02	3.00e-02		1.00	0.70	0.50	0.30	0.30	1.00
2	Variab.	5.00e-02	1.00e-02	2.00e-02		1.00	0.70	0.50	0.30	0.30	1.00

Elem.	Tipo	ID Arch.	Mat.	Spessore	Orditura	G1k daN/cm2	G2k daN/cm2	Qk daN/cm2	Nodo 1/6..	Nodo 2/7..	Nodo 3/8..	Nodo..	Nodo..
1	CM	1	m=1	6.0	90.0	5.00e-02	2.80e-02	3.00e-02	1524	1514	1504	1494	1484
									1474	134	1464	1454	1444
									1434	1424	1414	1404	1394
									1384	1374	1364	1354	1344
									1334	1324	1314	1304	73
									300	118	2942	2941	74
									326	336	346	75	125
									1008	4094	2943	76	372
									130	131	88	2812	2802
									2792	2791	126	87	2840
									2890	86	2870	2860	2842
									119	85			
2	CM	1	m=1	6.0	90.0	5.00e-02	2.80e-02	3.00e-02	138	128	137	85	119
									2842	2860	2870	86	2890
									2840	87	126	2791	2792
									2802	2812	88	2832	131
									132	100	127	2467	2516

									2506	99	2486	2485	98
									2427	2428	2438	2448	120
									2340	97			
3	CM	1	m=1	6.0	90.0	5.00e-02	2.80e-02	3.00e-02	1534	1544	1554	1564	1574
									1584	1594	1604	1614	1624
									1634	1644	1654	1664	1674
									1684	1694	1704	1714	1724
									1734	1744	1754	97	2340
									120	2448	2438	2428	2427
									98	2485	2486	99	2506
									2516	2467	127	100	132
									129	1204	112	123	111
									1178	1168	1158	110	121
									1132	109			
4	CM	1	m=1	6.0	90.0	5.00e-02	2.80e-02	3.00e-02	1956	1946	1936	1926	1916
									1906	1896	1886	1876	1866
									1856	1846	1836	1826	1816
									1806	1796	70	141	72
									182	2948	2952	2956	2960
									3127	84	83	133	
5	CM	1	m=1	6.0	90.0	5.00e-02	2.80e-02	3.00e-02	122	6121	2282	82	2016
									2006	1996	1986	1976	1966
									133	83	84	3127	3154
									3164	3174	3184	3194	3204
									3214	3224	3234	3244	134
									1474	1484	1494	1504	1514
									1524	85	137	128	138
									97	2400	2380	2370	2360
									2350	96	2330	2320	2319
									95	94			
6	CM	1	m=1	6.0	90.0	5.00e-02	2.80e-02	3.00e-02	2026	2036	2046	2056	2066
									2076	2086	2096	2106	2116
									2126	2136	2146	2156	2166
									2176	2186	2196	2206	2216
									2226	2236	2246	94	95
									2319	2320	2330	96	2350
									2360	2370	2380	2390	2400
									2301	97	1754	1744	1734
									1724	1714	1704	1694	1684
									1674	1664	1654	1644	1634
									1624	1614	1604	1594	1584
									1574	1564	1554	1544	1534
									109	1114	1104	1094	1084
									1074	1064	1054	1044	1034
									1024	1014	108	2906	2916
									2926	2936	2946	107	971
									106				
7	CM	2	m=1	6.0	90.0	5.00e-02	1.00e-02	2.00e-02	5062	5052	5042	5032	5022
									5012	5002	4992	4982	4972
									4962	4952	4942	4932	4922
									4912	4902	5963	3247	5981
									5982	3288	5967	5968	5986
									5969	5970	5985	5966	5965
8	CM	1	m=1	6.0	90.0	5.00e-02	2.80e-02	3.00e-02	132	2582	101	2562	2552
									2542	2541	102	2666	2707
									103	2680	2607	2604	2603
									104	105	938	928	918
									908	898	888	878	868
									858	848	838	828	818
									808	798	788	778	768
									758	748	738	728	711
									117	1294	116	115	1268
									1258	1248	114	113	1222
									129				
9	CM	1	m=1	6.0	90.0	5.00e-02	2.80e-02	3.00e-02	131	89	2718	2766	2756
									90	2736	2716	91	2618
									2621	2638	2648	92	2668
									93	135	124	136	105
									104	2603	2604	2607	2680
									103	2707	2666	102	2541
									2542	2552	2562	101	2582
									132				
10	CM	2	m=1	6.0	90.0	5.00e-02	1.00e-02	2.00e-02	4630	4620	4610	4600	4590
									4580	5992	4570	4560	4550
									4540	4530	4520	4510	4500
									4490	4480	4470	4460	4450

									4440	4430	4420	4410	5973
									3406	6024	6018	3432	3442
									3452	6028	6029	6033	3478
									6041	6008	5921	5991	5901
									5891	5881	5880	5999	5998
									5928	3444	5989	5957	5947
									5929	5977	5976		
11	CM	2	m=1	6.0	90.0	5.00e-02	1.00e-02	2.00e-02	6007	6006	5988	5976	5977
									5929	5947	5957	5989	3444
									5928	5998	5999	5880	5881
									5891	5901	5991	5921	6008
									6014	6013	6016	6022	5615
									5605	6000	5585	5584	5990
									5529	5530	5540	5550	5993
									5443	5978			
12	CM	2	m=1	6.0	90.0	5.00e-02	1.00e-02	2.00e-02	4640	4650	4660	4670	4680
									4690	4700	4710	4720	4730
									4740	4750	4760	4770	4780
									4790	4800	4810	4820	4830
									4840	4850	4860	5978	5443
									5993	5550	5540	5530	5529
									5990	5584	5585	6000	5605
									5615	6022	6016	6013	6014
									6040	4310	6032	6027	6026
									4284	4274	4264	6017	6023
									4238	6009			
13	CM	2	m=1	6.0	90.0	5.00e-02	1.00e-02	2.00e-02	5987	5996	4012	4748	5972
									5971	3338	3348	3358	3368
									3378	3388	5973	4410	4420
									4430	4440	4450	4460	4470
									4480	4490	4500	4510	4520
									4530	4540	4550	4560	4570
									5992	6054	6053	6052	6051
									6050	6049			
14	CM	2	m=1	6.0	90.0	5.00e-02	1.00e-02	2.00e-02	5370	4969	5388	5980	5122
									5112	5102	5092	5082	5072
									5965	5966	5985	5970	6011
									6046	6047	6048	6049	6050
									6051	6052	6053	6054	5992
									4580	4590	4600	4610	4620
									4630	5976	5988	6006	6007
									5978	6012	5503	5483	5463
									5997	5433	5423	5422	5975
									5974				
15	CM	2	m=1	6.0	90.0	5.00e-02	1.00e-02	2.00e-02	5132	5142	5152	5162	5172
									5182	5192	5202	5212	5222
									5232	5242	5252	5262	5272
									5282	5292	5302	5312	5322
									5332	5342	5352	5974	5975
									5422	5423	5433	5997	5453
									5473	5483	5493	5503	6012
									5978	4860	4850	4840	4830
									4820	4810	4800	4790	4780
									4770	4760	4750	4740	4730
									4720	4710	4700	4690	4680
									4670	4660	4650	4640	6009
									4220	4210	4200	4190	4180
									4170	4160	4150	4140	4130
									4120	5994	3668	3768	3892
									3992	4132	5979	4077	5962
16	CM	1	m=1	6.0	90.0	5.00e-02	2.80e-02	3.00e-02	130	390	77	4052	4042
									78	416	426	436	79
									4114	4112	4110	80	462
									81	480	490	500	510
									520	530	540	550	560
									570	580	590	600	610
									620	630	640	650	660
									670	680	690	700	93
									2668	92	2648	2638	2621
									2618	91	2716	2736	90
									2756	2766	2718	89	131
17	CM	2	m=1	6.0	90.0	5.00e-02	1.00e-02	2.00e-02	6014	5680	6019	5660	5650
									5640	5639	6030	5760	5801
									6034	5774	5703	5700	5699
									6039	5995	4044	4034	4024
									4014	4004	3994	3984	3974

									3964	3954	3944	3934	3924
									3914	3904	3894	3884	3874
									3864	3854	3844	3834	3817
									6010	4400	6043	6042	4374
									4364	4354	6036	6035	4328
									6040				
18	CM	2	m=1	6.0	90.0	5.00e-02	1.00e-02	2.00e-02	6008	6001	6002	5856	5846
									6015	5826	6025	6020	6021
									5715	5732	5742	6031	5762
									5983	5984	6004	6005	5995
									6039	5699	5700	5703	5774
									6034	5801	5760	6030	5639
									5640	5650	5660	6019	5680
									6014				
19	CM	2	m=1	6.0	90.0	5.00e-02	1.00e-02	2.00e-02	5969	5624	5475	5340	5240
									5987	6049	6048	6046	5970
20	CM	2	m=1	6.0	90.0	5.00e-02	1.00e-02	2.00e-02	5986	5968	5967	5043	4943
									4828	4728	5971	5972	4748
									4012	5996	5987	5240	5340
									5475	5624	5969		
21	CM	2	m=1	6.0	90.0	5.00e-02	1.00e-02	2.00e-02	3288	3298	3308	3318	3328
									3338	5971	4728	4828	4943
									5043	5967			
22	CM	2	m=1	6.0	90.0	5.00e-02	1.00e-02	2.00e-02	6041	3496	6037	6038	3522
									3532	3542	6044	6045	3568
									5964	3586	3596	3606	3616
									3626	3636	3646	3656	3666
									3676	3686	3696	3706	3716
									3726	3736	3746	3756	3766
									3776	3786	3796	3806	5983
									5762	6031	5742	5732	5715
									6021	6020	6025	5826	6015
									5846	5856	6002	6001	6008



Solaio di piano

52

The figure consists of two vertically stacked line graphs sharing a common horizontal axis representing the length of the beam in meters, from 0 to 30.

The top graph shows the variation of internal moment (MOMENTO) in kN·m. The vertical axis ranges from -200.00 to 200.00. A red line represents the maximum moment (MOMENTO MAX) and a blue line represents the minimum moment (MOMENTO MIN). The maximum moment starts at approximately 150 kN·m at x=0, drops to a minimum of about -100 kN·m at x=10, and then rises to a peak of about 180 kN·m at x=25. The minimum moment starts at approximately -100 kN·m at x=0, rises to a peak of about 50 kN·m at x=10, and then drops to a minimum of about -150 kN·m at x=25.

The bottom graph shows the variation of internal axial force (FUERZA AXIAL) in kN. The vertical axis ranges from -60.00 to 80.00. A red line represents the maximum axial force (FUERZA AXIAL MAX) and a blue line represents the minimum axial force (FUERZA AXIAL MIN). The maximum axial force starts at approximately 40 kN at x=0, drops to a minimum of about -10 kN at x=10, and then rises to a peak of about 60 kN at x=25. The minimum axial force starts at approximately -10 kN at x=0, rises to a peak of about 20 kN at x=10, and then drops to a minimum of about -40 kN at x=25.

PRIMO SOLAIO - 3 campate

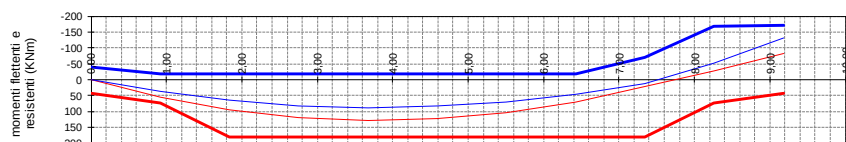
prima campata

Rck	Ec	fcd	fctd	Acciaio	fyd	Bsup	Binf	Sp_ala	h	c	d
MPa	(MPa)	MPa		tipo	MPa	cm			cm	cm	cm
30	31220	14,11	1,14	Feb44k	391	120	40	6	36	4	32

Luce di calcolo (m) 9,18

Verifica agli stati limite ultimi

Inviluppo Momento max	0,00	54,33	93,86	118,58	128,50	123,61	103,92	69,42	20,11	-26,69	-80,93
Inviluppo Momento min	0,00	37,27	64,29	81,05	87,56	83,82	69,82	45,56	11,05	-51,01	-130,71
As,sup,app	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	4,53	11,61
As,inf,app	0,00	4,82	8,33	10,53	11,41	10,98	9,23	6,36	1,79	0,00	0,00
X	0,00	0,92	1,84	2,75	3,67	4,59	5,51	6,43	7,34	8,26	9,18
Armatura (cmq)											
φ6											
φ12	3	5	5	5	5	5	5	5			
φ16									3	3	3
φ20										3	3
As,sup	3,39	1,41	1,41	1,41	1,41	1,41	1,41	1,41	6,03	15,46	15,46
As,inf	3,39	6,03	15,46	15,46	15,46	15,46	15,46	15,46	15,46	6,03	3,39
φ12	3										
φ16		3	3	3	3	3	3	3	3	3	
φ20			3	3	3	3	3	3	3		
φ5		0	0	0	0	0	0	0	0	0	0
Momenti positivi											
b	120,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00
psi	0,09	0,11	0,18	0,18	0,18	0,18	0,18	0,18	0,17	0,12	0,10
M+res	42,04	72,73	179,63	179,63	179,63	179,63	179,63	179,63	179,55	73,31	43,30
Momenti negativi											
b	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	60,00
psi	0,14	0,11	0,12	0,12	0,12	0,12	0,12	0,12	0,15	0,30	0,26
M-res	-40,10	-17,69	-17,90	-17,90	-17,90	-17,90	-17,90	-17,90	-69,23	-169,41	-172,02



VERIFICA ALLO S.L.U. DI TAGLIO					k = 1,79		V = 0,42		vbd = 53,56		
Vsd	50,42	39,73	29,05	18,36	7,68	-3,64	-14,33	-25,01	-35,70	-46,38	-57,07
ρ ₁	0,0027	0,0047	0,0121	0,0121	0,0121	0,0121	0,0121	0,0121	0,0121	0,0047	0,0027
Bmin	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00

VERIFICA AGLI S.L. DI ESERCIZIO

Caratteristiche geometriche sezioni

Per gruppo di esigenze cond. ambientali poco aggressive e armatura poco sensibile:											
	Beta,1 1,00		K2 0,40		Diam.min. 12		copr.netto 3,40				
	Beta,2 0,50		K3 0,13		Sig.SR 101,38		n 15				
As (cmq)	3,39	6,03	15,46	15,46	15,46	15,46	15,46	15,46	15,46	15,46	15,46
A's (cmq)	3,39	1,41	1,41	1,41	1,41	1,41	1,41	1,41	6,03	6,03	3,39
b resistente	40,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	40,00	60,00
Y	7,36	6,18	9,27	9,27	9,27	9,27	9,27	9,27	9,01	13,25	11,91
Wc	4999	11308	16420	16420	16420	16420	16420	16420	17092	9078	10961
Ws	1493	2705	6698	6698	6698	6698	6698	6698	6703	6414	6498
N. barre	3	3	6	6	6	6	6	6	6	6	6
dist. barre	16,00	16,80	16,80	16,80	16,80	16,80	16,80	16,80	16,80	6,40	10,40
Beff (cm)	40	42	92	92	92	92	92	92	92	40	60
Deff (cm)	12,40	12,40	12,40	12,40	12,40	12,40	12,40	12,40	12,40	11,38	12,05
Aeff	496,00	515,84	1140,80	1140,80	1140,80	1140,80	1140,80	1140,80	1140,80	455,02	722,70
RO,r	0,68%	1,17%	1,35%	1,35%	1,35%	1,35%	1,35%	1,35%	1,35%	3,40%	2,14%

Combinazioni di carico

Rara	0,00	40,06	69,21	87,43	94,73	91,10	76,56	51,09	14,71	-37,28	-96,03
Frequente	0,00	36,69	63,37	80,04	86,70	83,35	69,98	46,60	13,22	-33,46	-87,24
Quasi perm.	0,00	35,57	61,43	77,58	84,03	80,76	67,79	45,11	12,72	-32,19	-84,30

Verifica allo stato limite di tensione in esercizio

Combinazione rara											
Sigma,C	-0,01	-3,54	-4,21	-5,32	-5,77	-5,55	-4,66	-3,11	-0,86	-4,11	-8,76
Sigma,S	0,01	222,13	154,98	195,79	212,13	204,02	171,45	114,42	32,91	87,19	221,68
Combinazione quasi permanente											
Sigma,C	-0,01	-3,15	-3,74	-4,72	-5,12	-4,92	-4,13	-2,75	-0,74	-3,55	-7,69

Verifica allo stato limite di apertura fessure

Srm (mm)	187,71	152,91	145,88	145,88	145,88	145,88	145,88	145,88	145,88	98,46	116,85
Combinazione frequente											
Sigma,S	0,10	203,43	141,92	179,25	194,16	186,65	156,72	104,37	29,58	78,25	201,37
Eps,sm	0,000%	0,040%	0,045%	0,068%	0,077%	0,073%	0,055%	0,020%	0,006%	0,030%	0,092%
Wk (mm)	0,000	0,103	0,113	0,170	0,191	0,180	0,136	0,050	0,014	0,050	0,183
Combinazione quasi permanente											
Sigma,S	0,10	197,20	137,56	173,74	188,17	180,86	151,81	101,02	28,46	75,27	194,60
Eps,sm	0,000%	0,038%	0,043%	0,065%	0,074%	0,069%	0,052%	0,020%	0,006%	0,028%	0,089%
Wk (mm)	0,000	0,100	0,106	0,162	0,183	0,172	0,128	0,049	0,014	0,047	0,176

Verifica allo stato limite di deformazione

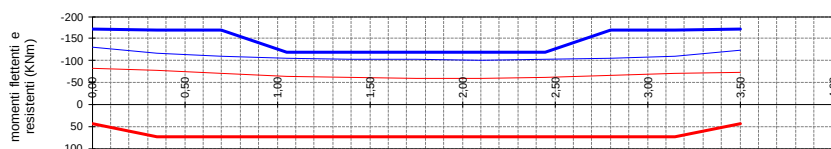
Verifica esatta: combinazione quasi permanente											
EpsCm	0,000%	-0,010%	-0,012%	-0,015%	-0,016%	-0,016%	-0,013%	-0,009%	-0,002%	-0,011%	-0,025%
EpsSm	0,000%	0,095%	0,065%	0,083%	0,090%	0,087%	0,072%	0,047%	0,007%	0,034%	0,094%
frecchia	0,000	0,948	1,707	2,230	2,502	2,501	2,238	1,758	1,142	0,505	0,000
frecchia massima:		2,50 cm			pari a L	367					
verifica sommaria:						25,50	<	26,00	Rapporto limite		

PRIMO SOLAIO - 3 campate**seconda campata**

Luce di calcolo (m)

3,50**Verifica agli stati limite ultimi**

Involuppo Momento max	Coeff. di redistribuzione delta= 1,00										psi-max
	-80,93	-77,71	-70,77	-64,85	-60,96	-59,12	-59,31	-61,54	-65,80	-71,09	-72,64
Involuppo Momento min	Coeff. di redistribuzione delta= 1,00										psi-max
	-130,71	-116,90	-110,24	-105,98	-103,08	-101,57	-101,43	-102,66	-105,28	-110,28	-122,43
As,sup,app	1161	10,38	9,79	9,41	9,15	9,02	9,01	9,12	9,35	9,79	10,87
As,inf,app	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00
X	0,00	0,35	0,70	1,05	1,40	1,75	2,10	2,45	2,80	3,15	3,50
Armatura (cmq)											
φ6	0			5	5	5	5	5			
φ12	0										
φ16	3	3	3	3	3	3	3	3	3	3	3
φ20	3	3	3	1	1	1	1	1	3	3	3
As,sup	15,46	15,46	15,46	10,59	10,59	10,59	10,59	10,59	15,46	15,46	15,46
As,inf	3,39	6,03	6,03	6,03	6,03	6,03	6,03	6,03	6,03	6,03	3,39
φ12	3										3
φ16	0	3	3	3	3	3	3	3	3	3	
φ20	0										
φ5	0										
Momenti positivi											
b	120	120	120	120	120	120	120	120	120	120	120
psi	0,10	0,12	0,12	0,11	0,11	0,11	0,11	0,11	0,12	0,12	0,10
M+res	43,30	73,31	73,31	73,18	73,18	73,18	73,18	73,18	73,31	73,31	43,30
Momenti negativi											
b	60	40	40	40	40	40	40	40	40	40	60
psi	0,26	0,30	0,30	0,22	0,22	0,22	0,22	0,22	0,30	0,30	0,26
M-res	-172,02	-169,41	-169,41	-118,95	-118,95	-118,95	-118,95	-118,95	-169,41	-169,41	-172,02



VERIFICA ALLO S.L.U. DI TAGLIO										
k = 1,79 V = 0,42 v _{bd} = 53,56										
V _{sd}	51,07	32,68	28,60	24,53	20,45	16,38	-14,99	-19,07	-23,14	-27,22
ρ ₁	0,0027	0,0047	0,0047	0,0047	0,0047	0,0047	0,0047	0,0047	0,0047	0,0027
B _{min}	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00

VERIFICA AGLI S.L. DI ESERCIZIO**Caratteristiche geometriche sezioni**

Per gruppo di esigenze cond. ambientali poco aggressive e armatura poco sensibile:

Beta,1 **1,00** K2 **0,40** Diam.min. **12** copr.netto 3,40Beta,2 **1,00** K3 **0,13** Sig.SR 101,38 n **15**

As (cmq)	15,46	15,46	15,46	10,59	10,59	10,59	10,59	10,59	15,46	15,46	15,46
A's (cmq)	3,39	6,03	6,03	6,03	6,03	6,03	6,03	6,03	6,03	6,03	3,39
b resistente	60,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	60,00
Y	11,91	13,25	13,25	11,40	11,40	11,40	11,40	11,40	13,25	13,25	11,91
Wc	10961	9078	9078	8076	8076	8076	8076	8076	9078	9078	10961
Ws	6498	6414	6414	4472	4472	4472	4472	4472	6414	6414	6498
N. barre	6	6	6	9	9	9	9	9	6	6	6
dist. barre	10,40	6,40	6,40	4,00	4,00	4,00	4,00	4,00	6,40	6,40	10,40
Beff (cm)	60	40	40	40	40	40	40	40	40	40	60
Deff (cm)	12,05	11,38	11,38	12,30	12,30	12,30	12,30	12,30	11,38	11,38	12,05
A _{eff}	722,70	455,02	455,02	491,92	491,92	491,92	491,92	491,92	455,02	455,02	722,70
RO,r	2,14%	3,40%	3,40%	2,15%	2,15%	2,15%	2,15%	2,15%	3,40%	3,40%	2,14%

Combinazioni di carico

Rara	-96,03	-86,11	-81,09	-77,81	-75,58	-74,42	-74,31	-75,26	-77,27	-81,01	-89,66
Frequente	-87,24	-78,67	-73,85	-70,57	-68,35	-67,18	-67,07	-68,02	-70,03	-73,57	-80,86
Quasi perm.	-84,30	-76,19	-71,44	-68,16	-65,93	-64,77	-64,66	-65,61	-67,62	-71,09	-77,93

Verifica allo stato limite di tensione in esercizio

Combinazione rara	Sigma,C,amm = 0.60*f _{ck} = 14,94 MPa										Sigma,S,amm = 0.80*f _{yk} = 360 MPa
Sigma,C	-8,76	-9,49	-8,93	-9,63	-9,36	-9,21	-9,20	-9,32	-8,51	-8,92	-8,18
Sigma,S	221,68	201,39	189,65	261,00	253,54	249,63	249,27	252,46	180,71	189,47	206,97
Combinazione quasi permanente	Sigma,C,amm = 0.45*f _{ck} = 11,21 MPa										
Sigma,C	-7,69	-8,39	-7,87	-8,44	-8,16	-8,02	-8,01	-8,12	-7,45	-7,83	-7,11

Verifica allo stato limite di apertura fessure

S _{rm} (mm)	116,85	98,46	98,46	103,88	103,88	103,88	103,88	103,88	98,46	98,46	116,85
Combinazione frequente	Apertura limite=W3= 0,20 mm										
Sigma,S	201,37	183,98	172,72	236,73	229,26	225,35	224,99	228,18	163,78	172,07	186,66
Eps,sm	0,087%	0,082%	0,076%	0,105%	0,101%	0,099%	0,099%	0,100%	0,072%	0,076%	0,079%
W _k (mm)	0,172	0,138	0,128	0,185	0,178	0,175	0,174	0,177	0,120	0,127	0,156
Combinazione quasi permanente	Apertura limite=W2= 0,20 mm										
Sigma,S	194,60	178,18	167,08	228,63	221,17	217,26	216,90	220,09	158,14	166,27	179,90
Eps,sm	0,083%	0,079%	0,073%	0,101%	0,097%	0,095%	0,094%	0,096%	0,069%	0,073%	0,075%
W _k (mm)	0,165	0,133	0,123	0,178	0,171	0,167	0,167	0,170	0,115	0,122	0,149

Verifica allo stato limite di deformazione**Verifica esatta: combinazione quasi permanente**

EpsCm	-0,025%	-0,027%	-0,025%	-0,027%	-0,026%	-0,026%	-0,026%	-0,026%	-0,024%	-0,025%	-0,023%
EpsSm	0,093%	0,084%	0,079%	0,109%	0,106%	0,104%	0,104%	0,105%	0,074%	0,079%	0,085%
f _{reccia}	0,000	-0,209	-0,375	-0,498	-0,571	-0,595	-0,568	-0,492	-0,369	-0,204	0,000
f _{reccia} massima:	0,00 cm										
verifica sommaria:	Rapporto di snellezza effettivo l/h = 9,72 < 26,00 Rapporto limite										

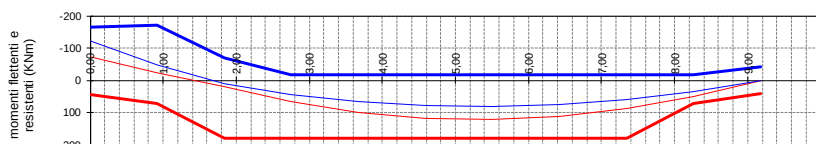
PRIMO SOLAIO + 3 campate

terza campata

Luce di calcolo (m) 9,18

Verifica agli stati limite ultimi

Involuppo Momento max	-72,64	-22,79	20,43	66,93	99,42	117,89	122,34	112,78	89,20	51,61	0,00
Coeff. di redistribuzione delta= 1,00 psi-max											
Involuppo Momento min	-122,43	-47,11	11,37	43,08	65,32	78,10	81,41	75,25	59,63	34,55	0,00
Coeff. di redistribuzione delta= 1,00 psi-max											
As,sup.app	10,87	4,18	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00
As,inf.app	0,00	0,00	1,81	5,94	8,83	10,47	10,86	10,02	7,92	4,58	0,00
X	0,00	0,92	1,84	2,75	3,67	4,59	5,51	6,43	7,34	8,26	9,18
Armatura (cmq)											
φ6	0			5	5	5	5	5	5	5	
φ12	0										3
φ16	3	3	3								
φ20	3	3									
As,sup	15,46	15,46	6,03	1,41	1,41	1,41	1,41	1,41	1,41	1,41	3,39
As,inf	3,39	6,03	15,46	15,46	15,46	15,46	15,46	15,46	15,46	6,03	3,39
φ12	3										3
φ16	0	3	3	3	3	3	3	3	3	3	
φ20	0		3	3	3	3	3	3	3		
φ5	0										
Momenti positivi											
b	120	120	120	120	120	120	120	120	120	120	120
psi	0,10	0,12	0,17	0,18	0,18	0,18	0,18	0,18	0,18	0,11	0,09
M+res	43,30	73,31	179,55	179,63	179,63	179,63	179,63	179,63	179,63	72,73	42,04
Momenti negativi											
b	40	40	40	40	40	40	40	40	40	40	40
psi	0,38	0,30	0,15	0,12	0,12	0,12	0,12	0,12	0,12	0,11	0,14
M-res	-164,26	-169,41	-69,23	-17,90	-17,90	-17,90	-17,90	-17,90	-17,90	-17,69	-40,10



VERIFICA ALLO S.L.U. DI TAGLIO											
k = 1,79 v = 0,42 v _{bd} = 53,56											
V _{sd}	76,85	60,70	50,02	39,33	28,65	17,96	7,66	-4,04	-14,73	-25,41	-36,10
ρ ₁	0,0027	0,0047	0,0121	0,0121	0,0121	0,0121	0,0121	0,0121	0,0121	0,0047	0,0027
B _{min}	59,58	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00

VERIFICA AGLI S.L. DI ESERCIZIO

Caratteristiche geometriche sezioni

Per gruppo di esigenze cond. ambientali poco aggressive e armatura poco sensibile:

Beta,1 1,00 K2 0,40 Diam.min. 12 copr.netto 3,40
Beta,2 1,00 K3 0,13 Sig.SR 101,38 n 15

As (cmq)	15,46	15,46	15,46	15,46	15,46	15,46	15,46	15,46	15,46	6,03	3,39
A's (cmq)	3,39	6,03	6,03	1,41	1,41	1,41	1,41	1,41	1,41	1,41	3,39
b resistente	60,00	40,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	40,00
Y	11,91	13,25	9,01	9,27	9,27	9,27	9,27	9,27	9,27	6,18	7,36
Wc	10961	9078	17092	16420	16420	16420	16420	16420	16420	11308	4999
Ws	6498	6414	6703	6698	6698	6698	6698	6698	6698	2705	1493
N. barre	6	6	6	6	6	6	6	6	6	3	3
dist. barre	10,40	6,40	16,80	16,80	16,80	16,80	16,80	16,80	16,80	16,80	16,00
Beff (cm)	60	40	92	92	92	92	92	92	92	42	40
Deff (cm)	12,05	11,38	12,40	12,40	12,40	12,40	12,40	12,40	12,40	12,40	12,40
A _{eff}	722,70	455,02	1140,80	1140,80	1140,80	1140,80	1140,80	1140,80	1140,80	515,84	496,00
RO,r	2,14%	3,40%	1,35%	1,35%	1,35%	1,35%	1,35%	1,35%	1,35%	1,17%	0,68%

Combinazioni di carico

Rara	-89,66	-34,28	14,95	49,18	73,10	86,71	89,99	82,97	65,63	37,97	0,00
Frequente	-90,86	-30,46	13,46	44,69	66,52	78,95	81,97	75,58	59,79	34,60	0,00
Quasi perm.	-77,93	-29,18	12,96	43,20	64,33	76,36	79,29	73,12	57,85	33,48	0,00

Verifica allo stato limite di tensione in esercizio

Formata una classe mista di tensioni in esercizio											
Combinazione rara		Sigma,C,amm = 0.60*f _{ck} =				14,94 MPa		Sigma,S,amm = 0.80*f _{yk} =		360 MPa	
Sigma,C	-8,18	-3,78	-0,87	-3,00	-4,45	-5,28	-5,48	-5,05	-4,00	-3,36	-0,01
Sigma,S	206,97	80,17	33,45	110,14	163,71	194,17	201,53	185,80	146,97	210,52	0,01
Combinazione quasi permanente								Sigma,C,amm = 0.45*f _{ck} =		11,21 MPa	
Sigma,C	-7,11	-3,21	-0,76	-2,63	-3,92	-4,65	-4,83	-4,45	-3,52	-2,96	-0,01

Verifica allo stato limite di apertura fessure

S _m (mm)	116,85	98,46	145,88	145,88	145,88	145,88	145,88	145,88	145,88	152,91	187,71
Combinazione frequente	Apertura limite=W3= 0,20 mm										
Sigma,S	186,66	71,23	30,12	100,09	148,97	176,80	183,56	169,26	133,90	191,83	0,10
Eps _{s,m}	0,079%	0,016%	0,006%	0,019%	0,029%	0,048%	0,053%	0,043%	0,026%	0,037%	0,000%
W _k (mm)	0,156	0,027	0,015	0,048	0,072	0,119	0,131	0,106	0,064	0,097	0,000
Combinazione quasi permanente	Apertura limite=W2= 0,20 mm										
Sigma,S	179,90	68,25	29,01	96,73	144,06	171,01	177,57	163,75	129,55	185,60	0,10
Eps _{s,m}	0,075%	0,014%	0,006%	0,019%	0,028%	0,044%	0,049%	0,039%	0,025%	0,036%	0,000%
W _k (mm)	0,149	0,023	0,014	0,047	0,069	0,109	0,121	0,096	0,062	0,094	0,000

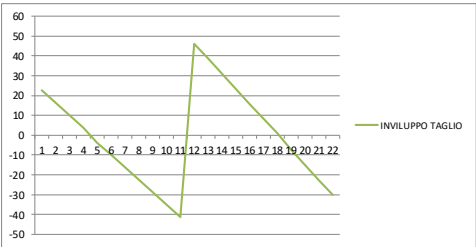
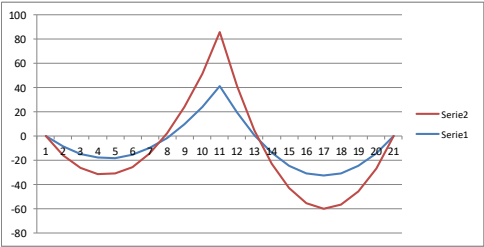
Verifica allo stato limite di deformazione

Verifica esatta: combinazione quasi permanente

Eps _{Cm}	-0,023%	-0,010%	-0,002%	-0,008%	-0,013%	-0,015%	-0,015%	-0,014%	-0,011%	-0,009%	0,000%
Eps _{S,m}	0,085%	0,028%	0,002%	0,043%	0,067%	0,081%	0,084%	0,077%	0,060%	0,088%	0,000%
f _{reccia}	0,000	0,467	1,053	1,625	2,074	2,320	2,322	2,070	1,584	0,880	0,000
f _{reccia massima}	2,32 cm pari a L/395										
verifica sommaria:	Rapporto di snellezza effettivo l/h = 25,50 < 26,00 Rapporto limite										

Solai Primo 5-6 ($G=5.0+2.8 \text{ kN/mq}$; $Q=3.0 \text{ kN/mq}$)

SOLAIO PRIMO - 2 campate																									
SLU						Rara		Frequente		Quasi Perm.		sbalzo a sinistra				sbalzo a destra									
$\gamma_{G1} =$		1,3	$\gamma_{G2} =$		1,3	$\gamma_Q =$		1,5	$\psi_{G1} =$		1	$\psi_{11} =$		0,5	$\psi_{21} =$		0,3	$a_s =$		1,9	m	$a_d =$		1,4	m
TRAVE A 2 CAMPATE + 2 SBALZI																									
		Q_1	L_1	Q_2	L_2	R_1	R_2	M_1	M_2	M_C	T_{sd}	T_{ss}	T_{sd}	T_{Cs}	DISPOSIZIONE CARICHI										
		kN/m	m	kN	m	kN	kN	kN	kNm	kNm	kN	kN	kN	kN	1° camp. 2° camp.										
G1		5,00	9,18	5,00	6,03	28,01	38,92	16,12	-9,03	-40,80	-4,90	28,01	-17,89	21,03	-16,12	G1	5,00	5,00							
G2		2,80	9,18	2,00	6,03	15,84	19,12	5,61	-5,05	-21,41	-1,96	15,84	-9,86	9,25	-5,61	G2	2,80	2,00							
Q1		3,00	9,18	3,00	6,03	16,80	23,35	9,67	-5,42	-24,48	-2,94	16,80	-10,74	12,62	-9,67	Q1	3,00	3,00							
Q2		3,00	9,18	0,00	6,03	17,39	13,31	-3,16	-5,42	-19,07	0,00	17,39	-10,15	3,16	3,16	Q2	3,00								
Q3		0,00	9,18	3,00	6,03	-0,59	10,04	12,84	0,00	-5,41	-2,94	-0,59	-0,59	9,45	-12,84	Q3			3,00						
FLESSIONE																									
		A										B										C			
		L	X	0,00	0,92	1,84	2,75	3,67	4,59	5,51	6,43	7,34	8,26	9,18	10,09	10,99	11,59	12,20	12,80	13,40	14,00	14,61	15,21		
G1				0,00	0,92	1,84	2,75	3,67	4,59	5,51	6,43	7,34	8,26	9,18	10,09	10,99	11,59	12,20	12,80	13,40	14,00	14,61	15,21		
G2				-9,03	14,88	25,55	32,00	34,24	32,27	26,08	15,68	1,07	-17,76	-40,80	-29,03	-19,07	-10,94	-4,62	-3,02	3,62	4,22	4,82	5,43		
Q1				-5,05	8,48	14,60	18,35	19,75	18,79	15,47	9,79	1,75	-8,65	-21,41	-16,19	-11,70	-7,94	-4,90	-2,59	-1,01	-0,16	-0,03	-0,63		
Q2				-5,42	8,93	15,33	19,20	20,55	19,36	15,65	9,41	0,64	-10,65	-24,48	-17,42	-11,44	-6,56	-2,77	-0,07	1,53	2,05	1,48	-0,19		
Q3				-5,42	9,47	16,41	20,82	22,71	22,07	18,89	13,19	4,97	-5,79	-19,07	-19,07	-17,17	-15,26	-13,35	-11,44	-9,54	-7,63	-5,72	-3,81		
MAX				0,00	-0,54	-1,08	-1,62	-2,16	-2,70	-3,24	-3,78	-4,32	-4,87	-5,41	-5,41	-0,25	3,81	6,79	8,67	9,46	9,16	7,77	5,29		
MIN	slu			-18,30	44,57	76,80	96,70	104,26	99,48	82,36	52,91	11,12	-41,62	-88,97	-88,97	-59,16	-34,28	-14,36	0,63	10,66	15,75	15,90	11,10		
MAX	slu			-26,43	29,56	50,57	63,03	66,95	62,33	49,16	27,44	-2,82	-50,31	-117,58	-117,58	-84,91	-62,89	-44,57	-29,55	-17,84	-9,44	-4,34	-2,56		
MIN	rara			-14,08	32,83	56,56	71,18	76,71	73,13	60,45	38,67	7,79	-31,27	-67,61	-67,61	-45,47	-26,96	-12,09	-0,85	6,75	10,71	11,04	7,73		
MAX	rara			-19,49	22,82	39,06	48,74	51,63	48,36	38,31	21,69	-1,50	-37,06	-86,68	-86,68	-62,63	-46,03	-32,23	-20,97	-12,25	-6,08	-2,46	-1,38		
MIN	frequente			-14,08	29,99	51,63	64,93	69,89	66,51	54,78	34,71	6,30	-29,81	-65,99	-65,99	-45,39	-28,10	-14,12	-3,45	3,91	7,96	8,70	6,14		
MAX	frequente			-17,67	22,98	39,39	49,22	52,48	49,17	39,29	22,63	-0,20	-33,86	-79,34	-79,34	-57,41	-41,45	-26,22	-17,53	-9,39	-3,80	-0,74	-0,24		
MIN	q permanente			-14,08	29,04	49,99	62,85	67,62	64,30	52,89	33,39	5,80	-29,32	-65,45	-65,45	-45,37	-28,49	-14,80	-4,32	2,96	7,04	7,93	5,61		
MAX	q permanente			-17,33	23,03	39,50	49,38	52,70	49,44	39,61	23,21	0,23	-32,80	-76,89	-76,89	-55,67	-39,93	-26,89	-16,39	-8,44	-3,03	-0,17	0,14		
TAGLIO																									
		A _x										B _x										C _x			
		L	X	0,00	0,92	1,84	2,75	3,67	4,59	5,51	6,43	7,34	8,26	9,18	10,09	10,99	11,59	12,20	12,80	13,40	14,00	14,61	15,21		
G1				0,00	0,92	1,84	2,75	3,67	4,59	5,51	6,43	7,34	8,26	9,18	10,09	10,99	11,59	12,20 <td>12,80<td>13,40</td><td>14,00</td><td>14,61</td><td>15,21</td></td>	12,80 <td>13,40</td> <td>14,00</td> <td>14,61</td> <td>15,21</td>	13,40	14,00	14,61	15,21		
G2				28,01	23,42	18,83	14,24	9,65	5,06	0,47	-4,12	-8,71	-13,30	-17,89	-21,03	-18,01	-15,00	-11,98	-8,97	-5,95	-2,94	-0,08	-3,09		
G1				15,84	13,27	10,70	8,13	5,56	2,99	0,42	-2,15	-4,72	-7,29	-9,86	-9,25	8,05	6,84	5,64	4,43	3,22	2,02	0,81	-0,39		
Q1				16,80	14,05	11,30	8,54	5,79	3,03	0,28	-2,47	-5,23	-7,98	-10,74	12,62	10,81	9,00	7,19	5,38	3,57	1,76	-0,05			
Q2				17,39	14,64	11,88	9,13	6,38	3,62	0,87	-1,89	-4,64	-7,39	-10,15	3,16	3,16	3,16	3,16	3,16	3,16	3,16	3,16	3,16		
Q3				-0,59	-0,59	-0,59	-0,59	-0,59	-0,59	-0,59	-0,59	-0,59	-0,59	-0,59	9,45	7,64	5,84	4,03	2,22	0,41	-1,40	-3,21			
inv	slu			83,09	69,65	56,21	42,77	29,33	15,89	2,45	-11,87	-25,31	-38,75	-52,19	58,29	50,09	41,89	33,69	25,49	17,29	11,19	5,70			



PRIMO SOLAIO - 2 campate

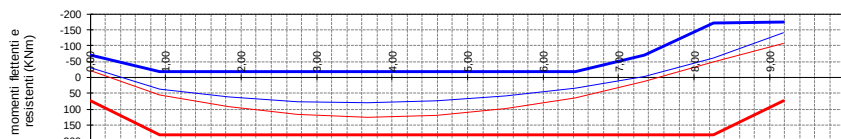
prima campata

Rck	Ec	fcd	fctd	Acciaio	fyd	Bsup	Binf	Sp_ala	h	c	d
MPa	(MPa)	MPa		tipo	MPa	cm			cm	cm	cm
30	31220	14,11	1,14	Feb44k	391	120	40	6	36	4	32

Luce di calcolo (m) 9,18

Verifica agli stati limite ultimi

Inviluppo Momento max	-21,96	53,49	92,17	116,04	125,11	119,38	98,84	63,49	13,34	-49,95	-106,77
Inviluppo Momento min	-31,71	35,47	60,68	75,64	80,34	74,79	58,99	32,93	-3,38	-60,37	-141,10
As,sup,app	2,82	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,30	5,36	12,53
As,inf,app	0,00	4,75	8,38	10,30	11,11	10,60	8,78	5,64	1,38	0,00	0,00
X	0,00	0,92	1,84	2,75	3,67	4,59	5,51	6,43	7,34	8,26	9,18
Armatura (cmq)											
φ6											
φ12		5	5	5	5	5	5	5			
φ16	3								3	3	3
φ20										3	3
As,sup	6,03	1,41	1,41	1,41	1,41	1,41	1,41	1,41	6,03	15,46	15,46
As,inf	6,03	15,46	15,46	15,46	15,46	15,46	15,46	15,46	15,46	15,46	6,03
φ12											
φ16	3	3	3	3	3	3	3	3	3	3	3
φ20		3	3	3	3	3	3	3	3	3	
φ5		0	0	0	0	0	0	0	0	0	0
Momenti positivi											
b	120,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00
psi	0,11	0,18	0,18	0,18	0,18	0,18	0,18	0,18	0,17	0,16	0,12
M+res	73,00	179,63	179,63	179,63	179,63	179,63	179,63	179,63	179,55	179,21	73,31
Momenti negativi											
b	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	60,00
psi	0,17	0,12	0,12	0,12	0,12	0,12	0,12	0,12	0,15	0,21	0,23
M-res	-69,45	-17,90	-17,90	-17,90	-17,90	-17,90	-17,90	-17,90	-69,23	-172,42	-173,23



VERIFICA ALLO S.L.U. DI TAGLIO					k = 1,79	V = 0,42	vbd = 53,56				
Vsd	99,71	83,58	67,45	51,32	35,20	19,07	2,94	-14,25	-30,37	-46,50	-62,63
ρ ₁	0,0047	0,0121	0,0121	0,0121	0,0121	0,0121	0,0121	0,0121	0,0121	0,0121	0,0047
Bmin	63,81	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00

VERIFICA AGLI S.L. DI ESERCIZIO

Caratteristiche geometriche sezioni

Per gruppo di esigenze cond. ambientali poco aggressive e armatura poco sensibile:

	Beta,1 1,00	K2 0,40	Diam.min. 12	copr.netto 3,40							
	Beta,2 0,50	K3 0,13	Sig.SR 101,38	n 15							
As (cmq)	6,03	15,46	15,46	15,46	15,46	15,46	15,46	15,46	15,46	15,46	15,46
A's (cmq)	6,03	1,41	1,41	1,41	1,41	1,41	1,41	1,41	6,03	15,46	6,03
b resistente	40,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	40,00	60,00
Y	9,02	9,27	9,27	9,27	9,27	9,27	9,27	9,27	9,01	11,90	11,61
Wc	6638	16420	16420	16420	16420	16420	16420	16420	17092	10979	11454
Ws	2604	6698	6698	6698	6698	6698	6698	6698	6703	6497	6518
N. barre	3	6	6	6	6	6	6	6	6	6	6
dist. barre	16,00	16,80	16,80	16,80	16,80	16,80	16,80	16,80	16,80	6,40	10,40
Beff (cm)	40	92	92	92	92	92	92	92	92	40	60
Deff (cm)	12,40	12,40	12,40	12,40	12,40	12,40	12,40	12,40	12,40	12,05	12,20
Aeff	496,00	1140,80	1140,80	1140,80	1140,80	1140,80	1140,80	1140,80	1140,80	482,08	731,84
RO,r	1.22%	1.35%	1.35%	1.35%	1.35%	1.35%	1.35%	1.35%	1.35%	3.21%	2.11%

Combinazioni di carico											
Rara	-23,39	39,39	67,87	85,42	92,05	87,75	72,54	46,40	9,35	-44,47	-104,02
Frequente	-21,44	35,99	61,96	77,92	83,87	79,81	65,74	41,65	7,56	-40,64	-95,21
Quasi perm.	-20,79	34,85	59,99	75,42	81,15	77,16	63,47	40,07	6,96	-39,36	-92,27

Verifica allo stato limite di tensione in esercizio

Combinazione rara											
Sigma,C	-3,52	-2,40	-4,13	-5,20	-5,61	-5,34	-4,42	-2,83	-0,55	-4,05	-9,08
Sigma,S	134,76	88,22	151,98	191,29	206,13	196,52	162,45	103,92	20,92	102,68	239,39
Combinazione quasi permanente											
Sigma,C	-3,13	-2,12	-3,65	-4,59	-4,94	-4,70	-3,87	-2,44	-0,41	-3,58	-8,06

Verifica allo stato limite di apertura fessure

Srm (mm)	149,34	145,88	145,88	145,88	145,88	145,88	145,88	145,88	145,88	99,51	117,21
Combinazione frequente											
Sigma,S	123,53	80,59	138,75	174,50	187,82	178,73	147,22	93,28	16,92	93,82	219,11
Eps,sm	0,036%	0,016%	0,043%	0,066%	0,073%	0,068%	0,049%	0,018%	0,003%	0,037%	0,101%
Wk (mm)	0,090	0,039	0,107	0,163	0,182	0,169	0,121	0,045	0,008	0,062	0,201
Combinazione quasi permanente											
Sigma,S	119,79	78,04	134,34	168,90	181,72	172,80	142,14	89,74	15,58	90,87	212,35
Eps,sm	0,033%	0,015%	0,040%	0,062%	0,070%	0,065%	0,046%	0,017%	0,003%	0,035%	0,098%
Wk (mm)	0,084	0,038	0,100	0,154	0,173	0,160	0,113	0,043	0,008	0,060	0,195

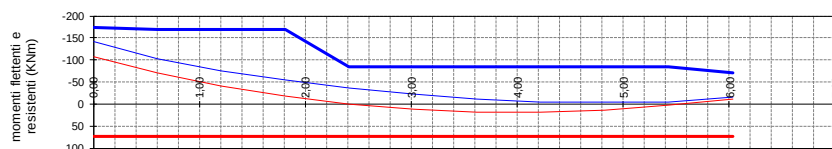
Verifica allo stato limite di deformazione

Verifica esatta: combinazione quasi permanente

EpsCm	-0,010%	-0,007%	-0,012%	-0,015%	-0,016%	-0,015%	-0,012%	-0,008%	-0,001%	-0,011%	-0,026%
EpsSm	0,057%	0,036%	0,064%	0,081%	0,087%	0,083%	0,068%	0,042%	0,003%	0,042%	0,102%
frecchia	0,000	0,763	1,465	1,977	2,245	2,250	2,005	1,558	0,990	0,419	0,000
frecchia massima:		2,25 cm			pari a L/	408					
verifica sommaria:						25,50	<	26,00	Rapporto limite		

PRIMO SOLAIO - 2 campate**seconda campata**Luce di calcolo (m) **6,03****Verifica agli stati limite ultimi**

Involuppo Momento max	-106,77	-70,99	-41,14	-17,23	0,75	12,79	18,91	19,08	13,32	1,63	-10,70
	Coeff. di redistribuzione delta= 1,00										
psi-max											
Involuppo Momento min	-141,10	-101,89	-75,47	-53,48	-35,46	-21,40	-11,32	-5,21	-3,07	-4,90	-15,99
	Coeff. di redistribuzione delta= 1,00										
psi-max											
As,sup.app	12,53	9,05	6,70	4,75	3,35	190	101	0,46	0,27	0,44	142
As,inf.app	0,00	0,00	0,00	0,00	0,07	114	168	169	138	0,34	0,00
X	0,00	0,60	1,21	1,81	2,41	3,02	3,62	4,22	4,82	5,43	6,03
Armatura (cmq)											
φ 6	0				5	5	5	5	5	5	
φ 12	0										
φ 16	3	3	3	3	3	3	3	3	3	3	3
φ 20	3	3	3	3							
As,sup	15,46	15,46	15,46	15,46	7,45	7,45	7,45	7,45	7,45	7,45	6,03
As,inf	6,03	6,03	6,03	6,03	6,03	6,03	6,03	6,03	6,03	6,03	6,03
φ 12	0										
φ 16	3	3	3	3	3	3	3	3	3	3	3
φ 20	0										
φ 5	0										
Momenti positivi											
b	120	120	120	120	120	120	120	120	120	120	120
psi	0,12	0,12	0,12	0,12	0,11	0,11	0,11	0,11	0,11	0,11	0,11
M+res	73,31	73,31	73,31	73,31	73,07	73,07	73,07	73,07	73,07	73,07	73,00
Momenti negativi											
b	60	40	40	40	40	40	40	40	40	40	60
psi	0,23	0,30	0,30	0,30	0,18	0,18	0,18	0,18	0,18	0,18	0,15
M-res	-173,23	-169,41	-169,41	-169,41	-84,98	-84,98	-84,98	-84,98	-84,98	-84,98	-70,73



VERIFICA ALLO S.L.U. DI TAGLIO											
	k = 1,79										
	V = 0,42										
	v _{bd} = 53,56										
V _{sd}	69,95	60,11	50,27	40,43	30,59	20,75	13,43	6,84	-14,47	-24,31	-57,00
ρ ₁	0,0047	0,0047	0,0047	0,0047	0,0047	0,0047	0,0047	0,0047	0,0047	0,0047	0,0047
B _{min}	44,77	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00

VERIFICA AGLI S.L. DI ESERCIZIO**Caratteristiche geometriche sezioni**

Per gruppo di esigenze cond. ambientali poco aggressive e armatura poco sensibile:											
	Beta,1 1,00		K2 0,40		Diam.min. 12		copr.netto 3,40				
	Beta,2 1,00		K3 0,13		Sig.SR 101,38		n 15				
As (cmq)	15,46	15,46	15,46	15,46	7,45	7,45	6,03	6,03	6,03	7,45	6,03
A's (cmq)	6,03	6,03	6,03	6,03	6,03	6,03	7,45	7,45	7,45	6,03	6,03
b resistente	60,00	40,00	40,00	40,00	40,00	40,00	120,00	120,00	120,00	40,00	60,00
Y	11,61	13,25	13,25	13,25	9,86	9,86	5,97	5,97	5,97	9,86	7,83
Wc	11454	9078	9078	9078	7166	7166	11774	11774	11774	7166	8144
Ws	6518	6414	6414	6414	3190	3190	2698	2698	2698	3190	2639
N. barre	6	6	6	6	8	8	3	3	3	8	3
dist. barre	10,40	6,40	6,40	6,40	4,57	4,57	16,80	16,80	16,80	4,57	16,80
Beff (cm)	60	40	40	40	40	40	42	42	42	40	42
Deff (cm)	12,20	11,38	11,38	11,38	12,40	12,40	12,40	12,40	12,40	12,40	12,40
A _{eff}	731,84	455,02	455,02	455,02	496,00	496,00	515,84	515,84	515,84	496,00	515,84
RO _r	2,11%	3,40%	3,40%	3,40%	1,50%	1,50%	1,17%	1,17%	1,17%	1,50%	1,17%

Combinazioni di carico											
Rara	-104,02	-75,16	-55,24	-38,67	-25,16	-14,70	12,85	13,24	9,27	-3,42	-11,76
Frequente	-95,21	-68,89	-49,75	-33,87	-21,04	-11,27	9,55	10,44	7,37	-2,73	-10,70
Quasi perm.	-92,27	-66,80	-47,91	-32,26	-19,67	-10,13	8,45	9,51	6,73	-2,50	-10,35

Verifica allo stato limite di tensione in esercizio											
Combinazione rara	Sigma,C,amm = 0.60*f _{ck} = 14,94 MPa										
Sigma,C	-9,08	-8,28	-6,09	-4,26	-3,51	-2,05	-1,09	-1,12	-0,79	-0,48	-1,44
Sigma,S	239,39	175,77	129,19	90,44	118,32	69,14	71,44	73,62	51,54	16,07	66,84
Combinazione quasi permanente	Sigma,C,amm = 0.45*f _{ck} = 11,21 MPa										
Sigma,C	-8,06	-7,36	-5,28	-3,55	-2,74	-1,41	-0,72	-0,81	-0,57	-0,35	-1,27

Verifica allo stato limite di apertura fessure											
S _{rm} (mm)	117,21	98,46	98,46	98,46	117,11	117,11	152,91	152,91	152,91	117,11	152,91
Combinazione frequente	Apertura limite=W3= 0,20 mm										
Sigma,S	219,11	161,11	116,34	79,20	98,95	53,00	53,10	58,06	40,95	12,84	60,82
E _{ps,sm}	0,096%	0,070%	0,045%	0,022%	0,019%	0,010%	0,010%	0,011%	0,008%	0,002%	0,012%
W _k (mm)	0,191	0,117	0,076	0,037	0,038	0,020	0,027	0,029	0,021	0,005	0,031
Combinazione quasi permanente	Apertura limite=W2= 0,20 mm										
Sigma,S	212,35	156,22	112,06	75,46	92,49	47,62	46,99	52,87	37,42	11,77	58,82
E _{ps,sm}	0,092%	0,067%	0,043%	0,019%	0,018%	0,009%	0,009%	0,010%	0,007%	0,002%	0,011%
W _k (mm)	0,184	0,113	0,072	0,032	0,036	0,018	0,024	0,027	0,019	0,005	0,030

Verifica allo stato limite di deformazione											
Verifica esatta: combinazione quasi permanente											
E _{ps,Cm}	-0,026%	-0,024%	-0,017%	-0,011%	-0,009%	-0,005%	-0,002%	-0,003%	-0,002%	-0,001%	-0,004%
E _{ps,Sm}	0,101%	0,074%	0,051%	0,032%	0,041%	0,015%	0,015%	0,019%	0,008%	0,003%	0,022%
f _{reccia}	0,000	-0,229	-0,348	-0,388	-0,370	-0,306	-0,222	-0,148	-0,093	-0,050	0,000
f _{reccia massima:}	0,00 cm										
verifica sommaria:	Rapporto di snellezza effettivo l/h = 16,75 < 26,00 Rapporto limite										

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Figure 10 consists of two line graphs. The top graph shows the evolution of the Involvement Ratio (green line) over 31 days. The y-axis ranges from -6000 to 8000. The bottom graph shows the evolution of the Moment of Inertia (red line) over 31 days. The y-axis ranges from -2500 to 2500. Both graphs have an x-axis labeled from 1 to 31.

Day	Involvement Ratio	Moment of Inertia
1	4000	1000
2	4000	1000
3	4000	1000
4	4000	1000
5	4000	1000
6	4000	1000
7	4000	1000
8	4000	1000
9	4000	1000
10	4000	1000
11	4000	1000
12	4000	1000
13	4000	1000
14	4000	1000
15	4000	1000
16	4000	1000
17	4000	1000
18	4000	1000
19	4000	1000
20	4000	1000
21	4000	1000
22	4000	1000
23	4000	1000
24	4000	1000
25	4000	1000
26	4000	1000
27	4000	1000
28	4000	1000
29	4000	1000
30	4000	1000
31	4000	1000

PRIMO SOLAIO - 3 campate

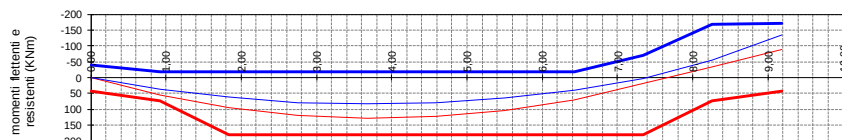
prima campata

Rck	Ec	fcd	fctd	Acciaio	fyd	Bsup	Binf	Sp_ala	h	c	d
MPa	(MPa)	MPa		tipo	MPa	cm			cm	cm	cm
30	31220	14,11	1,14	Feb44k	391	120	40	6	36	4	32

Luce di calcolo (m) 9,18

Verifica agli stati limite ultimi

Inviluppo Momento max	0,00	54,28	93,76	118,44	128,31	123,37	103,63	69,09	19,74	-32,47	-87,35
Inviluppo Momento min	0,00	36,31	62,36	78,15	83,70	78,98	64,02	38,80	3,32	-54,35	-134,42
As,sup.app	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	4,83	11,94
As,inf.app	0,00	4,82	8,33	10,52	11,39	10,96	9,20	6,34	1,75	0,00	0,00
X	0,00	0,92	1,84	2,75	3,67	4,59	5,51	6,43	7,34	8,26	9,18
Armatura (cmq)											
φ6											
φ12	3	5	5	5	5	5	5	5			
φ16									3	3	3
φ20										3	3
As,sup	3,39	1,41	1,41	1,41	1,41	1,41	1,41	1,41	6,03	15,46	15,46
As,inf	3,39	6,03	15,46	15,46	15,46	15,46	15,46	15,46	15,46	6,03	3,39
φ12	3										3
φ16		3	3	3	3	3	3	3	3	3	
φ20			3	3	3	3	3	3	3		
φ5		0	0	0	0	0	0	0	0	0	0
Momenti positivi											
b	120,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00
psi	0,09	0,11	0,18	0,18	0,18	0,18	0,18	0,18	0,17	0,12	0,10
M+res	42,04	72,73	179,63	179,63	179,63	179,63	179,63	179,63	179,55	73,31	43,30
Momenti negativi											
b	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	60,00
psi	0,14	0,11	0,12	0,12	0,12	0,12	0,12	0,12	0,15	0,30	0,26
M-res	-40,10	-17,69	-17,90	-17,90	-17,90	-17,90	-17,90	-17,90	-69,23	-169,41	-172,02



VERIFICA ALLO S.L.U. DI TAGLIO					k = 1,79		V = 0,42		vbd = 53,56		
Vsd	50,28	39,60	28,91	18,22	7,54	-3,99	-14,68	-25,36	-36,05	-46,74	-57,42
ρ ₁	0,0027	0,0047	0,0121	0,0121	0,0121	0,0121	0,0121	0,0121	0,0121	0,0047	0,0027
Bmin	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00

VERIFICA AGLI S.L. DI ESERCIZIO

Caratteristiche geometriche sezioni											
Per gruppo di esigenze cond. ambientali poco aggressive e armatura poco sensibile:											
	Beta,1 1,00	K2 0,40		Diam.min. 12				copr.netto 3,40			
	Beta,2 0,50	K3 0,13		Sig.SR 101,38				n 15			
As (cmq)	3,39	6,03	15,46	15,46	15,46	15,46	15,46	15,46	15,46	15,46	15,46
A's (cmq)	3,39	1,41	1,41	1,41	1,41	1,41	1,41	1,41	6,03	6,03	3,39
b resistente	40,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	40,00	60,00
Y	7,36	6,18	9,27	9,27	9,27	9,27	9,27	9,27	9,01	13,25	11,91
Wc	4999	11308	16420	16420	16420	16420	16420	16420	17092	9078	10961
Ws	1493	2705	6698	6698	6698	6698	6698	6698	6703	6414	6498
N. barre	3	3	6	6	6	6	6	6	6	6	6
dist. barre	16,00	16,80	16,80	16,80	16,80	16,80	16,80	16,80	16,80	6,40	10,40
Beff (cm)	40	42	92	92	92	92	92	92	92	40	60
Deff (cm)	12,40	12,40	12,40	12,40	12,40	12,40	12,40	12,40	12,40	11,38	12,05
Aeff	496,00	515,84	1140,80	1140,80	1140,80	1140,80	1140,80	1140,80	1140,80	455,02	722,70
RO,r	0,68%	1,17%	1,35%	1,35%	1,35%	1,35%	1,35%	1,35%	1,35%	3,40%	2,14%

Combinazioni di carico											
Rara	0,00	39,99	69,06	87,21	94,44	90,75	76,13	50,60	14,14	-39,87	-98,91
Frequente	0,00	36,55	63,09	79,62	86,14	82,65	69,14	45,63	12,10	-36,08	-90,14
Quasi perm.	0,00	35,41	61,10	77,09	83,38	79,95	66,81	43,97	11,42	-34,81	-87,22

Verifica allo stato limite di tensione in esercizio											
Combinazione rara											
Sigma,C	-0,01	-3,54	-4,21	-5,31	-5,75	-5,53	-4,64	-3,08	-0,83	-4,39	-9,02
Sigma,S	0,01	221,73	154,66	195,31	211,50	203,22	170,49	113,31	31,64	93,24	228,31
Combinazione quasi permanente											
Sigma,C	-0,01	-3,13	-3,72	-4,70	-5,08	-4,87	-4,07	-2,68	-0,67	-3,84	-7,96

Verifica allo stato limite di apertura fessure											
Srm (mm)	187,71	152,91	145,88	145,88	145,88	145,88	145,88	145,88	145,88	98,46	116,85
Combinazione frequente											
Sigma,S	0,10	202,66	141,29	178,31	192,91	185,09	154,84	102,18	27,08	84,37	208,08
Eps.sm	0,000%	0,039%	0,045%	0,068%	0,076%	0,072%	0,054%	0,020%	0,005%	0,033%	0,096%
Wk (mm)	0,000	0,102	0,112	0,168	0,189	0,178	0,133	0,049	0,013	0,056	0,190
Combinazione quasi permanente											
Sigma,S	0,10	196,30	136,84	172,65	186,71	179,04	149,63	98,47	25,56	81,42	201,34
Eps.sm	0,000%	0,038%	0,042%	0,065%	0,073%	0,068%	0,050%	0,019%	0,005%	0,032%	0,092%
Wk (mm)	0,000	0,099	0,104	0,160	0,181	0,169	0,125	0,047	0,012	0,053	0,183

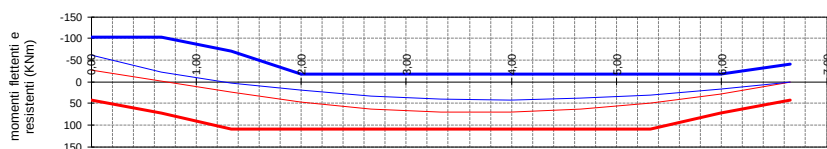
Verifica allo stato limite di deformazione											
Verifica esatta: combinazione quasi permanente											
EpsCm	0,000%	-0,010%	-0,012%	-0,015%	-0,016%	-0,016%	-0,013%	-0,009%	-0,002%	-0,012%	-0,025%
EpsSm	0,000%	0,094%	0,065%	0,083%	0,090%	0,086%	0,071%	0,046%	0,005%	0,037%	0,097%
frecchia	0,000	0,937	1,686	2,201	2,466	2,461	2,196	1,718	1,107	0,483	0,000
frecchia massima:		2,47 cm			pari a L/372						
verifica sommaria:		Rapporto di snellezza effettivo l/h =			25,50	<	26,00	Rapporto limite			

PRIMO SOLAIO - 3 campate1**terza campata**

Luce di calcolo (m)

6,65**Verifica agli stati limite ultimi**

Inviluppo Momento max	-26,73	-1,70	24,31	47,02	62,37	70,36	71,00	64,28	50,21	28,78	0,00
	Coeff. di redistribuzione delta= 1,00 psi-max										
Inviluppo Momento min	-61,55	-22,29	3,64	20,57	32,53	39,53	41,56	38,62	30,71	17,84	0,00
	Coeff. di redistribuzione delta= 1,00 psi-max										
As,sup.app	5,47	198	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00
As,inf.app	0,00	0,00	2,36	4,38	5,54	6,25	6,30	5,71	4,46	2,56	0,00
X	0,00	0,67	1,33	2,00	2,66	3,33	3,99	4,66	5,32	5,99	6,65
Armatura (cmq)											
φ6	0			5	5	5	5	5	5	5	
φ12	0										3
φ16	3	3	3								
φ20	1	1									
As,sup	9,17	9,17	6,03	1,41	1,41	1,41	1,41	1,41	1,41	1,41	3,39
As,inf	3,39	6,03	9,17	9,17	9,17	9,17	9,17	9,17	9,17	6,03	3,39
φ12	3										3
φ16	0	3	3	3	3	3	3	3	3	3	
φ20	0		1	1	1	1	1	1	1		
φ5	0										
Momenti positivi											
b	120	120	120	120	120	120	120	120	120	120	120
psi	0,10	0,11	0,13	0,13	0,13	0,13	0,13	0,13	0,13	0,11	0,09
M+res	42,81	73,13	109,00	109,12	109,12	109,12	109,12	109,12	109,12	72,73	42,04
Momenti negativi											
b	40	40	40	40	40	40	40	40	40	40	40
psi	0,23	0,20	0,16	0,11	0,11	0,11	0,11	0,11	0,11	0,11	0,14
M-res	-103,36	-103,75	-69,37	-17,79	-17,79	-17,79	-17,79	-17,79	-17,79	-17,69	-40,10



VERIFICA ALLO S.L.U. DI TAGLIO											
k = 1,79 V = 0,42 v _{bd} = 53,56											
V _{sd}	61,09	43,94	36,20	28,46	20,72	12,98	6,36	-3,98	-11,72	-19,46	-27,20
ρ ₁	0,0027	0,0047	0,0072	0,0072	0,0072	0,0072	0,0072	0,0072	0,0072	0,0047	0,0027
B _{min}	47,36	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00

VERIFICA AGLI S.L. DI ESERCIZIO**Caratteristiche geometriche sezioni**

Per gruppo di esigenze cond. ambientali poco aggressive e armatura poco sensibile:

Beta,1 **1,00** K2 **0,40**Diam.min. **12**copr.netto **3,40**Beta,2 **1,00** K3 **0,13**Sig.SR **101,38**n **15**

As (cmq)	9,17	9,17	9,17	9,17	9,17	9,17	9,17	9,17	9,17	6,03	3,39
A's (cmq)	3,39	6,03	6,03	1,41	1,41	1,41	1,41	1,41	1,41	1,41	3,39
b resistente	60,00	40,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	40,00
Y	9,64	10,75	7,21	7,43	7,43	7,43	7,43	7,43	7,43	6,18	7,36
W _c	9161	7702	13934	13429	13429	13429	13429	13429	13429	11308	4999
W _s	3951	3898	4054	4058	4058	4058	4058	4058	4058	2705	1493
N. barre	4	4	4	4	4	4	4	4	4	3	3
dist. barre	16,80	10,67	16,80	16,80	16,80	16,80	16,80	16,80	16,80	16,80	16,00
Beff (cm)	58	40	58	58	58	58	58	58	58	42	40
Deff (cm)	12,40	12,40	12,40	12,40	12,40	12,40	12,40	12,40	12,40	12,40	12,40
Aeff	724,16	496,00	724,16	724,16	724,16	724,16	724,16	724,16	724,16	515,84	496,00
RO _r	1,27%	1,85%	1,27%	1,27%	1,27%	1,27%	1,27%	1,27%	1,27%	1,17%	0,68%

Combinazioni di carico

Rara	-44,65	-15,83	17,39	34,16	45,52	51,46	52,00	47,12	36,82	21,12	0,00
Frequente	-39,40	-13,25	14,83	30,25	40,73	46,28	46,89	42,57	33,32	19,13	0,00
Quasi perm.	-37,65	-12,39	13,97	28,94	39,14	44,55	45,19	41,06	32,15	18,46	0,00

Verifica allo stato limite di tensione in esercizio

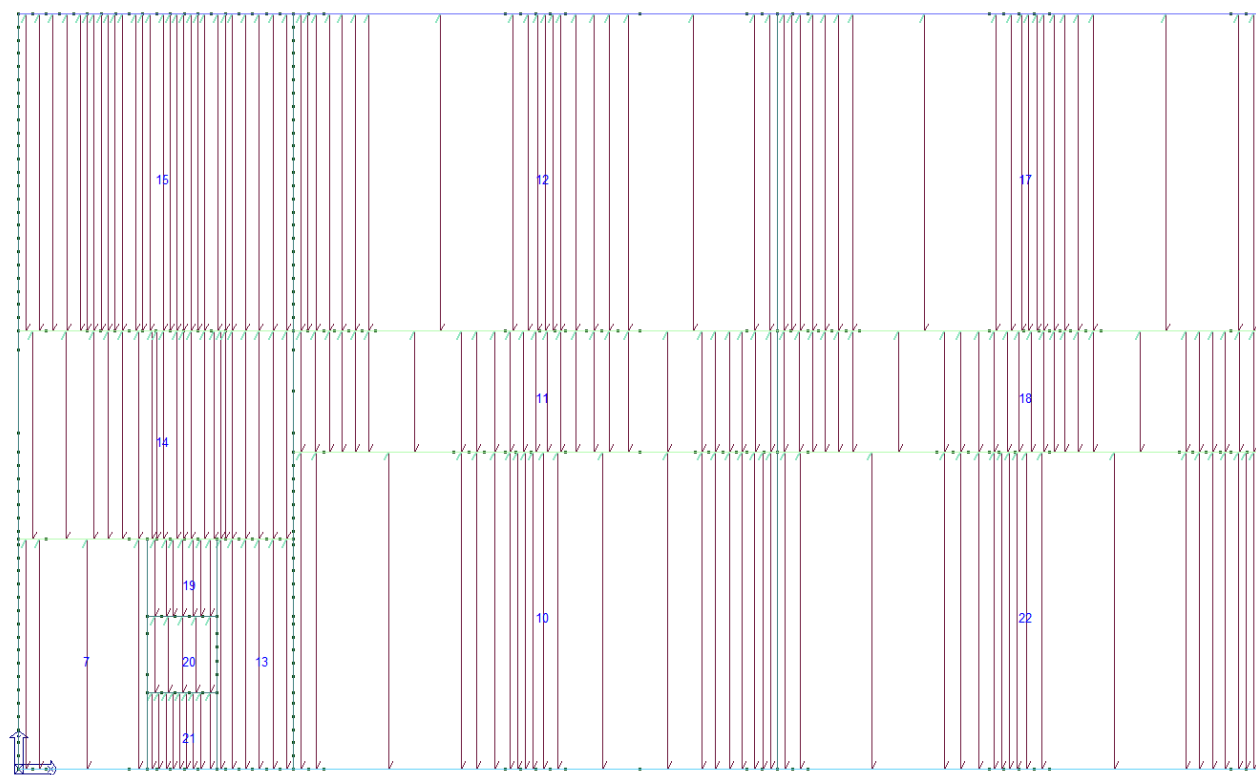
Combinazione rara	Sigma,C,amm = 0.60*f _{ck} = 14,94 MPa Sigma,S,amm = 0.80*f _{yk} = 360 MPa										
Sigma,C	-4,87	-2,06	-1,25	-2,54	-3,39	-3,83	-3,87	-3,51	-2,74	-1,87	-0,01
Sigma,S	169,52	60,91	64,34	126,27	168,25	190,23	192,20	174,16	136,11	117,09	0,01
Combinazione quasi permanente	Sigma,C,amm = 0.45*f _{ck} = 11,21 MPa										
Sigma,C	-4,11	-1,61	-1,00	-2,16	-2,91	-3,32	-3,37	-3,06	-2,39	-1,63	-0,01

Verifica allo stato limite di apertura fessure

S _{rm} (mm)	148,96	121,77	148,96	148,96	148,96	148,96	148,96	148,96	148,96	152,91	187,71
Combinazione frequente	Apertura limite=W3= 0,20 mm										
Sigma,S	149,59	50,99	54,86	111,80	150,55	171,07	173,34	157,37	123,15	106,04	0,10
Eps _s ,sm	0,038%	0,010%	0,011%	0,022%	0,029%	0,033%	0,034%	0,031%	0,024%	0,021%	0,000%
W _k (mm)	0,095	0,020	0,027	0,055	0,074	0,084	0,085	0,077	0,061	0,054	0,000
Combinazione quasi permanente	Apertura limite=W2= 0,20 mm										
Sigma,S	142,95	47,69	51,70	106,98	144,65	164,68	167,05	151,77	118,83	102,36	0,10
Eps _s ,sm	0,033%	0,009%	0,010%	0,021%	0,028%	0,032%	0,032%	0,029%	0,023%	0,020%	0,000%
W _k (mm)	0,083	0,019	0,025	0,053	0,071	0,081	0,082	0,075	0,058	0,052	0,000

Verifica allo stato limite di deformazione**Verifica esatta: combinazione quasi permanente**

Eps _{Cm}	-0,013%	-0,005%	-0,003%	-0,007%	-0,009%	-0,011%	-0,011%	-0,010%	-0,008%	-0,005%	0,000%
Eps _{Sm}	0,067%	0,016%	0,018%	0,049%	0,068%	0,078%	0,079%	0,071%	0,055%	0,046%	0,000%
frecchia	0,000	0,266	0,567	0,841	1,043	1,141	1,122	0,981	0,732	0,395	0,000
frecchia massima:	1,14 cm pari a L/										
verifica sommaria:	Rapporto di snellezza effettivo l/h = 18,47 < 26,00 Rapporto limite										



Solaio di copertura

64

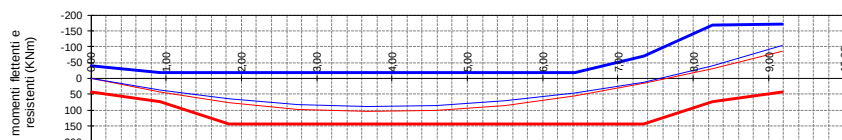
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SECONDO SOLAIO - 3 campate**prima campata**

Rck	Ec	fcd	fctd	Acciaio	fyd	Bsup	Binf	Sp_ala	h	c	d
MPa	(MPa)	MPa		tipo	MPa	cm			cm	cm	cm
30	31220	14,11	1,14	Feb44k	391	120	40	6	36	4	32

Luce di calcolo (m) **9,18****Verifica agli stati limite ultimi**

Inviluppo Momento max	0,00	44,22	76,36								
				Coeff. di redistribuzione delta=	1,00				psi-max		
						96,42	104,42	100,33	84,18	55,95	15,64
Inviluppo Momento min	0,00	37,39	64,53							-29,82	-84,40
				Coeff. di redistribuzione delta=	1,00				psi-max		
						81,41	88,04	84,42	70,54	46,40	12,02
										-39,55	-104,31
As,sup,app	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	3,51	9,26
As,inf,app	0,00	3,93	6,78	8,56	9,27	8,91	7,48	4,97	1,39	0,00	0,00
X	0,00	0,92	1,84	2,75	3,67	4,59	5,51	6,43	7,34	8,26	9,18
Armatura (cmq)											
φ6											
φ12	3	5	5	5	5	5	5	5			
φ16									3	3	3
φ20										3	3
As,sup	3,39	1,41	1,41	1,41	1,41	1,41	1,41	1,41	6,03	15,46	15,46
As,inf	3,39	6,03	12,32	12,32	12,32	12,32	12,32	12,32	12,32	6,03	3,39
φ12	3										
φ16		3	3	3	3	3	3	3	3	3	3
φ20			2	2	2	2	2	2	2	2	2
φ5		0	0	0	0	0	0	0	0	0	0
Momenti positivi											
b	120,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00
psi	0,09	0,11	0,16	0,16	0,16	0,16	0,16	0,16	0,15	0,12	0,10
M+res	42,04	72,73	144,79	144,79	144,79	144,79	144,79	144,79	144,54	73,31	43,30
Momenti negativi											
b	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	60,00
psi	0,14	0,11	0,11	0,11	0,11	0,11	0,11	0,11	0,15	0,30	0,26
M-res	-40,10	-17,69	-17,86	-17,86	-17,86	-17,86	-17,86	-17,86	-69,29	-169,41	-172,02



VERIFICA ALLO S.L.U. DI TAGLIO				k = 1,79		V = 0,42		vbd = 53,56			
Vsd	48,96	38,61	28,25	17,90	7,54	-2,81	-13,17	-23,53	-33,88	-44,24	-54,59
ρ ₁	0,0027	0,0047	0,0096	0,0096	0,0096	0,0096	0,0096	0,0096	0,0096	0,0047	0,0027
Bmin	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00

VERIFICA AGLI S.L. DI ESERCIZIOCaratteristiche geometriche sezioni
Per gruppo di esigenze cond. ambientali poco aggressive e armatura poco sensibile:

Per gruppo di esigenze cond. ambientali poco aggressive e armatura poco sensibile										
	Beta,1 1,00		K2 0,40		Diam.min. 12		copr.netto 3,40			
	Beta,2 0,50		K3 0,13		Sig.SR 101,38		n 15			
As (cmq)	3,39	6,03	12,32	12,32	12,32	12,32	12,32	12,32	12,32	15,46
A's (cmq)	3,39	1,41	1,41	1,41	1,41	1,41	1,41	1,41	6,03	3,39
b resistente	40,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	60,00
Y	7,36	6,18	8,43	8,43	8,43	8,43	8,43	8,43	8,19	13,25
Wc	4999	11308	15071	15071	15071	15071	15071	15071	15672	10961
Ws	1493	2705	5388	5388	5388	5388	5388	5388	5387	6414
N. barre	3	3	5	5	5	5	5	5	5	6
dist. barre	16,00	16,80	16,80	16,80	16,80	16,80	16,80	16,80	16,80	6,40
Beff (cm)	40	42	75	75	75	75	75	75	75	40
Deff (cm)	12,40	12,40	12,40	12,40	12,40	12,40	12,40	12,40	12,40	11,38
Aeff	496,00	515,84	932,48	932,48	932,48	932,48	932,48	932,48	932,48	455,02
RO,r	0,68%	1,17%	1,32%	1,32%	1,32%	1,32%	1,32%	1,32%	1,32%	3,40%

Combinazioni di carico											
Rara	0,00	33,32	57,54	72,66	78,67	75,59	63,40	42,11	11,73	-29,64	-78,44
Frequente	0,00	31,97	55,21	69,70	75,46	72,49	60,77	40,32	11,13	-28,11	-74,92
Quasi perm.	0,00	31,52	54,43	68,72	74,39	71,45	59,89	39,72	10,93	-27,60	-73,75

Verifica allo stato limite di tensione in esercizio

Combinazione rara											
Sigma,C	-0,01	-2,95	-3,82	-4,82	-5,22	-5,02	-4,21	-2,79	-0,75	-3,26	-7,16
Sigma,S	0,01	184,74	160,20	202,29	219,04	210,45	176,52	117,25	32,65	69,31	181,06
Combinazione quasi permanente											
Sigma,C	-0,01	-2,79	-3,61	-4,56	-4,94	-4,74	-3,97	-2,64	-0,70	-3,04	-6,73

Verifica allo stato limite di apertura fessure

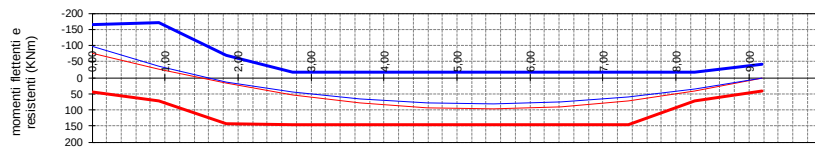
S _m (mm)	187,71	152,91	147,03	147,03	147,03	147,03	147,03	147,03	147,03	98,46	116,85
Combinazione frequente											
Sigma,S	0,10	177,26	153,70	194,07	210,10	201,81	169,20	112,25	30,99	65,74	172,94
Eps _s ,sm	0,000%	0,034%	0,042%	0,069%	0,078%	0,073%	0,053%	0,022%	0,006%	0,022%	0,078%
Wk (mm)	0,000	0,089	0,106	0,171	0,196	0,183	0,132	0,054	0,015	0,037	0,154
Combinazione quasi permanente											
Sigma,S	0,10	174,77	151,54	191,33	207,12	198,93	166,75	110,59	30,43	64,55	170,23
Eps _s ,sm	0,000%	0,034%	0,041%	0,067%	0,077%	0,072%	0,051%	0,021%	0,006%	0,021%	0,076%
Wk (mm)	0,000	0,088	0,102	0,167	0,191	0,179	0,128	0,054	0,015	0,036	0,151

Verifica allo stato limite di deformazione

Verifica esatta: combinazione quasi permanente											
Eps _s ,Cm	0,000%	-0,009%	-0,012%	-0,015%	-0,016%	-0,015%	-0,013%	-0,008%	-0,002%	-0,010%	-0,022%
Eps _s ,Sm	0,000%	0,084%	0,072%	0,092%	0,100%	0,096%	0,080%	0,052%	0,009%	0,029%	0,082%
freccia	0,000	0,995	1,812	2,387	2,691	2,700	2,426	1,917	1,261	0,575	0,000
freccia massima:		2,70 cm			pari a L/	340					
verifica sommaria:		Rapporto di snellezza effettivo l/h =				25,50	<	26,00	Rapporto limite		

SECONDO SOLAIO - 3 campate**terza campata**Luce di calcolo (m) **9,18****Verifica agli stati limite ultimi**

Involuppo Momento max	Coeff. di redistribuzione delta= 1,00										psi-max
	-76,12	-25,91	15,96	53,46	79,68	94,62	98,26	90,63	71,70	41,49	0,00
Involuppo Momento min	Coeff. di redistribuzione delta= 1,00										psi-max
	-96,03	-35,64	12,33	43,92	66,04	78,70	81,89	75,62	59,88	34,67	0,00
As,sup.app	8,53	3,17	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00
As,inf.app	0,00	0,00	1,42	4,75	7,08	8,40	8,73	8,05	6,37	3,68	0,00
X	0,00	0,92	1,84	2,75	3,67	4,59	5,51	6,43	7,34	8,26	9,18
Armatura (cmq)											
φ6	0			5	5	5	5	5	5	5	
φ12	0										3
φ16	3	3	3								
φ20	3	3									
As,sup	15,46	15,46	6,03	1,41	1,41	1,41	1,41	1,41	1,41	1,41	3,39
As,inf	3,39	6,03	12,32	12,32	12,32	12,32	12,32	12,32	12,32	6,03	3,39
φ12	3										3
φ16	0	3	3	3	3	3	3	3	3	3	
φ20	0		2	2	2	2	2	2	2		
φ5	0										
Momenti positivi											
b	120	120	120	120	120	120	120	120	120	120	120
psi	0,10	0,12	0,15	0,16	0,16	0,16	0,16	0,16	0,16	0,11	0,09
M+res	43,30	73,31	144,54	144,79	144,79	144,79	144,79	144,79	144,80	72,73	42,04
Momenti negativi											
b	40	40	40	40	40	40	40	40	40	40	40
psi	0,38	0,30	0,15	0,11	0,11	0,11	0,11	0,11	0,11	0,11	0,14
M-res	-164,26	-169,41	-69,29	-17,86	-17,86	-17,86	-17,86	-17,86	-17,86	-17,69	-40,10



VERIFICA ALLO S.L.U. DI TAGLIO											
	k = 1,79										vbd = 53,56
Vsd	68,37	53,55	44,19	34,82	25,46	16,09	7,53	-2,63	-12,00	-21,36	-30,72
ρ ₁	0,0027	0,0047	0,0096	0,0096	0,0096	0,0096	0,0096	0,0096	0,0096	0,0047	0,0027
Bmin	53,01	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00

VERIFICA AGLI S.L. DI ESERCIZIO**Caratteristiche geometriche sezioni**

Per gruppo di esigenze cond. ambientali poco aggressive e armatura poco sensibile:

Beta,1	1,00	K2	0,40	Diam.min.	12	copr.netto	3,40
Beta,2	1,00	K3	0,13	Sig.SR	101,38	n	15

As (cmq)	15,46	15,46	12,32	12,32	12,32	12,32	12,32	12,32	12,32	6,03	3,39
A's (cmq)	3,39	6,03	6,03	1,41	1,41	1,41	1,41	1,41	1,41	1,41	3,39
b resistente	60,00	40,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	40,00
Y	11,91	13,25	8,19	8,43	8,43	8,43	8,43	8,43	8,43	6,18	7,36
Wc	10961	9078	15672	15071	15071	15071	15071	15071	15071	11308	4999
Ws	6498	6414	5387	5388	5388	5388	5388	5388	5388	2705	1493
N. barre	6	6	5	5	5	5	5	5	5	3	3
dist. barre	10,40	6,40	16,80	16,80	16,80	16,80	16,80	16,80	16,80	16,80	16,00
Beff (cm)	60	40	75	75	75	75	75	75	75	42	40
Deff (cm)	12,05	11,38	12,40	12,40	12,40	12,40	12,40	12,40	12,40	12,40	12,40
Aeff	722,70	455,02	932,48	932,48	932,48	932,48	932,48	932,48	932,48	515,84	496,00
RO,r	2,14%	3,40%	1,32%	1,32%	1,32%	1,32%	1,32%	1,32%	1,32%	1,17%	0,68%

Combinazioni di carico

Rara	-72,07	-26,63	11,97	40,20	59,94	71,19	73,94	68,20	53,96	31,23	0,00
Frequente	-68,55	-25,11	11,37	38,41	57,31	68,09	70,73	65,24	51,63	29,88	0,00
Quasi perm.	-67,38	-24,60	11,17	37,81	56,43	67,05	69,66	64,26	50,85	29,43	0,00

Verifica allo stato limite di tensione in esercizio

Combinazione rara	Sigma,C,amm = 0.60*fck = 14,94 MPa										Sigma,S,amm = 0.80*fyk = 360 MPa
Sigma,C	-6,57	-2,93	-0,76	-2,67	-3,98	-4,72	-4,91	-4,53	-3,58	-2,76	-0,01
Sigma,S	166,36	62,29	33,32	111,93	166,89	198,20	205,86	189,87	150,23	173,13	0,01
Combinazione quasi permanente	Sigma,C,amm = 0.45*fck = 11,21 MPa										
Sigma,C	-6,15	-2,71	-0,71	-2,51	-3,74	-4,45	-4,62	-4,26	-3,37	-2,60	-0,01

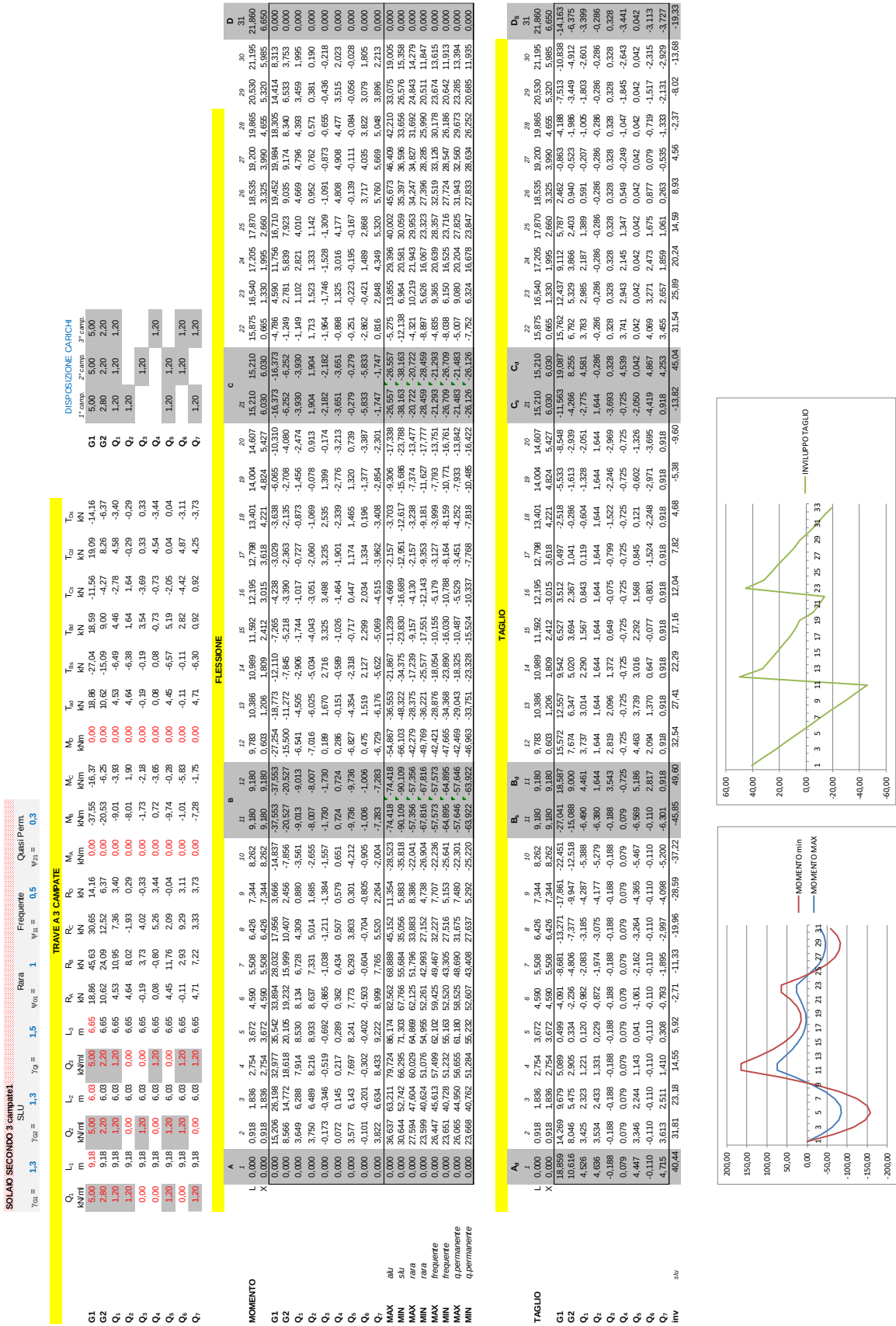
Verifica allo stato limite di apertura fessure

S _m (mm)	116,85	98,46	147,03	147,03	147,03	147,03	147,03	147,03	147,03	152,91	187,71
Combinazione frequente	Apertura limite=W3= 0,20 mm										
Sigma,S	158,23	58,71	31,66	106,93	159,57	189,56	196,93	181,65	143,74	165,65	0,10
Eps _{s,m}	0,063%	0,011%	0,006%	0,021%	0,031%	0,040%	0,045%	0,035%	0,028%	0,032%	0,000%
W _k (mm)	0,125	0,019	0,015	0,052	0,077	0,099	0,113	0,088	0,070	0,084	0,000
Combinazione quasi permanente	Apertura limite=W2= 0,20 mm										
Sigma,S	155,53	57,52	31,11	105,26	157,12	186,68	193,95	178,91	141,57	163,16	0,10
Eps _{s,m}	0,061%	0,011%	0,006%	0,020%	0,031%	0,037%	0,043%	0,035%	0,027%	0,032%	0,000%
W _k (mm)	0,122	0,019	0,015	0,051	0,076	0,093	0,107	0,087	0,069	0,082	0,000

Verifica allo stato limite di deformazione**Verifica esatta: combinazione quasi permanente**

Eps _{Cm}	-0,020%	-0,009%	-0,002%	-0,008%	-0,012%	-0,014%	-0,015%	-0,014%	-0,011%	-0,008%	0,000%
Eps _{Sm}	0,073%	0,022%	0,003%	0,048%	0,074%	0,089%	0,092%	0,085%	0,066%	0,077%	0,000%
f _{reccia}	0,000	0,533	1,163	1,769	2,241	2,495	2,487	2,205	1,673	0,918	0,000
f _{reccia massima:}	Rapporto di snellezza effettivo l/h =										
verifica sommaria:	pari a L/25,50 < 26,00 Rapporto limite										

Solai Secondo 15-14-7 e 15-14-13 ($G=5.0+1.0$ kN/mq ; $Q=2.0$ kN/mq)

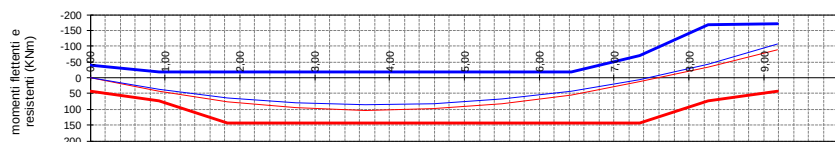


SECONDO SOLAIO - 3 campate1**prima campata**

Rck	Ec	fcd	fctd	Acciaio	fyd	Bsup	Binf	Sp_ala	h	c	d
MPa	(MPa)	MPa		tipo	MPa	cm			cm	cm	cm
30	31220	14,11	1,14	Feb44k	391	120	40	6	36	4	32

Luce di calcolo (m) **9,18****Verifica agli stati limite ultimi**

Involuppo Momento max		Coeff. di redistribuzione delta= 1,00									
	0,00	43,96	75,85	95,67	103,41	99,07	82,67	54,18	13,63	-34,23	-89,30
Involuppo Momento min		Coeff. di redistribuzione delta= 1,00									
	0,00	36,77	63,29	79,55	85,56	81,32	66,82	42,07	7,06	-42,98	-108,13
As,sup.app	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	3,82	9,60
As,inf.app	0,00	3,90	6,74	8,50	9,38	8,80	7,34	4,81	1,21	0,00	0,00
X	0,00	0,92	1,84	2,75	3,67	4,59	5,51	6,43	7,34	8,26	9,18
Armatura (cmq)											
φ6											
φ12	3	5	5	5	5	5	5	5			
φ16									3	3	3
φ20									3	3	3
As,sup	3,39	1,41	1,41	1,41	1,41	1,41	1,41	1,41	6,03	15,46	15,46
As,inf	3,39	6,03	12,32	12,32	12,32	12,32	12,32	12,32	12,32	6,03	3,39
φ12	3										3
φ16		3	3	3	3	3	3	3	3	3	
φ20			2	2	2	2	2	2	2	2	
φ5		0	0	0	0	0	0	0	0	0	0
Momenti positivi											
b	120,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00
psi	0,09	0,11	0,16	0,16	0,16	0,16	0,16	0,16	0,15	0,12	0,10
M+res	42,04	72,73	144,79	144,79	144,79	144,79	144,79	144,79	144,54	73,31	43,30
Momenti negativi											
b	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	60,00
psi	0,14	0,11	0,11	0,11	0,11	0,11	0,11	0,11	0,15	0,30	0,26
M-res	-40,10	-17,69	-17,86	-17,86	-17,86	-17,86	-17,86	-17,86	-69,29	-169,41	-172,02



VERIFICA ALLO S.L.U. DI TAGLIO											
Vsd	48,53	38,17	27,82	17,46	7,11	-3,25	-13,60	-23,96	-34,31	-44,67	-55,02
ρ ₁	0,0027	0,0047	0,0096	0,0096	0,0096	0,0096	0,0096	0,0096	0,0096	0,0047	0,0027
Bmin	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00

VERIFICA AGLI S.L. DI ESERCIZIO**Caratteristiche geometriche sezioni**

Per gruppo di esigenze cond. ambientali poco aggressive e armatura poco sensibile:

Beta,1 1,00		K2 0,40		Diam.min. 12		copr.netto 3,40					
Beta,2 0,50		K3 0,13		Sig.SR 101,38		n 15					
As (cmq)	3,39	6,03	12,32	12,32	12,32	12,32	12,32	12,32	12,32	15,46	15,46
A's (cmq)	3,39	1,41	1,41	1,41	1,41	1,41	1,41	1,41	6,03	6,03	3,39
b resistente	40,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	40,00	60,00
Y	7,36	6,18	8,43	8,43	8,43	8,43	8,43	8,43	8,19	13,25	11,91
Wc	4999	11308	15071	15071	15071	15071	15071	15071	15672	9078	10961
Ws	1493	2705	5388	5388	5388	5388	5388	5388	5387	6414	6498
N. barre	3	3	5	5	5	5	5	5	5	6	6
dist. barre	16,00	16,80	16,80	16,80	16,80	16,80	16,80	16,80	16,80	6,40	10,40
Beff (cm)	40	42	75	75	75	75	75	75	75	40	60
Deff (cm)	12,40	12,40	12,40	12,40	12,40	12,40	12,40	12,40	12,40	11,38	12,05
Aeff	496,00	515,84	932,48	932,48	932,48	932,48	932,48	932,48	932,48	455,02	722,70
RO,r	0,68%	1,17%	1,32%	1,32%	1,32%	1,32%	1,32%	1,32%	1,32%	3,40%	2,14%

Combinazioni di carico

Rara	0,00	33,11	57,12	72,03	77,84	74,55	62,16	40,66	10,06	-32,29	-81,38
Frequente	0,00	31,74	54,74	69,00	74,52	71,31	59,36	38,67	9,25	-30,77	-77,87
Quasi perm.	0,00	31,28	53,94	67,99	73,42	70,23	58,43	38,01	8,98	-30,26	-76,71

Verifica allo stato limite di tensione in esercizio

Combinazione rara		Sigma,C,amm = 0.60*fck = 14,94 MPa				Sigma,S,amm = 0.80*fyk = 360 MPa					
Sigma,C	-0,01	-2,93	-3,79	-4,78	-5,17	-4,95	-4,12	-2,70	-0,64	-3,56	-7,42
Sigma,S	0,01	183,59	159,04	200,56	216,73	207,56	173,05	113,20	28,02	75,51	187,85
Combinazione quasi permanente		Sigma,C,amm = 0.45*fck = 11,21 MPa									
Sigma,C	-0,01	-2,77	-3,58	-4,51	-4,87	-4,66	-3,88	-2,52	-0,57	-3,33	-7,00

Verifica allo stato limite di apertura fessure

S _{rm} (mm)	187,71	152,91	147,03	147,03	147,03	147,03	147,03	147,03	147,03	98,46	116,85
Combinazione frequente		Apertura limite=W3= 0,20 mm									
Sigma,S	0,10	175,96	152,40	192,10	207,48	198,54	165,27	107,67	25,75	71,96	179,76
Eps,sm	0,000%	0,034%	0,041%	0,067%	0,077%	0,071%	0,050%	0,021%	0,005%	0,026%	0,081%
Wk (mm)	0,000	0,089	0,103	0,168	0,192	0,178	0,125	0,052	0,012	0,043	0,161
Combinazione quasi permanente		Apertura limite=W2= 0,20 mm									
Sigma,S	0,10	173,41	150,18	189,29	204,40	195,53	162,67	105,83	24,99	70,78	177,06
Eps,sm	0,000%	0,034%	0,040%	0,066%	0,075%	0,070%	0,048%	0,021%	0,005%	0,025%	0,080%
Wk (mm)	0,000	0,088	0,100	0,164	0,187	0,174	0,121	0,051	0,012	0,042	0,158

Verifica allo stato limite di deformazione**Verifica esatta: combinazione quasi permanente**

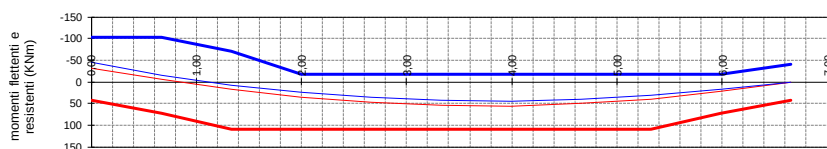
EpsCm	0,000%	-0,009%	-0,011%	-0,014%	-0,016%	-0,015%	-0,012%	-0,008%	-0,002%	-0,011%	-0,022%
EpsSm	0,000%	0,083%	0,072%	0,091%	0,098%	0,094%	0,078%	0,050%	0,005%	0,032%	0,085%
frecchia	0,000	0,977	1,777	2,339	2,631	2,633	2,357	1,852	1,207	0,543	0,000
frecchia massima:		2,63 cm			pari a L/	349					
verifica sommaria:		Rapporto di snellezza effettivo l/h =				25,50	<	26,00	Rapporto limite		

SECONDO SOLAIO - 3 campate1**terza campata**

Luce di calcolo (m)

6,65**Verifica agli stati limite ultimi**

Inviluppo Momento max	-31,87	-6,33	16,63	35,28	48,00	54,81	55,69	50,65	39,69	22,81	0,00
				Coeff. di redistribuzione delta= 1,00				psi-max			
Inviluppo Momento min	-45,80	-14,57	8,36	24,70	36,07	42,48	43,92	40,39	31,89	18,43	0,00
				Coeff. di redistribuzione delta= 1,00				psi-max			
As,sup.app	4,07	129	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00
As,inf.app	0,00	0,00	148	3,13	4,26	4,87	4,95	4,50	3,52	2,03	0,00
X	0,00	0,67	1,33	2,00	2,66	3,33	3,99	4,66	5,32	5,99	6,65
Armatura (cmq)											
φ 6	0			5	5	5	5	5	5	5	
φ 12	0										3
φ 16	3	3	3								
φ 20	1	1									
As,sup	9,17	9,17	6,03	1,41	1,41	1,41	1,41	1,41	1,41	1,41	3,39
As,inf	3,39	6,03	9,17	9,17	9,17	9,17	9,17	9,17	9,17	6,03	3,39
φ 12	3										3
φ 16	0	3	3	3	3	3	3	3	3	3	
φ 20	0		1	1	1	1	1	1	1		
φ 5	0										
Momenti positivi											
b	120	120	120	120	120	120	120	120	120	120	120
psi	0,10	0,11	0,13	0,13	0,13	0,13	0,13	0,13	0,13	0,11	0,09
M+res	42,81	73,13	109,00	109,12	109,12	109,12	109,12	109,12	109,12	72,73	42,04
Momenti negativi											
b	40	40	40	40	40	40	40	40	40	40	40
psi	0,23	0,20	0,16	0,11	0,11	0,11	0,11	0,11	0,11	0,11	0,14
M-res	-103,36	-103,75	-69,37	-17,79	-17,79	-17,79	-17,79	-17,79	-17,79	-17,69	-40,10



VERIFICA ALLO S.L.U. DI TAGLIO											
	k = 1,79 V = 0,42 v _{bd} = 53,56										
V _{sd}	54,04	37,85	31,07	24,29	17,50	10,72	5,47	-2,85	-9,63	-16,41	-23,19
ρ ₁	0,0027	0,0047	0,0072	0,0072	0,0072	0,0072	0,0072	0,0072	0,0072	0,0047	0,0027
B _{min}	41,90	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00

VERIFICA AGLI S.L. DI ESERCIZIO**Caratteristiche geometriche sezioni**

Per gruppo di esigenze cond. ambientali poco aggressive e armatura poco sensibile:

Beta,1 **1,00** K2 **0,40** Diam.min. **12** copr.netto 3,40
 Beta,2 **1,00** K3 **0,13** Sig.SR 101,38 n **15**

As (cmq)	9,17	9,17	9,17	9,17	9,17	9,17	9,17	9,17	9,17	6,03	3,39
A's (cmq)	3,39	6,03	6,03	1,41	1,41	1,41	1,41	1,41	1,41	1,41	3,39
b resistente	60,00	40,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	40,00
Y	9,64	10,75	7,21	7,43	7,43	7,43	7,43	7,43	7,43	6,18	7,36
W _c	9161	7702	13934	13429	13429	13429	13429	13429	13429	11308	4999
W _s	3951	3898	4054	4058	4058	4058	4058	4058	4058	2705	1493
N. barre	4	4	4	4	4	4	4	4	4	3	3
dist. barre	16,80	10,67	16,80	16,80	16,80	16,80	16,80	16,80	16,80	16,80	16,00
Beff (cm)	58	40	58	58	58	58	58	58	58	42	40
Deff (cm)	12,40	12,40	12,40	12,40	12,40	12,40	12,40	12,40	12,40	12,40	12,40
A _{eff}	724,16	496,00	724,16	724,16	724,16	724,16	724,16	724,16	724,16	515,84	496,00
RO _r	1,27%	1,85%	1,27%	1,27%	1,27%	1,27%	1,27%	1,27%	1,27%	1,17%	0,68%

Combinazioni di carico

Rara	-34,15	-10,68	12,26	26,33	35,94	41,10	41,79	38,03	29,81	17,13	0,00
Frequente	-32,05	-9,65	11,24	24,77	34,03	39,02	39,75	36,21	28,41	16,34	0,00
Quasi perm.	-31,35	-9,30	10,90	24,24	33,39	38,33	39,07	35,61	27,94	16,07	0,00

Verifica allo stato limite di tensione in esercizio

Combinazione rara	Sigma,C,amm = 0.60*f _{ck} = 14,94 MPa Sigma,S,amm = 0.80*f _{yk} = 360 MPa										
Sigma,C	-3,73	-1,39	-0,88	-1,96	-2,68	-3,06	-3,11	-2,83	-2,22	-1,52	-0,01
Sigma,S	129,66	41,08	45,38	97,33	132,86	151,91	154,48	140,57	110,19	95,00	0,01
Combinazione quasi permanente	Sigma,C,amm = 0.45*f _{ck} = 11,21 MPa										
Sigma,C	-3,42	-1,21	-0,78	-1,81	-2,49	-2,85	-2,91	-2,65	-2,08	-1,42	-0,01

Verifica allo stato limite di apertura fessure

S _{rm} (mm)	148,96	121,77	148,96	148,96	148,96	148,96	148,96	148,96	148,96	152,91	187,71
Combinazione frequente	Apertura limite=W3= 0,20 mm										
Sigma,S	121,68	37,12	41,58	91,54	125,78	144,24	146,93	133,86	105,01	90,58	0,10
Eps _{sm}	0,024%	0,007%	0,008%	0,018%	0,024%	0,028%	0,029%	0,026%	0,020%	0,018%	0,000%
W _k (mm)	0,060	0,015	0,020	0,045	0,062	0,071	0,072	0,066	0,052	0,046	0,000
Combinazione quasi permanente	Apertura limite=W2= 0,20 mm										
Sigma,S	119,03	35,80	40,32	89,61	123,42	141,69	144,42	131,62	103,28	89,11	0,10
Eps _{sm}	0,023%	0,007%	0,008%	0,017%	0,024%	0,028%	0,028%	0,026%	0,020%	0,017%	0,000%
W _k (mm)	0,059	0,014	0,020	0,044	0,061	0,070	0,071	0,065	0,051	0,045	0,000

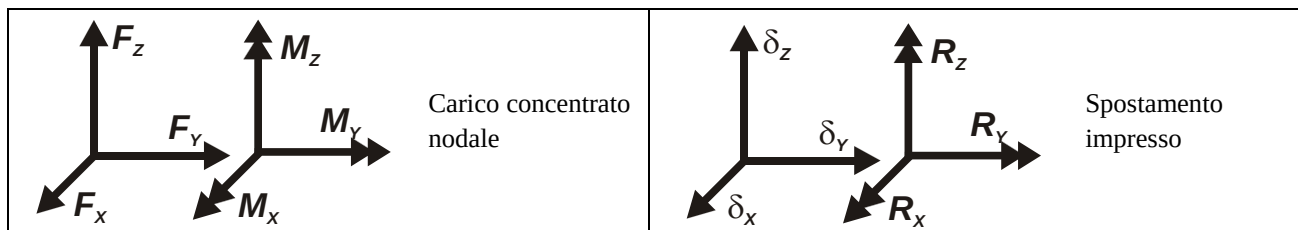
Verifica allo stato limite di deformazione**Verifica esatta: combinazione quasi permanente**

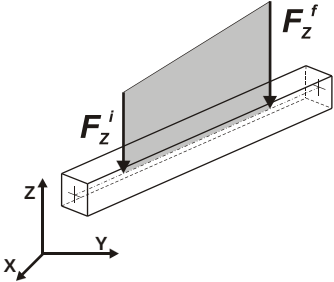
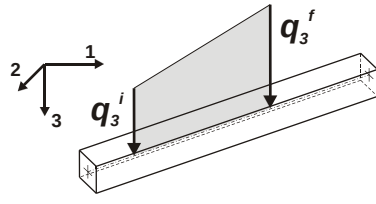
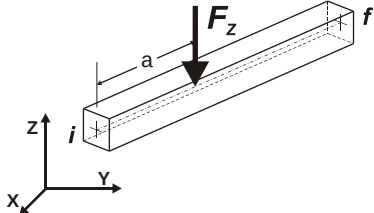
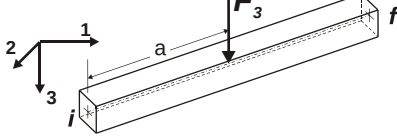
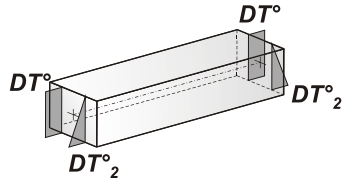
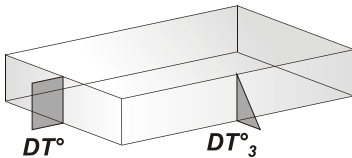
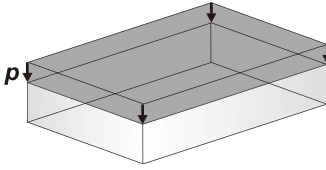
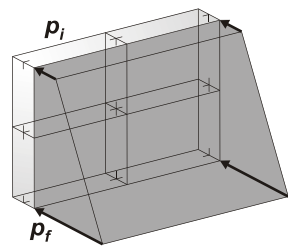
Eps _{Cm}	-0,011%	-0,004%	-0,003%	-0,006%	-0,008%	-0,009%	-0,009%	-0,008%	-0,007%	-0,005%	0,000%
Eps _{Sm}	0,055%	0,007%	0,011%	0,039%	0,057%	0,066%	0,068%	0,061%	0,047%	0,039%	0,000%
frecchia	0,000	0,226	0,478	0,709	0,881	0,967	0,952	0,834	0,623	0,336	0,000
frecchia massima:	0,97 cm pari a L/ 687										
verifica sommaria:	Rapporto di snellezza effettivo l/h = 18,47 < 26,00 Rapporto limite										

MODELLAZIONE DELLE AZIONI

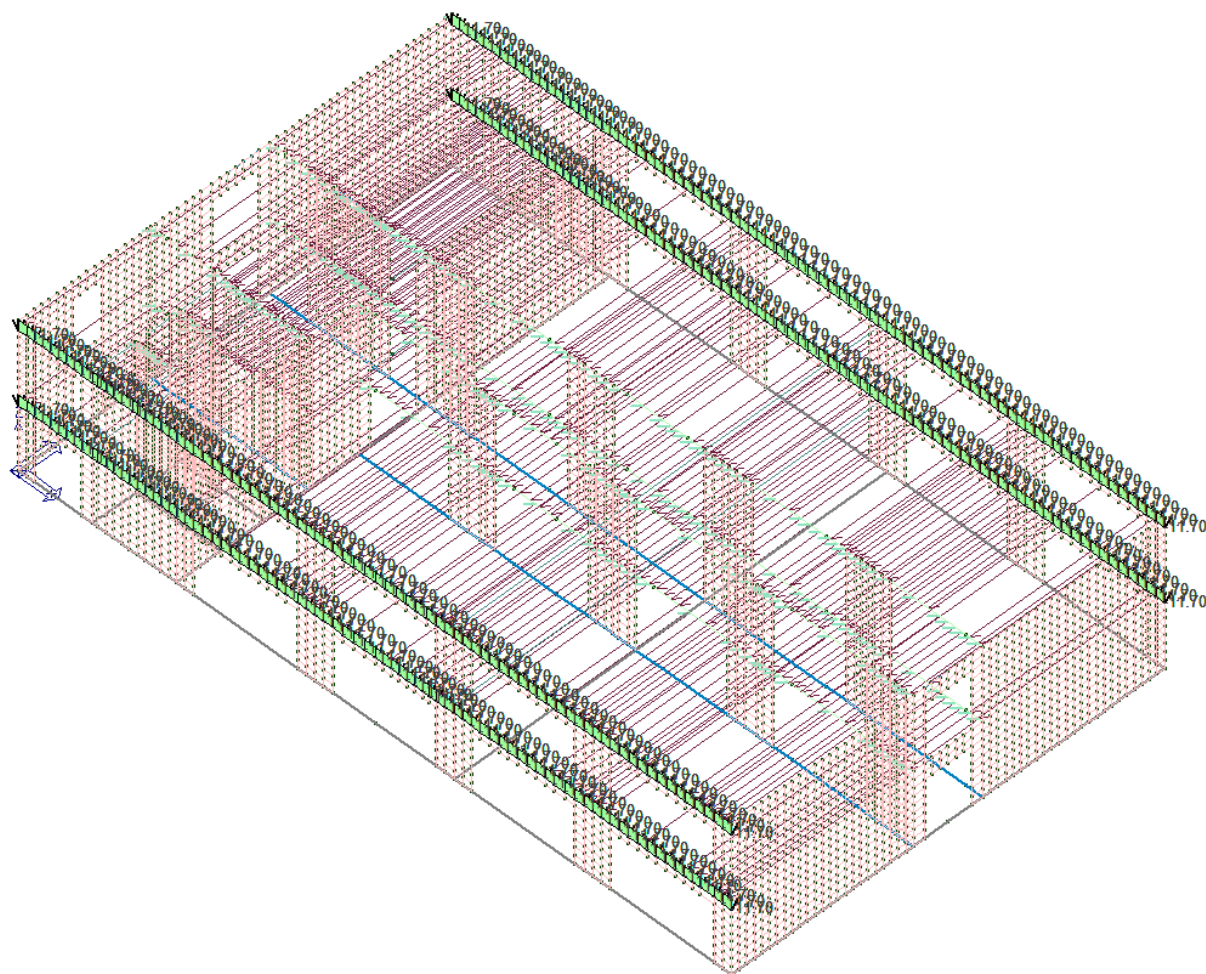
Il programma consente l'uso di diverse tipologie di carico (azioni). Le azioni utilizzate nella modellazione sono individuate da una sigla identificativa ed un codice numerico (gli elementi strutturali richiamano quest'ultimo nella propria descrizione). Per ogni azione applicata alla struttura viene di riportato il codice, il tipo e la sigla identificativa. Le tabelle successive dettagliano i valori caratteristici di ogni azione in relazione al tipo. Le tabelle riportano infatti i seguenti dati in relazione al tipo:

1	carico concentrato nodale 6 dati (forza F_x , F_y , F_z , momento M_x , M_y , M_z)
2	spostamento nodale impresso 6 dati (spostamento T_x , T_y , T_z , rotazione R_x , R_y , R_z)
3	carico distribuito globale su elemento tipo trave 7 dati (f_x , f_y , f_z , m_x , m_y , m_z , ascissa di inizio carico) 7 dati (f_x , f_y , f_z , m_x , m_y , m_z , ascissa di fine carico)
4	carico distribuito locale su elemento tipo trave 7 dati (f_1 , f_2 , f_3 , m_1 , m_2 , m_3 , ascissa di inizio carico) 7 dati (f_1 , f_2 , f_3 , m_1 , m_2 , m_3 , ascissa di fine carico)
5	carico concentrato globale su elemento tipo trave 7 dati (F_x , F_y , F_z , M_x , M_y , M_z , ascissa di carico)
6	carico concentrato locale su elemento tipo trave 7 dati (F_1 , F_2 , F_3 , M_1 , M_2 , M_3 , ascissa di carico)
7	variazione termica applicata ad elemento tipo trave 7 dati (variazioni termiche: uniforme, media e differenza in altezza e larghezza al nodo iniziale e finale)
8	carico di pressione uniforme su elemento tipo piastra 1 dato (pressione)
9	carico di pressione variabile su elemento tipo piastra 4 dati (pressione, quota, pressione, quota)
10	variazione termica applicata ad elemento tipo piastra 2 dati (variazioni termiche: media e differenza nello spessore)
11	carico variabile generale su elementi tipo trave e piastra 1 dato descrizione della tipologia 4 dati per segmento (posizione, valore, posizione, valore) la tipologia precisa l'ascissa di definizione, la direzione del carico, la modalità di carico e la larghezza d'influenza per gli elementi tipo trave
12	gruppo di carichi con impronta su piastra 9 dati (numero di ripetizioni in direzione X e Y, valore di ciascun carico, posizione centrale del primo, dimensioni dell'impronta, interasse tra i carichi)

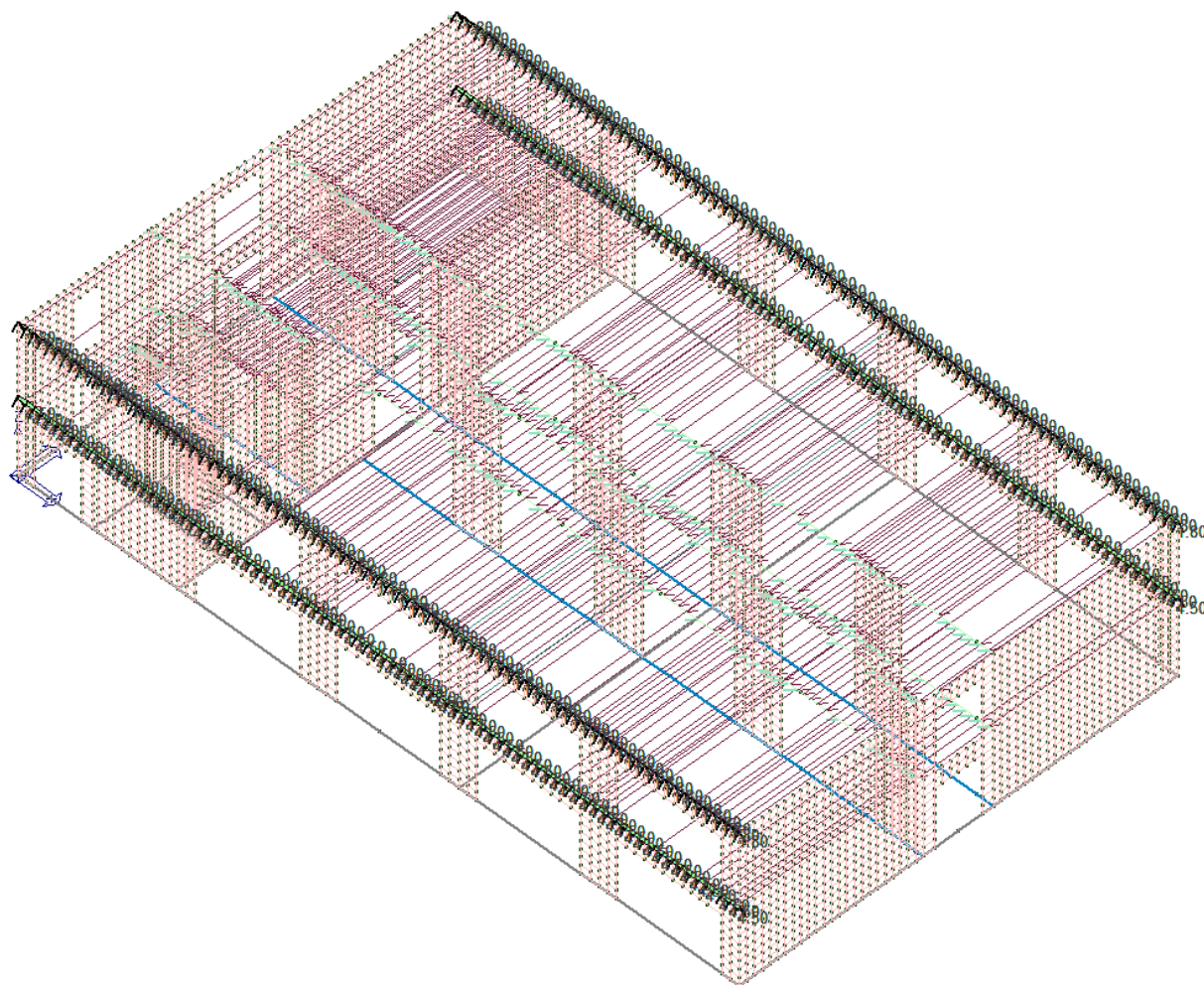


 Carico distribuito globale	 Carico distribuito locale
 Carico concentrato globale	 Carico concentrato locale
 Carico termico 2D	 Carico termico 3D
 Carico pressione uniforme	 Carico pressione variabile

carico distribuito globale su trave								
Id	Tipo	Pos.	fx	fy	fz	mx	my	mz
		cm	daN/cm	daN/cm	daN/cm	daN	daN	daN
1	DG:Fzi=-11.70 Fzf=-11.70	0.0	0.0	0.0	-11.70	0.0	0.0	0.0
		0.0	0.0	0.0	-11.70	0.0	0.0	0.0
2	DG:Fzi=4.50 Fzf=4.50	0.0	0.0	0.0	4.50	0.0	0.0	0.0
		0.0	0.0	0.0	4.50	0.0	0.0	0.0
3	DG:Fzi=1.80 Fzf=1.80	0.0	0.0	0.0	1.80	0.0	0.0	0.0
		0.0	0.0	0.0	1.80	0.0	0.0	0.0



Permanente sbalzo solai
 $G = 11.70 \text{ kN/m}$



Accidentale sbalzo solai
 $Q = 4.50 \text{ kN/m di piano}$
 $Q = 1.80 \text{ kN/m di copertura}$

SCHEMATIZZAZIONE DEI CASI DI CARICO

Il programma consente l'applicazione di diverse tipologie di casi di carico.

Sono previsti i seguenti 11 tipi di casi di carico:

	Sigla	Tipo	Descrizione
1	Ggk	A	caso di carico comprensivo del peso proprio struttura
2	Gk	NA	caso di carico con azioni permanenti
3	Qk	NA	caso di carico con azioni variabili
4	Gsk	A	caso di carico comprensivo dei carichi permanenti sui solai e sulle coperture
5	Qsk	A	caso di carico comprensivo dei carichi variabili sui solai
6	Qnk	A	caso di carico comprensivo dei carichi di neve sulle coperture
7	Qtk	SA	caso di carico comprensivo di una variazione termica agente sulla struttura
8	Qvk	NA	caso di carico comprensivo di azioni da vento sulla struttura
9	Esk	SA	caso di carico sismico con analisi statica equivalente
10	Edk	SA	caso di carico sismico con analisi dinamica
11	Etk	NA	caso di carico comprensivo di azioni derivanti dall' incremento di spinta delle terre in condizione sismica
12	Pk	NA	caso di carico comprensivo di azioni derivanti da coazioni, cedimenti e precompressioni

Sono di tipo automatico A (ossia non prevedono introduzione dati da parte dell'utente) i seguenti casi di carico: 1-Ggk; 4-Gsk; 5-Qsk; 6-Qnk.

Sono di tipo semi-automatico SA (ossia prevedono una minima introduzione dati da parte dell'utente) i seguenti casi di carico:

7-Qtk, in quanto richiede solo il valore della variazione termica;

9-Esk e 10-Edk, in quanto richiedono il valore dell'angolo di ingresso del sisma e l'individuazione dei casi di carico partecipanti alla definizione delle masse.

Sono di tipo non automatico NA ossia prevedono la diretta applicazione di carichi generici agli elementi strutturali (si veda il precedente punto Modellazione delle Azioni) i restanti casi di carico.

Nella tabella successiva vengono riportati i casi di carico agenti sulla struttura, con l'indicazione dei dati relativi al caso di carico stesso:

Numero Tipo e Sigla identificativa, Valore di riferimento del caso di carico (se previsto).

In successione, per i casi di carico non automatici, viene riportato l'elenco di nodi ed elementi direttamente caricati con la sigla identificativa del carico.

Per i casi di carico di tipo sismico (9-Esk e 10-Edk), viene riportata la tabella di definizione delle masse: per ogni caso di carico partecipante alla definizione delle masse viene indicata la relativa aliquota (partecipazione) considerata. Si precisa che per i caso di carico 5-Qsk e 6-Qnk la partecipazione è prevista localmente per ogni elemento solaio o copertura presente nel modello (si confronti il valore Sksol nel capitolo relativo agli elementi solaio) e pertanto la loro partecipazione è di norma pari a uno.

CDC	Tipo	Sigla Id	Note
1	Ggk	CDC=Ggk (peso proprio della struttura)	
2	Gsk	CDC=G1sk (permanente solai-coperture)	
3	Gsk	CDC=G2sk (permanente solai-coperture n.c.d.)	
4	Qsk	CDC=Qsk (variabile solai)	
5	Edk	CDC=Ed (dinamico SLU) alfa=0.0 (ecc. +)	partecipazione:1.00 per 1 CDC=Ggk (peso proprio della struttura)
			partecipazione:1.00 per 2 CDC=G1sk (permanente solai-coperture)
			partecipazione:1.00 per 3 CDC=G2sk (permanente solai-coperture n.c.d.)
			partecipazione:1.00 per 4 CDC=Qsk (variabile solai)
			partecipazione:1.00 per 13 CDC=G1k (permanente generico)
			partecipazione:0.80 per 14 CDC=Qk (variabile generico)
6	Edk	CDC=Ed (dinamico SLU) alfa=0.0 (ecc. -)	come precedente CDC sismico
7	Edk	CDC=Ed (dinamico SLU) alfa=90.00 (ecc. +)	come precedente CDC sismico
8	Edk	CDC=Ed (dinamico SLU) alfa=90.00 (ecc. -)	come precedente CDC sismico
9	Edk	CDC=Ed (dinamico SLD) alfa=0.0 (ecc. +)	come precedente CDC sismico
10	Edk	CDC=Ed (dinamico SLD) alfa=0.0 (ecc. -)	come precedente CDC sismico
11	Edk	CDC=Ed (dinamico SLD) alfa=90.00 (ecc. +)	come precedente CDC sismico
12	Edk	CDC=Ed (dinamico SLD) alfa=90.00 (ecc. -)	come precedente CDC sismico

CDC	Tipo	Sigla Id	Note
13	Gk	CDC=G1k (permanente generico)	D2 : 466 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 : 477 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 : 698 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 : 700 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 : 714 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 : 716 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 : 728 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 : 730 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 : 738 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 : 740 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 : 755 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 : 770 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 : 772 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 : 782 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 : 790 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 : 792 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 :da 810 a 811 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 : 814 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 :da 820 a 821 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 :da 824 a 825 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 :da 835 a 836 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 : 839 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 :da 845 a 846 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 :da 849 a 850 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 :da 854 a 855 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 :da 862 a 863 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 : 866 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 :da 871 a 872 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 :da 875 a 876 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 :da 878 a 879 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 :da 886 a 887 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 :da 893 a 894 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 :da 897 a 898 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 :da 900 a 901 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 :da 908 a 909 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 :da 914 a 915 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 :da 917 a 918 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 :da 920 a 921 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 :da 926 a 927 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 :da 932 a 935 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 :da 939 a 940 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 :da 945 a 948 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 :da 952 a 953 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 :da 957 a 960 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 :da 967 a 1055 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 :da 1067 a 1144 Azione : DG:Fzi=-11.70 Fzf=-11.70
			D2 :da 1153 a 1228 Azione : DG:Fzi=-11.70 Fzf=-11.70
14	Qk	CDC=Qk (variabile generico)	D2 : 466 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 : 477 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 : 698 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 : 700 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 : 714 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 : 716 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 : 728 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 : 730 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 : 738 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 : 740 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 : 755 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 : 770 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 : 772 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 : 782 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 : 790 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 : 792 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 :da 810 a 811 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 : 814 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 :da 820 a 821 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 :da 824 a 825 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 :da 835 a 836 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 : 839 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 :da 845 a 846 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 :da 849 a 850 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 :da 854 a 855 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 :da 862 a 863 Azione : DG:Fzi=1.80 Fzf=1.80

CDC	Tipo	Sigla Id	Note
			D2 : 866 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 :da 871 a 872 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 :da 875 a 876 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 :da 878 a 879 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 :da 886 a 887 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 :da 893 a 894 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 :da 897 a 898 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 :da 900 a 901 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 :da 908 a 909 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 :da 914 a 915 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 :da 917 a 918 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 :da 920 a 921 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 :da 926 a 927 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 :da 932 a 935 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 :da 939 a 940 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 :da 945 a 948 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 :da 952 a 953 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 :da 957 a 960 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 :da 967 a 968 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 :da 969 a 1055 Azione : DG:Fzi=4.50 Fzf=4.50
			D2 :da 1067 a 1071 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 :da 1072 a 1106 Azione : DG:Fzi=4.50 Fzf=4.50
			D2 :da 1107 a 1144 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 :da 1153 a 1182 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 :da 1183 a 1212 Azione : DG:Fzi=4.50 Fzf=4.50
			D2 :da 1213 a 1217 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 :da 1218 a 1222 Azione : DG:Fzi=4.50 Fzf=4.50
			D2 :da 1223 a 1225 Azione : DG:Fzi=1.80 Fzf=1.80
			D2 :da 1226 a 1228 Azione : DG:Fzi=4.50 Fzf=4.50

DEFINIZIONE DELLE COMBINAZIONI

Il programma combina i diversi tipi di casi di carico (CDC) secondo le regole previste dalla normativa vigente.

Le combinazioni previste sono destinate al controllo di sicurezza della struttura ed alla verifica degli spostamenti e delle sollecitazioni.

La prima tabella delle combinazioni riportata di seguito comprende le seguenti informazioni: Numero, Tipo, Sigla identificativa. Una seconda tabella riporta il peso nella combinazione assunto per ogni caso di carico.

Ai fini delle verifiche degli stati limite si definiscono le seguenti combinazioni delle azioni:

Combinazione fondamentale SLU

$$\gamma G_1 \cdot G_1 + \gamma G_2 \cdot G_2 + \gamma P \cdot P + \gamma Q_1 \cdot Q_{k1} + \gamma Q_2 \cdot \psi_{02} \cdot Q_{k2} + \gamma Q_3 \cdot \psi_{03} \cdot Q_{k3} + \dots$$

Combinazione caratteristica (rara) SLE

$$G_1 + G_2 + P + Q_{k1} + \psi_{02} \cdot Q_{k2} + \psi_{03} \cdot Q_{k3} + \dots$$

Combinazione frequente SLE

$$G_1 + G_2 + P + \psi_{11} \cdot Q_{k1} + \psi_{22} \cdot Q_{k2} + \psi_{23} \cdot Q_{k3} + \dots$$

Combinazione quasi permanente SLE

$$G_1 + G_2 + P + \psi_{21} \cdot Q_{k1} + \psi_{22} \cdot Q_{k2} + \psi_{23} \cdot Q_{k3} + \dots$$

Combinazione sismica, impiegata per gli stati limite ultimi e di esercizio connessi all'azione sismica E

$$E + G_1 + G_2 + P + \psi_{21} \cdot Q_{k1} + \psi_{22} \cdot Q_{k2} + \dots$$

Combinazione eccezionale, impiegata per gli stati limite connessi alle azioni eccezionali

$$G_1 + G_2 + A_d + P + \psi_{21} \cdot Q_{k1} + \psi_{22} \cdot Q_{k2} + \dots$$

Dove:

NTC 2018 Tabella 2.5.I

Destinazione d'uso/azione	ψ_0	ψ_1	ψ_2
Categoria A residenziali	0,70	0,50	0,30

Categoria B uffici	0,70	0,50	0,30
Categoria C ambienti suscettibili di affollamento	0,70	0,70	0,60
Categoria D ambienti ad uso commerciale	0,70	0,70	0,60
Categoria E biblioteche, archivi, magazzini, ...	1,00	0,90	0,80
Categoria F Rimesse e parcheggi (autoveicoli $\leq 30\text{kN}$)	0,70	0,70	0,60
Categoria G Rimesse e parcheggi (autoveicoli $> 30\text{kN}$)	0,70	0,50	0,30
Categoria H Coperture	0,00	0,00	0,00
Vento	0,60	0,20	0,00
Neve a quota $\leq 1000\text{ m}$	0,50	0,20	0,00
Neve a quota $> 1000\text{ m}$	0,70	0,50	0,20
Variazioni Termiche	0,60	0,50	0,00

Nelle verifiche possono essere adottati in alternativa due diversi approcci progettuali:

- per l'approccio 1 si considerano due diverse combinazioni di gruppi di coefficienti di sicurezza parziali per le azioni, per i materiali e per la resistenza globale (combinazione 1 con coefficienti A1 e combinazione 2 con coefficienti A2),
- per l'approccio 2 si definisce un'unica combinazione per le azioni, per la resistenza dei materiali e per la resistenza globale (con coefficienti A1).

NTC 2018 Tabella 2.6.I

		Coefficiente γ	EQU	A1	A2
Carichi permanenti	Favorevoli	γ_{G1}	0,9	1,0	1,0
	Sfavorevoli		1,1	1,3	1,0
Carichi permanenti non strutturali (Non compiutamente definiti)	Favorevoli	γ_{G2}	0,8	0,8	0,8
	Sfavorevoli		1,5	1,5	1,3
Carichi variabili	Favorevoli	γ_{Qi}	0,0	0,0	0,0
	Sfavorevoli		1,5	1,5	1,3

Cmb	Tipo	Sigla Id	effetto P-delta
1	SLU	Comb. SLU A1 1	
2	SLU	Comb. SLU A1 2	
3	SLU	Comb. SLU A1 3	
4	SLU	Comb. SLU A1 4	
5	SLU	Comb. SLU A1 5	
6	SLU	Comb. SLU A1 6	
7	SLU	Comb. SLU A1 7	
8	SLU	Comb. SLU A1 8	
9	SLU	Comb. SLU A1 9	
10	SLU	Comb. SLU A1 10	
11	SLU	Comb. SLU A1 11	
12	SLU	Comb. SLU A1 12	
13	SLU	Comb. SLU A1 (SLV sism.) 13	
14	SLU	Comb. SLU A1 (SLV sism.) 14	
15	SLU	Comb. SLU A1 (SLV sism.) 15	
16	SLU	Comb. SLU A1 (SLV sism.) 16	
17	SLU	Comb. SLU A1 (SLV sism.) 17	
18	SLU	Comb. SLU A1 (SLV sism.) 18	
19	SLU	Comb. SLU A1 (SLV sism.) 19	
20	SLU	Comb. SLU A1 (SLV sism.) 20	
21	SLU	Comb. SLU A1 (SLV sism.) 21	
22	SLU	Comb. SLU A1 (SLV sism.) 22	
23	SLU	Comb. SLU A1 (SLV sism.) 23	
24	SLU	Comb. SLU A1 (SLV sism.) 24	
25	SLU	Comb. SLU A1 (SLV sism.) 25	
26	SLU	Comb. SLU A1 (SLV sism.) 26	
27	SLU	Comb. SLU A1 (SLV sism.) 27	
28	SLU	Comb. SLU A1 (SLV sism.) 28	
29	SLU	Comb. SLU A1 (SLV sism.) 29	
30	SLU	Comb. SLU A1 (SLV sism.) 30	
31	SLU	Comb. SLU A1 (SLV sism.) 31	
32	SLU	Comb. SLU A1 (SLV sism.) 32	
33	SLU	Comb. SLU A1 (SLV sism.) 33	
34	SLU	Comb. SLU A1 (SLV sism.) 34	
35	SLU	Comb. SLU A1 (SLV sism.) 35	
36	SLU	Comb. SLU A1 (SLV sism.) 36	
37	SLU	Comb. SLU A1 (SLV sism.) 37	
38	SLU	Comb. SLU A1 (SLV sism.) 38	

Cmb	Tipo	Sigla Id	effetto P-delta
39	SLU	Comb. SLU A1 (SLV sism.) 39	
40	SLU	Comb. SLU A1 (SLV sism.) 40	
41	SLU	Comb. SLU A1 (SLV sism.) 41	
42	SLU	Comb. SLU A1 (SLV sism.) 42	
43	SLU	Comb. SLU A1 (SLV sism.) 43	
44	SLU	Comb. SLU A1 (SLV sism.) 44	
45	SLD(sis)	Comb. SLE (SLD Danno sism.) 45	
46	SLD(sis)	Comb. SLE (SLD Danno sism.) 46	
47	SLD(sis)	Comb. SLE (SLD Danno sism.) 47	
48	SLD(sis)	Comb. SLE (SLD Danno sism.) 48	
49	SLD(sis)	Comb. SLE (SLD Danno sism.) 49	
50	SLD(sis)	Comb. SLE (SLD Danno sism.) 50	
51	SLD(sis)	Comb. SLE (SLD Danno sism.) 51	
52	SLD(sis)	Comb. SLE (SLD Danno sism.) 52	
53	SLD(sis)	Comb. SLE (SLD Danno sism.) 53	
54	SLD(sis)	Comb. SLE (SLD Danno sism.) 54	
55	SLD(sis)	Comb. SLE (SLD Danno sism.) 55	
56	SLD(sis)	Comb. SLE (SLD Danno sism.) 56	
57	SLD(sis)	Comb. SLE (SLD Danno sism.) 57	
58	SLD(sis)	Comb. SLE (SLD Danno sism.) 58	
59	SLD(sis)	Comb. SLE (SLD Danno sism.) 59	
60	SLD(sis)	Comb. SLE (SLD Danno sism.) 60	
61	SLD(sis)	Comb. SLE (SLD Danno sism.) 61	
62	SLD(sis)	Comb. SLE (SLD Danno sism.) 62	
63	SLD(sis)	Comb. SLE (SLD Danno sism.) 63	
64	SLD(sis)	Comb. SLE (SLD Danno sism.) 64	
65	SLD(sis)	Comb. SLE (SLD Danno sism.) 65	
66	SLD(sis)	Comb. SLE (SLD Danno sism.) 66	
67	SLD(sis)	Comb. SLE (SLD Danno sism.) 67	
68	SLD(sis)	Comb. SLE (SLD Danno sism.) 68	
69	SLD(sis)	Comb. SLE (SLD Danno sism.) 69	
70	SLD(sis)	Comb. SLE (SLD Danno sism.) 70	
71	SLD(sis)	Comb. SLE (SLD Danno sism.) 71	
72	SLD(sis)	Comb. SLE (SLD Danno sism.) 72	
73	SLD(sis)	Comb. SLE (SLD Danno sism.) 73	
74	SLD(sis)	Comb. SLE (SLD Danno sism.) 74	
75	SLD(sis)	Comb. SLE (SLD Danno sism.) 75	
76	SLD(sis)	Comb. SLE (SLD Danno sism.) 76	
77	SLU(acc.)	Comb. SLU (Accid.) 77	
78	SLU(acc.)	Comb. SLU (Accid.) 78	
79	SLU(acc.)	Comb. SLU (Accid.) 79	
80	SLU(acc.)	Comb. SLU (Accid.) 80	
81	SLE(r)	Comb. SLE(rara) 81	
82	SLE(r)	Comb. SLE(rara) 82	
83	SLE(r)	Comb. SLE(rara) 83	
84	SLE(r)	Comb. SLE(rara) 84	
85	SLE(r)	Comb. SLE(rara) 85	
86	SLE(r)	Comb. SLE(rara) 86	
87	SLE(f)	Comb. SLE(freq.) 87	
88	SLE(f)	Comb. SLE(freq.) 88	
89	SLE(f)	Comb. SLE(freq.) 89	
90	SLE(f)	Comb. SLE(freq.) 90	
91	SLE(f)	Comb. SLE(freq.) 91	
92	SLE(f)	Comb. SLE(freq.) 92	
93	SLE(f)	Comb. SLE(freq.) 93	
94	SLE(p)	Comb. SLE(perm.) 94	
95	SLE(p)	Comb. SLE(perm.) 95	
96	SLE(p)	Comb. SLE(perm.) 96	
97	SLE(p)	Comb. SLE(perm.) 97	

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
1	1.30	1.30	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.30	0.0
2	1.30	1.30	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.30	1.50
3	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.30	0.0
4	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.30	1.50
5	1.00	1.00	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.00	0.0
6	1.00	1.00	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.00	1.50
7	1.00	1.00	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.00	0.0
8	1.00	1.00	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.00	1.50
9	1.30	1.30	1.50	1.05	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.30	0.0

[illegible]

AZIONE SISMICA

L'azione sismica sulle costruzioni è valutata a partire dalla “pericolosità sismica di base”, in condizioni ideali di sito di riferimento rigido con superficie topografica orizzontale.

Allo stato attuale, la pericolosità sismica su reticolo di riferimento nell'intervallo di riferimento è fornita dai dati pubblicati sul sito <http://esse1.mi.ingv.it/>. Per punti non coincidenti con il reticolo di riferimento e periodi di ritorno non contemplati direttamente si opera come indicato nell'allegato alle NTC (rispettivamente media pesata e interpolazione).

L'azione sismica viene definita in relazione ad un periodo di riferimento V_r che si ricava, per ciascun tipo di costruzione, moltiplicandone la vita nominale per il coefficiente d'uso (vedi tabella Parametri della struttura). Fissato il periodo di riferimento V_r e la probabilità di superamento P_{ver} associata a ciascuno degli stati limite considerati, si ottiene il periodo di ritorno T_r e i relativi parametri di pericolosità sismica (vedi tabella successiva):

ag: accelerazione orizzontale massima del terreno;

Fo: valore massimo del fattore di amplificazione dello spettro in accelerazione orizzontale;

T*c: periodo di inizio del tratto a velocità costante dello spettro in accelerazione orizzontale;

Parametri della struttura					
Classe d'uso	Vita Vn [anni]	Coeff. Uso	Periodo Vr [anni]	Tipo di suolo	Categoria topografica
III	100.0	1.5	150	B	T1

Individuati su reticolo di riferimento i parametri di pericolosità sismica si valutano i parametri spettrali riportati in tabella:

S è il coefficiente che tiene conto della categoria di sottosuolo e delle condizioni topografiche mediante la relazione seguente $S = S_s \cdot S_t$ (3.2.3)

Fo è il fattore che quantifica l'amplificazione spettrale massima, su sito di riferimento rigido orizzontale

Fv è il fattore che quantifica l'amplificazione spettrale massima verticale, in termini di accelerazione orizzontale massima del terreno ag su sito di riferimento rigido orizzontale

Tb è il periodo corrispondente all'inizio del tratto dello spettro ad accelerazione costante.

T_c è il periodo corrispondente all'inizio del tratto dello spettro a velocità costante.

Td è il periodo corrispondente all'inizio del tratto dello spettro a spostamento costante.

			Km		
Loc.	12.207	45.719			
11637	12.204	45.678	4.566		
11638	12.275	45.679	6.922		
11416	12.274	45.729	5.334		
11415	12.203	45.728	1.017		
SL	Pver	Tr	ag	Fo	T*c
		Anni	g		sec

SLO	81.0	90.0	0.079	2.440	0.280		
SLD	63.0	151.0	0.101	2.430	0.290		
SLV	10.0	1424.0	0.259	2.490	0.350		
SLC	5.0	2475.0	0.322	2.490	0.360		
SL	ag	S	Fo	Fv	Tb	Tc	Td
	g				sec	sec	sec
SLO	0.079	1.200	2.440	0.926	0.132	0.397	1.916
SLD	0.101	1.200	2.430	1.043	0.136	0.409	2.004
SLV	0.259	1.142	2.490	1.712	0.158	0.475	2.637
SLC	0.322	1.079	2.490	1.909	0.162	0.486	2.890

RISULTATI ANALISI SISMICHE

Il programma consente l'analisi di diverse configurazioni sismiche.

Sono previsti, infatti, i seguenti casi di carico:

9. Esk caso di carico sismico con analisi statica equivalente

10. Edk caso di carico sismico con analisi dinamica

Ciascun caso di carico è caratterizzato da un angolo di ingresso e da una configurazione di masse determinante la forza sismica complessiva (si rimanda al capitolo relativo ai casi di carico per chiarimenti inerenti questo aspetto).

Nella colonna Note, in funzione della norma in uso sono riportati i parametri fondamentali che caratterizzano l'azione sismica: in particolare possono essere presenti i seguenti valori:

Angolo di ingresso	Angolo di ingresso dell'azione sismica orizzontale
Fattore di importanza	Fattore di importanza dell'edificio, in base alla categoria di appartenenza
Zona sismica	Zona sismica
Accelerazione ag	Accelerazione orizzontale massima sul suolo
Categoria suolo	Categoria di profilo stratigrafico del suolo di fondazione
Fattore q	Fattore di struttura/di comportamento. Dipendente dalla tipologia strutturale
Fattore di sito S	Fattore dipendente dalla stratigrafia e dal profilo topografico
Classe di duttilità CD	Classe di duttilità della struttura – “A” duttilità alta, “B” duttilità bassa
Fattore riduz. SLD	Fattore di riduzione dello spettro elastico per lo stato limite di danno
Periodo proprio T1	Periodo proprio di vibrazione della struttura
Coefficiente Lambda	Coefficiente dipendente dal periodo proprio T1 e dal numero di piani della struttura
Ordinata spettro Sd(T1)	Valore delle ordinate dello spettro di progetto per lo stato limite ultimo, componente orizzontale (verticale Svd)
Ordinata spettro Se(T1)	Valore delle ordinate dello spettro elastico ridotta del fattore SLD per lo stato limite di danno, componente orizzontale (verticale Sve)
Ordinata spettro S (Tb-Tc)	Valore dell' ordinata dello spettro in uso nel tratto costante
numero di modi considerati	Numero di modi di vibrare della struttura considerati nell'analisi dinamica

Per ciascun caso di carico sismico viene riportato l'insieme di dati sotto riportati (le masse sono espresse in unità di forza):

a) **analisi sismica statica equivalente:**

- quota, posizione del centro di applicazione e azione orizzontale risultante, posizione del baricentro delle rigidezze, rapporto r/L_s (per strutture a nucleo), indici di regolarità e/r secondo EC8 4.2.3.2
- azione sismica complessiva

b) **analisi sismica dinamica con spettro di risposta:**

- quota, posizione del centro di massa e massa risultante, posizione del baricentro delle rigidezze, rapporto r/L_s (per strutture a nucleo) , indici di regolarità e/r secondo EC8 4.2.3.2
- frequenza, periodo, accelerazione spettrale, massa eccitata nelle tre direzioni globali per tutti i modi
- massa complessiva ed aliquota di massa complessiva eccitata.

Per ciascuna combinazione sismica definita SLD o SLO viene riportato il livello di deformazione η_T (dr) degli elementi strutturali verticali. Per semplicità di consultazione il livello è espresso anche in unità $1000 \cdot \eta_T/h$ da confrontare direttamente con i valori forniti nella norma (es. 5 per edifici con tamponamenti collegati rigidamente alla struttura, 10.0 per edifici con tamponamenti collegati elasticamente, 3 per edifici in muratura ordinaria, 4 per edifici in muratura armata).

Qualora si applichi il D.M. 96 (vedi NOTA sul capitolo "normativa di riferimento") l'analisi sismica dinamica può essere comprensiva di sollecitazione verticale contemporanea a quella orizzontale, nel qual caso è effettuata una sovrapposizione degli effetti in ragione della radice dei quadrati degli effetti stessi. Per ciascuna combinazione sismica - analisi effettuate con il D.M. 96 (vedi NOTA sul capitolo "normativa di riferimento") - viene riportato il livello di deformazione η_T , η_P e η_D degli elementi strutturali verticali. Per semplicità di consultazione il livello è espresso in unità $1000 \cdot \eta_T/h$ da confrontare direttamente con il valore 2 o 4 per la verifica.

Per gli edifici sismicamente isolati si riportano di seguito le verifiche condotte sui dispositivi di isolamento. Le verifiche sono effettuate secondo la circolare 619/2009 del C.S.LL.PP nelle combinazioni in SLC come previsto dal DM 17-01-2018. Per ogni combinazione è riportato il codice di verifica ed i valori utilizzati per la verifica: spostamento d_E , area ridotta e dimensione A_2 , azione verticale, deformazioni di taglio dell'elastomero e tensioni nell'acciaio.

Qualora si applichi l'Ordinanza 3274 e s.m.i. le verifiche sono eseguite in accordo con l'allegato 10.A.

In particolare la tabella, per ogni combinazione di calcolo, riporta:

Nodo	Nodo di appoggio dell' isolatore
Cmb	Combinazione oggetto della verifica
Verif.	Codice di verifica ok – verifica positiva , NV – verifica negativa, ND – verifica non completata
dE	Spostamento relativo tra le due facce (amplificato del 20% per Ordinanza 3274 e smi) combinato con la regola del 30%
Ang fi	Angolo utilizzato per il calcolo dell' area ridotta A_r (per dispositivi circolari)
V	Azione verticale agente
Ar	Area ridotta efficace
Dim A2	Dimensione utile per il calcolo della deformazione per rotazione
Sig s	Tensione nell' inserto in acciaio
Gam c(a,s,t)	Deformazioni di taglio dell' elastomero
Vcr	Carico critico per instabilità

Affinché la verifica sia positiva deve essere:

- 1) $V > 0$
- 2) $\text{Sig } s < f_{yk}$
- 3) $\text{Gam } t < 5$
- 4) $\text{Gam } s < \text{Gam} * (\text{caratteristica dell' elastomero})$
- 5) $\text{Gam } s < 2$
- 6) $V < 0.5 V_{cr}$

La costruzione, nuova, è caratterizzata da regolarità sia in pianta sia in altezza ed è progettata in classe di duttilità media (CD"B").

Parametri fattore in direzione x e y

Sistema costruttivo: calcestruzzo
 Tipologia strutturale: strutture a pareti non accoppiate
 Valore base fattore $q_0 = 3.000$
 Fattore pareti $k_w = 1.000$
 Fattore di regolarità $K_R = 1.0$
 Fattore dissipativo $q_D = q_0 \cdot k_w \cdot K_R = 3.000$

Fattori di comportamento utilizzati

Dissipativi
 q SLU x 3.000
 q SLU y 3.000
 q SLU z 1.500

CDC	Tipo	Sigla Id	Note
5	Edk	CDC=Ed (dinamico SLU) alfa=0.0 (ecc. +)	
			categoria suolo: B
			fattore di sito S = 1.142
			ordinata spettro (tratto Tb-Tc) = 0.246 g
			angolo di ingresso:0.0
			eccentricità aggiuntiva: positiva
			periodo proprio T1: 0.206 sec.
			fattore q: 3.000
			fattore per spost. μ d: 5.608
			classe di duttilità CD: B
			numero di modi considerati: 9
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
cm	daN	cm	cm	cm	cm	cm	cm			
760.00	7.480e+05	1780.86	1087.25	0.0	-109.30	1715.91	1092.49	1.311	0.023	0.004
717.78	4.474e+04	1602.59	1052.81	0.0	-109.30	1715.76	1198.60	2.020	0.050	0.084
675.56	3.762e+04	1545.95	1046.25	0.0	-109.30	1804.81	1095.84	2.087	0.116	0.028
633.33	3.050e+04	1462.87	1036.61	0.0	-109.30	1804.81	1095.84	2.087	0.154	0.034
591.11	3.050e+04	1462.87	1036.61	0.0	-109.30	1804.81	1095.84	2.087	0.154	0.034
548.89	3.050e+04	1462.87	1036.61	0.0	-109.30	1804.81	1095.84	2.087	0.154	0.034
506.67	3.092e+04	1448.38	1052.25	0.0	-109.30	1804.80	1198.60	1.959	0.157	0.086
464.44	3.134e+04	1434.27	1067.46	0.0	-109.30	1804.80	1198.60	1.959	0.164	0.077
422.22	3.134e+04	1434.27	1067.46	0.0	-109.30	1804.80	1400.80	2.097	0.171	0.190
380.00	8.890e+05	1813.80	1109.37	0.0	-109.30	1715.91	1092.49	1.311	0.035	0.012
337.78	4.474e+04	1602.59	1052.81	0.0	-109.30	1804.80	1198.60	1.959	0.089	0.086
295.56	3.762e+04	1545.95	1046.25	0.0	-109.30	1804.81	1095.84	2.087	0.116	0.028
253.33	3.050e+04	1462.87	1036.61	0.0	-109.30	1804.81	1095.84	2.087	0.154	0.034
211.11	3.050e+04	1462.87	1036.61	0.0	-109.30	1804.81	1095.84	2.087	0.154	0.034
168.89	3.050e+04	1462.87	1036.61	0.0	-109.30	1804.81	1095.84	2.087	0.154	0.034
126.67	3.092e+04	1448.38	1052.25	0.0	-109.30	1804.80	1198.60	1.959	0.157	0.086
84.44	3.134e+04	1434.27	1067.46	0.0	-109.30	1804.80	1198.60	1.959	0.164	0.077
42.22	3.134e+04	1434.27	1067.46	0.0	-109.30	1804.80	1198.60	1.959	0.164	0.077
Risulta	2.172e+06									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	3.950	0.253	0.246	1972.79	9.08e-02	1.863e+06	85.8	165.85	7.64e-03	0.0	0.0
2	4.850	0.206	0.246	1.953e+06	89.9	2.177e+04	1.0	93.16	4.29e-03	0.0	0.0
3	5.403	0.185	0.246	1.360e+05	6.3	1.728e+05	8.0	560.17	2.58e-02	0.0	0.0
4	10.377	0.096	0.265	26.51	1.22e-03	4.363e+04	2.0	5.578e+05	25.7	0.0	0.0
5	10.600	0.094	0.266	8941.79	0.4	2.289e+04	1.1	5.404e+05	24.9	0.0	0.0
6	12.538	0.080	0.271	9545.24	0.4	155.50	7.16e-03	7.790e+05	35.9	0.0	0.0
7	13.806	0.072	0.273	1.089e+04	0.5	8305.65	0.4	1.936e+05	8.9	0.0	0.0
8	15.095	0.066	0.275	42.57	1.96e-03	2.776e+04	1.3	9.342e+04	4.3	0.0	0.0
9	18.464	0.054	0.279	4.767e+04	2.2	1344.03	6.19e-02	1901.48	8.75e-02	0.0	0.0
Risulta				2.168e+06		2.162e+06		2.167e+06			
In percentuale				99.83		99.54		99.77			

CDC	Tipo	Sigla Id	Note
6	Edk	CDC=Ed (dinamico SLU) alfa=0.0 (ecc. -)	
			categoria suolo: B
			fattore di sito S = 1.142
			ordinata spettro (tratto Tb-Tc) = 0.246 g
			angolo di ingresso:0.0
			eccentricità aggiuntiva: negativa

CDC	Tipo	Sigla Id	Note								
			periodo proprio T1: 0.208 sec.								
			fattore q: 3.000								
			fattore per spost. mu d: 5.562								
			classe di duttilità CD: B								
			numero di modi considerati: 9								
			combinaz. modale: CQC								
Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry	
cm	daN	cm	cm	cm	cm	cm	cm				
760.00	7.480e+05	1780.86	1087.25	0.0	109.30	1715.91	1092.49	1.311	0.023	0.004	
717.78	4.474e+04	1602.59	1052.81	0.0	109.30	1715.76	1198.60	2.020	0.050	0.084	
675.56	3.762e+04	1545.95	1046.25	0.0	109.30	1804.81	1095.84	2.087	0.116	0.028	
633.33	3.050e+04	1462.87	1036.61	0.0	109.30	1804.81	1095.84	2.087	0.154	0.034	
591.11	3.050e+04	1462.87	1036.61	0.0	109.30	1804.81	1095.84	2.087	0.154	0.034	
548.89	3.050e+04	1462.87	1036.61	0.0	109.30	1804.81	1095.84	2.087	0.154	0.034	
506.67	3.092e+04	1448.38	1052.25	0.0	109.30	1804.80	1198.60	1.959	0.157	0.086	
464.44	3.134e+04	1434.27	1067.46	0.0	109.30	1804.80	1198.60	1.959	0.164	0.077	
422.22	3.134e+04	1434.27	1067.46	0.0	109.30	1804.80	1400.80	2.097	0.171	0.190	
380.00	8.890e+05	1813.80	1109.37	0.0	109.30	1715.91	1092.49	1.311	0.035	0.012	
337.78	4.474e+04	1602.59	1052.81	0.0	109.30	1804.80	1198.60	1.959	0.089	0.086	
295.56	3.762e+04	1545.95	1046.25	0.0	109.30	1804.81	1095.84	2.087	0.116	0.028	
253.33	3.050e+04	1462.87	1036.61	0.0	109.30	1804.81	1095.84	2.087	0.154	0.034	
211.11	3.050e+04	1462.87	1036.61	0.0	109.30	1804.81	1095.84	2.087	0.154	0.034	
168.89	3.050e+04	1462.87	1036.61	0.0	109.30	1804.81	1095.84	2.087	0.154	0.034	
126.67	3.092e+04	1448.38	1052.25	0.0	109.30	1804.80	1198.60	1.959	0.157	0.086	
84.44	3.134e+04	1434.27	1067.46	0.0	109.30	1804.80	1198.60	1.959	0.164	0.077	
42.22	3.134e+04	1434.27	1067.46	0.0	109.30	1804.80	1198.60	1.959	0.164	0.077	
Risulta	2.172e+06										
Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	3.943	0.254	0.246	2.419e+04	1.1	1.829e+06	84.2	131.46	6.05e-03	0.0	0.0
2	4.802	0.208	0.246	1.805e+06	83.1	9.213e+04	4.2	435.55	2.01e-02	0.0	0.0
3	5.452	0.183	0.246	2.629e+05	12.1	1.368e+05	6.3	101.14	4.66e-03	0.0	0.0
4	10.371	0.096	0.265	1363.39	6.28e-02	3.402e+04	1.6	6.445e+05	29.7	0.0	0.0
5	10.720	0.093	0.266	1802.62	8.30e-02	2.925e+04	1.3	5.129e+05	23.6	0.0	0.0
6	12.733	0.079	0.271	1.648e+04	0.8	1.395e+04	0.6	5.281e+05	24.3	0.0	0.0
7	13.144	0.076	0.272	1.190e+04	0.5	9004.36	0.4	4.199e+05	19.3	0.0	0.0
8	15.655	0.064	0.276	1.694e+04	0.8	1.570e+04	0.7	5.266e+04	2.4	0.0	0.0
9	20.122	0.050	0.280	2.661e+04	1.2	1039.34	4.79e-02	8947.25	0.4	0.0	0.0
Risulta				2.167e+06		2.161e+06		2.168e+06			
In percentuale				99.76		99.49		99.80			

CDC	Tipo	Sigla Id	Note								
7	Edk	CDC=Ed (dinamico SLU) alfa=90.00 (ecc. +)									
			categoria suolo: B								
			fattore di sito S = 1.142								
			ordinata spettro (tratto Tb-Tc) = 0.246 g								
			angolo di ingresso: 90.00								
			eccentricità aggiuntiva: positiva								
			periodo proprio T1: 0.264 sec.								
			fattore q: 3.000								
			fattore per spost. mu d: 4.592								
			classe di duttilità CD: B								
			numero di modi considerati: 9								
			combinaz. modale: CQC								
Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry	
cm	daN	cm	cm	cm	cm	cm	cm				
760.00	7.480e+05	1780.86	1087.25	179.76	0.0	1715.91	1092.49	1.311	0.023	0.004	
717.78	4.474e+04	1602.59	1052.81	179.75	0.0	1715.76	1198.60	2.020	0.050	0.084	
675.56	3.762e+04	1545.95	1046.25	179.75	0.0	1804.81	1095.84	2.087	0.116	0.028	
633.33	3.050e+04	1462.87	1036.61	179.75	0.0	1804.81	1095.84	2.087	0.154	0.034	
591.11	3.050e+04	1462.87	1036.61	179.75	0.0	1804.81	1095.84	2.087	0.154	0.034	
548.89	3.050e+04	1462.87	1036.61	179.75	0.0	1804.81	1095.84	2.087	0.154	0.034	
506.67	3.092e+04	1448.38	1052.25	179.75	0.0	1804.80	1198.60	1.959	0.157	0.086	
464.44	3.134e+04	1434.27	1067.46	179.75	0.0	1804.80	1198.60	1.959	0.164	0.077	
422.22	3.134e+04	1434.27	1067.46	179.75	0.0	1804.80	1400.80	2.097	0.171	0.190	
380.00	8.890e+05	1813.80	1109.37	179.76	0.0	1715.91	1092.49	1.311	0.035	0.012	
337.78	4.474e+04	1602.59	1052.81	179.75	0.0	1804.80	1198.60	1.959	0.089	0.086	
295.56	3.762e+04	1545.95	1046.25	179.75	0.0	1804.81	1095.84	2.087	0.116	0.028	
253.33	3.050e+04	1462.87	1036.61	179.75	0.0	1804.81	1095.84	2.087	0.154	0.034	

CDC	Tipo	Sigla Id	Note								
211.11	3.050e+04	1462.87	1036.61	179.75	0.0	1804.81	1095.84	2.087	0.154	0.034	
168.89	3.050e+04	1462.87	1036.61	179.75	0.0	1804.81	1095.84	2.087	0.154	0.034	
126.67	3.092e+04	1448.38	1052.25	179.75	0.0	1804.80	1198.60	1.959	0.157	0.086	
84.44	3.134e+04	1434.27	1067.46	179.75	0.0	1804.80	1198.60	1.959	0.164	0.077	
42.22	3.134e+04	1434.27	1067.46	179.75	0.0	1804.80	1198.60	1.959	0.164	0.077	
Risulta	2.172e+06										
Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	3.781	0.264	0.246	2515.10	0.1	1.766e+06	81.3	99.27	4.57e-03	0.0	0.0
2	4.886	0.205	0.246	2.084e+06	95.9	6080.67	0.3	275.98	1.27e-02	0.0	0.0
3	5.566	0.180	0.246	5097.44	0.2	2.838e+05	13.1	491.99	2.27e-02	0.0	0.0
4	10.415	0.096	0.265	1607.52	7.40e-02	2.207e+04	1.0	8.780e+05	40.4	0.0	0.0
5	10.893	0.092	0.267	6622.26	0.3	5.547e+04	2.6	2.461e+05	11.3	0.0	0.0
6	12.057	0.083	0.270	1.609e+04	0.7	27.66	1.27e-03	2.543e+05	11.7	0.0	0.0
7	13.094	0.076	0.272	346.68	1.60e-02	3277.15	0.2	7.063e+05	32.5	0.0	0.0
8	15.483	0.065	0.275	1803.64	8.30e-02	2.330e+04	1.1	8.092e+04	3.7	0.0	0.0
9	18.702	0.053	0.279	5.171e+04	2.4	180.05	8.29e-03	374.75	1.73e-02	0.0	0.0
Risulta				2.170e+06		2.160e+06		2.167e+06			
In percentuale				99.89		99.44		99.76			

CDC	Tipo	Sigla Id	Note								
8	Edk	CDC=Ed (dinamico SLU) alfa=90.00 (ecc. -)									
			categoria suolo: B								
			fattore di sito S = 1.142								
			ordinata spettro (tratto Tb-Tc) = 0.246 g								
			angolo di ingresso:90.00								
			eccentricità aggiuntiva: negativa								
			periodo proprio T1: 0.245 sec.								
			fattore q: 3.000								
			fattore per spost. mu d: 4.873								
			classe di duttilità CD: B								
			numero di modi considerati: 9								
			combinaz. modale: CQC								
Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry	
cm	daN	cm	cm	cm	cm	cm	cm				
760.00	7.480e+05	1780.86	1087.25	-179.76	0.0	1715.91	1092.49	1.311	0.023	0.004	
717.78	4.474e+04	1602.59	1052.81	-179.75	0.0	1715.76	1198.60	2.020	0.050	0.084	
675.56	3.762e+04	1545.95	1046.25	-179.75	0.0	1804.81	1095.84	2.087	0.116	0.028	
633.33	3.050e+04	1462.87	1036.61	-179.75	0.0	1804.81	1095.84	2.087	0.154	0.034	
591.11	3.050e+04	1462.87	1036.61	-179.75	0.0	1804.81	1095.84	2.087	0.154	0.034	
548.89	3.050e+04	1462.87	1036.61	-179.75	0.0	1804.81	1095.84	2.087	0.154	0.034	
506.67	3.092e+04	1448.38	1052.25	-179.75	0.0	1804.80	1198.60	1.959	0.157	0.086	
464.44	3.134e+04	1434.27	1067.46	-179.75	0.0	1804.80	1198.60	1.959	0.164	0.077	
422.22	3.134e+04	1434.27	1067.46	-179.75	0.0	1804.80	1400.80	2.097	0.171	0.190	
380.00	8.890e+05	1813.80	1109.37	-179.76	0.0	1715.91	1092.49	1.311	0.035	0.012	
337.78	4.474e+04	1602.59	1052.81	-179.75	0.0	1804.80	1198.60	1.959	0.089	0.086	
295.56	3.762e+04	1545.95	1046.25	-179.75	0.0	1804.81	1095.84	2.087	0.116	0.028	
253.33	3.050e+04	1462.87	1036.61	-179.75	0.0	1804.81	1095.84	2.087	0.154	0.034	
211.11	3.050e+04	1462.87	1036.61	-179.75	0.0	1804.81	1095.84	2.087	0.154	0.034	
168.89	3.050e+04	1462.87	1036.61	-179.75	0.0	1804.81	1095.84	2.087	0.154	0.034	
126.67	3.092e+04	1448.38	1052.25	-179.75	0.0	1804.80	1198.60	1.959	0.157	0.086	
84.44	3.134e+04	1434.27	1067.46	-179.75	0.0	1804.80	1198.60	1.959	0.164	0.077	
42.22	3.134e+04	1434.27	1067.46	-179.75	0.0	1804.80	1198.60	1.959	0.164	0.077	
Risulta	2.172e+06										
Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	4.077	0.245	0.246	2362.26	0.1	2.002e+06	92.2	230.21	1.06e-02	0.0	0.0
2	4.881	0.205	0.246	2.057e+06	94.7	6669.09	0.3	294.63	1.36e-02	0.0	0.0
3	5.281	0.189	0.246	3.241e+04	1.5	5.136e+04	2.4	121.69	5.60e-03	0.0	0.0
4	10.390	0.096	0.265	1210.33	5.57e-02	2.784e+04	1.3	7.700e+05	35.5	0.0	0.0
5	10.866	0.092	0.267	4259.25	0.2	4.144e+04	1.9	4.160e+05	19.2	0.0	0.0
6	12.079	0.083	0.270	2.047e+04	0.9	3215.49	0.1	9.791e+04	4.5	0.0	0.0
7	13.052	0.077	0.272	6.31	2.90e-04	1793.11	8.26e-02	7.970e+05	36.7	0.0	0.0
8	15.021	0.067	0.275	2932.18	0.1	2.690e+04	1.2	8.344e+04	3.8	0.0	0.0
9	18.959	0.053	0.279	4.916e+04	2.3	0.59	2.73e-05	1376.38	6.34e-02	0.0	0.0
Risulta				2.170e+06		2.162e+06		2.166e+06			
In percentuale				99.88		99.52		99.74			

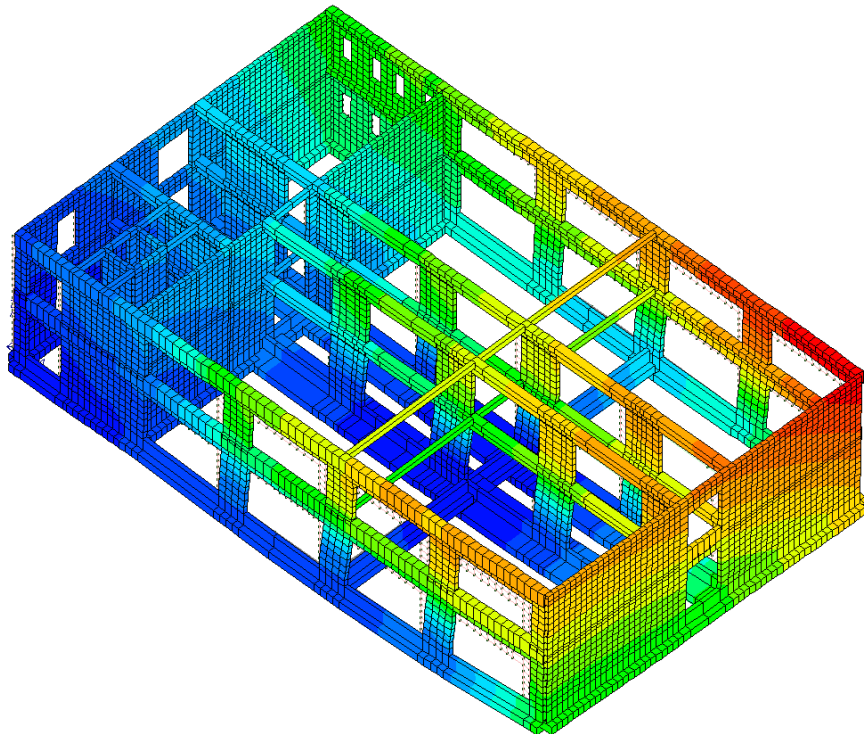
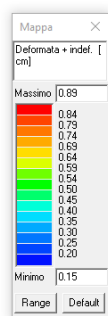
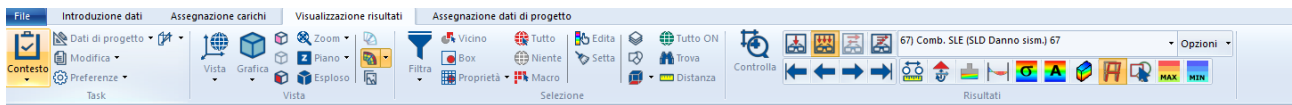
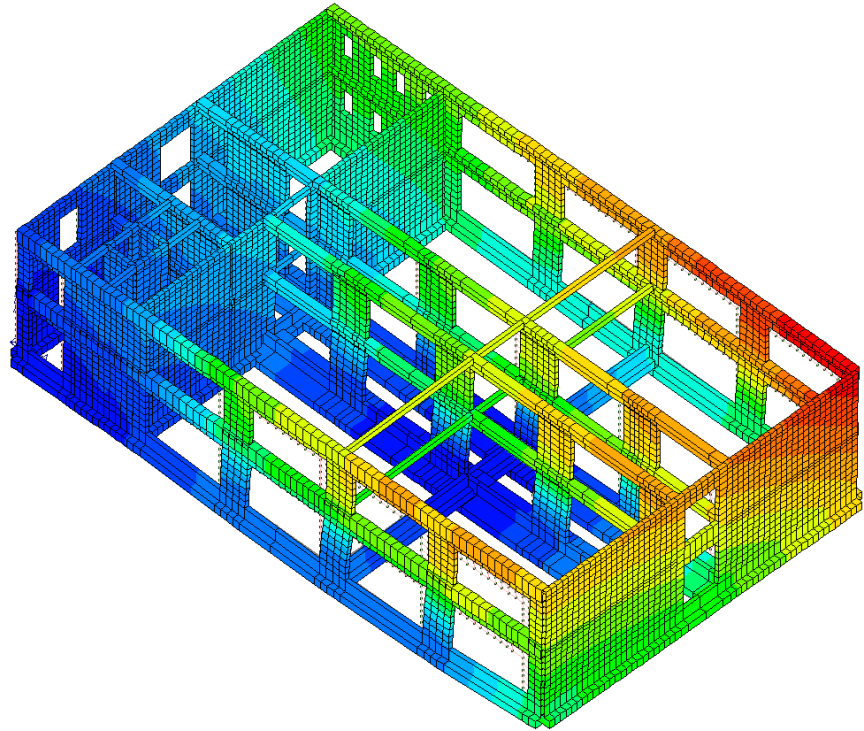
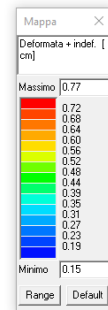
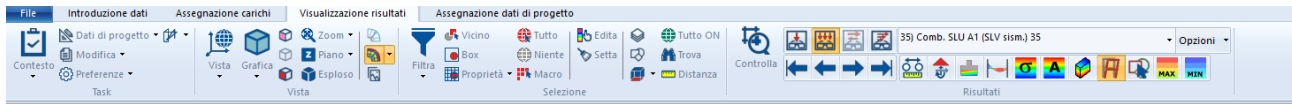
CDC	Tipo	Sigla Id	Note								
9	Edk	CDC=Ed (dinamico SLD) alfa=0.0 (ecc. +)									
			categoria suolo: B								
			fattore di sito S = 1.200								
			ordinata spettro (tratto Tb-Tc) = 0.295 g								
			angolo di ingresso:0.0								
			eccentricità aggiuntiva: positiva								
			periodo proprio T1: 0.206 sec.								
			numero di modi considerati: 9								
			combinaz. modale: CQC								
Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry	
cm	daN	cm	cm	cm	cm	cm	cm				
760.00	7.480e+05	1780.86	1087.25	0.0	-109.30	1715.91	1092.49	1.311	0.023	0.004	
717.78	4.474e+04	1602.59	1052.81	0.0	-109.30	1715.76	1198.60	2.020	0.050	0.084	
675.56	3.762e+04	1545.95	1046.25	0.0	-109.30	1804.81	1095.84	2.087	0.116	0.028	
633.33	3.050e+04	1462.87	1036.61	0.0	-109.30	1804.81	1095.84	2.087	0.154	0.034	
591.11	3.050e+04	1462.87	1036.61	0.0	-109.30	1804.81	1095.84	2.087	0.154	0.034	
548.89	3.050e+04	1462.87	1036.61	0.0	-109.30	1804.81	1095.84	2.087	0.154	0.034	
506.67	3.092e+04	1448.38	1052.25	0.0	-109.30	1804.80	1198.60	1.959	0.157	0.086	
464.44	3.134e+04	1434.27	1067.46	0.0	-109.30	1804.80	1198.60	1.959	0.164	0.077	
422.22	3.134e+04	1434.27	1067.46	0.0	-109.30	1804.80	1400.80	2.097	0.171	0.190	
380.00	8.890e+05	1813.80	1109.37	0.0	-109.30	1715.91	1092.49	1.311	0.035	0.012	
337.78	4.474e+04	1602.59	1052.81	0.0	-109.30	1804.80	1198.60	1.959	0.089	0.086	
295.56	3.762e+04	1545.95	1046.25	0.0	-109.30	1804.81	1095.84	2.087	0.116	0.028	
253.33	3.050e+04	1462.87	1036.61	0.0	-109.30	1804.81	1095.84	2.087	0.154	0.034	
211.11	3.050e+04	1462.87	1036.61	0.0	-109.30	1804.81	1095.84	2.087	0.154	0.034	
168.89	3.050e+04	1462.87	1036.61	0.0	-109.30	1804.81	1095.84	2.087	0.154	0.034	
126.67	3.092e+04	1448.38	1052.25	0.0	-109.30	1804.80	1198.60	1.959	0.157	0.086	
84.44	3.134e+04	1434.27	1067.46	0.0	-109.30	1804.80	1198.60	1.959	0.164	0.077	
42.22	3.134e+04	1434.27	1067.46	0.0	-109.30	1804.80	1198.60	1.959	0.164	0.077	
Risulta	2.172e+06										
Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	3.950	0.253	0.295	1972.79	9.08e-02	1.863e+06	85.8	165.85	7.64e-03	0.0	0.0
2	4.850	0.206	0.295	1.953e+06	89.9	2.177e+04	1.0	93.16	4.29e-03	0.0	0.0
3	5.403	0.185	0.295	1.360e+05	6.3	1.728e+05	8.0	560.17	2.58e-02	0.0	0.0
4	10.377	0.096	0.244	26.51	1.22e-03	4.363e+04	2.0	5.578e+05	25.7	0.0	0.0
5	10.600	0.094	0.241	8941.79	0.4	2.289e+04	1.1	5.404e+05	24.9	0.0	0.0
6	12.538	0.080	0.223	9545.24	0.4	155.50	7.16e-03	7.790e+05	35.9	0.0	0.0
7	13.806	0.072	0.214	1.089e+04	0.5	8305.65	0.4	1.936e+05	8.9	0.0	0.0
8	15.095	0.066	0.206	42.57	1.96e-03	2.776e+04	1.3	9.342e+04	4.3	0.0	0.0
9	18.464	0.054	0.190	4.767e+04	2.2	1344.03	6.19e-02	1901.48	8.75e-02	0.0	0.0
Risulta				2.168e+06		2.162e+06		2.167e+06			
In percentuale				99.83		99.54		99.77			

CDC	Tipo	Sigla Id	Note								
10	Edk	CDC=Ed (dinamico SLD) alfa=0.0 (ecc. -)									
			categoria suolo: B								
			fattore di sito S = 1.200								
			ordinata spettro (tratto Tb-Tc) = 0.295 g								
			angolo di ingresso:0.0								
			eccentricità aggiuntiva: negativa								
			periodo proprio T1: 0.208 sec.								
			numero di modi considerati: 9								
			combinaz. modale: CQC								
Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry	
cm	daN	cm	cm	cm	cm	cm	cm				
760.00	7.480e+05	1780.86	1087.25	0.0	109.30	1715.91	1092.49	1.311	0.023	0.004	
717.78	4.474e+04	1602.59	1052.81	0.0	109.30	1715.76	1198.60	2.020	0.050	0.084	
675.56	3.762e+04	1545.95	1046.25	0.0	109.30	1804.81	1095.84	2.087	0.116	0.028	
633.33	3.050e+04	1462.87	1036.61	0.0	109.30	1804.81	1095.84	2.087	0.154	0.034	
591.11	3.050e+04	1462.87	1036.61	0.0	109.30	1804.81	1095.84	2.087	0.154	0.034	
548.89	3.050e+04	1462.87	1036.61	0.0	109.30	1804.81	1095.84	2.087	0.154	0.034	
506.67	3.092e+04	1448.38	1052.25	0.0	109.30	1804.80	1198.60	1.959	0.157	0.086	
464.44	3.134e+04	1434.27	1067.46	0.0	109.30	1804.80	1198.60	1.959	0.164	0.077	
422.22	3.134e+04	1434.27	1067.46	0.0	109.30	1804.80	1400.80	2.097	0.171	0.190	
380.00	8.890e+05	1813.80	1109.37	0.0	109.30	1715.91	1092.49	1.311	0.035	0.012	

CDC	Tipo	Sigla Id				Note					
337.78	4.474e+04	1602.59	1052.81	0.0	109.30	1804.80	1198.60	1.959	0.089	0.086	
295.56	3.762e+04	1545.95	1046.25	0.0	109.30	1804.81	1095.84	2.087	0.116	0.028	
253.33	3.050e+04	1462.87	1036.61	0.0	109.30	1804.81	1095.84	2.087	0.154	0.034	
211.11	3.050e+04	1462.87	1036.61	0.0	109.30	1804.81	1095.84	2.087	0.154	0.034	
168.89	3.050e+04	1462.87	1036.61	0.0	109.30	1804.81	1095.84	2.087	0.154	0.034	
126.67	3.092e+04	1448.38	1052.25	0.0	109.30	1804.80	1198.60	1.959	0.157	0.086	
84.44	3.134e+04	1434.27	1067.46	0.0	109.30	1804.80	1198.60	1.959	0.164	0.077	
42.22	3.134e+04	1434.27	1067.46	0.0	109.30	1804.80	1198.60	1.959	0.164	0.077	
Risulta	2.172e+06										
Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	3.943	0.254	0.295	2.419e+04	1.1	1.829e+06	84.2	131.46	6.05e-03	0.0	0.0
2	4.802	0.208	0.295	1.805e+06	83.1	9.213e+04	4.2	435.55	2.01e-02	0.0	0.0
3	5.452	0.183	0.295	2.629e+05	12.1	1.368e+05	6.3	101.14	4.66e-03	0.0	0.0
4	10.371	0.096	0.244	1363.39	6.28e-02	3.402e+04	1.6	6.445e+05	29.7	0.0	0.0
5	10.720	0.093	0.240	1802.62	8.30e-02	2.925e+04	1.3	5.129e+05	23.6	0.0	0.0
6	12.733	0.079	0.221	1.648e+04	0.8	1.395e+04	0.6	5.281e+05	24.3	0.0	0.0
7	13.144	0.076	0.218	1.190e+04	0.5	9004.36	0.4	4.199e+05	19.3	0.0	0.0
8	15.655	0.064	0.203	1.694e+04	0.8	1.570e+04	0.7	5.266e+04	2.4	0.0	0.0
9	20.122	0.050	0.185	2.661e+04	1.2	1039.34	4.79e-02	8947.25	0.4	0.0	0.0
Risulta				2.167e+06		2.161e+06		2.168e+06			
In percentuale				99.76		99.49		99.80			

CDC	Tipo	Sigla Id	Note								
11	Edk	CDC=Ed (dinamico SLD) alfa=90.00 (ecc. +)									
			categoria suolo: B								
			fattore di sito S = 1.200								
			ordinata spettro (tratto Tb-Tc) = 0.295 g								
			angolo di ingresso:90.00								
			eccentricità aggiuntiva: positiva								
			periodo proprio T1: 0.264 sec.								
			numero di modi considerati: 9								
			combinaz. modale: CQC								
Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry	
cm	daN	cm	cm	cm	cm	cm	cm				
760.00	7.480e+05	1780.86	1087.25	179.76	0.0	1715.91	1092.49	1.311	0.023	0.004	
717.78	4.474e+04	1602.59	1052.81	179.75	0.0	1715.76	1198.60	2.020	0.050	0.084	
675.56	3.762e+04	1545.95	1046.25	179.75	0.0	1804.81	1095.84	2.087	0.116	0.028	
633.33	3.050e+04	1462.87	1036.61	179.75	0.0	1804.81	1095.84	2.087	0.154	0.034	
591.11	3.050e+04	1462.87	1036.61	179.75	0.0	1804.81	1095.84	2.087	0.154	0.034	
548.89	3.050e+04	1462.87	1036.61	179.75	0.0	1804.81	1095.84	2.087	0.154	0.034	
506.67	3.092e+04	1448.38	1052.25	179.75	0.0	1804.80	1198.60	1.959	0.157	0.086	
464.44	3.134e+04	1434.27	1067.46	179.75	0.0	1804.80	1198.60	1.959	0.164	0.077	
422.22	3.134e+04	1434.27	1067.46	179.75	0.0	1804.80	1400.80	2.097	0.171	0.190	
380.00	8.890e+05	1813.80	1109.37	179.76	0.0	1715.91	1092.49	1.311	0.035	0.012	
337.78	4.474e+04	1602.59	1052.81	179.75	0.0	1804.80	1198.60	1.959	0.089	0.086	
295.56	3.762e+04	1545.95	1046.25	179.75	0.0	1804.81	1095.84	2.087	0.116	0.028	
253.33	3.050e+04	1462.87	1036.61	179.75	0.0	1804.81	1095.84	2.087	0.154	0.034	
211.11	3.050e+04	1462.87	1036.61	179.75	0.0	1804.81	1095.84	2.087	0.154	0.034	
168.89	3.050e+04	1462.87	1036.61	179.75	0.0	1804.81	1095.84	2.087	0.154	0.034	
126.67	3.092e+04	1448.38	1052.25	179.75	0.0	1804.80	1198.60	1.959	0.157	0.086	
84.44	3.134e+04	1434.27	1067.46	179.75	0.0	1804.80	1198.60	1.959	0.164	0.077	
42.22	3.134e+04	1434.27	1067.46	179.75	0.0	1804.80	1198.60	1.959	0.164	0.077	
Risulta	2.172e+06										
Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	3.781	0.264	0.295	2515.10	0.1	1.766e+06	81.3	99.27	4.57e-03	0.0	0.0
2	4.886	0.205	0.295	2.084e+06	95.9	6080.67	0.3	275.98	1.27e-02	0.0	0.0
3	5.566	0.180	0.295	5097.44	0.2	2.838e+05	13.1	491.99	2.27e-02	0.0	0.0
4	10.415	0.096	0.244	1607.52	7.40e-02	2.207e+04	1.0	8.780e+05	40.4	0.0	0.0
5	10.893	0.092	0.238	6622.26	0.3	5.547e+04	2.6	2.461e+05	11.3	0.0	0.0
6	12.057	0.083	0.227	1.609e+04	0.7	27.66	1.27e-03	2.543e+05	11.7	0.0	0.0
7	13.094	0.076	0.219	346.68	1.60e-02	3277.15	0.2	7.063e+05	32.5	0.0	0.0
8	15.483	0.065	0.204	1803.64	8.30e-02	2.330e+04	1.1	8.092e+04	3.7	0.0	0.0
9	18.702	0.053	0.189	5.171e+04	2.4	180.05	8.29e-03	374.75	1.73e-02	0.0	0.0
Risulta				2.170e+06		2.160e+06		2.167e+06			
In percentuale				99.89		99.44		99.76			

CDC	Tipo	Sigla Id	Note									
12	Edk	CDC=Ed (dinamico SLD) alfa=90.00 (ecc. -)										
			categoria suolo: B									
			fattore di sito S = 1.200									
			ordinata spettro (tratto Tb-Tc) = 0.295 g									
			angolo di ingresso:90.00									
			eccentricità aggiuntiva: negativa									
			periodo proprio T1: 0.245 sec.									
			numero di modi considerati: 9									
			combinaz. modale: CQC									
Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry		
cm	daN	cm	cm	cm	cm	cm	cm					
760.00	7.480e+05	1780.86	1087.25	-179.76	0.0	1715.91	1092.49	1.311	0.023	0.004		
717.78	4.474e+04	1602.59	1052.81	-179.75	0.0	1715.76	1198.60	2.020	0.050	0.084		
675.56	3.762e+04	1545.95	1046.25	-179.75	0.0	1804.81	1095.84	2.087	0.116	0.028		
633.33	3.050e+04	1462.87	1036.61	-179.75	0.0	1804.81	1095.84	2.087	0.154	0.034		
591.11	3.050e+04	1462.87	1036.61	-179.75	0.0	1804.81	1095.84	2.087	0.154	0.034		
548.89	3.050e+04	1462.87	1036.61	-179.75	0.0	1804.81	1095.84	2.087	0.154	0.034		
506.67	3.092e+04	1448.38	1052.25	-179.75	0.0	1804.80	1198.60	1.959	0.157	0.086		
464.44	3.134e+04	1434.27	1067.46	-179.75	0.0	1804.80	1198.60	1.959	0.164	0.077		
422.22	3.134e+04	1434.27	1067.46	-179.75	0.0	1804.80	1400.80	2.097	0.171	0.190		
380.00	8.890e+05	1813.80	1109.37	-179.76	0.0	1715.91	1092.49	1.311	0.035	0.012		
337.78	4.474e+04	1602.59	1052.81	-179.75	0.0	1804.80	1198.60	1.959	0.089	0.086		
295.56	3.762e+04	1545.95	1046.25	-179.75	0.0	1804.81	1095.84	2.087	0.116	0.028		
253.33	3.050e+04	1462.87	1036.61	-179.75	0.0	1804.81	1095.84	2.087	0.154	0.034		
211.11	3.050e+04	1462.87	1036.61	-179.75	0.0	1804.81	1095.84	2.087	0.154	0.034		
168.89	3.050e+04	1462.87	1036.61	-179.75	0.0	1804.81	1095.84	2.087	0.154	0.034		
126.67	3.092e+04	1448.38	1052.25	-179.75	0.0	1804.80	1198.60	1.959	0.157	0.086		
84.44	3.134e+04	1434.27	1067.46	-179.75	0.0	1804.80	1198.60	1.959	0.164	0.077		
42.22	3.134e+04	1434.27	1067.46	-179.75	0.0	1804.80	1198.60	1.959	0.164	0.077		
Risulta	2.172e+06											
Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v	
	Hz	sec	g	daN		daN		daN				
1	4.077	0.245	0.295	2362.26	0.1	2.002e+06	92.2	230.21	1.06e-02	0.0	0.0	
2	4.881	0.205	0.295	2.057e+06	94.7	6669.09	0.3	294.63	1.36e-02	0.0	0.0	
3	5.281	0.189	0.295	3.241e+04	1.5	5.136e+04	2.4	121.69	5.60e-03	0.0	0.0	
4	10.390	0.096	0.244	1210.33	5.57e-02	2.784e+04	1.3	7.700e+05	35.5	0.0	0.0	
5	10.866	0.092	0.238	4259.25	0.2	4.144e+04	1.9	4.160e+05	19.2	0.0	0.0	
6	12.079	0.083	0.227	2.047e+04	0.9	3215.49	0.1	9.791e+04	4.5	0.0	0.0	
7	13.052	0.077	0.219	6.31	2.90e-04	1793.11	8.26e-02	7.970e+05	36.7	0.0	0.0	
8	15.021	0.067	0.206	2932.18	0.1	2.690e+04	1.2	8.344e+04	3.8	0.0	0.0	
9	18.959	0.053	0.188	4.916e+04	2.3	0.59	2.73e-05	1376.38	6.34e-02	0.0	0.0	
Risulta				2.170e+06		2.162e+06		2.166e+06				
In percentuale				99.88		99.52		99.74				



VERIFICHE ELEMENTI TRAVE E/O PILASTRO IN C.A.

Legenda tabella verifiche elementi trave e/o pilastro in c.a.

In tabella vengono riportati per ogni elemento il numero identificativo ed il codice di verifica con le sigle **Ok** o **NV**.

Nel caso in cui si sia proceduto alla progettazione con le tensioni ammissibili (**T.A.**) vengono riportate le massime tensioni nell'elemento (massima compressione nel calcestruzzo, massima compressione media nel calcestruzzo, massima tensione nell'acciaio, massima tensione tangenziale) con l'indicazione delle combinazioni in cui si sono attinti i rispettivi valori.

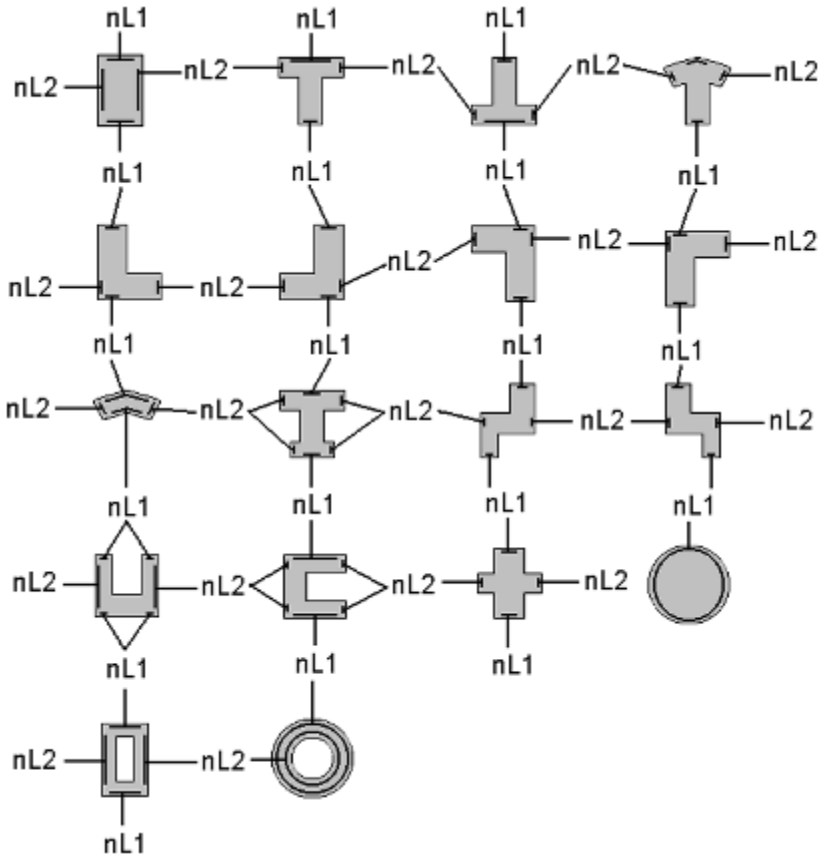
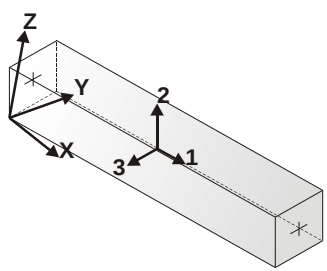
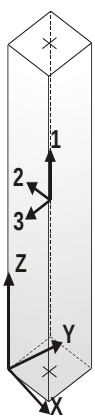
Nel caso in cui si sia proceduto alla progettazione con il metodo degli stati limite (**S.L.**) vengono riportati: il rapporto x/d , le verifiche per sollecitazioni proporzionali e la verifica per compressione media con l'indicazione delle combinazioni in cui si sono attinti i rispettivi valori.

Nel caso in cui la struttura abbia comportamento dissipativo e sia prevista la progettazione con il criterio della gerarchia delle resistenze (**G.R.**) vengono riportate le verifiche di sovrarresistenza e del nodo.

Per gli elementi tipo pilastro sono riportati numero e diametro dei ferri di vertice, numero e diametro di ferri disposti lungo i lati L1 (paralleli alla base della sezione) e lungo i lati L2 (paralleli all'altezza della sezione).

Per gli elementi tipo trave sono riportati infine le quantità di armatura inferiore e superiore.

Schema della distribuzione delle armature longitudinali

							
						Orientamento elementi 2D non verticali	
							
						Orientamento elementi 2D verticali	

Trave	Note	Pos. cm	%Af	Af inf.	Af. sup	Af long.	M _T =1 x/d	Z=0.0 V N/M	N=1 V V/T cls	N=37 V V/T acc	Staffe L=cm	Rif. cmb
1	ok,ok s=1,m=1	0.0 38.3	0.35 0.35	23.7 23.7	22.9 22.9	0.0 0.0	0.05 0.05	0.07 0.07	0.12 0.17	0.05 0.12	2d8/25 L=38 2d8/25 L=38	41,13,13 41,13,13

101

1098	s=5,m=1	40.1	0.40	10.3	12.3	0.0	0.05	0.14	0.16	0.18	2d8/25 L=40	15,13,14
	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.13	0.13	0.14	2d8/25 L=40	15,13,14
	s=5,m=1	40.1	0.40	10.3	12.3	0.0	0.08	0.15	0.17	0.21	2d8/25 L=40	15,13,14
1014	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.15	0.16	0.18	2d8/25 L=40	15,13,14
	s=5,m=1	39.6	0.40	10.3	12.3	0.0	0.08	0.16	0.20	0.25	2d8/25 L=40	15,13,14
1032	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.16	0.18	0.22	2d8/25 L=40	15,13,14
	s=5,m=1	39.6	0.40	10.3	12.3	0.0	0.08	0.22	0.22	0.29	2d8/25 L=40	14,13,14
1026	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.23	0.17	0.23	2d8/25 L=35	14,13,14
	s=5,m=1	35.4	0.40	10.3	12.3	0.0	0.08	0.32	0.21	0.29	2d8/25 L=35	18,13,14
1092	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.35	0.12	0.14	2d8/25 L=35	18,18,14
	s=5,m=1	35.4	0.40	10.3	12.3	0.0	0.08	0.42	0.15	0.20	2d8/25 L=35	18,18,14
1000	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.40	0.27	0.37	2d8/25 L=44	18,14,14
	s=5,m=1	43.8	0.40	10.3	12.3	0.0	0.08	0.25	0.22	0.32	2d8/25 L=44	18,14,15
1021	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.25	0.44	0.60	2d8/25 L=44	18,18,13
	s=5,m=1	43.8	0.40	10.3	12.3	0.0	0.08	0.09	0.39	0.53	2d8/25 L=44	16,18,13
1012	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.10	0.40	0.51	2d8/25 L=44	18,16,16
	s=5,m=1	43.8	0.40	10.3	12.3	0.0	0.08	0.23	0.45	0.58	2d8/25 L=44	16,16,16
1024	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.25	0.24	0.30	2d8/25 L=44	16,16,13
	s=5,m=1	43.8	0.40	10.3	12.3	0.0	0.08	0.39	0.29	0.36	2d8/25 L=44	16,16,16
1010	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.43	0.24	0.24	2d8/25 L=47	16,32,3
	s=5,m=1	46.8	0.40	10.3	12.3	0.0	0.08	0.33	0.19	0.16	2d8/25 L=47	16,32,16
1077	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.29	0.22	0.30	2d8/25 L=47	16,16,16
	s=5,m=1	46.8	0.40	10.3	12.3	0.0	0.08	0.17	0.17	0.22	2d8/25 L=47	16,16,16
1078	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.15	0.20	0.26	2d8/25 L=47	16,16,16
	s=5,m=1	46.9	0.40	10.3	12.3	0.0	0.08	0.15	0.15	0.18	2d8/25 L=47	13,16,16
1079	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.15	0.17	0.21	2d8/25 L=47	13,19,16
	s=5,m=1	46.8	0.40	10.3	12.3	0.0	0.05	0.13	0.12	0.13	2d8/25 L=47	13,19,16
1080	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.13	0.15	0.18	2d8/25 L=47	13,19,16
	s=5,m=1	46.8	0.40	10.3	12.3	0.0	0.05	0.15	0.10	0.10	2d8/25 L=47	3,29,13
1081	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.14	0.13	0.14	2d8/25 L=47	3,19,16
	s=5,m=1	46.9	0.40	10.3	12.3	0.0	0.05	0.15	0.14	0.13	2d8/25 L=47	3,29,13
1082	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.15	0.12	0.11	2d8/25 L=47	3,29,16
	s=5,m=1	46.8	0.40	10.3	12.3	0.0	0.05	0.13	0.17	0.16	2d8/25 L=47	16,29,13
1083	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.13	0.16	0.11	2d8/25 L=47	3,29,13
	s=5,m=1	46.8	0.40	10.3	12.3	0.0	0.08	0.15	0.21	0.19	2d8/25 L=47	16,29,13
1031	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.15	0.18	0.16	2d8/25 L=45	16,29,13
	s=5,m=1	45.0	0.40	10.3	12.3	0.0	0.08	0.15	0.23	0.23	2d8/25 L=45	16,29,13
1023	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.15	0.16	0.20	2d8/25 L=53	16,13,13
	s=5,m=1	52.6	0.40	10.3	12.3	0.0	0.08	0.21	0.22	0.29	2d8/25 L=53	13,3,13
1091	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.23	0.17	0.15	2d8/25 L=53	13,29,13
	s=5,m=1	52.6	0.40	10.3	12.3	0.0	0.08	0.33	0.23	0.24	2d8/25 L=53	13,29,13
1019	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.32	0.26	0.34	2d8/25 L=44	13,13,13
	s=5,m=1	43.7	0.40	10.3	12.3	0.0	0.08	0.20	0.21	0.27	2d8/25 L=44	13,13,13
1033	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.19	0.34	0.46	2d8/25 L=44	13,29,13
	s=5,m=1	43.8	0.40	10.3	12.3	0.0	0.08	0.08	0.29	0.38	2d8/25 L=44	30,29,13
1040	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.09	0.37	0.49	2d8/25 L=44	34,29,29
	s=5,m=1	43.8	0.40	10.3	12.3	0.0	0.08	0.23	0.33	0.42	2d8/25 L=44	32,29,29
1047	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.23	0.40	0.43	2d8/25 L=44	32,29,29
	s=5,m=1	43.8	0.40	10.3	12.3	0.0	0.08	0.36	0.36	0.35	2d8/25 L=44	32,29,29
1029	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.43	0.27	0.26	2d8/25 L=47	32,32,32
	s=5,m=1	46.9	0.40	10.3	12.3	0.0	0.08	0.30	0.22	0.18	2d8/25 L=47	32,32,32
1084	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.26	0.29	0.30	2d8/25 L=47	32,32,32
	s=5,m=1	46.9	0.40	10.3	12.3	0.0	0.08	0.24	0.23	0.22	2d8/25 L=47	29,32,32
1085	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.24	0.25	0.26	2d8/25 L=47	29,32,32
	s=5,m=1	46.9	0.40	10.3	12.3	0.0	0.08	0.21	0.20	0.18	2d8/25 L=47	29,32,32
1086	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.21	0.20	0.21	2d8/25 L=47	29,32,32
	s=5,m=1	46.9	0.40	10.3	12.3	0.0	0.05	0.20	0.18	0.14	2d8/25 L=47	3,29,29
1087	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.20	0.19	0.17	2d8/25 L=47	3,32,32
	s=5,m=1	46.9	0.40	10.3	12.3	0.0	0.05	0.20	0.21	0.17	2d8/25 L=47	3,29,29
1088	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.20	0.20	0.13	2d8/25 L=47	3,29,32
	s=5,m=1	46.9	0.40	10.3	12.3	0.0	0.05	0.18	0.25	0.19	2d8/25 L=47	3,29,29
1089	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.18	0.24	0.14	2d8/25 L=47	3,29,29
	s=5,m=1	46.9	0.40	10.3	12.3	0.0	0.05	0.17	0.29	0.22	2d8/25 L=47	32,29,29
1090	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.16	0.28	0.18	2d8/25 L=47	32,29,29
	s=5,m=1	46.9	0.40	10.3	12.3	0.0	0.08	0.17	0.33	0.25	2d8/25 L=47	32,29,29
1051	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.17	0.31	0.23	2d8/25 L=40	32,29,29
	s=5,m=1	39.6	0.40	10.3	12.3	0.0	0.08	0.18	0.35	0.29	2d8/25 L=40	32,29,29
1046	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.18	0.26	0.26	2d8/25 L=40	29,29,29
	s=5,m=1	39.6	0.40	10.3	12.3	0.0	0.08	0.28	0.30	0.33	2d8/25 L=40	29,29,29
1039	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.32	0.23	0.23	2d8/25 L=71	29,29,29
	s=5,m=1	70.8	0.40	10.3	12.3	0.0	0.08	0.53	0.31	0.41	2d8/25 L=71	29,29,3
1037	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.53	0.47	0.59	2d8/25 L=44	29,29,29
	s=5,m=1	43.7	0.40	10.3	12.3	0.0	0.08	0.28	0.42	0.51	2d8/25 L=44	29,29,29
1044	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.23	0.46	0.62	2d8/25 L=44	29,29,29
	s=5,m=1	43.8	0.40	10.3	12.3	0.0	0.08	0.02	0.41	0.54	2d8/25 L=44	3,29,29
M_T= 39 Z=380.0 N=106 N=117												
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
970	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	5.26e-03	0.06	0.07	2d8/25 L=39	24,44,3
	s=6,m=1	39.3	0.40	10.3	12.3	0.0	0.08	0.01	0.05	0.04	2d8/25 L=39	22,28,3
974	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.01	0.05	0.07	2d8/25 L=39	22,3,3
	s=6,m=1	39.3	0.40	10.3	12.3	0.0	0.08	0.02	0.04	0.04	2d8/25 L=39	22,28,3
972	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.02	0.07	0.08	2d8/25 L=40	22,28,3
	s=6,m=1	40.2	0.40	10.3	12.3	0.0	0.05	0.02	0.04	0.05	2d8/25 L=40	3,25,22
1002	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.02	0.05	0.06	2d8/25 L=40	3,28,3
	s=6,m=1	40.2	0.40	10.3	12.3	0.0	0.05	0.02	0.05	0.05	2d8/25 L=40	24,25,22
992	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.02	0.04	0.04	2d8/25 L=40	24,38,22
	s=6,m=1	40.2	0.40	10.3	12.3	0.0	0.05	0.02	0.05	0.07	2d8/25 L=40	3,39,3
985	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.02	0.06	0.07	2d8/25 L=40	3,22,22
	s=6,m=1	40.2	0.40	10.3	12.3	0.0	0.08	0.02	0.06	0.08	2d8/25 L=40	34,23,23
980	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.02	0.04	0.06	2d8/25 L=40	34,22,3
	s=6,m=1	40.2	0.40	10.3	12.3	0.0	0.08	0.03	0.04	0.05	2d8/25 L=40	22,23,3
977	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.03	0.05	0.07	2d8/25 L=40	22,35,3
	s=6,m=1	40.2	0.40	10.3	12.3	0.0	0.05	0.02	0.04	0.05	2d8/25 L=40	22,34,22
976	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.02	0.04	0.05	2d8/25 L=40	22,23,23
	s=6,m=1	39.7	0.40	10.3	12.3	0.0	0.05	0.02	0.04	0.06	2d8/25 L=40	3,22,22
982	ok,ok	0.0	0.40	10.3	12.3</							

1009	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.02	0.03	0.04	2d8/25 L=40	23,23,23
	s=6,m=1	39.7	0.40	10.3	12.3	0.0	0.08	0.02	0.05	0.07	2d8/25 L=40	23,3,3
1018	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.02	0.04	0.05	2d8/25 L=40	23,22,22
	s=6,m=1	39.7	0.40	10.3	12.3	0.0	0.08	0.01	0.05	0.07	2d8/25 L=40	23,23,3
1028	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.01	0.05	0.08	2d8/25 L=40	23,22,22
	s=6,m=1	39.7	0.40	10.3	12.3	0.0	0.08	0.01	0.06	0.07	2d8/25 L=40	18,23,23
1036	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.01	0.04	0.05	2d8/25 L=40	18,3,3
	s=6,m=1	39.7	0.40	10.3	12.3	0.0	0.08	0.01	0.04	0.06	2d8/25 L=40	30,3,3
1043	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.01	0.04	0.06	2d8/25 L=40	30,23,23
	s=6,m=1	39.7	0.40	10.3	12.3	0.0	0.08	0.01	0.07	0.11	2d8/25 L=40	21,14,22
1050	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.01	0.05	0.07	2d8/25 L=40	21,26,22
	s=6,m=1	39.7	0.40	10.3	12.3	0.0	0.08	0.04	0.10	0.14	2d8/25 L=40	22,26,22
1053	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.04	0.08	0.10	2d8/25 L=40	22,38,44
	s=6,m=1	39.7	0.40	10.3	12.3	0.0	0.08	0.07	0.12	0.18	2d8/25 L=40	3,38,3
1055	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.08	0.17	0.22	2d8/25 L=40	3,44,28
	s=6,m=1	39.7	0.40	10.3	12.3	0.0	0.08	0.15	0.21	0.29	2d8/25 L=40	44,44,28
979	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.16	0.25	0.34	2d8/25 L=44	44,28,28
	s=6,m=1	43.8	0.40	10.3	12.3	0.0	0.08	0.29	0.30	0.41	2d8/25 L=44	28,28,28
994	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.33	0.24	0.30	2d8/25 L=44	28,44,28
	s=6,m=1	43.8	0.40	10.3	12.3	0.0	0.08	0.49	0.29	0.37	2d8/25 L=44	28,44,28
987	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.57	0.32	0.33	2d8/25 L=48	28,44,3
	s=6,m=1	47.7	0.40	10.3	12.3	0.0	0.08	0.43	0.27	0.20	2d8/25 L=48	28,44,28
1183	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.37	0.32	0.33	2d8/25 L=48	28,40,3
	s=6,m=1	47.7	0.40	10.3	12.3	0.0	0.08	0.23	0.26	0.23	2d8/25 L=48	28,40,28
1184	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.20	0.29	0.29	2d8/25 L=48	28,44,28
	s=6,m=1	47.7	0.40	10.3	12.3	0.0	0.08	0.14	0.24	0.21	2d8/25 L=48	25,44,28
1185	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.14	0.25	0.24	2d8/25 L=48	25,44,28
	s=6,m=1	47.7	0.40	10.3	12.3	0.0	0.08	0.13	0.19	0.16	2d8/25 L=48	25,44,28
1186	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.14	0.21	0.21	2d8/25 L=48	25,44,28
	s=6,m=1	47.7	0.40	10.3	12.3	0.0	0.05	0.15	0.15	0.13	2d8/25 L=48	3,44,28
1187	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.15	0.17	0.18	2d8/25 L=48	3,44,28
	s=6,m=1	47.7	0.40	10.3	12.3	0.0	0.05	0.16	0.12	0.12	2d8/25 L=48	3,44,25
1188	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.16	0.15	0.15	2d8/25 L=48	3,44,28
	s=6,m=1	47.7	0.40	10.3	12.3	0.0	0.05	0.16	0.13	0.16	2d8/25 L=48	28,41,25
1189	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.16	0.14	0.12	2d8/25 L=48	3,44,28
	s=6,m=1	47.7	0.40	10.3	12.3	0.0	0.08	0.18	0.17	0.20	2d8/25 L=48	28,41,25
1190	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.18	0.17	0.17	2d8/25 L=48	28,41,25
	s=6,m=1	47.7	0.40	10.3	12.3	0.0	0.08	0.20	0.22	0.25	2d8/25 L=48	28,41,25
1191	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.20	0.20	0.21	2d8/25 L=48	28,41,25
	s=6,m=1	47.7	0.40	10.3	12.3	0.0	0.08	0.23	0.25	0.29	2d8/25 L=48	25,41,25
1192	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.26	0.19	0.16	2d8/25 L=48	25,41,25
	s=6,m=1	47.7	0.40	10.3	12.3	0.0	0.08	0.36	0.24	0.24	2d8/25 L=48	25,41,25
984	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.32	0.35	0.32	2d8/25 L=44	25,41,25
	s=6,m=1	43.8	0.40	10.3	12.3	0.0	0.08	0.20	0.39	0.36	2d8/25 L=44	25,44,28
996	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.20	0.27	0.41	2d8/25 L=44	25,25,25
	s=6,m=1	43.8	0.40	10.3	12.3	0.0	0.08	0.07	0.32	0.46	2d8/25 L=44	3,28,28
1007	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.07	0.26	0.38	2d8/25 L=44	3,28,25
	s=6,m=1	43.8	0.40	10.3	12.3	0.0	0.08	0.18	0.31	0.44	2d8/25 L=44	24,28,28
1016	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.19	0.22	0.27	2d8/25 L=44	24,26,21
	s=6,m=1	43.8	0.40	10.3	12.3	0.0	0.08	0.30	0.24	0.32	2d8/25 L=44	24,24,24
991	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.32	0.24	0.25	2d8/25 L=54	24,36,28
	s=6,m=1	53.7	0.40	10.3	12.3	0.0	0.08	0.22	0.18	0.16	2d8/25 L=54	24,36,28
1226	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.20	0.23	0.28	2d8/25 L=54	24,36,24
	s=6,m=1	53.7	0.40	10.3	12.3	0.0	0.08	0.17	0.17	0.19	2d8/25 L=54	21,36,24
1227	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.17	0.19	0.23	2d8/25 L=54	21,36,24
	s=6,m=1	53.7	0.40	10.3	12.3	0.0	0.08	0.15	0.13	0.14	2d8/25 L=54	25,36,24
1228	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.15	0.17	0.17	2d8/25 L=54	25,36,24
	s=6,m=1	53.7	0.40	10.3	12.3	0.0	0.05	0.15	0.11	0.10	2d8/25 L=54	3,36,21
1005	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.15	0.17	0.13	2d8/25 L=52	3,32,24
	s=6,m=1	51.7	0.40	10.3	12.3	0.0	0.05	0.15	0.15	0.13	2d8/25 L=52	3,34,21
1218	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.15	0.13	0.10	2d8/25 L=52	3,36,24
	s=6,m=1	51.7	0.40	10.3	12.3	0.0	0.05	0.13	0.16	0.17	2d8/25 L=52	3,22,21
1219	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.13	0.13	0.12	2d8/25 L=52	3,22,21
	s=6,m=1	51.7	0.40	10.3	12.3	0.0	0.08	0.13	0.18	0.21	2d8/25 L=52	24,22,21
1220	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.13	0.15	0.18	2d8/25 L=52	24,22,21
	s=6,m=1	51.7	0.40	10.3	12.3	0.0	0.08	0.14	0.21	0.26	2d8/25 L=52	21,22,21
1221	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.15	0.17	0.22	2d8/25 L=52	25,25,21
	s=6,m=1	51.7	0.40	10.3	12.3	0.0	0.08	0.28	0.23	0.31	2d8/25 L=52	25,3,3
1222	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.32	0.14	0.15	2d8/25 L=52	25,25,21
	s=6,m=1	51.7	0.40	10.3	12.3	0.0	0.08	0.43	0.20	0.25	2d8/25 L=52	25,25,3
1001	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.38	0.26	0.36	2d8/25 L=44	21,21,21
	s=6,m=1	43.8	0.40	10.3	12.3	0.0	0.08	0.25	0.22	0.29	2d8/25 L=44	25,21,21
1022	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.25	0.41	0.57	2d8/25 L=44	25,21,21
	s=6,m=1	43.8	0.40	10.3	12.3	0.0	0.08	0.11	0.36	0.49	2d8/25 L=44	3,21,21
1013	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.10	0.36	0.45	2d8/25 L=44	3,23,23
	s=6,m=1	43.8	0.40	10.3	12.3	0.0	0.08	0.21	0.41	0.53	2d8/25 L=44	23,23,23
1025	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.22	0.31	0.28	2d8/25 L=44	23,35,22
	s=6,m=1	43.8	0.40	10.3	12.3	0.0	0.08	0.35	0.36	0.33	2d8/25 L=44	23,35,23
1011	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.40	0.27	0.23	2d8/25 L=48	23,35,3
	s=6,m=1	47.7	0.40	10.3	12.3	0.0	0.08	0.31	0.22	0.13	2d8/25 L=48	23,35,23
1193	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.27	0.27	0.29	2d8/25 L=48	23,35,3
	s=6,m=1	47.7	0.40	10.3	12.3	0.0	0.08	0.16	0.21	0.20	2d8/25 L=48	23,35,23
1194	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.14	0.21	0.25	2d8/25 L=48	23,23,23
	s=6,m=1	47.7	0.40	10.3	12.3	0.0	0.08	0.14	0.16	0.17	2d8/25 L=48	22,23,23
1195	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.14	0.18	0.20	2d8/25 L=48	22,23,23
	s=6,m=1	47.7	0.40	10.3	12.3	0.0	0.05	0.13	0.12	0.12	2d8/25 L=48	3,23,23
1196	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.13	0.14	0.16	2d8/25 L=48	22,23,23
	s=6,m=1	47.7	0.40	10.3	12.3	0.0	0.05	0.15	0.10	0.10	2d8/25 L=48	3,34,22
1197	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.14	0.12	0.13	2d8/25 L=48	3,28,23
	s=6,m=1	47.7	0.40	10.3	12.3	0.0	0.05	0.15	0.10	0.13	2d8/25 L=48	3,34,22
1198	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.15	0.10	0.10	2d8/25 L=48	3,28,23
	s=6,m=1	47.7	0.40	10.3	12.3	0.0	0.05	0.13	0.14	0.16	2d8/25 L=48	23,34,22
1199	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.13	0.13	0.12	2d8/25 L=48	23,30,22
	s=6,m=1	47.7	0.40	10.3	12.3	0.0	0.08	0.14	0.18	0.20	2d8/25 L=48	23,30,22
1200	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.14	0.19	0.17	2d8/25 L=48	23,30,22
	s=6,m=1	47.7	0.40	10.3	12.3	0.0	0.08	0.14	0.24	0.25	2d8/25 L=48	23,30,22
1201	ok,ok	0.0	0.4									

1034	s=6,m=1	43.7	0.40	10.3	12.3	0.0	0.08	0.21	0.25	0.26	2d8/25 L=44	22,34,22
	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.19	0.39	0.44	2d8/25 L=44	22,34,22
	s=6,m=1	43.8	0.40	10.3	12.3	0.0	0.08	0.09	0.35	0.37	2d8/25 L=44	33,34,22
1041	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.09	0.38	0.50	2d8/25 L=44	29,34,34
	s=6,m=1	43.8	0.40	10.3	12.3	0.0	0.08	0.24	0.33	0.43	2d8/25 L=44	35,34,34
1048	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.25	0.47	0.43	2d8/25 L=44	35,34,34
	s=6,m=1	43.8	0.40	10.3	12.3	0.0	0.08	0.39	0.42	0.36	2d8/25 L=44	35,34,34
1030	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.46	0.31	0.26	2d8/25 L=48	35,31,35
	s=6,m=1	47.7	0.40	10.3	12.3	0.0	0.08	0.33	0.25	0.18	2d8/25 L=48	35,31,35
1203	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.28	0.32	0.31	2d8/25 L=48	35,35,35
	s=6,m=1	47.7	0.40	10.3	12.3	0.0	0.08	0.23	0.27	0.23	2d8/25 L=48	34,35,35
1204	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.23	0.28	0.26	2d8/25 L=48	34,35,35
	s=6,m=1	47.7	0.40	10.3	12.3	0.0	0.08	0.20	0.23	0.18	2d8/25 L=48	34,35,35
1205	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.21	0.23	0.21	2d8/25 L=48	34,35,35
	s=6,m=1	47.7	0.40	10.3	12.3	0.0	0.05	0.20	0.19	0.14	2d8/25 L=48	3,34,34
1206	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.19	0.19	0.17	2d8/25 L=48	3,35,35
	s=6,m=1	47.7	0.40	10.3	12.3	0.0	0.05	0.19	0.20	0.17	2d8/25 L=48	3,34,34
1207	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.20	0.16	0.14	2d8/25 L=48	3,34,35
	s=6,m=1	47.7	0.40	10.3	12.3	0.0	0.05	0.17	0.21	0.20	2d8/25 L=48	3,34,34
1208	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.18	0.21	0.15	2d8/25 L=48	3,34,34
	s=6,m=1	47.7	0.40	10.3	12.3	0.0	0.05	0.17	0.26	0.23	2d8/25 L=48	35,34,34
1209	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.17	0.26	0.18	2d8/25 L=48	35,34,34
	s=6,m=1	47.7	0.40	10.3	12.3	0.0	0.08	0.18	0.31	0.26	2d8/25 L=48	35,34,34
1210	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.18	0.32	0.23	2d8/25 L=48	35,34,34
	s=6,m=1	47.7	0.40	10.3	12.3	0.0	0.08	0.20	0.37	0.31	2d8/25 L=48	34,34,34
1211	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.23	0.36	0.27	2d8/25 L=48	34,34,34
	s=6,m=1	47.7	0.40	10.3	12.3	0.0	0.08	0.38	0.41	0.36	2d8/25 L=48	34,34,3
1212	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.43	0.36	0.25	2d8/25 L=48	34,34,3
	s=6,m=1	47.7	0.40	10.3	12.3	0.0	0.08	0.59	0.41	0.39	2d8/25 L=48	34,34,3
1038	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.54	0.57	0.59	2d8/25 L=44	34,34,34
	s=6,m=1	43.7	0.40	10.3	12.3	0.0	0.08	0.28	0.52	0.52	2d8/25 L=44	34,34,34
1045	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.24	0.50	0.63	2d8/25 L=44	34,34,34
	s=6,m=1	43.8	0.40	10.3	12.3	0.0	0.08	0.02	0.45	0.55	2d8/25 L=44	3,34,34
M_T= 14 Z=760.0 N=5962 N=5963												
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T	cls	V V/T acc	Staffe
699	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.01	0.04		0.03	2d8/25 L=38
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	0.01	0.05		0.03	2d8/25 L=38
750	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.01	0.03	9.63e-03		2d8/25 L=38
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	9.00e-03	0.03	8.70e-03		2d8/25 L=38
798	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	9.08e-03	0.03	8.60e-03		2d8/25 L=38
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	5.95e-03	0.02	7.41e-03		2d8/25 L=38
828	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	5.97e-03	0.02	8.64e-03		2d8/25 L=38
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	7.41e-03	0.02	5.66e-03		2d8/25 L=38
857	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	7.48e-03	0.02	0.01		2d8/25 L=38
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	0.02	0.02	7.81e-03		2d8/25 L=38
881	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.02	0.02	0.02		2d8/25 L=38
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	0.03	0.01	0.01		2d8/25 L=38
903	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.03	0.02	0.01		2d8/25 L=38
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	0.04	0.01	3.41e-03		2d8/25 L=38
923	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.04	0.01	0.01		2d8/25 L=38
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	0.03	0.01	0.02		2d8/25 L=38
936	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.03	0.02	0.02		2d8/25 L=38
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	4.03e-03	0.02	0.03		2d8/25 L=38
949	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	4.14e-03	0.02	0.02		2d8/25 L=38
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	0.02	0.03	0.03		2d8/25 L=38
961	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.03	0.01	0.01		2d8/25 L=38
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	0.04	0.02	0.02		2d8/25 L=38
341	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.04	9.76e-03	7.01e-03		2d8/25 L=38
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	0.04	8.65e-03	9.23e-03		2d8/25 L=38
487	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.04	0.03	0.02		2d8/25 L=38
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	0.02	0.02	0.01		2d8/25 L=38
539	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.02	0.03	0.01		2d8/25 L=38
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	0.01	0.02	8.29e-03		2d8/25 L=38
587	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.01	0.04	6.70e-03		2d8/25 L=38
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	0.01	0.04	6.71e-03		2d8/25 L=38
339	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.01	0.07	7.19e-03		2d8/25 L=38
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	0.01	0.07	3.16e-03		2d8/25 L=38
490	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.01	0.20	0.07		2d8/25 L=38
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	0.06	0.20	0.06		2d8/25 L=38
555	ok,ok	0.0	0.45	4.0	4.0	4.0	0.14	0.06	0.25	0.92		2d8/25 L=15
	s=3,m=1	14.8	0.45	4.0	4.0	4.0	0.14	0.06	0.25	0.92		2d8/25 L=15
729	ok,ok	0.0	0.45	4.0	4.0	4.0	0.14	0.04	0.23	0.82		2d8/25 L=23
	s=3,m=1	23.5	0.45	4.0	4.0	4.0	0.14	0.03	0.23	0.84		2d8/25 L=23
764	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.03	0.15	0.04		2d8/25 L=38
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	0.01	0.16	0.05		2d8/25 L=38
805	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.01	0.06	5.73e-03		2d8/25 L=38
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	0.01	0.06	5.09e-03		2d8/25 L=38
831	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.01	0.04	6.99e-03		2d8/25 L=38
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	0.01	0.04	5.59e-03		2d8/25 L=38
859	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.01	0.02	7.69e-03		2d8/25 L=38
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	0.02	0.02	0.01		2d8/25 L=38
883	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.02	0.02	0.01		2d8/25 L=38
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	0.04	0.02	0.02		2d8/25 L=38
905	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.04	0.03	0.03		2d8/25 L=38
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	0.08	0.03	0.04		2d8/25 L=38
715	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.08	0.03	0.03		2d8/25 L=54
	s=3,m=1	54.5	0.45	4.0	4.0	0.0	0.14	0.12	0.03	0.03		2d8/25 L=54
756	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.14	0.04	0.02		2d8/25 L=40
	s=3,m=1	40.2	0.45	4.0	4.0	0.0	0.14	0.12	0.04	0.01		2d8/25 L=40
1062	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.10	0.06	0.05		2d8/25 L=40
	s=3,m=1	40.2	0.45	4.0	4.0	0.0	0.14	0.04	0.06	0.04		2d8/25 L=40
1063	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.03	0.06	0.04		2d8/25 L=40
	s=3,m=1	40.2	0.45	4.0	4.0	0.0	0.14	9.48e-03	0.06	0.03		2d8/25 L=40
1064	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	9.59e-03	0.05	0.04		2d8/25 L=40
	s=3,m=1	40.2	0.45	4.0	4.0	0.0	0.14	0.04	0.04	0.03		2d8/25 L=40
1065	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.04	0.06	0.04		2d8/25 L=40
	s=3,m=1	40.2	0.45	4.0	4.0	0.0	0.14	0.07	0.05	0.04		2d8/25 L=40
1066	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.07	0.08	0.05		2d8/25 L=40
	s=3,m=1	40.2	0.45	4.0	4.0	0.0	0.14	0.10	0.08	0.04		2d8/25 L=40
800	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.11	0.20	0.07		2d8/25 L=54
	s=3,m=1	54.5	0.45	4.0	4.0	0.0	0.14	0.06	0.21	0.07		2d8/25 L=54

739	ok,ok	0.0	0.45	4.0	4.0	4.0	0.14	0.07	0.22	0.62	2d8/25 L=38	4,23,4
	s=3,m=1	38.3	0.45	4.0	4.0	4.0	0.14	0.06	0.23	0.65	2d8/25 L=38	44,23,4
431	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.06	0.13	0.07	2d8/25 L=38	44,4,44
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	0.02	0.13	0.07	2d8/25 L=38	39,4,44
594	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.02	0.05	0.01	2d8/25 L=38	39,4,41
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	0.01	0.05	0.01	2d8/25 L=38	3,4,44
550	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.01	0.04	9.10e-03	2d8/25 L=38	3,4,3
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	8.91e-03	0.03	3.11e-03	2d8/25 L=38	3,4,18
462	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	8.96e-03	0.03	7.31e-03	2d8/25 L=38	3,4,3
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	6.56e-03	0.02	3.16e-03	2d8/25 L=38	3,4,2
600	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	6.58e-03	0.02	6.18e-03	2d8/25 L=38	3,4,3
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	5.33e-03	0.01	3.98e-03	2d8/25 L=38	3,4,2
573	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	5.32e-03	0.01	5.87e-03	2d8/25 L=38	3,21,4
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	4.40e-03	0.01	4.28e-03	2d8/25 L=38	3,21,1
512	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	4.37e-03	9.69e-03	5.59e-03	2d8/25 L=38	3,21,3
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	3.74e-03	9.42e-03	4.44e-03	2d8/25 L=38	3,21,2
396	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	3.73e-03	0.01	5.56e-03	2d8/25 L=38	3,25,1
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	3.52e-03	0.01	4.50e-03	2d8/25 L=38	39,25,4
601	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	3.52e-03	0.01	5.32e-03	2d8/25 L=38	39,44,4
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	3.08e-03	0.01	4.85e-03	2d8/25 L=38	19,44,1
562	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	3.07e-03	9.05e-03	5.76e-03	2d8/25 L=38	19,27,4
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	2.46e-03	8.18e-03	4.43e-03	2d8/25 L=38	15,27,1
517	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	2.43e-03	0.01	5.75e-03	2d8/25 L=38	15,42,3
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	2.22e-03	0.01	4.29e-03	2d8/25 L=38	39,26,2
381	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	2.23e-03	0.01	3.58e-03	2d8/25 L=38	39,25,25
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	3.61e-03	0.01	7.07e-03	2d8/25 L=38	15,44,3
964	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	3.85e-03	0.02	4.43e-03	2d8/25 L=38	23,44,2
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	4.51e-03	0.02	5.65e-03	2d8/25 L=38	23,44,3
954	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	4.27e-03	0.02	6.45e-03	2d8/25 L=38	23,44,3
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	2.91e-03	0.02	3.94e-03	2d8/25 L=38	19,44,25
941	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	2.90e-03	8.42e-03	5.09e-03	2d8/25 L=38	19,38,1
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	2.91e-03	8.12e-03	4.85e-03	2d8/25 L=38	19,42,4
928	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	2.90e-03	9.25e-03	4.98e-03	2d8/25 L=38	19,22,2
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	2.98e-03	9.16e-03	4.97e-03	2d8/25 L=38	19,22,3
910	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	2.97e-03	0.01	4.91e-03	2d8/25 L=38	19,22,2
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	3.10e-03	0.01	5.04e-03	2d8/25 L=38	19,22,3
889	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	3.08e-03	0.02	4.84e-03	2d8/25 L=38	19,22,2
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	3.25e-03	0.02	5.12e-03	2d8/25 L=38	19,22,3
867	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	3.22e-03	0.02	4.89e-03	2d8/25 L=38	19,22,3
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	3.32e-03	0.02	5.05e-03	2d8/25 L=38	39,22,2
841	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	3.29e-03	0.02	4.59e-03	2d8/25 L=38	39,22,1
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	3.62e-03	0.02	5.35e-03	2d8/25 L=38	39,22,4
816	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	3.59e-03	0.03	4.81e-03	2d8/25 L=38	39,21,23
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	4.27e-03	0.03	5.85e-03	2d8/25 L=38	25,21,22
791	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	4.25e-03	0.03	7.11e-03	2d8/25 L=38	25,21,3
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	3.89e-03	0.03	4.78e-03	2d8/25 L=38	22,21,18
771	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	3.86e-03	0.06	0.03	2d8/25 L=38	22,25,25
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	0.02	0.05	0.03	2d8/25 L=38	25,25,25
M_T= 25 Z=600.0 N=5973 N=6009												
Trave	Note	Pos.	%Af	Af inf.	Af sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
709	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.07	0.09	0.07	2d8/25 L=38	3,38,3
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	7.07e-03	0.10	0.08	2d8/25 L=38	19,38,3
753	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	7.21e-03	0.04	4.84e-03	2d8/25 L=38	19,3,16
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	8.41e-03	0.05	0.01	2d8/25 L=38	18,3,3
799	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	8.49e-03	0.03	6.63e-03	2d8/25 L=38	18,3,18
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	6.90e-03	0.03	6.48e-03	2d8/25 L=38	3,3,19
829	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	7.16e-03	0.04	5.68e-03	2d8/25 L=38	3,3,4
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	6.47e-03	0.04	4.34e-03	2d8/25 L=38	3,3,1
858	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	6.51e-03	0.04	5.40e-03	2d8/25 L=38	3,43,4
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	6.09e-03	0.04	4.61e-03	2d8/25 L=38	3,43,1
882	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	6.24e-03	0.04	5.38e-03	2d8/25 L=31	3,31,3
	s=3,m=1	31.3	0.45	4.0	4.0	0.0	0.14	5.15e-03	0.04	2.96e-03	2d8/25 L=31	3,31,2
904	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	5.03e-03	0.03	6.61e-03	2d8/25 L=45	3,31,3
	s=3,m=1	45.3	0.45	4.0	4.0	0.0	0.14	4.19e-03	0.03	5.29e-03	2d8/25 L=45	40,35,2
924	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	4.21e-03	0.01	5.16e-03	2d8/25 L=38	3,23,3
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	4.01e-03	0.01	4.81e-03	2d8/25 L=38	3,23,2
937	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	4.05e-03	0.02	4.95e-03	2d8/25 L=38	3,15,2
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	4.08e-03	0.02	4.99e-03	2d8/25 L=38	3,15,3
950	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	4.10e-03	0.02	5.14e-03	2d8/25 L=38	3,15,3
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	3.92e-03	0.02	4.81e-03	2d8/25 L=38	3,15,2
962	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	3.93e-03	0.02	4.72e-03	2d8/25 L=38	3,20,4
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	4.20e-03	0.02	5.24e-03	2d8/25 L=38	3,20,1
357	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	4.28e-03	0.03	2.93e-03	2d8/25 L=22	3,15,1
	s=3,m=1	21.8	0.45	4.0	4.0	0.0	0.14	4.23e-03	0.03	2.75e-03	2d8/25 L=22	3,15,4
496	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	4.24e-03	0.02	6.58e-03	2d8/25 L=55	3,16,2
	s=3,m=1	54.8	0.45	4.0	4.0	0.0	0.14	5.15e-03	0.02	7.72e-03	2d8/25 L=55	3,16,3
542	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	5.22e-03	0.03	4.65e-03	2d8/25 L=38	3,16,1
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	5.70e-03	0.03	5.45e-03	2d8/25 L=38	3,16,4
589	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	5.78e-03	0.03	4.06e-03	2d8/25 L=38	3,20,2
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	7.00e-03	0.03	6.11e-03	2d8/25 L=38	3,15,3
355	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	7.03e-03	0.03	2.96e-03	2d8/25 L=38	3,15,21
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	0.01	0.03	8.34e-03	2d8/25 L=38	3,15,3
503	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.01	0.05	0.01	2d8/25 L=38	3,29,23
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	0.03	0.05	0.02	2d8/25 L=38	23,29,23
558	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.03	0.08	0.03	2d8/25 L=15	23,35,35
	s=3,m=1	14.8	0.45	4.0	4.0	0.0	0.14	0.04	0.08	0.03	2d8/25 L=15	35,35,35
734	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.02	0.17	0.02	2d8/25 L=23	38,37,18
	s=3,m=1	23.5	0.45	4.0	4.0	0.0	0.14	0.01	0.17	0.03	2d8/25 L=23	39,37,18
766	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.01	0.05	5.81e-03	2d8/25 L=38	39,20,19
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	0.01	0.05	0.01	2d8/25 L=38	3,28,18
807	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.01	0.08	3.26e-03	2d8/25 L=38	3,20,44
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	0.01	0.09	7.15e-03	2d8/25 L=38	3,20,3
833	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.01	0.11	1.29e-03	2d8/25 L=38	3,16,39
	s=3,m=1	38.3	0.45									

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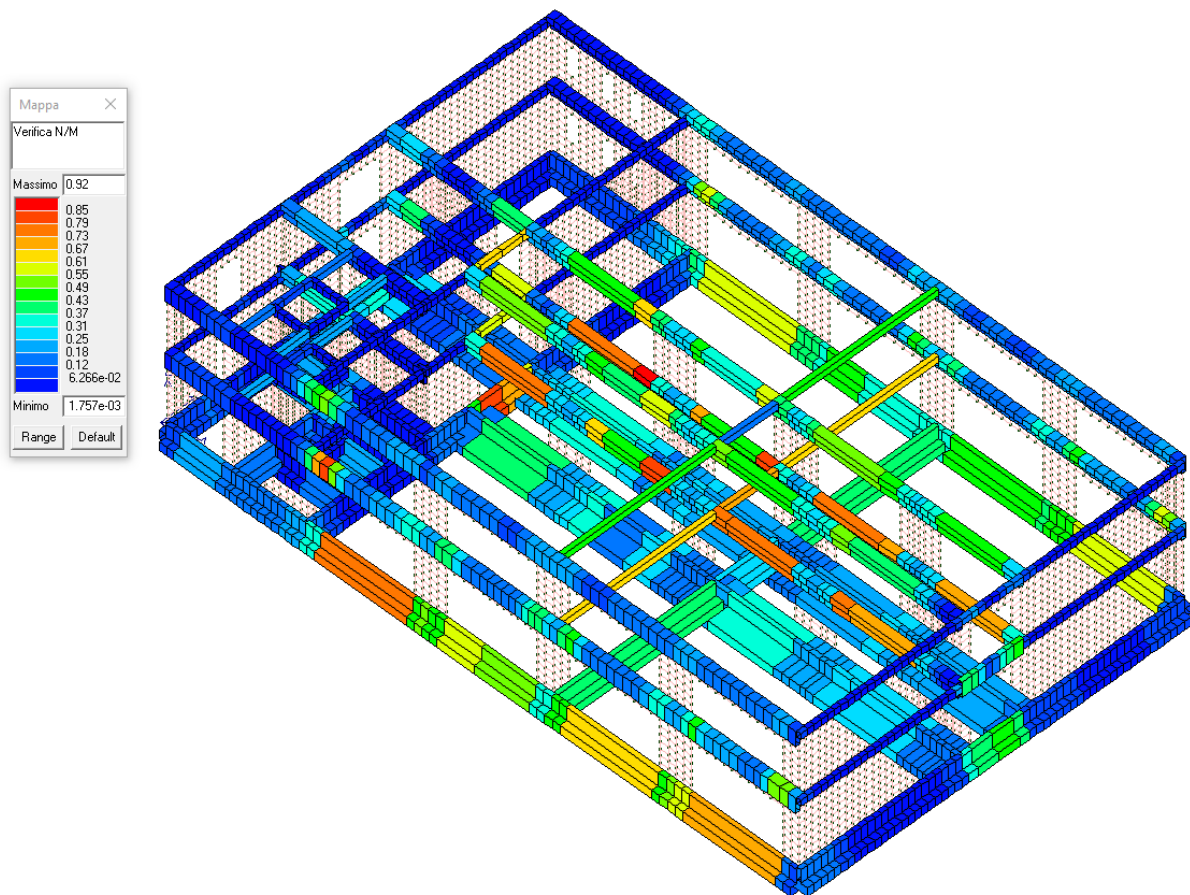
574	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.02	0.04	0.02	2d8/25 L=38	32,35,35
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	0.04	0.04	0.03	2d8/25 L=38	32,35,34
423	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.05	0.09	0.05	2d8/25 L=38	32,35,35
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	0.11	0.08	0.05	2d8/25 L=38	34,34,34
717	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.11	0.08	0.05	2d8/25 L=54	34,29,29
	s=3,m=1	54.5	0.45	4.0	4.0	0.0	0.14	0.17	0.07	0.04	2d8/25 L=54	32,29,32
784	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.19	0.04	0.03	2d8/25 L=40	32,14,32
	s=3,m=1	40.2	0.45	4.0	4.0	0.0	0.14	0.15	0.04	0.02	2d8/25 L=40	32,13,32
1151	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.12	0.06	0.06	2d8/25 L=40	32,30,36
	s=3,m=1	40.2	0.45	4.0	4.0	0.0	0.14	0.05	0.05	0.05	2d8/25 L=40	32,13,36
1152	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.05	0.06	0.05	2d8/25 L=40	33,30,36
	s=3,m=1	40.2	0.45	4.0	4.0	0.0	0.14	0.01	0.06	0.04	2d8/25 L=40	3,13,33
757	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.01	0.06	0.05	2d8/25 L=40	3,34,36
	s=3,m=1	40.2	0.45	4.0	4.0	0.0	0.14	0.06	0.06	0.05	2d8/25 L=40	36,34,33
1149	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.05	0.08	0.05	2d8/25 L=40	36,30,32
	s=3,m=1	40.2	0.45	4.0	4.0	0.0	0.14	0.11	0.07	0.06	2d8/25 L=40	29,30,29
1150	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.13	0.12	0.05	2d8/25 L=40	29,14,36
	s=3,m=1	40.2	0.45	4.0	4.0	0.0	0.14	0.18	0.11	0.04	2d8/25 L=40	29,14,36
801	ok,ok	0.0	0.45	4.0	4.0	4.0	0.14	0.16	0.28	0.88	2d8/25 L=54	29,29,4
	s=3,m=1	54.5	0.45	4.0	4.0	4.0	0.14	0.08	0.27	0.84	2d8/25 L=54	4,29,4
741	ok,ok	0.0	0.45	4.0	4.0	4.0	0.14	0.08	0.32	0.94	2d8/20 L=38	4,4,4
	s=3,m=1	38.3	0.45	4.0	4.0	4.0	0.14	0.07	0.32	0.96	2d8/20 L=38	34,4,4
455	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.07	0.20	0.07	2d8/25 L=38	34,4,34
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	0.03	0.21	0.08	2d8/25 L=38	29,4,34
379	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.03	0.10	0.02	2d8/25 L=38	29,4,29
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	0.02	0.10	0.01	2d8/25 L=38	3,4,32
556	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.02	0.07	0.01	2d8/25 L=38	3,4,3
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	0.01	0.06	2.57e-03	2d8/25 L=38	3,4,32
491	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.01	0.05	8.15e-03	2d8/25 L=38	3,4,3
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	0.01	0.05	2.48e-03	2d8/25 L=38	3,4,2
608	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.01	0.03	6.91e-03	2d8/25 L=38	3,4,3
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	8.46e-03	0.02	3.46e-03	2d8/25 L=38	3,4,2
580	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	8.30e-03	0.02	6.35e-03	2d8/25 L=38	3,4,4
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	6.81e-03	0.02	3.95e-03	2d8/25 L=38	3,4,1
541	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	6.78e-03	0.01	5.59e-03	2d8/25 L=38	3,35,3
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	6.10e-03	0.01	4.44e-03	2d8/25 L=38	3,35,2
451	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	6.06e-03	0.01	5.45e-03	2d8/25 L=38	3,35,3
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	5.54e-03	0.01	4.55e-03	2d8/25 L=38	3,35,2
609	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	5.50e-03	0.01	5.40e-03	2d8/25 L=38	3,34,3
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	5.04e-03	0.01	4.61e-03	2d8/25 L=38	3,34,2
576	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	5.01e-03	0.01	5.38e-03	2d8/25 L=38	3,34,3
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	4.57e-03	0.01	4.63e-03	2d8/25 L=38	3,34,2
520	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	4.53e-03	0.01	5.16e-03	2d8/25 L=38	3,35,3
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	4.32e-03	0.01	4.80e-03	2d8/25 L=38	3,35,2
413	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	4.32e-03	0.02	4.95e-03	2d8/25 L=38	3,34,2
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	4.34e-03	0.02	4.99e-03	2d8/25 L=38	3,34,3
965	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	4.33e-03	0.02	4.96e-03	2d8/25 L=38	3,34,2
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	4.34e-03	0.02	4.98e-03	2d8/25 L=38	3,34,3
955	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	4.32e-03	0.03	4.98e-03	2d8/25 L=38	3,34,3
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	4.30e-03	0.02	4.95e-03	2d8/25 L=38	3,34,2
942	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	4.28e-03	0.03	5.09e-03	2d8/25 L=38	3,34,3
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	4.82e-03	0.03	4.87e-03	2d8/25 L=38	29,34,2
929	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	4.82e-03	0.04	5.27e-03	2d8/25 L=38	29,36,3
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	5.50e-03	0.04	4.74e-03	2d8/25 L=38	29,36,2
911	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	5.51e-03	0.06	4.39e-03	2d8/25 L=38	29,34,33
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	5.03e-03	0.07	6.19e-03	2d8/25 L=38	29,30,3
890	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	5.24e-03	0.08	5.47e-03	2d8/25 L=38	3,34,3
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	5.02e-03	0.07	4.63e-03	2d8/25 L=38	37,34,2
868	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	4.98e-03	0.11	0.01	2d8/25 L=38	37,34,34
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	6.75e-03	0.11	5.72e-03	2d8/25 L=38	35,34,35
842	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	6.69e-03	0.10	0.02	2d8/25 L=38	35,34,34
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	0.02	0.09	8.43e-03	2d8/25 L=38	34,34,34
817	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.02	0.11	0.03	2d8/25 L=38	34,30,34
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	0.04	0.11	0.02	2d8/25 L=38	34,30,34
793	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.04	0.12	0.03	2d8/25 L=38	34,3,3
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	0.06	0.12	0.02	2d8/25 L=38	34,3,22
773	ok,ok	0.0	0.45	4.0	4.0	0.0	0.14	0.06	0.17	0.16	2d8/25 L=38	34,35,34
	s=3,m=1	38.3	0.45	4.0	4.0	0.0	0.14	0.09	0.17	0.16	2d8/25 L=38	34,3,34
M_T=27 Z=760.0 N=5965 N=5992												
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
702	ok,ok	0.0	0.37	10.3	11.2	0.0	0.08	0.06	0.25	0.19	2d8/12 L=78	19,4,4
	s=4,m=1	78.5	0.37	10.3	11.2	0.0	0.06	0.16	0.14	0.10	2d8/12 L=78	4,19,19
718	ok,ok	0.0	0.37	10.3	11.2	0.0	0.06	0.16	0.13	0.09	2d8/12 L=7	4,19,19
	s=4,m=1	120.5	0.37	10.3	11.2	0.0	0.06	0.23	0.10	0.16	2d8/25 L=147	19,18,18
		241.0	0.37	10.3	11.2	0.0	0.08	0.24	0.28	0.21	2d8/12 L=86	18,3,3
742	ok,ok	0.0	0.37	10.3	11.2	0.0	0.08	0.24	0.11	0.15	2d8/25 L=53	18,19,19
	s=4,m=1	53.5	0.37	10.3	11.2	0.0	0.08	0.20	0.17	0.24	2d8/25 L=53	18,19,19
774	ok,ok	0.0	0.37	10.3	11.2	0.0	0.08	0.11	0.06	0.06	2d8/25 L=26	18,19,19
	s=4,m=1	25.8	0.37	10.3	11.2	0.0	0.08	0.10	0.08	0.08	2d8/25 L=26	18,19,19
465	ok,ok	0.0	0.37	10.3	11.2	0.0	0.08	0.10	0.10	0.14	2d8/25 L=40	18,18,18
	s=4,m=1	39.7	0.37	10.3	11.2	0.0	0.08	0.06	0.07	0.10	2d8/25 L=40	18,18,18
476	ok,ok	0.0	0.37	10.3	11.2	0.0	0.08	0.06	0.08	0.10	2d8/25 L=40	18,38,18
	s=4,m=1	39.7	0.37	10.3	11.2	0.0	0.08	0.04	0.05	0.07	2d8/25 L=40	3,38,18
480	ok,ok	0.0	0.37	10.3	11.2	0.0	0.08	0.04	0.06	0.07	2d8/25 L=40	3,18,3
	s=4,m=1	39.7	0.37	10.3	11.2	0.0	0.08	0.02	0.03	0.03	2d8/25 L=40	3,18,18
495	ok,ok	0.0	0.37	10.3	11.2	0.0	0.08	0.02	0.06	0.08	2d8/25 L=55	3,3,3
	s=4,m=1	55.2	0.37	10.3	11.2	0.0	0.08	8.38e-03	0.02	0.01	2d8/25 L=55	32,24,36
516	ok,ok	0.0	0.37	10.3	11.2	0.0	0.08	0.02	0.07	0.05	2d8/25 L=24	23,44,3
	s=4,m=1	24.2	0.37	10.3	11.2	0.0	0.08	0.01	0.05	0.01	2d8/25 L=24	23,44,21
519	ok,ok	0.0	0.37	10.3	11.2	0.0	0.08	0.01	0.08	0.08	2d8/25 L=40	23,44,3
	s=4,m=1	39.7	0.37	10.3	11.2	0.0	0.08	5.32e-03	0.05	0.02	2d8/25 L=40	18,44,22
527	ok,ok	0.0	0.37	10.3	11.2	0.0	0.08	5.29e-03	0.07	0.06	2d8/25 L=40	18,44,3
	s=4,m=1	39.7	0.37	10.3	11.2	0.0	0.08	7.96e-03	0.05	0.03	2d8/25 L=40	18,44,4
534	ok,ok	0.0	0.37	10.3	11.2	0.0	0.08	7.96e-03	0.06	0.06	2d8/25 L=40	18,44,3
	s=4,m=1	39.7	0.37	10.3	11.2	0.0	0.06	9.58e-03	0.06	0.04	2d8/25 L=40	13,44,4
538	ok,ok	0.0	0.37	10.3	11.2	0.0	0.06	9.54e-03	0.05	0.05	2d8/25 L=40	13,3,3

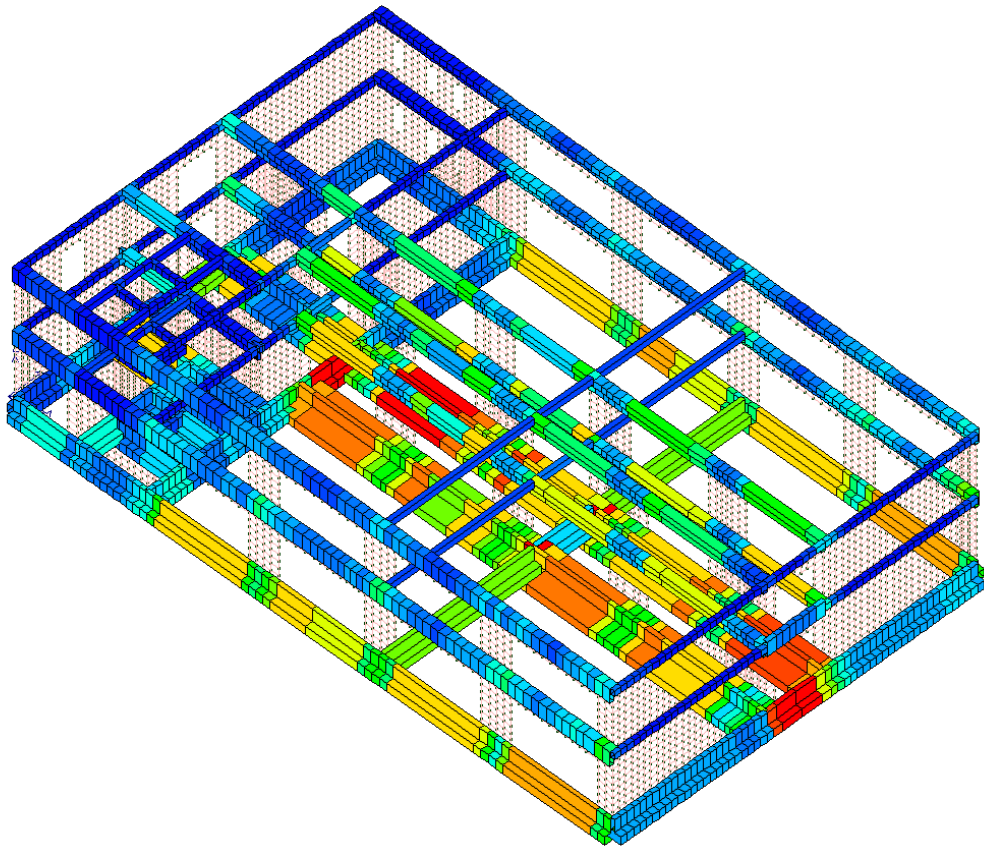
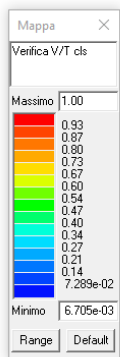
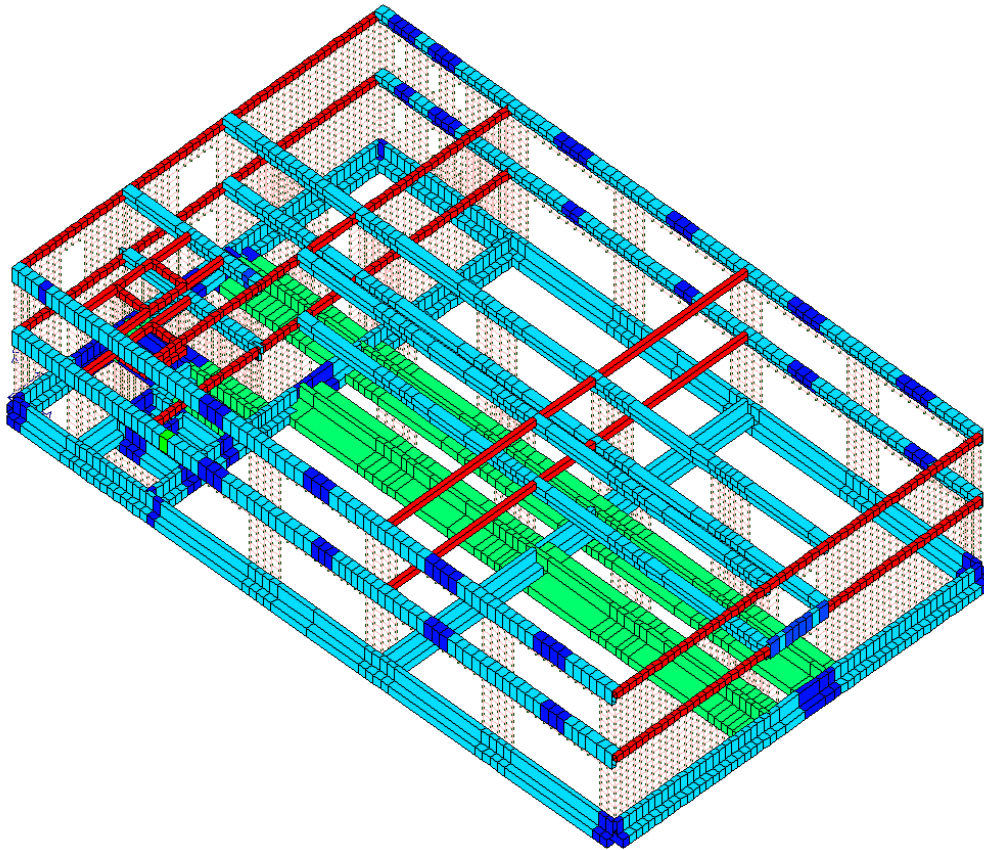
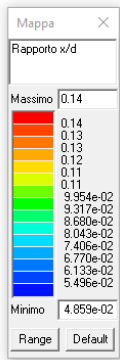
698	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	1.75e-03	0.05	0.06	2d8/25 L=39	3,25,3
	s=6,m=1	39.3	0.40	10.3	12.3	0.0	0.08	8.24e-03	0.03	0.03	2d8/25 L=39	22,39,23
728	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	8.19e-03	0.05	0.06	2d8/25 L=39	22,3,3
	s=6,m=1	39.3	0.40	10.3	12.3	0.0	0.05	0.01	0.03	0.02	2d8/25 L=39	22,41,3
714	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.01	0.05	0.08	2d8/25 L=40	22,3,3
	s=6,m=1	40.2	0.40	10.3	12.3	0.0	0.05	0.02	0.03	0.03	2d8/25 L=40	3,25,22
866	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.02	0.04	0.06	2d8/25 L=40	3,27,3
	s=6,m=1	40.2	0.40	10.3	12.3	0.0	0.05	0.03	0.03	0.04	2d8/25 L=40	3,41,21
839	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.03	0.04	0.04	2d8/25 L=40	3,38,22
	s=6,m=1	40.2	0.40	10.3	12.3	0.0	0.05	0.02	0.04	0.05	2d8/25 L=40	3,27,3
814	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.02	0.04	0.05	2d8/25 L=40	3,30,22
	s=6,m=1	40.2	0.40	10.3	12.3	0.0	0.05	0.02	0.06	0.06	2d8/25 L=40	14,23,23
782	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.02	0.03	0.05	2d8/25 L=40	14,3,3
	s=6,m=1	40.2	0.40	10.3	12.3	0.0	0.08	0.03	0.03	0.04	2d8/25 L=40	22,23,3
755	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.03	0.04	0.05	2d8/25 L=40	22,23,3
	s=6,m=1	40.2	0.40	10.3	12.3	0.0	0.05	0.02	0.03	0.04	2d8/25 L=40	14,22,22
738	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.02	0.03	0.05	2d8/25 L=40	14,23,23
	s=6,m=1	39.7	0.40	10.3	12.3	0.0	0.05	0.02	0.04	0.05	2d8/25 L=40	3,22,22
790	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.02	0.03	0.04	2d8/25 L=40	3,3,3
	s=6,m=1	39.7	0.40	10.3	12.3	0.0	0.05	0.02	0.04	0.05	2d8/25 L=40	3,3,3
824	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.02	0.04	0.04	2d8/25 L=40	3,44,3
	s=6,m=1	39.7	0.40	10.3	12.3	0.0	0.05	0.02	0.04	0.05	2d8/25 L=40	3,38,3
854	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.02	0.03	0.04	2d8/25 L=40	3,28,23
	s=6,m=1	39.7	0.40	10.3	12.3	0.0	0.05	0.02	0.04	0.06	2d8/25 L=40	24,22,22
878	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.02	0.03	0.03	2d8/25 L=40	24,39,23
	s=6,m=1	39.7	0.40	10.3	12.3	0.0	0.08	0.02	0.05	0.07	2d8/25 L=40	23,25,3
900	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.02	0.03	0.03	2d8/25 L=40	23,25,22
	s=6,m=1	39.7	0.40	10.3	12.3	0.0	0.08	0.01	0.05	0.06	2d8/25 L=40	24,39,3
920	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.01	0.05	0.06	2d8/25 L=40	24,25,22
	s=6,m=1	39.7	0.40	10.3	12.3	0.0	0.08	5.83e-03	0.05	0.07	2d8/25 L=40	39,28,23
934	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	5.86e-03	0.04	0.04	2d8/25 L=40	39,41,25
	s=6,m=1	39.7	0.40	10.3	12.3	0.0	0.08	0.02	0.06	0.07	2d8/25 L=40	23,44,3
947	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.02	0.04	0.05	2d8/25 L=40	23,38,38
	s=6,m=1	39.7	0.40	10.3	12.3	0.0	0.08	0.03	0.08	0.11	2d8/25 L=40	44,3,3
959	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.03	0.07	0.08	2d8/25 L=40	44,38,30
	s=6,m=1	39.7	0.40	10.3	12.3	0.0	0.08	0.07	0.11	0.14	2d8/25 L=40	44,3,3
967	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.07	0.11	0.10	2d8/25 L=40	44,44,44
	s=6,m=1	39.7	0.40	10.3	12.3	0.0	0.08	0.11	0.15	0.17	2d8/25 L=40	44,3,3
466	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.12	0.17	0.18	2d8/25 L=40	44,44,28
	s=6,m=1	39.7	0.40	10.3	12.3	0.0	0.08	0.19	0.20	0.24	2d8/25 L=40	44,44,28
770	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.19	0.17	0.17	2d8/25 L=44	44,25,25
	s=6,m=1	43.8	0.40	10.3	12.3	0.0	0.08	0.27	0.16	0.22	2d8/25 L=44	28,24,28
845	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.27	0.20	0.17	2d8/25 L=44	28,25,25
	s=6,m=1	43.8	0.40	10.3	12.3	0.0	0.08	0.31	0.16	0.13	2d8/25 L=44	28,25,28
820	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.32	0.20	0.22	2d8/25 L=48	28,41,3
	s=6,m=1	47.7	0.40	10.3	12.3	0.0	0.08	0.27	0.15	0.11	2d8/25 L=48	28,41,3
1153	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.24	0.22	0.26	2d8/25 L=48	28,44,3
	s=6,m=1	47.7	0.40	10.3	12.3	0.0	0.08	0.15	0.18	0.18	2d8/25 L=48	28,44,28
1154	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.14	0.21	0.24	2d8/25 L=48	28,44,28
	s=6,m=1	47.7	0.40	10.3	12.3	0.0	0.08	0.13	0.16	0.17	2d8/25 L=48	25,44,28
1155	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.13	0.17	0.20	2d8/25 L=48	25,44,28
	s=6,m=1	47.7	0.40	10.3	12.3	0.0	0.05	0.13	0.12	0.13	2d8/25 L=48	25,44,28
1156	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.13	0.13	0.17	2d8/25 L=48	25,44,28
	s=6,m=1	47.7	0.40	10.3	12.3	0.0	0.05	0.13	0.09	0.10	2d8/25 L=48	3,44,28
1157	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.12	0.11	0.14	2d8/25 L=48	3,44,28
	s=6,m=1	47.7	0.40	10.3	12.3	0.0	0.05	0.14	0.08	0.09	2d8/25 L=48	3,41,25
1158	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.14	0.11	0.11	2d8/25 L=48	3,44,28
	s=6,m=1	47.7	0.40	10.3	12.3	0.0	0.05	0.13	0.12	0.12	2d8/25 L=48	3,41,25
1159	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.13	0.11	0.09	2d8/25 L=48	3,41,28
	s=6,m=1	47.7	0.40	10.3	12.3	0.0	0.05	0.14	0.16	0.16	2d8/25 L=48	28,41,25
1160	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.14	0.15	0.13	2d8/25 L=48	28,41,25
	s=6,m=1	47.7	0.40	10.3	12.3	0.0	0.08	0.15	0.20	0.21	2d8/25 L=48	28,41,25
1161	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.15	0.18	0.16	2d8/25 L=48	28,41,25
	s=6,m=1	47.7	0.40	10.3	12.3	0.0	0.08	0.16	0.23	0.23	2d8/25 L=48	28,41,25
1162	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.16	0.17	0.09	2d8/25 L=48	28,39,3
	s=6,m=1	47.7	0.40	10.3	12.3	0.0	0.08	0.20	0.22	0.20	2d8/25 L=48	25,39,3
810	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.19	0.23	0.17	2d8/25 L=44	25,44,28
	s=6,m=1	43.8	0.40	10.3	12.3	0.0	0.08	0.16	0.27	0.24	2d8/25 L=44	25,44,28
849	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.17	0.17	0.24	2d8/25 L=44	41,25,25
	s=6,m=1	43.8	0.40	10.3	12.3	0.0	0.08	0.13	0.20	0.30	2d8/25 L=44	41,28,28
875	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.11	0.18	0.27	2d8/25 L=44	41,25,25
	s=6,m=1	43.8	0.40	10.3	12.3	0.0	0.08	0.13	0.18	0.27	2d8/25 L=44	23,28,28
897	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.13	0.15	0.21	2d8/25 L=44	23,25,25
	s=6,m=1	43.8	0.40	10.3	12.3	0.0	0.08	0.16	0.11	0.15	2d8/25 L=44	23,25,25
835	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.16	0.14	0.21	2d8/25 L=54	23,3,3
	s=6,m=1	53.7	0.40	10.3	12.3	0.0	0.08	0.13	0.08	0.08	2d8/25 L=54	21,39,3
1223	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.12	0.15	0.22	2d8/25 L=54	21,27,24
	s=6,m=1	53.7	0.40	10.3	12.3	0.0	0.08	0.13	0.10	0.14	2d8/25 L=54	25,27,24
1224	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.12	0.13	0.18	2d8/25 L=54	25,27,24
	s=6,m=1	53.7	0.40	10.3	12.3	0.0	0.05	0.12	0.08	0.10	2d8/25 L=54	25,27,24
1225	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.13	0.11	0.13	2d8/25 L=54	25,43,24
	s=6,m=1	53.7	0.40	10.3	12.3	0.0	0.05	0.13	0.08	0.06	2d8/25 L=54	3,41,21
871	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.12	0.09	0.09	2d8/25 L=52	3,28,24
	s=6,m=1	51.7	0.40	10.3	12.3	0.0	0.05	0.12	0.10	0.09	2d8/25 L=52	3,41,21
1213	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.12	0.06	0.07	2d8/25 L=52	3,28,24
	s=6,m=1	51.7	0.40	10.3	12.3	0.0	0.05	0.11	0.10	0.13	2d8/25 L=52	3,21,21
1214	ok,ok	0.0	0.40	10.3	12.3	0.0	0.05	0.11	0.07	0.09	2d8/25 L=52	3,21,21
	s=6,m=1	51.7	0.40	10.3	12.3	0.0	0.08	0.10	0.12	0.16	2d8/25 L=52	23,21,21
1215	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.10	0.10	0.13	2d8/25 L=52	23,25,22
	s=6,m=1	51.7	0.40	10.3	12.3	0.0	0.08	0.09	0.15	0.21	2d8/25 L=52	24,25,22
1216	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.09	0.12	0.16	2d8/25 L=52	24,33,21
	s=6,m=1	51.7	0.40	10.3	12.3	0.0	0.08	0.18	0.18	0.25	2d8/25 L=52	25,3,3
1217	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.20	0.13	0.10	2d8/25 L=52	25,43,3
	s=6,m=1	51.7	0.40	10.3	12.3	0.0	0.08	0.26	0.18	0.22	2d8/25 L=52	25,43,3
862	ok,ok	0.0	0.40	10.3	12.3	0.0	0.08	0.24	0.15	0.15	2d8/25 L=44	25,35,23
	s=6,m=1	43.8	0.40	10.3	12.3	0.0	0.08	0.21	0.19	0.22	2d8/25 L=44	25,35,23
914	ok,ok	0.0	0.40	10.3	12.3	0.0						

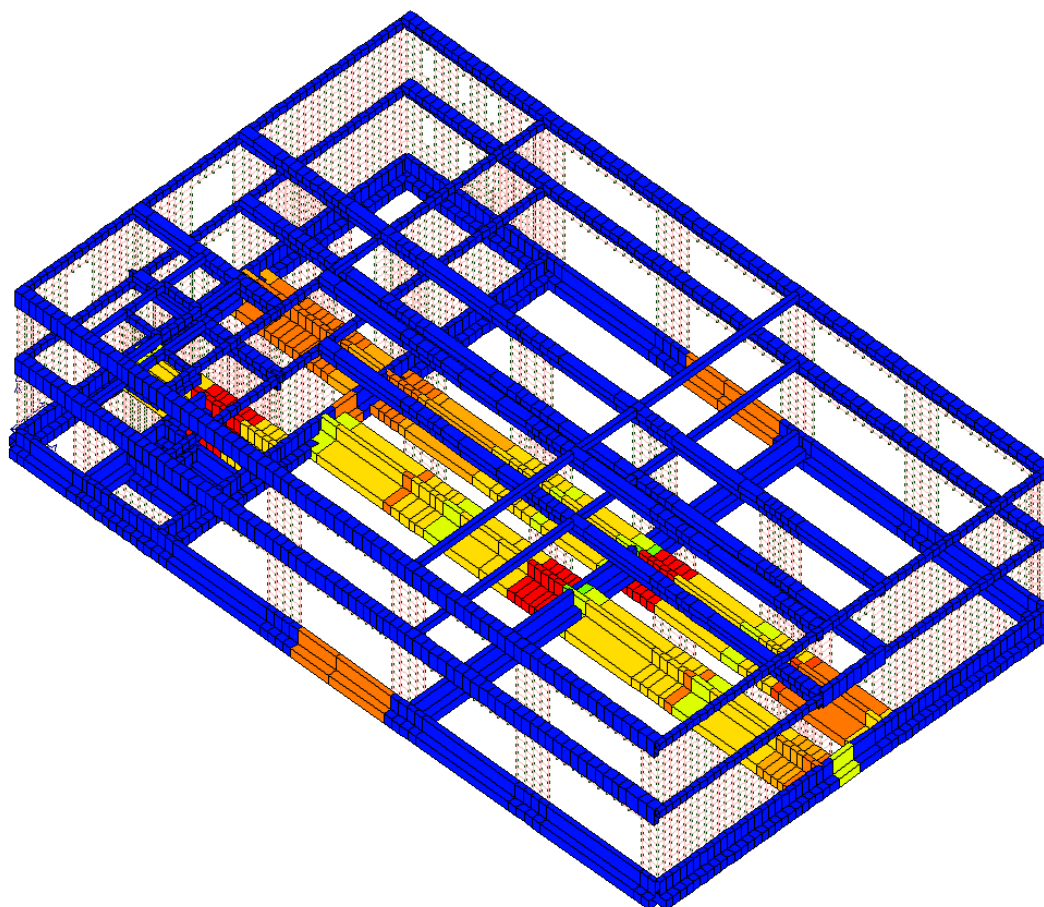
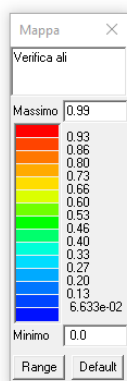
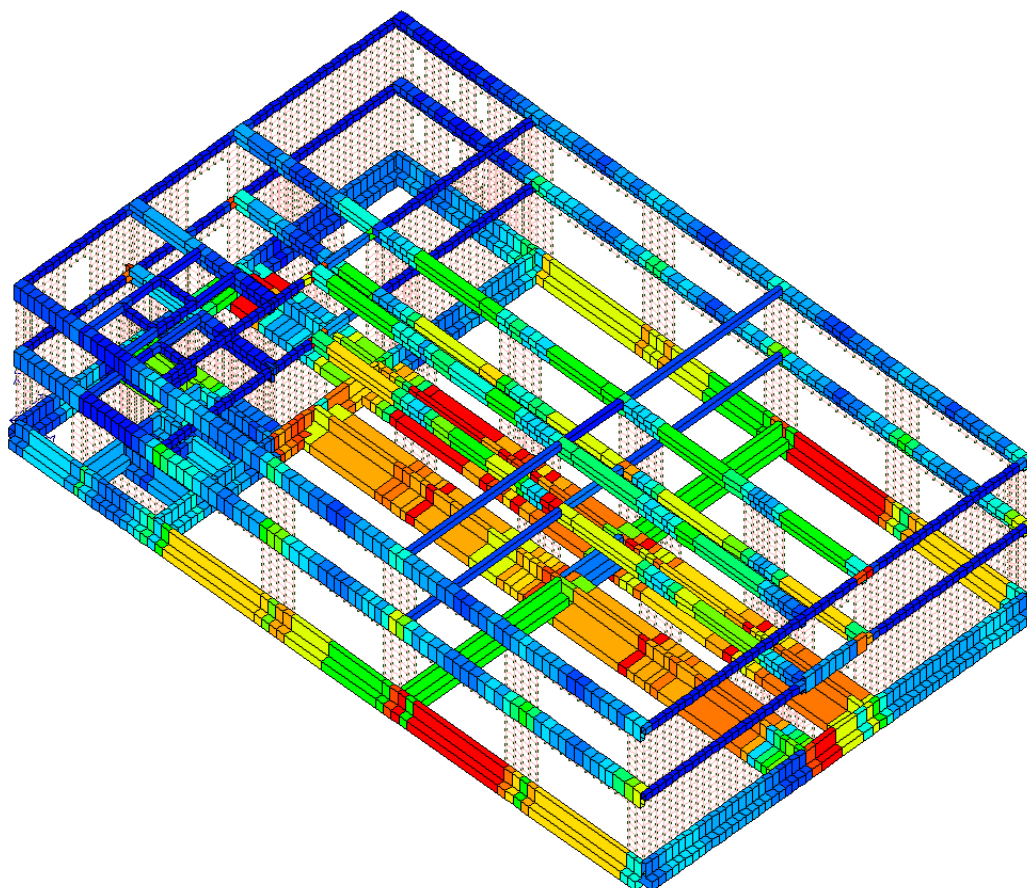
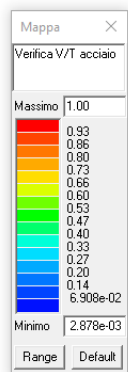
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809	ok,ok	0.0	0.37	10.3	11.2	0.0	0.08	0.25	0.22	0.26	2d8/25 L=31	3,14,18
	s=4,m=1	31.3	0.37	10.3	11.2	0.0	0.08	0.26	0.23	0.29	2d8/25 L=31	3,19,19
727	ok,ok	0.0	0.37	10.3	11.2	0.0	0.08	0.27	0.23	0.22	2d8/25 L=48	3,14,18
	s=4,m=1	47.9	0.37	10.3	11.2	0.0	0.08	0.35	0.25	0.29	2d8/25 L=48	19,16,19
788	ok,ok	0.0	0.37	10.3	11.2	0.0	0.08	0.36	0.39	0.39	2d8/25 L=40	19,3,3
	s=4,m=1	39.6	0.37	10.3	11.2	0.0	0.08	0.23	0.31	0.30	2d8/25 L=40	19,3,15
763	ok,ok	0.0	0.37	10.3	11.2	0.0	0.08	0.50	0.50	0.36	2d8/12 L=86	19,3,3
	s=4,m=1	87.5	0.37	10.3	11.2	0.0	0.08	0.22	0.33	0.46	2d8/25 L=1	18,3,3
749	ok,ok	0.0	0.37	10.3	11.2	0.0	0.08	0.22	0.33	0.46	2d8/25 L=289	18,3,3
	s=4,m=1	374.8	0.37	10.3	11.2	0.0	0.08	0.47	0.47	0.34	2d8/12 L=86	18,3,4
797	ok,ok	0.0	0.37	10.3	11.2	0.0	0.08	0.21	0.18	0.24	2d8/25 L=45	13,14,14
	s=4,m=1	45.0	0.37	10.3	11.2	0.0	0.08	0.34	0.26	0.35	2d8/25 L=45	13,3,3
848	ok,ok	0.0	0.37	10.3	11.2	0.0	0.08	0.31	0.19	0.28	2d8/25 L=45	18,14,14
	s=4,m=1	45.0	0.37	10.3	11.2	0.0	0.08	0.23	0.19	0.27	2d8/25 L=45	3,15,15
827	ok,ok	0.0	0.37	10.3	11.2	0.0	0.08	0.23	0.17	0.25	2d8/25 L=60	3,13,14
	s=4,m=1	60.1	0.37	10.3	11.2	0.0	0.08	0.26	0.24	0.35	2d8/25 L=60	3,15,15
779	ok,ok	0.0	0.37	10.3	11.2	0.0	0.08	0.27	0.18	0.25	2d8/25 L=30	3,15,15
	s=4,m=1	29.9	0.37	10.3	11.2	0.0	0.08	0.33	0.22	0.30	2d8/25 L=30	16,15,15
847	ok,ok	0.0	0.37	10.3	11.2	0.0	0.08	0.33	0.25	0.38	2d8/25 L=45	16,3,3
	s=4,m=1	45.0	0.37	10.3	11.2	0.0	0.08	0.21	0.16	0.24	2d8/25 L=45	16,3,3
823	ok,ok	0.0	0.37	10.3	11.2	0.0	0.08	0.49	0.48	0.38	2d8/12 L=86	16,3,3
	s=4,m=1	100.1	0.37	10.3	11.2	0.0	0.08	0.19	0.29	0.45	2d8/25 L=14	18,3,3
813	ok,ok	0.0	0.37	10.3	11.2	0.0	0.08	0.19	0.29	0.45	2d8/25 L=289	18,3,3
	s=4,m=1	374.9	0.37	10.3	11.2	0.0	0.08	0.39	0.44	0.35	2d8/12 L=86	18,4,4
852	ok,ok	0.0	0.37	10.3	11.2	0.0	0.08	0.16	0.17	0.23	2d8/25 L=40	14,22,14
	s=4,m=1	39.6	0.37	10.3	11.2	0.0	0.08	0.25	0.22	0.31	2d8/25 L=40	14,22,4
877	ok,ok	0.0	0.37	10.3	11.2	0.0	0.08	0.25	0.18	0.24	2d8/25 L=40	14,14,14
	s=4,m=1	39.6	0.37	10.3	11.2	0.0	0.08	0.18	0.13	0.17	2d8/25 L=40	14,14,14
899	ok,ok	0.0	0.37	10.3	11.2	0.0	0.08	0.17	0.18	0.26	2d8/25 L=40	14,14,14
	s=4,m=1	39.6	0.37	10.3	11.2	0.0	0.08	0.09	0.13	0.19	2d8/25 L=40	14,14,14
919	ok,ok	0.0	0.37	10.3	11.2	0.0	0.08	0.09	0.13	0.19	2d8/25 L=31	14,14,14
	s=4,m=1	31.3	0.37	10.3	11.2	0.0	0.08	0.05	0.09	0.13	2d8/25 L=31	4,14,14
838	ok,ok	0.0	0.37	10.3	11.2	0.0	0.08	0.05	0.11	0.16	2d8/25 L=48	4,4,4
	s=4,m=1	47.9	0.37	10.3	11.2	0.0	0.08	0.01	0.04	0.05	2d8/25 L=48	3,22,14
865	ok,ok	0.0	0.37	10.3	11.2	0.0	0.08	0.01	0.09	0.09	2d8/25 L=40	3,34,3
	s=4,m=1	39.6	0.37	10.3	11.2	0.0	0.08	4.69e-03	0.07	0.03	2d8/25 L=40	14,35,15

Trave	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc
	0.51	45.74	44.86	12.06	0.14	0.92	1.00	1.00







STATI LIMITE D' ESERCIZIO

Legenda tabella stati limite d' esercizio

In tabella vengono riportati i valori di interesse per il controllo degli stati limite d'esercizio.

In particolare vengono riportati, in relazione al tipo di elemento strutturale, i risultati relativi alle tre categorie di combinazione considerate:

- Combinazioni rare
- Combinazioni frequenti
- Combinazioni quasi permanenti.

I valori di interesse sono i seguenti:

rRfck	rapporto tra la massima compressione nel calcestruzzo e la tensione fck in combinazioni rare [normalizzato a 1]
rRfyk	rapporto tra la massima tensione nell'acciaio e la tensione fyk in combinazioni rare [normalizzato a 1]
rPfck	rapporto tra la massima compressione nel calcestruzzo e la tensione fck in combinazioni quasi permanenti [normalizzato a 1]
wR	apertura caratteristica delle fessure in combinazioni rare [mm]
wF	apertura caratteristica delle fessure in combinazioni frequenti [mm]
wP	apertura caratteristica delle fessure in combinazioni quasi permanenti [mm]
dR	massima deformazione in combinazioni rare
dF	massima deformazione in combinazioni frequenti
dP	massima deformazione in combinazioni quasi permanenti

Per ognuno dei nove valori soprariportati viene indicata (Rif.cmb) la combinazione in cui si è verificato.

In relazione al tipo di elemento strutturale i valori sono selezionati nel modo seguente:

pilastr	rRfck	rRfyk	rPfck	per sezioni significative
travi	rRfck	rRfyk	rPfck	per sezioni significative
	wR	wF	wP	per sezioni significative
	dR	dF	dP	massimi in campata
setti e gusci	rRfck	rRfyk	rPfck	massimi nei nodi dell'elemento
	wR	wF	wP	massimi nei nodi dell'elemento

Si precisa che i valori di massima deformazione per travi sono riferiti al piano verticale (piano locale 1-2 con momenti flettenti 3-3).

48	0.0	0.01	0.04	0.02	81,81,94	0.0	0.0	0.0	0,0,0	0.06	0.06	0.05	84,90,97
	100.1	0.08	0.11	0.09	84,84,97	0.0	0.0	0.0	0,0,0				
49	0.0	0.24	0.47	0.29	83,83,96	0.18	0.0	0.0	83,0,0	-0.19	-0.15	-0.14	83,89,96
	262.5	0.05	0.19	0.06	83,83,96	0.0	0.0	0.0	0,0,0				
	524.9	0.04	0.15	0.04	83,83,96	0.0	0.0	0.0	0,0,0				
50	0.0	0.25	0.50	0.30	83,83,96	0.19	0.0	0.0	83,0,0	0.21	0.16	0.15	83,89,96
	262.5	0.04	0.19	0.05	83,83,96	0.0	0.0	0.0	0,0,0				
	524.9	0.04	0.17	0.04	83,83,96	0.0	0.0	0.0	0,0,0				
51	0.0	0.01	0.02	0.02	81,81,94	0.0	0.0	0.0	0,0,0	-0.05	-0.03	-0.04	81,87,94
	187.5	0.04	0.12	0.05	83,83,96	0.0	0.0	0.0	0,0,0				
	374.9	0.05	0.05	0.07	81,81,94	0.0	0.0	0.0	0,0,0				
52	0.0	0.05	0.19	0.06	83,84,96	0.0	0.0	0.0	0,0,0	-1.42e-03	-1.39e-03	-1.38e-03	83,89,96
	30.0	0.05	0.19	0.06	84,84,97	0.0	0.0	0.0	0,0,0				
53	0.0	0.02	0.09	0.02	84,84,97	0.0	0.0	0.0	0,0,0	0.11	0.10	0.09	83,89,96
	262.5	0.04	0.19	0.05	83,83,96	0.0	0.0	0.0	0,0,0				
	524.9	0.19	0.41	0.23	83,83,96	0.0	0.0	0.0	0,0,0				
54	0.0	0.03	0.15	0.03	83,83,96	0.0	0.0	0.0	0,0,0	-0.22	-0.20	-0.19	83,89,96
	262.5	0.03	0.16	0.04	83,83,96	0.0	0.0	0.0	0,0,0				
	524.9	0.24	0.49	0.28	83,83,96	0.18	0.0	0.0	83,0,0				
55	0.0	0.02	0.09	0.02	84,83,97	0.0	0.0	0.0	0,0,0	-0.02	-0.02	-0.02	84,89,96
	187.4	0.03	0.13	0.04	83,83,96	0.0	0.0	0.0	0,0,0				
	374.8	0.10	0.16	0.10	84,84,97	0.0	0.0	0.0	0,0,0				
56	0.0	0.02	0.13	0.03	83,83,96	0.0	0.0	0.0	0,0,0	-3.45e-03	-3.31e-03	3.25e-03	83,89,96
	31.3	0.03	0.14	0.04	83,83,96	0.0	0.0	0.0	0,0,0				
57	0.0	0.16	0.38	0.19	83,83,96	0.0	0.0	0.0	0,0,0	-0.03	-0.03	-0.03	83,89,96
	214.6	0.03	0.17	0.03	84,83,97	0.0	0.0	0.0	0,0,0				
58	0.0	0.14	0.38	0.17	83,83,96	0.0	0.0	0.0	0,0,0	0.05	0.05	0.05	83,89,96
	214.6	0.01	0.17	0.02	82,83,95	0.0	0.0	0.0	0,0,0				
59	0.0	4.40e-03	0.01	5.02e-03	83,84,96	0.0	0.0	0.0	0,0,0	0.02	0.02	0.02	83,89,96
	214.6	0.02	0.09	0.03	83,83,96	0.0	0.0	0.0	0,0,0				
60	0.0	0.04	0.16	0.04	84,84,97	0.0	0.0	0.0	0,0,0	-1.56e-03	-1.56e-03	-1.56e-03	81,87,94
	60.1	0.05	0.18	0.06	83,84,96	0.0	0.0	0.0	0,0,0				
61	0.0	0.02	0.05	0.02	83,83,96	0.0	0.0	0.0	0,0,0	-5.60e-03	-5.36e-03	-5.29e-03	84,90,97
	43.7	7.38e-03	0.02	8.58e-03	83,83,96	0.0	0.0	0.0	0,0,0				
62	0.0	0.02	0.05	0.02	83,83,96	0.0	0.0	0.0	0,0,0	5.16e-03	4.86e-03	4.77e-03	84,90,97
	43.7	7.01e-03	0.02	8.19e-03	83,83,96	0.0	0.0	0.0	0,0,0				
63	0.0	0.02	0.05	0.02	83,83,96	0.0	0.0	0.0	0,0,0	9.12e-03	8.75e-03	8.60e-03	83,89,96
	47.9	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
64	0.0	0.03	0.10	0.03	83,83,96	0.0	0.0	0.0	0,0,0	0.03	0.03	0.03	81,87,94
	87.5	0.02	0.02	0.03	81,81,94	0.0	0.0	0.0	0,0,0				
65	0.0	0.01	0.26	0.02	82,83,95	0.0	0.0	0.0	0,0,0	7.09e-04	6.78e-04	6.65e-04	83,89,96
	43.8	0.03	0.28	0.04	83,83,96	0.0	0.0	0.0	0,0,0				
66	0.0	5.99e-03	0.29	7.77e-03	82,83,95	0.0	0.0	0.0	0,0,0	-4.52e-04	-3.67e-04	-3.35e-04	84,90,97
	43.8	0.02	0.31	0.03	83,83,96	0.0	0.0	0.0	0,0,0				
67	0.0	0.06	0.10	0.07	83,83,96	0.0	0.0	0.0	0,0,0	-0.49	-0.50	-0.48	83,89,96
	459.0	0.10	0.32	0.12	83,83,96	0.09	0.09	0.09	83,89,96				
	918.0	0.15	0.25	0.16	84,84,97	0.0	0.0	0.0	0,0,0				
68	0.0	0.02	0.02	0.03	84,84,97	0.0	0.0	0.0	0,0,0	-0.05	-0.05	-0.05	84,90,97
	87.5	0.02	0.06	0.03	83,84,96	0.0	0.0	0.0	0,0,0				
69	0.0	0.01	0.06	0.01	83,83,96	0.0	0.0	0.0	0,0,0	3.91e-03	3.52e-03	3.37e-03	83,89,96
	39.6	0.02	0.06	0.02	84,84,97	0.0	0.0	0.0	0,0,0				
70	0.0	0.11	0.19	0.13	84,84,97	0.0	0.0	0.0	0,0,0	-0.02	-0.02	-0.02	84,90,97
	175.0	0.06	0.10	0.07	84,84,97	0.0	0.0	0.0	0,0,0				
	350.0	0.11	0.19	0.12	84,84,97	0.0	0.0	0.0	0,0,0				
71	0.0	0.15	0.25	0.16	84,84,97	0.0	0.0	0.0	0,0,0	-0.52	0.53	0.52	83,89,96
	459.0	0.10	0.33	0.12	83,83,96	0.10	0.10	0.09	83,89,96				
	918.0	0.06	0.10	0.07	83,83,96	0.0	0.0	0.0	0,0,0				
72	0.0	0.03	0.03	0.04	83,83,96	0.0	0.0	0.0	0,0,0	2.01e-03	1.81e-03	1.73e-03	83,89,96
	23.5	0.02	0.02	0.03	83,83,96	0.0	0.0	0.0	0,0,0				
73	0.0	0.02	0.02	0.02	83,83,96	0.0	0.0	0.0	0,0,0	1.85e-04	1.17e-04	9.16e-05	84,90,97
	23.5	0.02	0.02	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
74	0.0	0.04	0.04	0.05	83,83,96	0.0	0.0	0.0	0,0,0	-2.43e-03	-2.44e-03	-2.44e-03	83,89,96
	54.5	0.05	0.04	0.06	83,83,96	0.0	0.0	0.0	0,0,0				
75	0.0	0.04	0.04	0.04	83,83,96	0.0	0.0	0.0	0,0,0	9.32e-03	7.91e-03	7.29e-03	83,89,96
	54.5	0.06	0.06	0.06	84,83,96	0.0	0.0	0.0	0,0,0				
76	0.0	0.05	0.05	0.06	83,83,96	0.0	0.0	0.0	0,0,0	-0.01	-0.01	-0.01	84,90,97
	120.5	0.04	0.04	0.05	83,83,96	0.0	0.0	0.0	0,0,0				
77	0.0	0.06	0.06	0.07	83,83,96	0.0	0.0	0.0	0,0,0	-0.05	-0.04	-0.03	84,90,97
	120.5	0.04	0.04	0.05	83,83,96	0.0	0.0	0.0	0,0,0				
78	0.0	1.64e-03	2.22e-03	1.80e-03	83,84,96	0.0	0.0	0.0	0,0,0	6.50e-04	5.56e-04	5.21e-04	84,90,97
	38.3	2.79e-03	2.64e-03	3.72e-03	81,81,94	0.0	0.0	0.0	0,0,0				
79	0.0	0.0	9.39e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	2.57e-03	-2.20e-03	-2.05e-03	83,89,96
	39.3	0.0	9.32e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
80	0.0	2.23e-03	4.32e-03	2.47e-03	83,83,96	0.0	0.0	0.0	0,0,0	1.45e-03	1.41e-03	1.39e-03	83,89,96
	38.3	1.99e-03	3.90e-03	2.29e-03	83,83,96	0.0	0.0	0.0	0,0,0				
81	0.0	3.84e-03	9.03e-03	4.72e-03	83,83,96	0.0	0.0	0.0	0,0,0	6.28e-04	4.61e-04	3.93e-04	83,89,96
	39.3	6.59e-03	0.02	8.13e-03	83,83,96	0.0	0.0	0.0	0,0,0				
82	0.0	2.46e-03	2.45e-03	3.06e-03	83,83,96	0.0	0.0	0.0	0,0,0	-1.07e-03	-1.07e-03	-1.07e-03	81,87,94
	38.3	2.85e-03	2.71e-03	3.30e-03	83,83,96	0.0	0.0	0.0	0,0,0				
83	0.0	0.01	0.01	0.02	81,81,94	0.0	0.0	0.0	0,0,0	6.94e-03	5.21e-03	4.20e-03	83,89,96
	54.5	0.02	0.02	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
84	0.0	0.02	0.02	0.02	83,83,96	0.0	0.0	0.0	0,0,0	-0.02	-0.02	-0.02	83,89,96
	120.5	0.02	0.02	0.03	83,83,96	0.0	0.0	0.0	0,0,0				
85	0.0	5.63e-04	5.66e-03	6.19e-04	83,83,96	0.0	0.0	0.0	0,0,0	-5.01e-03	-4.69e-03	-4.56e-03	83,89,96
	38.3	0.0	3.26e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
86	0.0	0.02	0.27	0.03	83,83,96	0.0	0.0	0.0	0,0,0	-1.18e-03	-1.07e-03	-1.03e-03	83,89,96
	43.8	0.01	0.25	0.01	82,83,95	0.0	0.0	0.0	0,0,0				
87	0.0	7.71e-04	3.91e-03	9.78e-04	84,84,97	0.0	0.0	0.0	0,0,0	2.14e-03	2.06e-03	2.02e-03	83,89,96
	38.3	3.39e-03	0.01	4.02e-03	83,83,96	0.0	0.0	0.0	0,0,0				
88	0.0	0.02	0.31	0.03	83,83,96	0.0	0.0	0.0	0,0,0	2.44e-03	2.21e-03	2.12e-03	83,89,96
	43.8	4.48e-03	0.29	5.74e-03	82,83,95	0.0	0.0	0.0	0,0,0				
89	0.0	0.0	0.01	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-4.08e-03	-3.93e-03	-3.87e-03	83,89,96
	38.3	2.00e-03	0.02	1.83e-03	84,84,97	0.0	0.0	0.0	0,0,0				
90	0.0	0.0	0.07	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-3.39e-03	-2.84e-03	-2.63e-03	83,89,96
	39.7	0.0	0.08	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
91	0.0	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.18e-03	-1.08e-03	-1.04e-03	83,89,96
	25.8	3.13e-03	0.04	3.75e-03	83,83,96	0.0	0.0	0.0	0,0,0				
92	0.0	3.06e-03	0.14	3.26e-03	82,84,95	0.0	0.0	0.0	0,0,0	-3.30e-03	-3.25e-03	-3.24e-03	84

94	0.0	0.04	0.39	0.04	83,83,96	0.0	0.0	0.0	0,0,0	-2.19e-03	-2.00e-03	-1.92e-03	83,89,96
	43.8	0.07	0.44	0.08	83,83,96	0.0	0.0	0.0	0,0,0				
95	0.0	0.03	0.41	0.04	83,83,96	0.0	0.0	0.0	0,0,0	-1.77e-03	-1.63e-03	-1.58e-03	83,89,96
	43.8	0.07	0.47	0.08	83,83,96	0.0	0.0	0.0	0,0,0				
96	0.0	0.05	0.41	0.06	83,83,96	0.0	0.0	0.0	0,0,0	4.26e-03	3.89e-03	3.74e-03	83,89,96
	43.8	0.06	0.43	0.07	83,83,96	0.0	0.0	0.0	0,0,0				
97	0.0	0.05	0.46	0.07	83,83,96	0.0	0.0	0.0	0,0,0	7.99e-03	7.25e-03	6.96e-03	83,89,96
	43.8	0.05	0.46	0.06	83,83,96	0.0	0.0	0.0	0,0,0				
98	0.0	7.69e-03	0.02	8.79e-03	83,83,96	0.0	0.0	0.0	0,0,0	-6.07e-03	-5.80e-03	-5.71e-03	84,90,97
	43.8	1.34e-03	3.44e-03	1.60e-03	83,83,96	0.0	0.0	0.0	0,0,0				
99	0.0	7.62e-03	0.03	8.81e-03	83,83,96	0.0	0.0	0.0	0,0,0	5.61e-03	5.28e-03	5.17e-03	84,90,97
	43.8	3.87e-04	4.94e-03	4.20e-04	83,83,96	0.0	0.0	0.0	0,0,0				
100	0.0	0.03	0.28	0.04	83,83,96	0.0	0.0	0.0	0,0,0	2.73e-03	2.55e-03	2.47e-03	83,89,96
	43.8	0.0	0.22	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
101	0.0	0.03	0.31	0.03	83,83,96	0.0	0.0	0.0	0,0,0	-1.64e-03	-1.57e-03	-1.54e-03	83,89,96
	43.8	0.0	0.25	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
102	0.0	0.02	0.02	0.03	83,83,96	0.0	0.0	0.0	0,0,0	-3.90e-03	-3.54e-03	-3.40e-03	83,89,96
	38.3	0.02	0.02	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
103	0.0	0.02	0.02	0.02	83,83,96	0.0	0.0	0.0	0,0,0	2.77e-04	1.84e-04	1.42e-04	84,90,97
	38.3	0.02	0.02	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
104	0.0	1.25e-03	3.14e-03	1.43e-03	83,83,96	0.0	0.0	0.0	0,0,0	-5.23e-03	-4.88e-03	-4.74e-03	83,89,96
	38.3	5.72e-04	5.54e-04	6.15e-04	83,83,96	0.0	0.0	0.0	0,0,0				
105	0.0	1.54e-03	1.48e-03	1.68e-03	83,83,96	0.0	0.0	0.0	0,0,0	8.47e-04	8.13e-04	8.00e-04	83,89,96
	38.3	1.01e-03	9.86e-04	9.61e-04	83,83,96	0.0	0.0	0.0	0,0,0				
106	0.0	2.13e-03	0.02	2.42e-03	84,84,97	0.0	0.0	0.0	0,0,0	-4.97e-03	-4.81e-03	-4.74e-03	83,89,96
	38.3	0.0	0.01	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
107	0.0	2.34e-03	2.20e-03	3.12e-03	81,81,94	0.0	0.0	0.0	0,0,0	-1.54e-03	-1.31e-03	-1.23e-03	84,90,97
	38.3	6.01e-03	8.18e-03	7.89e-03	83,81,96	0.0	0.0	0.0	0,0,0				
108	0.0	5.52e-03	5.43e-03	6.40e-03	83,83,96	0.0	0.0	0.0	0,0,0	1.46e-03	1.42e-03	1.40e-03	83,89,96
	38.3	2.33e-03	2.25e-03	2.76e-03	83,83,96	0.0	0.0	0.0	0,0,0				
109	0.0	5.36e-03	5.31e-03	6.60e-03	83,83,96	0.0	0.0	0.0	0,0,0	3.53e-04	3.53e-04	3.53e-04	81,87,94
	38.3	4.50e-03	4.36e-03	5.31e-03	83,83,96	0.0	0.0	0.0	0,0,0				
110	0.0	0.0	0.08	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-3.13e-03	-2.62e-03	-2.41e-03	83,89,96
	39.7	0.0	0.09	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
111	0.0	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-4.94e-03	-4.50e-03	-4.32e-03	83,89,96
	39.7	8.76e-03	0.06	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
112	0.0	0.06	0.44	0.07	83,83,96	0.0	0.0	0.0	0,0,0	5.96e-03	5.48e-03	5.29e-03	83,89,96
	43.8	0.06	0.44	0.07	83,83,96	0.0	0.0	0.0	0,0,0				
113	0.0	0.06	0.46	0.07	83,83,96	0.0	0.0	0.0	0,0,0	5.59e-03	5.17e-03	5.01e-03	83,89,96
	43.8	0.06	0.47	0.07	83,83,96	0.0	0.0	0.0	0,0,0				
114	0.0	0.06	0.43	0.07	83,83,96	0.0	0.0	0.0	0,0,0	7.23e-04	6.26e-04	5.87e-04	83,89,96
	43.8	0.04	0.40	0.05	83,83,96	0.0	0.0	0.0	0,0,0				
115	0.0	0.06	0.46	0.07	83,83,96	0.0	0.0	0.0	0,0,0	-4.33e-03	-3.88e-03	-3.69e-03	83,89,96
	43.8	0.03	0.41	0.03	83,83,96	0.0	0.0	0.0	0,0,0				
116	0.0	0.02	0.02	0.02	83,83,96	0.0	0.0	0.0	0,0,0	4.87e-03	4.47e-03	4.31e-03	83,89,96
	38.3	0.01	0.01	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
117	0.0	0.02	0.02	0.03	83,83,96	0.0	0.0	0.0	0,0,0	2.47e-04	1.46e-04	9.90e-05	84,90,97
	38.3	0.02	0.02	0.03	83,83,96	0.0	0.0	0.0	0,0,0				
118	0.0	1.61e-03	1.75e-03	1.84e-03	83,83,96	0.0	0.0	0.0	0,0,0	5.52e-03	5.15e-03	5.00e-03	83,89,96
	38.3	1.06e-03	1.05e-03	1.20e-03	83,83,96	0.0	0.0	0.0	0,0,0				
119	0.0	2.09e-03	2.05e-03	2.38e-03	83,83,96	0.0	0.0	0.0	0,0,0	-2.01e-03	-1.93e-03	-1.89e-03	83,89,96
	38.3	3.89e-03	3.74e-03	4.32e-03	83,83,96	0.0	0.0	0.0	0,0,0				
120	0.0	2.80e-03	0.02	3.39e-03	83,84,96	0.0	0.0	0.0	0,0,0	4.66e-03	4.49e-03	4.43e-03	83,89,96
	38.3	2.76e-03	0.02	3.68e-03	81,84,94	0.0	0.0	0.0	0,0,0				
121	0.0	6.46e-03	8.30e-03	8.39e-03	83,81,96	0.0	0.0	0.0	0,0,0	1.42e-03	1.19e-03	1.11e-03	84,90,97
	38.3	8.64e-03	0.01	0.01	83,81,96	0.0	0.0	0.0	0,0,0				
122	0.0	6.11e-03	5.87e-03	7.21e-03	83,83,96	0.0	0.0	0.0	0,0,0	-1.48e-03	-1.44e-03	-1.42e-03	83,89,96
	38.3	2.00e-03	1.99e-03	2.39e-03	83,83,96	0.0	0.0	0.0	0,0,0				
123	0.0	6.78e-03	6.76e-03	8.34e-03	83,83,96	0.0	0.0	0.0	0,0,0	1.12e-03	1.12e-03	1.12e-03	81,87,94
	38.3	7.75e-03	7.44e-03	9.25e-03	83,83,96	0.0	0.0	0.0	0,0,0				
124	0.0	0.0	0.09	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.82e-03	-2.34e-03	-2.14e-03	83,89,96
	39.7	0.0	0.09	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
125	0.0	0.0	0.06	0.0	0,83,0	0.0	0.0	0.0	0,0,0	4.50e-03	4.09e-03	3.93e-03	83,89,96
	39.7	8.38e-03	0.08	9.92e-03	83,83,96	0.0	0.0	0.0	0,0,0				
126	0.0	0.07	0.45	0.09	83,83,96	0.0	0.0	0.0	0,0,0	9.69e-03	8.93e-03	8.62e-03	83,89,96
	43.8	0.0	0.35	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
127	0.0	0.07	0.47	0.08	83,83,96	0.0	0.0	0.0	0,0,0	9.41e-03	8.70e-03	8.41e-03	83,89,96
	43.8	0.0	0.37	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
128	0.0	0.06	0.40	0.07	83,83,96	0.0	0.0	0.0	0,0,0	2.48e-03	2.32e-03	2.26e-03	84,90,97
	43.8	0.0	0.30	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
129	0.0	0.05	0.41	0.06	83,83,96	0.0	0.0	0.0	0,0,0	-1.33e-03	-1.10e-03	1.01e-03	83,89,96
	43.8	0.0	0.31	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
130	0.0	0.01	0.01	0.02	83,83,96	0.0	0.0	0.0	0,0,0	-6.96e-03	-6.70e-03	-6.35e-03	83,89,96
	38.3	0.01	0.01	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
131	0.0	0.02	0.02	0.03	83,83,96	0.0	0.0	0.0	0,0,0	-1.84e-03	-5.02e-04	-2.70e-04	84,90,97
	38.3	0.02	0.02	0.03	83,83,96	0.0	0.0	0.0	0,0,0				
132	0.0	1.97e-03	1.89e-03	2.24e-03	83,83,96	0.0	0.0	0.0	0,0,0	5.77e-03	5.40e-03	5.25e-03	83,89,96
	38.3	1.44e-03	1.45e-03	1.69e-03	83,83,96	0.0	0.0	0.0	0,0,0				
133	0.0	2.01e-03	2.01e-03	2.34e-03	83,83,96	0.0	0.0	0.0	0,0,0	-2.00e-03	-1.91e-03	-1.87e-03	83,89,96
	38.3	4.59e-03	4.46e-03	5.24e-03	83,83,96	0.0	0.0	0.0	0,0,0				
134	0.0	2.80e-03	0.02	3.52e-03	83,84,96	0.0	0.0	0.0	0,0,0	4.69e-03	4.51e-03	4.45e-03	83,89,96
	38.3	5.45e-03	0.02	7.09e-03	83,84,96	0.0	0.0	0.0	0,0,0				
135	0.0	0.01	0.01	0.01	83,81,96	0.0	0.0	0.0	0,0,0	1.21e-03	9.83e-04	8.98e-04	84,90,97
	38.3	0.01	0.01	0.01	83,81,96	0.0	0.0	0.0	0,0,0				
136	0.0	5.81e-03	5.68e-03	6.95e-03	83,83,96	0.0	0.0	0.0	0,0,0	-1.43e-03	-1.38e-03	-1.37e-03	83,89,96
	38.3	1.74e-03	1.79e-03	2.05e-03	83,83,96	0.0	0.0	0.0	0,0,0				
137	0.0	5.96e-03	6.10e-03	7.38e-03	83,83,96	0.0	0.0	0.0	0,0,0	8.99e-04	8.99e-04	8.99e-04	81,87,94
	38.3	0.01	0.01	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
138	0.0	0.0	0.09	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.51e-03	-2.06e-03	-1.88e-03	83,89,96
	39.7	0.0	0.10	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
139	0.0	0.0	0.07	0.0	0,83,0	0.0	0.0	0.0	0,0,0	4.12e-03	3.72e-03	3.56e-03	83,89,96
	39.7	4.82e-03	0.08	5.43e-03	84,83,97	0.0	0.0	0.0	0,0,0				
140	0.0	0.01	0.01	0.01	83,83,96	0.0	0.0	0.0	0,0,0	-0.01	-1.36e-03	-1.30e-03	83,89,96
	38.3	0.01	0.01	0.01	83,83,96	0							

	38.3	6.86e-03	0.02	8.84e-03	83,84,96	0.0	0.0	0.0	0,0,0				
145	0.0	0.01	0.01	0.02	83,81,96	0.0	0.0	0.0	0,0,0	9.60e-04	7.30e-04	6.47e-04	84,90,97
	38.3	8.16e-03	7.81e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
146	0.0	5.73e-03	5.66e-03	6.93e-03	83,83,96	0.0	0.0	0.0	0,0,0	-1.27e-03	-1.23e-03	-1.21e-03	83,89,96
	38.3	2.94e-03	2.96e-03	3.39e-03	83,83,96	0.0	0.0	0.0	0,0,0				
147	0.0	9.96e-03	9.83e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0	-5.08e-04	-5.08e-04	-5.08e-04	81,87,94
	31.3	0.02	0.02	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
148	0.0	0.0	0.10	0.0	0,83,0	0.0	0.0	0.0	0,0,0	2.20e-03	1.78e-03	1.61e-03	83,89,96
	39.7	0.0	0.11	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
149	0.0	0.0	0.08	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-3.74e-03	-3.36e-03	-3.21e-03	83,89,96
	39.7	2.06e-04	0.08	0.0	84,83,0	0.0	0.0	0.0	0,0,0				
150	0.0	0.01	0.01	0.01	83,83,96	0.0	0.0	0.0	0,0,0	-9.85e-03	-1.35e-03	-1.29e-03	83,89,96
	38.3	0.01	0.01	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
151	0.0	0.03	0.03	0.03	83,83,96	0.0	0.0	0.0	0,0,0	-1.12e-03	-7.15e-04	-5.55e-04	84,90,97
	38.3	0.04	0.04	0.05	83,83,96	0.0	0.0	0.0	0,0,0				
152	0.0	2.73e-03	2.69e-03	3.13e-03	83,83,96	0.0	0.0	0.0	0,0,0	6.24e-03	5.90e-03	5.76e-03	83,89,96
	38.3	1.93e-03	1.98e-03	2.37e-03	83,83,96	0.0	0.0	0.0	0,0,0				
153	0.0	2.24e-03	2.28e-03	2.49e-03	83,83,96	0.0	0.0	0.0	0,0,0	1.67e-03	1.60e-03	1.57e-03	83,89,96
	38.3	4.64e-03	4.59e-03	5.48e-03	83,83,96	0.0	0.0	0.0	0,0,0				
154	0.0	2.30e-03	7.01e-03	2.91e-03	83,84,97	0.0	0.0	0.0	0,0,0	-4.71e-03	-4.51e-03	-4.43e-03	83,89,96
	38.3	7.38e-03	0.01	9.44e-03	83,84,96	0.0	0.0	0.0	0,0,0				
155	0.0	0.01	0.01	0.02	83,83,96	0.0	0.0	0.0	0,0,0	7.32e-04	5.15e-04	4.39e-04	84,90,97
	38.3	3.19e-03	3.11e-03	3.74e-03	83,83,96	0.0	0.0	0.0	0,0,0				
156	0.0	5.73e-03	5.71e-03	7.01e-03	83,83,96	0.0	0.0	0.0	0,0,0	-7.02e-04	-8.64e-04	-8.62e-04	83,89,96
	38.3	4.09e-03	4.09e-03	4.77e-03	83,83,96	0.0	0.0	0.0	0,0,0				
157	0.0	9.74e-03	9.81e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0	7.61e-04	7.61e-04	7.61e-04	81,87,94
	45.3	9.96e-03	0.01	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
158	0.0	0.0	0.11	0.0	0,83,0	0.0	0.0	0.0	0,0,0	1.85e-03	1.46e-03	1.30e-03	83,89,96
	39.7	0.0	0.12	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
159	0.0	0.0	0.08	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-3.38e-03	-3.02e-03	-2.87e-03	83,89,96
	39.7	0.0	0.08	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
160	0.0	0.01	0.01	0.01	83,83,94	0.0	0.0	0.0	0,0,0	-6.72e-03	-7.29e-03	-7.97e-03	83,89,96
	38.3	0.01	0.01	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
161	0.0	0.04	0.04	0.04	83,83,96	0.0	0.0	0.0	0,0,0	-1.80e-03	-1.36e-03	-1.18e-03	84,90,97
	38.3	0.06	0.05	0.07	83,83,96	0.0	0.0	0.0	0,0,0				
162	0.0	3.08e-03	3.05e-03	3.55e-03	83,83,96	0.0	0.0	0.0	0,0,0	-6.40e-03	-6.08e-03	-5.96e-03	83,89,96
	38.3	2.14e-03	2.20e-03	2.63e-03	83,83,96	0.0	0.0	0.0	0,0,0				
163	0.0	2.99e-03	3.03e-03	3.38e-03	83,83,96	0.0	0.0	0.0	0,0,0	1.26e-03	1.34e-03	1.32e-03	83,89,96
	38.3	4.68e-03	4.66e-03	5.60e-03	83,83,96	0.0	0.0	0.0	0,0,0				
164	0.0	1.77e-03	1.78e-03	2.36e-03	81,81,94	0.0	0.0	0.0	0,0,0	4.59e-03	4.38e-03	4.29e-03	83,89,96
	38.3	7.09e-03	8.46e-03	9.01e-03	83,84,96	0.0	0.0	0.0	0,0,0				
165	0.0	0.03	0.03	0.04	83,83,96	0.0	0.0	0.0	0,0,0	-1.07e-03	-8.48e-04	-7.07e-04	84,90,97
	38.3	0.01	0.01	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
166	0.0	5.82e-03	5.85e-03	7.21e-03	83,83,96	0.0	0.0	0.0	0,0,0	-7.06e-04	-6.82e-04	-6.72e-04	83,89,96
	38.3	5.18e-03	5.16e-03	6.11e-03	83,83,96	0.0	0.0	0.0	0,0,0				
167	0.0	8.95e-03	9.19e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0	-1.42e-04	-1.42e-04	-1.42e-04	81,87,94
	38.3	0.01	0.01	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
168	0.0	0.0	0.12	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.43e-03	-1.08e-03	-9.47e-04	83,89,96
	39.7	0.0	0.13	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
169	0.0	0.0	0.08	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-3.07e-03	-2.72e-03	-2.57e-03	83,89,96
	39.7	0.0	0.08	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
170	0.0	3.36e-03	3.34e-03	3.89e-03	83,83,96	0.0	0.0	0.0	0,0,0	-6.60e-03	-6.27e-03	-6.17e-03	83,89,96
	38.3	2.54e-03	2.60e-03	2.87e-03	83,83,96	0.0	0.0	0.0	0,0,0				
171	0.0	3.67e-03	3.70e-03	4.19e-03	83,83,96	0.0	0.0	0.0	0,0,0	-9.47e-04	-9.05e-04	-8.88e-04	83,89,96
	38.3	4.80e-03	4.82e-03	5.83e-03	83,83,96	0.0	0.0	0.0	0,0,0				
172	0.0	2.03e-03	2.08e-03	2.70e-03	81,81,94	0.0	0.0	0.0	0,0,0	-4.31e-03	-4.10e-03	-4.02e-03	83,89,96
	38.3	6.43e-03	6.27e-03	8.45e-03	83,83,96	0.0	0.0	0.0	0,0,0				
173	0.0	0.01	0.01	0.02	83,83,96	0.0	0.0	0.0	0,0,0	-1.07e-03	-8.48e-04	-7.07e-04	81,87,94
	38.3	9.20e-03	9.05e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
174	0.0	5.99e-03	6.07e-03	7.49e-03	83,83,96	0.0	0.0	0.0	0,0,0	-3.34e-03	-6.80e-04	-6.71e-04	83,89,96
	38.3	6.19e-03	6.18e-03	7.38e-03	83,83,96	0.0	0.0	0.0	0,0,0				
175	0.0	9.92e-03	0.01	0.01	83,83,96	0.0	0.0	0.0	0,0,0	-8.52e-04	-8.52e-04	-8.52e-04	81,87,94
	38.3	0.01	0.01	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
176	0.0	0.0	0.13	0.0	0,83,0	0.0	0.0	0.0	0,0,0	9.50e-04	6.54e-04	5.35e-04	83,89,96
	39.7	0.0	0.14	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
177	0.0	0.0	0.08	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.84e-03	-2.49e-03	-2.34e-03	83,89,96
	39.7	0.0	0.07	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
178	0.0	3.56e-03	3.55e-03	4.15e-03	83,83,96	0.0	0.0	0.0	0,0,0	6.81e-03	6.52e-03	6.44e-03	83,89,96
	38.3	2.89e-03	2.95e-03	3.29e-03	83,83,96	0.0	0.0	0.0	0,0,0				
179	0.0	4.25e-03	4.29e-03	4.90e-03	83,83,96	0.0	0.0	0.0	0,0,0	-9.51e-04	-9.10e-04	-8.93e-04	83,89,96
	38.3	5.00e-03	5.05e-03	6.14e-03	83,83,96	0.0	0.0	0.0	0,0,0				
180	0.0	3.14e-03	3.18e-03	4.18e-03	81,81,94	0.0	0.0	0.0	0,0,0	3.90e-03	-3.68e-03	-3.60e-03	83,89,96
	38.3	6.52e-03	6.44e-03	8.69e-03	81,81,94	0.0	0.0	0.0	0,0,0				
181	0.0	9.20e-03	9.06e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0	-1.07e-03	-8.48e-04	-7.07e-04	84,90,94
	38.3	0.01	0.01	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
182	0.0	6.23e-03	6.36e-03	7.87e-03	83,83,96	0.0	0.0	0.0	0,0,0	3.05e-03	2.98e-03	3.06e-03	83,89,96
	38.3	7.15e-03	7.14e-03	8.60e-03	83,83,96	0.0	0.0	0.0	0,0,0				
183	0.0	0.01	0.01	0.01	83,83,96	0.0	0.0	0.0	0,0,0	5.30e-04	5.30e-04	5.30e-04	81,87,94
	38.3	0.01	0.01	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
184	0.0	0.0	0.14	0.0	0,83,0	0.0	0.0	0.0	0,0,0	4.00e-04	2.11e-04	1.97e-04	83,91,95
	39.7	0.0	0.15	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
185	0.0	0.0	0.07	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.80e-03	-2.40e-03	-2.25e-03	83,89,96
	39.7	0.0	0.05	0.0	0,84,0	0.0	0.0	0.0	0,0,0				
186	0.0	3.68e-03	3.69e-03	4.33e-03	83,83,96	0.0	0.0	0.0	0,0,0	7.14e-03	6.96e-03	6.85e-03	83,89,96
	38.3	3.16e-03	3.22e-03	3.63e-03	83,83,96	0.0	0.0	0.0	0,0,0				
187	0.0	4.72e-03	4.78e-03	5.50e-03	83,83,96	0.0	0.0	0.0	0,0,0	9.54e-04	9.14e-04	8.98e-04	83,89,96
	38.3	5.29e-03	5.36e-03	6.55e-03	83,83,96	0.0	0.0	0.0	0,0,0				
188	0.0	4.16e-03	4.21e-03	5.55e-03	81,81,94	0.0	0.0	0.0	0,0,0	-3.41e-03	-3.13e-03	-3.07e-03	83,89,96
	38.3	6.79e-03	6.75e-03	9.05e-03	81,81,94	0.0	0.0	0.0	0,0,0				
189	0.0	0.01	0.01	0.02	83,83,96	0.0	0.0	0.0	0,0,0	-1.07e-03	-8.48e-04	-7.07e-04	84,90,97
	38.3	0.02	0.02	0.02	83,81,96	0.0	0.0	0.0	0,0,0				
190	0.0	6.52e-03	6.68e-03	8.29e-03	83,83,96	0.0	0.0	0.0	0,0,0	2.95e-03	2.87e-03	2.92e-03	83,89,96
	38.3	8.05e-03	8.04e-03	9.76e-03	83,83,96	0.0	0.0	0.0	0,0,0				
191	0.0	0.01	0.01</										

195	0.0	5.08e-03	5.16e-03	5.98e-03	83,83,96	0.0	0.0	0.0	0,0,0	-9.58e-04	-9.19e-04	-9.04e-04	83,89,96
	38.3	5.67e-03	5.76e-03	7.07e-03	83,83,96	0.0	0.0	0.0	0,0,0				
196	0.0	5.10e-03	5.16e-03	6.80e-03	81,81,94	0.0	0.0	0.0	0,0,0	-2.70e-03	-2.57e-03	-2.52e-03	83,89,96
	38.3	7.14e-03	7.15e-03	9.52e-03	81,81,94	0.0	0.0	0.0	0,0,0				
197	0.0	9.93e-03	9.93e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0	1.48e-03	1.14e-03	1.02e-03	84,90,97
	38.3	0.01	0.01	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
198	0.0	6.86e-03	7.06e-03	8.76e-03	83,83,96	0.0	0.0	0.0	0,0,0	2.91e-03	2.86e-03	2.90e-03	83,89,96
	38.3	8.90e-03	8.90e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
199	0.0	0.02	0.02	0.02	83,83,96	0.0	0.0	0.0	0,0,0	3.81e-04	2.09e-04	1.50e-04	84,90,97
	21.8	0.02	0.02	0.03	83,83,96	0.0	0.0	0.0	0,0,0				
200	0.0	1.03e-03	0.15	1.02e-03	82,83,95	0.0	0.0	0.0	0,0,0	-1.35e-03	-1.33e-03	-1.32e-03	82,91,95
	39.7	5.57e-03	0.16	6.76e-03	82,84,95	0.0	0.0	0.0	0,0,0				
201	0.0	0.0	0.04	0.0	0,84,0	0.0	0.0	0.0	0,0,0	2.06e-03	1.74e-03	1.62e-03	83,89,96
	39.7	0.0	0.04	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
202	0.0	3.63e-03	3.69e-03	4.38e-03	83,83,96	0.0	0.0	0.0	0,0,0	-8.83e-03	-1.83e-03	-1.78e-03	83,89,96
	38.3	3.45e-03	3.52e-03	4.03e-03	83,83,96	0.0	0.0	0.0	0,0,0				
203	0.0	5.34e-03	5.45e-03	6.36e-03	83,83,96	0.0	0.0	0.0	0,0,0	-9.65e-04	-1.28e-03	-1.14e-03	83,89,96
	38.3	6.16e-03	6.26e-03	7.72e-03	83,83,96	0.0	0.0	0.0	0,0,0				
204	0.0	5.93e-03	6.01e-03	7.91e-03	81,81,94	0.0	0.0	0.0	0,0,0	2.64e-03	2.21e-03	2.18e-03	83,89,96
	38.3	7.56e-03	7.61e-03	0.01	81,81,94	0.0	0.0	0.0	0,0,0				
205	0.0	0.01	0.01	0.01	83,83,96	0.0	0.0	0.0	0,0,0	1.59e-03	1.27e-03	1.16e-03	84,90,97
	38.3	0.01	0.01	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
206	0.0	7.75e-03	7.95e-03	9.37e-03	83,83,96	0.0	0.0	0.0	0,0,0	2.79e-03	2.86e-03	2.77e-03	83,89,96
	38.3	9.70e-03	9.70e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
207	0.0	0.02	0.02	0.02	83,83,96	0.0	0.0	0.0	0,0,0	1.68e-03	1.13e-03	9.17e-04	84,90,97
	54.8	0.02	0.02	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
208	0.0	3.47e-03	3.55e-03	4.25e-03	83,83,96	0.0	0.0	0.0	0,0,0	-1.93e-03	-1.82e-03	-1.78e-03	83,89,96
	38.3	3.46e-03	3.54e-03	4.19e-03	83,83,94	0.0	0.0	0.0	0,0,0				
209	0.0	5.49e-03	5.64e-03	6.62e-03	83,83,96	0.0	0.0	0.0	0,0,0	9.76e-04	9.39e-04	9.24e-04	83,89,96
	38.3	6.78e-03	6.88e-03	8.52e-03	83,83,96	0.0	0.0	0.0	0,0,0				
210	0.0	6.68e-03	6.78e-03	8.91e-03	81,81,94	0.0	0.0	0.0	0,0,0	-2.71e-03	-2.19e-03	-2.19e-03	83,89,96
	38.3	8.11e-03	8.19e-03	0.01	81,81,94	0.0	0.0	0.0	0,0,0				
211	0.0	0.01	0.01	0.01	83,83,96	0.0	0.0	0.0	0,0,0	-1.80e-03	-1.48e-03	-1.37e-03	84,90,97
	38.3	0.01	0.01	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
212	0.0	8.59e-03	8.79e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0	2.78e-03	2.76e-03	2.80e-03	83,89,96
	38.3	0.01	0.01	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
213	0.0	0.01	0.01	0.02	83,83,96	0.0	0.0	0.0	0,0,0	-3.08e-04	-1.93e-04	-1.52e-04	84,90,97
	38.3	0.01	0.01	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
214	0.0	3.61e-03	3.69e-03	4.58e-03	83,83,96	0.0	0.0	0.0	0,0,0	-1.93e-03	-1.82e-03	-1.78e-03	83,89,96
	38.3	3.50e-03	3.57e-03	4.66e-03	81,81,94	0.0	0.0	0.0	0,0,0				
215	0.0	6.36e-03	6.51e-03	7.75e-03	83,83,96	0.0	0.0	0.0	0,0,0	9.93e-04	1.00e-03	1.02e-03	83,89,96
	38.3	7.55e-03	7.65e-03	9.52e-03	83,83,96	0.0	0.0	0.0	0,0,0				
216	0.0	7.35e-03	7.48e-03	9.80e-03	81,81,94	0.0	0.0	0.0	0,0,0	-2.12e-03	-2.36e-03	-2.43e-03	83,89,96
	38.3	8.78e-03	8.88e-03	0.01	81,81,94	0.0	0.0	0.0	0,0,0				
217	0.0	0.01	0.01	0.01	83,83,96	0.0	0.0	0.0	0,0,0	1.99e-03	1.68e-03	1.57e-03	84,90,97
	38.3	0.01	0.01	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
218	0.0	9.38e-03	9.59e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0	2.72e-03	2.76e-03	2.72e-03	83,89,96
	38.3	0.01	0.01	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
219	0.0	0.01	0.01	0.02	83,83,96	0.0	0.0	0.0	0,0,0	1.54e-03	5.59e-04	3.92e-04	84,90,97
	38.3	0.02	0.02	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
220	0.0	4.26e-03	4.32e-03	5.40e-03	83,83,96	0.0	0.0	0.0	0,0,0	1.94e-03	1.83e-03	1.79e-03	83,89,96
	38.3	3.96e-03	4.02e-03	5.28e-03	81,81,94	0.0	0.0	0.0	0,0,0				
221	0.0	7.44e-03	7.57e-03	9.08e-03	83,83,96	0.0	0.0	0.0	0,0,0	-1.40e-03	-1.38e-03	-1.37e-03	83,89,96
	38.3	8.56e-03	8.64e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
222	0.0	7.97e-03	8.13e-03	0.01	81,81,94	0.0	0.0	0.0	0,0,0	-2.10e-03	-2.03e-03	-2.00e-03	83,89,96
	38.3	9.61e-03	9.74e-03	0.01	81,81,94	0.0	0.0	0.0	0,0,0				
223	0.0	0.01	0.01	0.02	83,83,96	0.0	0.0	0.0	0,0,0	2.13e-03	1.84e-03	1.73e-03	84,90,97
	38.3	0.02	0.02	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
224	0.0	0.01	0.01	0.01	83,83,96	0.0	0.0	0.0	0,0,0	2.68e-03	2.72e-03	2.73e-03	83,89,96
	38.3	0.01	0.01	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
225	0.0	0.01	0.02	0.02	83,83,96	0.0	0.0	0.0	0,0,0	-2.91e-04	-1.76e-04	-1.35e-04	84,90,97
	38.3	0.02	0.02	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
226	0.0	5.01e-03	5.04e-03	6.35e-03	83,83,96	0.0	0.0	0.0	0,0,0	2.89e-03	2.81e-03	2.77e-03	83,89,96
	38.3	4.55e-03	4.59e-03	6.07e-03	81,81,94	0.0	0.0	0.0	0,0,0				
227	0.0	8.60e-03	8.71e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0	1.72e-03	1.66e-03	1.64e-03	83,89,96
	38.3	9.84e-03	9.90e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
228	0.0	8.57e-03	8.77e-03	0.01	81,81,94	0.0	0.0	0.0	0,0,0	2.42e-03	2.05e-03	2.02e-03	83,89,96
	38.3	0.01	0.01	0.01	81,81,94	0.0	0.0	0.0	0,0,0				
229	0.0	0.02	0.02	0.02	83,83,96	0.0	0.0	0.0	0,0,0	2.41e-03	2.12e-03	2.01e-03	84,90,97
	38.3	0.03	0.02	0.03	83,83,96	0.0	0.0	0.0	0,0,0				
230	0.0	0.01	0.01	0.01	83,83,96	0.0	0.0	0.0	0,0,0	-2.73e-03	-2.71e-03	-2.72e-03	83,89,96
	38.3	0.01	0.01	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
231	0.0	0.02	0.02	0.02	83,83,96	0.0	0.0	0.0	0,0,0	1.70e-03	9.89e-04	7.58e-04	84,90,97
	38.3	0.02	0.02	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
232	0.0	5.86e-03	5.85e-03	7.41e-03	83,83,96	0.0	0.0	0.0	0,0,0	-3.70e-03	-3.48e-03	-3.39e-03	83,89,96
	38.3	5.35e-03	5.37e-03	7.14e-03	81,81,94	0.0	0.0	0.0	0,0,0				
233	0.0	9.80e-03	9.90e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0	-1.98e-03	-1.90e-03	-1.87e-03	83,89,96
	38.3	0.01	0.01	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
234	0.0	9.20e-03	9.44e-03	0.01	81,81,94	0.0	0.0	0.0	0,0,0	-3.06e-03	-2.49e-03	-2.27e-03	83,89,96
	38.3	0.01	0.01	0.02	81,81,94	0.0	0.0	0.0	0,0,0				
235	0.0	0.02	0.02	0.03	83,83,96	0.0	0.0	0.0	0,0,0	1.08e-03	9.68e-04	9.21e-04	84,90,97
	14.8	0.03	0.03	0.03	83,83,96	0.0	0.0	0.0	0,0,0				
236	0.0	0.01	0.01	0.01	83,83,96	0.0	0.0	0.0	0,0,0	-2.82e-03	-2.79e-03	-2.77e-03	83,89,96
	38.3	0.01	0.01	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
237	0.0	0.02	0.02	0.02	83,83,96	0.0	0.0	0.0	0,0,0	1.18e-04	7.42e-05	5.83e-05	84,90,97
	14.8	0.02	0.02	0.03	83,83,96	0.0	0.0	0.0	0,0,0				
238	0.0	6.81e-03	6.76e-03	8.56e-03	83,83,96	0.0	0.0	0.0	0,0,0	-4.15e-03	-3.88e-03	-3.78e-03	83,89,96
	38.3	6.40e-03	6.38e-03	8.53e-03	81,81,94	0.0	0.0	0.0	0,0,0				
239	0.0	0.01	0.01	0.01	83,83,96	0.0	0.0	0.0	0,0,0	-2.19e-03	-2.10e-03	-2.06e-03	83,89,96
	38.3	0.01	0.01	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
240	0.0	0.01	0.01	0.01	83,83,94	0.0	0.0	0.0	0,0,0	3.57e-03	3.00e-03	2.74e-03	83,89,96
	38.3	0.01	0.01	0.02	81,81,94	0.0	0.0	0.0	0,0,0				
241	0.0	0.01	0.01	0.02	83,8								

	38.3	0.01	0.01	0.02	81,81,94	0.0	0.0	0.0	0,0,0				
246	0.0	8.79e-03	8.68e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0	4.73e-03	4.40e-03	4.27e-03	83,89,96
	38.3	9.33e-03	9.23e-03	0.01	81,81,94	0.0	0.0	0.0	0,0,0				
247	0.0	0.01	0.01	0.01	83,83,96	0.0	0.0	0.0	0,0,0	2.46e-03	2.34e-03	2.30e-03	83,89,96
	38.3	0.02	0.02	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
248	0.0	0.01	0.01	0.02	83,83,94	0.0	0.0	0.0	0,0,0	-4.32e-03	-3.68e-03	-3.38e-03	83,89,96
	38.3	0.02	0.02	0.02	81,81,94	0.0	0.0	0.0	0,0,0				
249	0.0	0.01	0.01	0.02	83,83,96	0.0	0.0	0.0	0,0,0	2.08e-03	5.14e-04	5.10e-04	83,89,96
	38.3	0.01	0.01	0.02	81,81,94	0.0	0.0	0.0	0,0,0				
250	0.0	9.42e-03	9.32e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0	4.95e-03	4.58e-03	4.43e-03	83,89,96
	38.3	0.01	0.01	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
251	0.0	0.01	0.01	0.02	83,83,96	0.0	0.0	0.0	0,0,0	-2.35e-03	2.24e-03	2.20e-03	83,89,96
	38.3	0.02	0.02	0.03	83,83,96	0.0	0.0	0.0	0,0,0				
252	0.0	0.01	0.01	0.02	83,83,94	0.0	0.0	0.0	0,0,0	4.60e-03	3.84e-03	3.47e-03	83,89,96
	38.3	0.02	0.02	0.03	81,81,94	0.0	0.0	0.0	0,0,0				
253	0.0	0.01	0.01	0.02	83,83,96	0.0	0.0	0.0	0,0,0	5.48e-04	5.29e-04	5.22e-04	83,89,96
	38.3	0.01	0.01	0.02	81,81,94	0.0	0.0	0.0	0,0,0				
254	0.0	9.07e-03	9.03e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0	5.09e-03	4.66e-03	4.48e-03	83,89,96
	38.3	0.01	0.01	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
255	0.0	0.02	0.02	0.02	83,83,96	0.0	0.0	0.0	0,0,0	-3.22e-03	-3.03e-03	-2.40e-03	83,89,96
	38.3	0.02	0.02	0.03	83,83,96	0.0	0.0	0.0	0,0,0				
256	0.0	0.02	0.02	0.02	81,81,94	0.0	0.0	0.0	0,0,0	4.70e-03	3.71e-03	3.34e-03	83,89,96
	38.3	0.02	0.02	0.03	83,83,96	0.0	0.0	0.0	0,0,0				
257	0.0	0.02	0.02	0.02	83,83,96	0.0	0.0	0.0	0,0,0	8.92e-04	6.82e-04	5.78e-04	83,89,96
	38.3	0.02	0.02	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
258	0.0	8.26e-03	8.31e-03	0.01	81,81,94	0.0	0.0	0.0	0,0,0	4.93e-03	4.33e-03	4.09e-03	83,89,96
	38.3	0.01	0.01	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
259	0.0	0.03	0.03	0.04	83,83,96	0.0	0.0	0.0	0,0,0	-4.58e-03	-4.43e-03	-4.37e-03	83,89,96
	38.3	0.02	0.02	0.03	83,83,96	0.0	0.0	0.0	0,0,0				
260	0.0	0.02	0.02	0.03	81,81,94	0.0	0.0	0.0	0,0,0	-4.29e-03	2.90e-03	2.39e-03	83,89,96
	38.3	0.02	0.02	0.03	83,83,96	0.0	0.0	0.0	0,0,0				
261	0.0	0.02	0.02	0.03	83,83,96	0.0	0.0	0.0	0,0,0	1.27e-03	1.08e-03	9.89e-04	83,89,96
	38.3	0.02	0.02	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
262	0.0	0.0	0.06	0.0	84,0	0.0	0.0	0.0	0,0,0	-4.70e-03	-3.87e-03	-3.57e-03	83,89,96
	40.0	0.02	0.10	0.02	84,84,97	0.0	0.0	0.0	0,0,0				
263	0.0	0.03	0.08	0.02	84,84,97	0.0	0.0	0.0	0,0,0	8.74e-03	6.92e-03	6.35e-03	84,90,97
	198.0	0.05	0.10	0.06	81,83,94	0.0	0.0	0.0	0,0,0				
264	0.0	7.20e-03	0.11	9.60e-03	81,83,94	0.0	0.0	0.0	0,0,0	4.33e-03	4.14e-03	4.06e-03	83,89,96
	47.9	0.02	0.13	0.03	83,83,96	0.0	0.0	0.0	0,0,0				
265	0.0	0.09	0.12	0.12	83,83,96	0.0	0.0	0.0	0,0,0	0.06	0.06	0.05	81,87,94
	187.5	0.03	0.11	0.04	83,84,96	0.0	0.0	0.0	0,0,0				
	374.9	0.02	0.04	0.02	81,81,94	0.0	0.0	0.0	0,0,0				
266	0.0	6.49e-03	0.12	5.34e-03	84,84,97	0.0	0.0	0.0	0,0,0	-1.82e-03	-1.51e-03	-1.39e-03	83,89,96
	40.0	5.28e-03	0.12	5.05e-03	84,84,97	0.0	0.0	0.0	0,0,0				
267	0.0	0.04	0.13	0.04	83,83,96	0.0	0.0	0.0	0,0,0	-7.75e-03	-7.40e-03	-7.26e-03	83,89,96
	39.6	0.0	0.08	0.0	0.83,0	0.0	0.0	0.0	0,0,0				
268	0.0	7.09e-03	0.10	3.81e-03	84,84,97	0.0	0.0	0.0	0,0,0	-3.84e-03	-3.16e-03	-2.89e-03	83,89,96
	40.0	0.02	0.12	0.02	84,84,97	0.0	0.0	0.0	0,0,0				
269	0.0	0.04	0.15	0.05	83,83,96	0.0	0.0	0.0	0,0,0	-6.52e-03	-6.24e-03	-6.13e-03	83,89,96
	39.6	0.03	0.13	0.03	83,83,96	0.0	0.0	0.0	0,0,0				
270	0.0	5.47e-03	0.12	4.57e-03	84,84,97	0.0	0.0	0.0	0,0,0	-1.21e-03	-1.01e-03	9.31e-04	83,89,96
	40.0	1.94e-03	0.12	1.37e-03	84,84,97	0.0	0.0	0.0	0,0,0				
271	0.0	9.44e-03	0.11	7.09e-03	84,84,97	0.0	0.0	0.0	0,0,0	3.29e-03	2.72e-03	2.49e-03	83,89,96
	42.0	0.02	0.12	0.02	84,84,97	0.0	0.0	0.0	0,0,0				
272	0.0	0.03	0.14	0.04	83,83,96	0.0	0.0	0.0	0,0,0	-5.35e-03	-5.13e-03	-5.04e-03	83,89,96
	39.6	0.03	0.15	0.04	83,83,96	0.0	0.0	0.0	0,0,0				
273	0.0	6.15e-03	0.12	5.42e-03	84,84,97	0.0	0.0	0.0	0,0,0	-6.30e-04	-5.27e-04	-4.87e-04	83,89,96
	40.0	2.98e-04	0.11	0.0	84,84,0	0.0	0.0	0.0	0,0,0				
274	0.0	8.27e-03	0.11	7.67e-03	84,84,97	0.0	0.0	0.0	0,0,0	-6.82e-05	-6.16e-05	-5.90e-05	83,89,96
	40.0	0.0	0.10	0.0	0.84,0	0.0	0.0	0.0	0,0,0				
275	0.0	0.01	0.11	9.85e-03	84,84,97	0.0	0.0	0.0	0,0,0	5.83e-04	4.74e-04	4.41e-04	84,90,97
	40.0	0.0	0.09	0.0	0.84,0	0.0	0.0	0.0	0,0,0				
276	0.0	6.01e-03	0.09	5.12e-03	84,84,97	0.0	0.0	0.0	0,0,0	1.08e-03	8.90e-04	8.26e-04	84,90,97
	40.0	0.0	0.07	0.0	0.83,0	0.0	0.0	0.0	0,0,0				
277	0.0	0.0	0.07	0.0	0.84,0	0.0	0.0	0.0	0,0,0	2.45e-03	1.85e-03	1.62e-03	84,90,97
	45.0	0.05	0.14	0.05	84,84,97	0.0	0.0	0.0	0,0,0				
278	0.0	0.13	0.15	0.15	83,84,96	0.0	0.0	0.0	0,0,0	0.04	0.04	0.04	83,89,96
	64.5	0.04	0.04	0.05	83,83,96	0.0	0.0	0.0	0,0,0				
279	0.0	0.06	0.18	0.06	83,84,96	0.0	0.0	0.0	0,0,0	-3.39e-03	-3.21e-03	-3.14e-03	83,89,96
	45.0	0.05	0.17	0.05	83,84,96	0.0	0.0	0.0	0,0,0				
280	0.0	0.04	0.14	0.04	84,84,97	0.0	0.0	0.0	0,0,0	7.24e-04	4.65e-04	3.67e-04	84,90,97
	29.9	0.06	0.16	0.06	84,84,97	0.0	0.0	0.0	0,0,0				
281	0.0	0.06	0.17	0.06	83,84,96	0.0	0.0	0.0	0,0,0	5.42e-03	5.00e-03	4.84e-03	83,89,96
	45.0	9.28e-03	0.11	0.01	83,84,96	0.0	0.0	0.0	0,0,0				
282	0.0	0.07	0.09	0.08	83,84,96	0.0	0.0	0.0	0,0,0	-0.04	-0.03	-0.03	83,89,96
	187.5	0.03	0.09	0.03	83,84,96	0.0	0.0	0.0	0,0,0				
	374.9	4.46e-03	5.50e-03	5.94e-03	81,83,94	0.0	0.0	0.0	0,0,0				
283	0.0	0.0	0.05	0.0	0.84,0	0.0	0.0	0.0	0,0,0	-4.90e-03	4.34e-03	4.11e-03	83,89,96
	47.9	0.04	0.11	0.05	83,84,96	0.0	0.0	0.0	0,0,0				
284	0.0	0.04	0.11	0.04	83,84,96	0.0	0.0	0.0	0,0,0	-3.30e-04	-3.00e-04	-2.91e-04	84,90,97
	39.6	1.59e-03	0.06	2.13e-03	81,84,94	0.0	0.0	0.0	0,0,0				
285	0.0	0.04	0.13	0.05	83,84,96	0.0	0.0	0.0	0,0,0	6.78e-04	5.94e-04	5.60e-04	83,89,96
	39.6	0.03	0.11	0.03	83,84,96	0.0	0.0	0.0	0,0,0				
286	0.0	0.04	0.13	0.04	83,84,96	0.0	0.0	0.0	0,0,0	1.89e-03	1.68e-03	1.59e-03	83,89,96
	39.6	0.04	0.13	0.04	83,84,96	0.0	0.0	0.0	0,0,0				
287	0.0	0.0	0.10	0.0	0.84,0	0.0	0.0	0.0	0,0,0	-5.23e-03	-4.81e-03	-4.65e-03	83,89,96
	45.0	0.05	0.17	0.06	84,84,97	0.0	0.0	0.0	0,0,0				
288	0.0	0.10	0.13	0.10	84,84,97	0.0	0.0	0.0	0,0,0	0.03	0.03	0.03	81,87,94
	187.4	0.04	0.14	0.05	83,83,96	0.0	0.0	0.0	0,0,0				
	374.8	0.03	0.10	0.04	83,83,96	0.0	0.0	0.0	0,0,0				
289	0.0	0.05	0.19	0.06	84,84,97	0.0	0.0	0.0	0,0,0	-1.33e-03	-9.09e-04	-7.50e-04	84,90,97
	45.0	0.03	0.16	0.03	84,84,97	0.0	0.0	0.0	0,0,0				
290	0.0	0.04	0.17	0.05	83,84,96	0.0	0.0	0.0	0,0,0	-2.41e-03	-2.26e-03	-2.20e-03	83,89,96
	29.9	0.06	0.19	0.06	84,84,97	0.0	0.0	0.0	0,0,0				
291	0.0	0.05	0.16	0.05	84,84,97	0.0	0.0	0.0	0,0,0	-3.04e-03	-2.34e-03	-2.07e-03	84,90,97
	45.0	0.0	0.09	0.0	0.84,0	0.0	0.0	0.0	0,0,0				
292	0.0	0.05	0.19	0.06									

	39.6	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
295	0.0	0.02	0.07	0.03	81,83,94	0.0	0.0	0.0	0,0,0	-8.76e-03	-8.42e-03	-8.29e-03	83,89,96
	39.6	0.03	0.08	0.03	83,83,96	0.0	0.0	0.0	0,0,0				
296	0.0	0.02	0.08	0.03	83,83,96	0.0	0.0	0.0	0,0,0	8.09e-03	7.77e-03	7.64e-03	83,89,96
	39.6	0.02	0.07	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
297	0.0	0.02	0.07	0.03	83,83,96	0.0	0.0	0.0	0,0,0	5.95e-03	5.72e-03	5.62e-03	83,89,96
	31.3	0.01	0.05	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
298	0.0	6.54e-03	0.10	8.72e-03	81,84,94	0.0	0.0	0.0	0,0,0	-5.76e-03	-5.36e-03	-5.20e-03	83,89,96
	45.0	0.05	0.16	0.06	83,84,96	0.0	0.0	0.0	0,0,0				
299	0.0	0.11	0.13	0.12	84,84,97	0.0	0.0	0.0	0,0,0	-0.05	-0.03	-0.04	84,90,97
	100.1	0.01	0.02	0.02	81,81,94	0.0	0.0	0.0	0,0,0				
300	0.0	0.05	0.15	0.06	84,84,97	0.0	0.0	0.0	0,0,0	2.36e-03	1.70e-03	1.46e-03	84,90,97
	45.0	0.0	0.09	0.0	0,84,0	0.0	0.0	0.0	0,0,0				
301	0.0	0.05	0.18	0.06	83,84,96	0.0	0.0	0.0	0,0,0	2.23e-03	2.23e-03	2.23e-03	81,87,94
	60.1	0.04	0.17	0.05	84,84,97	0.0	0.0	0.0	0,0,0				
302	0.0	0.04	0.16	0.05	83,84,96	0.0	0.0	0.0	0,0,0	-3.86e-03	-3.69e-03	-3.62e-03	83,89,96
	45.0	0.06	0.18	0.06	83,84,96	0.0	0.0	0.0	0,0,0				
303	0.0	0.0	0.07	0.0	0,84,0	0.0	0.0	0.0	0,0,0	9.93e-04	9.20e-04	8.91e-04	83,89,96
	39.6	0.03	0.11	0.04	84,84,97	0.0	0.0	0.0	0,0,0				
304	0.0	0.02	0.08	0.03	83,84,96	0.0	0.0	0.0	0,0,0	-3.03e-03	-2.73e-03	-2.61e-03	84,90,97
	39.6	6.10e-03	0.06	8.13e-03	81,84,94	0.0	0.0	0.0	0,0,0				
305	0.0	0.02	0.11	0.02	84,84,97	0.0	0.0	0.0	0,0,0	1.66e-04	1.66e-04	1.66e-04	81,87,94
	39.6	0.04	0.14	0.04	84,84,97	0.0	0.0	0.0	0,0,0				
306	0.0	0.03	0.13	0.04	84,84,97	0.0	0.0	0.0	0,0,0	-1.08e-03	-9.10e-04	-8.46e-04	84,90,97
	39.6	0.04	0.14	0.04	83,84,96	0.0	0.0	0.0	0,0,0				
307	0.0	0.04	0.14	0.05	83,84,96	0.0	0.0	0.0	0,0,0	-1.73e-03	-1.50e-03	-1.41e-03	84,90,97
	31.3	0.03	0.13	0.04	83,84,96	0.0	0.0	0.0	0,0,0				
308	0.0	0.13	0.19	0.14	83,83,96	0.0	0.0	0.0	0,0,0	0.02	0.02	0.02	83,89,96
	100.1	4.42e-03	0.01	5.03e-03	83,84,96	0.0	0.0	0.0	0,0,0				
309	0.0	0.0	0.13	0.0	0,84,0	0.0	0.0	0.0	0,0,0	4.75e-03	3.93e-03	3.62e-03	84,90,97
	45.0	0.05	0.19	0.05	84,84,97	0.0	0.0	0.0	0,0,0				
310	0.0	0.05	0.21	0.06	83,84,96	0.0	0.0	0.0	0,0,0	-3.91e-03	-3.60e-03	-3.48e-03	83,89,96
	45.0	1.31e-03	0.14	1.75e-03	81,83,94	0.0	0.0	0.0	0,0,0				
311	0.0	0.03	0.19	0.03	84,84,97	0.0	0.0	0.0	0,0,0	2.81e-03	2.29e-03	2.09e-03	84,90,97
	45.0	0.05	0.22	0.06	84,84,97	0.0	0.0	0.0	0,0,0				
312	0.0	0.04	0.22	0.04	84,84,97	0.0	0.0	0.0	0,0,0	-4.83e-04	-4.22e-04	-3.98e-04	84,90,97
	60.1	0.04	0.22	0.05	83,84,96	0.0	0.0	0.0	0,0,0				
313	0.0	0.0	0.06	0.0	0,83,0	0.0	0.0	0.0	0,0,0	3.77e-03	3.19e-03	2.96e-03	83,89,96
	40.2	0.0	0.06	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
314	0.0	0.0	0.05	0.0	0,83,0	0.0	0.0	0.0	0,0,0	4.30e-03	3.63e-03	3.36e-03	83,89,96
	40.2	0.0	0.06	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
315	0.0	0.0	0.04	0.0	0,83,0	0.0	0.0	0.0	0,0,0	5.08e-03	4.14e-03	3.79e-03	83,89,96
	40.2	0.0	0.05	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
316	0.0	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.17e-03	-1.01e-03	-9.40e-04	83,89,96
	40.2	0.0	0.04	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
317	0.0	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.74e-03	-1.48e-03	-1.38e-03	83,89,96
	40.2	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
318	0.0	8.22e-03	0.02	9.68e-03	83,83,96	0.0	0.0	0.0	0,0,0	3.78e-03	3.42e-03	3.27e-03	83,89,96
	40.0	0.0	5.25e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
319	0.0	4.29e-03	4.12e-03	4.87e-03	83,83,96	0.0	0.0	0.0	0,0,0	-1.02e-03	-7.51e-04	-6.57e-04	84,90,97
	50.0	3.32e-03	5.70e-03	3.54e-03	83,83,96	0.0	0.0	0.0	0,0,0				
320	0.0	3.88e-03	6.62e-03	5.17e-03	81,82,94	0.0	0.0	0.0	0,0,0	5.43e-03	4.90e-03	4.72e-03	83,89,96
	40.0	2.29e-03	2.25e-03	3.05e-03	81,81,94	0.0	0.0	0.0	0,0,0				
321	0.0	0.03	0.09	0.04	83,83,96	0.0	0.0	0.0	0,0,0	3.05e-03	2.97e-03	2.94e-03	83,89,96
	50.0	0.03	0.07	0.03	83,83,96	0.0	0.0	0.0	0,0,0				
322	0.0	0.03	0.12	0.04	83,83,96	0.0	0.0	0.0	0,0,0	-0.05	-0.05	-0.04	83,89,96
	222.5	0.02	0.04	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
323	0.0	0.02	0.07	0.02	83,83,96	0.0	0.0	0.0	0,0,0	0.05	0.04	0.04	83,89,96
	222.5	9.78e-03	0.03	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
324	0.0	0.02	0.04	0.03	83,83,96	0.0	0.0	0.0	0,0,0	0.04	0.04	0.04	83,89,96
	222.5	0.04	0.12	0.04	83,83,96	0.0	0.0	0.0	0,0,0				
325	0.0	0.01	0.02	0.01	83,83,96	0.0	0.0	0.0	0,0,0	-4.88e-03	-4.39e-03	-4.19e-03	83,89,96
	40.0	0.02	0.03	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
326	0.0	2.71e-03	2.91e-03	2.86e-03	83,83,96	0.0	0.0	0.0	0,0,0	-8.81e-04	-6.62e-04	-5.85e-04	84,90,97
	40.0	4.22e-03	7.23e-03	4.48e-03	83,83,96	0.0	0.0	0.0	0,0,0				
327	0.0	5.98e-03	5.62e-03	5.30e-03	83,83,96	0.0	0.0	0.0	0,0,0	-5.41e-03	-4.92e-03	-4.73e-03	83,89,96
	40.0	9.90e-03	0.02	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
328	0.0	0.03	0.08	0.03	83,83,96	0.0	0.0	0.0	0,0,0	1.18e-03	1.11e-03	1.05e-03	84,89,96
	120.0	0.01	0.03	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
329	0.0	7.35e-03	9.58e-03	8.27e-03	83,83,96	0.0	0.0	0.0	0,0,0	4.33e-03	3.90e-03	3.72e-03	83,89,96
	40.0	0.01	0.03	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
330	0.0	2.69e-03	2.68e-03	2.22e-03	83,83,95	0.0	0.0	0.0	0,0,0	-5.29e-03	-4.87e-03	-4.71e-03	83,89,96
	40.0	6.91e-03	9.59e-03	6.34e-03	83,83,96	0.0	0.0	0.0	0,0,0				
331	0.0	3.01e-03	3.02e-03	3.12e-03	83,83,96	0.0	0.0	0.0	0,0,0	-1.68e-03	-1.32e-03	-1.18e-03	84,90,97
	50.0	1.76e-03	1.77e-03	1.60e-03	83,83,96	0.0	0.0	0.0	0,0,0				
332	0.0	0.02	0.05	0.02	83,83,96	0.0	0.0	0.0	0,0,0	-2.70e-03	-2.08e-03	-1.84e-03	84,90,97
	50.0	8.67e-03	0.02	7.49e-03	83,83,96	0.0	0.0	0.0	0,0,0				
333	0.0	2.85e-03	2.71e-03	3.07e-03	83,83,96	0.0	0.0	0.0	0,0,0	3.95e-03	3.55e-03	3.39e-03	83,89,96
	40.0	9.61e-03	0.02	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
334	0.0	2.56e-03	2.50e-03	3.40e-03	82,81,95	0.0	0.0	0.0	0,0,0	-5.58e-03	-5.57e-03	-1.73e-03	83,89,96
	40.0	3.52e-03	3.33e-03	2.55e-03	83,83,96	0.0	0.0	0.0	0,0,0				
335	0.0	3.71e-03	4.61e-03	3.80e-03	83,83,96	0.0	0.0	0.0	0,0,0	1.19e-03	9.26e-04	8.30e-04	84,90,97
	40.0	2.87e-03	2.71e-03	3.04e-03	83,83,96	0.0	0.0	0.0	0,0,0				
336	0.0	3.27e-03	4.05e-03	4.05e-03	83,82,96	0.0	0.0	0.0	0,0,0	3.74e-03	3.36e-03	3.21e-03	83,89,96
	40.0	4.90e-03	0.01	5.43e-03	83,83,96	0.0	0.0	0.0	0,0,0				
337	0.0	2.35e-03	2.35e-03	2.61e-03	83,83,96	0.0	0.0	0.0	0,0,0	-1.95e-03	-3.54e-03	-3.64e-03	83,89,96
	40.0	2.72e-03	2.64e-03	3.60e-03	82,82,95	0.0	0.0	0.0	0,0,0				
338	0.0	3.83e-03	5.37e-03	4.02e-03	83,83,96	0.0	0.0	0.0	0,0,0	1.03e-03	7.92e-04	7.06e-04	84,90,97
	40.0	3.98e-03	5.80e-03	4.20e-03	83,83,96	0.0	0.0	0.0	0,0,0				
339	0.0	0.0	0.09	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.69e-03	-2.41e-03	-2.30e-03	84,90,97
	38.3	0.0	0.09	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
340	0.0	7.72e-03	0.02	9.01e-03	83,83,96	0.0	0.0	0.0	0,0,0	-1.72e-03	-1.56e-03	-1.49e-03	84,90,97
	38.3	0.0	0.01	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
341	0.0	0.0	0.11	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-8.22e-04	-5.91e-04	-5.10e-04	84,90,97
	38.3	0.0	0.11	0.0	0,83,0	0.0	0.0	0.0	0				

	222.5	0.12	0.19	0.15	83,83,96	0.0	0.0	0.0	0,0,0				
345	0.0	0.07	0.13	0.08	83,83,96	0.0	0.0	0.0	0,0,0	-1.67e-03	-1.45e-03	-1.37e-03	84,90,97
	50.0	0.0	0.04	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
346	0.0	0.06	0.12	0.06	83,83,96	0.0	0.0	0.0	0,0,0	-0.03	-0.03	-0.03	83,89,96
	111.3	0.0	0.04	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
	222.5	0.03	0.08	0.03	83,83,96	0.0	0.0	0.0	0,0,0				
347	0.0	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.79e-03	-1.65e-03	-1.59e-03	83,89,96
	40.0	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
348	0.0	1.24e-03	5.03e-03	1.65e-03	81,81,94	0.0	0.0	0.0	0,0,0	-1.69e-03	-1.46e-03	-1.38e-03	84,90,97
	50.0	5.58e-04	4.43e-03	6.20e-04	83,84,96	0.0	0.0	0.0	0,0,0				
349	0.0	8.56e-04	0.02	1.14e-03	81,83,94	0.0	0.0	0.0	0,0,0	-1.55e-03	-1.38e-03	-1.32e-03	83,89,96
	40.0	0.0	0.01	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
350	0.0	0.05	0.07	0.06	83,83,96	0.0	0.0	0.0	0,0,0	7.02e-04	7.02e-04	7.02e-04	81,87,94
	38.3	7.45e-03	0.01	9.13e-03	83,83,96	0.0	0.0	0.0	0,0,0				
351	0.0	0.04	0.06	0.04	84,84,97	0.0	0.0	0.0	0,0,0	-0.04	-0.03	-0.03	84,90,97
	78.5	0.09	0.20	0.09	84,84,97	0.0	0.0	0.0	0,0,0				
352	0.0	0.07	0.12	0.07	84,84,97	0.0	0.0	0.0	0,0,0	-0.17	-0.05	-0.05	84,90,97
	87.5	0.13	0.29	0.14	83,83,96	0.0	0.0	0.0	0,0,0				
353	0.0	0.04	0.02	0.04	84,84,97	0.0	0.0	0.0	0,0,0	5.44e-04	4.90e-04	4.73e-04	84,90,97
	39.6	0.05	0.04	0.05	84,84,97	0.0	0.0	0.0	0,0,0				
354	0.0	0.07	0.14	0.08	83,83,96	0.0	0.0	0.0	0,0,0	7.01e-03	6.09e-03	5.73e-03	84,90,97
	39.6	0.13	0.23	0.15	83,83,96	0.0	0.0	0.0	0,0,0				
355	0.0	0.0	0.12	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-9.55e-04	-7.10e-04	-6.22e-04	84,90,97
	38.3	0.0	0.12	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
356	0.0	0.0	0.09	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-4.20e-03	-3.80e-03	-3.63e-03	83,89,96
	54.5	0.0	0.13	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
357	0.0	0.0	0.09	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.80e-04	9.54e-05	9.54e-05	84,87,94
	21.8	0.0	0.09	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
358	0.0	0.0	0.09	0.0	0,83,0	0.0	0.0	0.0	0,0,0	2.84e-04	1.95e-04	1.59e-04	83,89,96
	54.5	0.0	0.10	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
359	0.0	0.07	0.16	0.08	83,83,96	0.0	0.0	0.0	0,0,0	-0.01	-0.01	-0.01	82,91,95
	120.5	0.07	0.17	0.08	84,84,97	0.0	0.0	0.0	0,0,0				
	241.0	0.10	0.16	0.12	83,83,96	0.0	0.0	0.0	0,0,0				
360	0.0	2.14e-03	0.04	2.86e-03	81,83,94	0.0	0.0	0.0	0,0,0	-1.70e-03	-1.06e-03	-8.30e-04	84,90,97
	120.0	0.02	0.05	0.02	81,83,94	0.0	0.0	0.0	0,0,0				
361	0.0	0.0	8.92e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.13e-03	-1.96e-03	-1.89e-03	83,89,96
	40.0	8.55e-04	0.01	8.51e-04	83,83,96	0.0	0.0	0.0	0,0,0				
362	0.0	0.0	5.19e-03	0.0	0,84,0	0.0	0.0	0.0	0,0,0	-1.28e-03	-1.10e-03	-1.03e-03	84,90,97
	40.0	0.0	4.84e-03	0.0	0,84,0	0.0	0.0	0.0	0,0,0				
363	0.0	0.0	6.63e-03	0.0	0,84,0	0.0	0.0	0.0	0,0,0	-1.80e-03	-1.61e-03	-1.54e-03	83,89,96
	40.0	0.0	5.80e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
364	0.0	0.07	0.17	0.07	84,83,97	0.0	0.0	0.0	0,0,0	-1.43e-03	-1.27e-03	-1.21e-03	84,90,97
	54.5	0.06	0.15	0.06	84,83,97	0.0	0.0	0.0	0,0,0				
365	0.0	0.09	0.20	0.09	84,84,97	0.0	0.0	0.0	0,0,0	-0.04	-0.03	-0.03	84,90,97
	119.0	0.06	0.13	0.05	84,84,97	0.0	0.0	0.0	0,0,0				
366	0.0	0.08	0.17	0.09	84,83,97	0.0	0.0	0.0	0,0,0	-2.27e-03	-2.03e-03	-1.93e-03	83,89,96
	29.9	0.09	0.19	0.10	84,84,97	0.0	0.0	0.0	0,0,0				
367	0.0	0.0	0.05	0.0	0,84,0	0.0	0.0	0.0	0,0,0	-0.06	-0.05	-0.04	83,89,96
	100.1	0.35	0.59	0.41	83,83,96	0.18	0.18	0.17	83,89,96				
368	0.0	0.09	0.20	0.09	83,83,96	0.0	0.0	0.0	0,0,0	-4.59e-03	-4.13e-03	-3.95e-03	83,89,96
	47.9	0.11	0.24	0.12	84,83,97	0.0	0.0	0.0	0,0,0				
369	0.0	0.0	0.10	0.0	0,83,0	0.0	0.0	0.0	0,0,0	9.13e-04	9.13e-04	9.13e-04	81,87,94
	38.3	0.0	0.10	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
370	0.0	0.01	0.05	0.01	84,83,97	0.0	0.0	0.0	0,0,0	-1.24e-03	-1.13e-03	-1.09e-03	83,89,96
	23.5	9.06e-03	0.05	8.75e-03	84,83,97	0.0	0.0	0.0	0,0,0				
371	0.0	0.0	0.08	0.0	0,83,0	0.0	0.0	0.0	0,0,0	1.26e-03	1.24e-03	1.23e-03	83,89,96
	38.3	0.0	0.08	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
372	0.0	0.02	0.02	0.03	83,83,96	0.0	0.0	0.0	0,0,0	1.19e-03	1.14e-03	1.13e-03	83,89,96
	38.3	0.01	4.98e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
373	0.0	0.0	0.01	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.14e-03	-1.96e-03	-1.89e-03	83,89,96
	40.0	0.0	0.01	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
374	0.0	0.0	8.92e-03	0.0	0,84,0	0.0	0.0	0.0	0,0,0	-1.86e-03	-1.66e-03	-1.59e-03	83,89,96
	40.0	0.0	9.59e-03	0.0	0,84,0	0.0	0.0	0.0	0,0,0				
375	0.0	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-9.22e-04	-7.67e-04	-7.09e-04	84,90,97
	23.5	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
376	0.0	0.13	0.29	0.14	83,83,96	0.0	0.0	0.0	0,0,0	-0.17	-0.05	-0.05	84,87,94
	374.8	0.34	0.53	0.40	83,83,96	0.15	0.16	0.15	83,89,96				
377	0.0	0.04	0.08	0.04	84,84,97	0.0	0.0	0.0	0,0,0	-1.46e-03	-1.23e-03	-1.14e-03	83,89,96
	31.3	0.05	0.09	0.05	84,84,97	0.0	0.0	0.0	0,0,0				
378	0.0	0.13	0.25	0.14	83,83,96	0.0	0.0	0.0	0,0,0	1.99e-03	1.67e-03	1.55e-03	84,90,97
	39.6	0.10	0.20	0.11	83,83,96	0.0	0.0	0.0	0,0,0				
379	0.0	0.0	0.15	0.0	0,83,0	0.0	0.0	0.0	0,0,0	7.26e-04	5.53e-04	4.91e-04	84,90,97
	38.3	0.0	0.15	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
380	0.0	0.03	0.06	0.03	84,83,97	0.0	0.0	0.0	0,0,0	-2.82e-03	-2.66e-03	-2.59e-03	83,89,96
	38.3	0.02	0.05	0.02	84,83,97	0.0	0.0	0.0	0,0,0				
381	0.0	0.0	0.06	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-3.56e-03	-3.35e-03	-3.26e-03	83,89,96
	38.3	0.0	0.06	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
382	0.0	0.02	0.10	0.02	84,83,97	0.0	0.0	0.0	0,0,0	-2.88e-04	-2.88e-04	-2.88e-04	81,87,94
	38.3	2.32e-03	0.08	0.0	84,83,0	0.0	0.0	0.0	0,0,0				
383	0.0	0.10	0.17	0.12	83,83,96	0.0	0.0	0.0	0,0,0	2.74e-03	2.35e-03	2.21e-03	84,90,97
	53.5	0.10	0.17	0.12	83,83,96	0.0	0.0	0.0	0,0,0				
384	0.0	0.02	0.05	0.02	81,83,94	0.0	0.0	0.0	0,0,0	-2.28e-03	-2.04e-03	-1.94e-03	84,90,97
	50.0	0.03	0.07	0.04	83,83,96	0.0	0.0	0.0	0,0,0				
385	0.0	0.0	4.87e-03	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-1.45e-03	-1.24e-03	-1.16e-03	84,90,97
	50.0	2.76e-03	0.01	3.32e-03	83,83,96	0.0	0.0	0.0	0,0,0				
386	0.0	0.03	0.10	0.02	84,83,97	0.0	0.0	0.0	0,0,0	-1.78e-03	-1.78e-03	-1.78e-03	81,87,94
	38.3	0.0	0.06	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
387	0.0	2.28e-03	0.02	3.03e-03	81,83,94	0.0	0.0	0.0	0,0,0	-7.05e-04	-5.50e-04	-4.96e-04	83,89,96
	38.0	7.62e-04	0.02	1.02e-03	81,83,94	0.0	0.0	0.0	0,0,0				
388	0.0	0.06	0.15	0.06	83,83,96	0.0	0.0	0.0	0,0,0	-0.07	-0.06	-0.05	84,90,97
	214.6	0.10	0.24	0.11	84,84,97	0.0	0.0	0.0	0,0,0				
389	0.0	0.10	0.22	0.11	83,83,96	0.0	0.0	0.0	0,0,0	6.29e-04	5.59e-04	5.31e-04	83,89,96
	60.1	0.08	0.19	0.08	84,83,97	0.0	0.0	0.0	0,0,0				
390	0.0	0.0	0.06	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-0.11	-0.08	-0.06	83,89,96
	374.8	0.25	0.44	0.27	83,83,96	0.12	0.0	0.0	83,0,0				
391	0.0	1.23e-03	7.04e-03	1.64e-03	83,83,96	0.0	0.0	0.0	0,0,0	-1.66e-03	-1.49e-03	-1.42e-03	84,90,97
	38.3	0.0	4.18e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
392	0.0	0.0	0.02	0.0	0,83,0	0							

394	0.0	7.87e-03	9.07e-03	9.64e-03	83,83,96	0.0	0.0	0.0	0,0,0	8.28e-04	8.28e-04	8.28e-04	81,87,94
	38.3	9.99e-04	5.51e-04	1.18e-03	83,83,96	0.0	0.0	0.0	0,0,0				
395	0.0	0.05	0.06	0.05	84,84,97	0.0	0.0	0.0	0,0,0	-1.38e-03	-1.14e-03	-1.04e-03	83,89,96
	47.9	0.04	0.05	0.05	84,84,97	0.0	0.0	0.0	0,0,0				
396	0.0	0.0	0.08	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-3.28e-03	-3.10e-03	-3.02e-03	83,89,96
	38.3	0.0	0.08	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
397	0.0	9.89e-03	0.02	7.71e-03	83,83,96	0.0	0.0	0.0	0,0,0	0.02	0.02	0.02	83,89,96
	222.5	0.02	0.02	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
398	0.0	0.0	0.06	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-8.38e-04	-8.38e-04	-8.38e-04	81,87,94
	40.2	0.0	0.06	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
399	0.0	0.0	5.29e-03	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-1.19e-03	-1.01e-03	-9.48e-04	84,90,97
	40.0	0.0	4.65e-03	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
400	0.0	0.0	0.08	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-0.05	-0.04	-0.04	84,90,97
	120.5	0.0	0.12	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
401	0.0	0.02	0.03	0.01	84,84,97	0.0	0.0	0.0	0,0,0	-6.00e-04	-2.77e-04	-1.48e-04	83,89,96
	40.0	9.61e-03	0.02	5.28e-03	84,84,97	0.0	0.0	0.0	0,0,0				
402	0.0	0.23	0.36	0.24	84,84,97	0.0	0.0	0.0	0,0,0	-0.07	-0.06	-0.05	84,90,97
	100.1	0.06	0.14	0.07	83,83,96	0.0	0.0	0.0	0,0,0				
403	0.0	0.06	0.13	0.08	83,83,96	0.0	0.0	0.0	0,0,0	7.94e-03	7.16e-03	6.85e-03	83,89,96
	45.0	0.13	0.23	0.15	83,83,96	0.0	0.0	0.0	0,0,0				
404	0.0	0.28	0.50	0.31	84,83,97	0.14	0.14	0.0	83,89,0	-0.11	-0.08	-0.06	83,89,96
	87.5	0.0	0.06	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
405	0.0	7.89e-03	0.05	7.17e-03	84,83,97	0.0	0.0	0.0	0,0,0	-1.53e-03	-1.41e-03	-1.36e-03	83,89,96
	38.3	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
406	0.0	0.01	5.28e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0	1.68e-03	1.60e-03	1.57e-03	83,89,96
	38.3	5.27e-03	3.00e-03	6.26e-03	83,83,96	0.0	0.0	0.0	0,0,0				
407	0.0	8.16e-04	0.02	0.0	84,83,0	0.0	0.0	0.0	0,0,0	-1.71e-03	-1.45e-03	-1.35e-03	84,90,97
	38.3	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
408	0.0	0.06	0.10	0.08	83,83,96	0.0	0.0	0.0	0,0,0	7.88e-03	7.02e-03	6.68e-03	83,89,96
	45.0	0.13	0.21	0.15	83,83,96	0.0	0.0	0.0	0,0,0				
409	0.0	0.21	0.39	0.21	84,84,97	0.0	0.0	0.0	0,0,0	-0.06	-0.05	-0.04	84,90,97
	374.9	0.0	0.06	0.0	0,84,0	0.0	0.0	0.0	0,0,0				
410	0.0	0.10	0.21	0.11	83,83,96	0.0	0.0	0.0	0,0,0	-4.27e-04	-4.27e-04	-4.27e-04	81,87,94
	39.6	0.08	0.18	0.09	83,83,96	0.0	0.0	0.0	0,0,0				
411	0.0	0.0	0.14	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.71e-03	-1.71e-03	-1.71e-03	81,87,94
	38.3	0.0	0.13	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
412	0.0	0.0	9.51e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-4.19e-03	-3.90e-03	-3.79e-03	83,89,96
	38.3	0.02	0.03	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
413	0.0	0.0	0.10	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.71e-03	-1.65e-03	-1.63e-03	83,89,96
	38.3	0.0	0.10	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
414	0.0	0.02	0.03	0.03	83,83,96	0.0	0.0	0.0	0,0,0	-1.52e-04	-1.52e-04	-1.51e-04	82,91,95
	38.3	3.17e-03	1.69e-03	3.18e-03	83,83,96	0.0	0.0	0.0	0,0,0				
415	0.0	0.03	0.07	0.03	83,83,96	0.0	0.0	0.0	0,0,0	-1.05e-04	-1.05e-04	-1.05e-04	81,87,94
	25.8	0.03	0.07	0.04	83,83,96	0.0	0.0	0.0	0,0,0				
416	0.0	1.31e-03	0.01	1.75e-03	81,83,94	0.0	0.0	0.0	0,0,0	-5.17e-03	-4.89e-03	-4.79e-03	83,89,96
	38.3	0.05	0.08	0.06	83,83,96	0.0	0.0	0.0	0,0,0				
417	0.0	0.06	0.05	0.06	84,84,97	0.0	0.0	0.0	0,0,0	0.02	0.01	0.01	84,90,97
	198.0	0.22	0.23	0.24	84,84,97	0.0	0.0	0.0	0,0,0				
418	0.0	0.10	0.25	0.10	84,84,97	0.0	0.0	0.0	0,0,0	-0.07	-0.06	-0.05	83,89,96
	160.3	0.35	0.58	0.39	83,83,96	0.18	0.17	0.16	83,89,96				
419	0.0	0.0	0.05	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-0.05	-0.03	-0.03	83,89,96
	87.5	0.32	0.54	0.36	83,83,96	0.16	0.16	0.15	83,89,96				
420	0.0	0.09	0.24	0.10	83,83,96	0.0	0.0	0.0	0,0,0	-2.65e-03	-2.42e-03	-2.33e-03	83,89,96
	29.9	0.11	0.27	0.13	83,83,96	0.0	0.0	0.0	0,0,0				
421	0.0	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.03e-03	-1.86e-03	-1.80e-03	83,89,96
	40.0	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
422	0.0	0.0	0.01	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-9.36e-04	-8.38e-04	-7.99e-04	83,89,96
	40.0	0.0	0.01	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
423	0.0	0.0	0.14	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-5.80e-04	-4.83e-04	-4.46e-04	84,90,97
	38.3	0.0	0.15	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
424	0.0	0.0	0.19	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-5.35e-03	-4.77e-03	-4.53e-03	83,89,96
	40.2	0.0	0.16	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
425	0.0	0.0	0.07	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-4.47e-04	-4.47e-04	-4.47e-04	81,87,94
	40.2	0.0	0.10	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
426	0.0	0.0	5.22e-03	0.0	0,84,0	0.0	0.0	0.0	0,0,0	-1.23e-03	-1.05e-03	-9.85e-04	84,90,97
	40.0	0.0	4.91e-03	0.0	0,84,0	0.0	0.0	0.0	0,0,0				
427	0.0	0.05	0.18	0.04	84,83,97	0.0	0.0	0.0	0,0,0	-0.05	-0.04	-0.04	84,90,97
	120.5	0.0	0.09	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
428	0.0	0.09	0.18	0.10	84,84,97	0.0	0.0	0.0	0,0,0	-7.25e-03	-6.35e-03	-6.00e-03	83,89,96
	45.0	0.04	0.09	0.04	84,84,97	0.0	0.0	0.0	0,0,0				
429	0.0	0.11	0.23	0.12	84,83,97	0.0	0.0	0.0	0,0,0	-8.48e-03	-7.53e-03	-7.15e-03	83,89,96
	39.6	0.05	0.14	0.06	84,83,97	0.0	0.0	0.0	0,0,0				
430	0.0	0.09	0.19	0.09	84,84,97	0.0	0.0	0.0	0,0,0	-8.03e-03	-6.79e-03	-6.30e-03	84,90,97
	39.6	0.04	0.12	0.04	84,84,97	0.0	0.0	0.0	0,0,0				
431	0.0	0.01	0.08	0.0	84,83,0	0.0	0.0	0.0	0,0,0	-1.42e-03	-1.42e-03	-1.42e-03	81,87,94
	38.3	0.0	0.06	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
432	0.0	0.0	6.69e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-4.16e-03	-3.88e-03	-3.77e-03	83,89,96
	38.3	0.0	9.55e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
433	0.0	0.0	0.13	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-3.94e-03	-3.80e-03	-3.74e-03	83,89,96
	38.3	0.0	0.13	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
434	0.0	0.01	5.48e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0	-1.68e-03	-1.61e-03	-1.58e-03	83,89,96
	38.3	0.02	0.02	0.03	83,83,96	0.0	0.0	0.0	0,0,0				
435	0.0	0.0	6.93e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-5.01e-03	-4.76e-03	-4.66e-03	83,89,96
	38.3	2.60e-03	0.01	3.47e-03	81,83,94	0.0	0.0	0.0	0,0,0				
436	0.0	1.22e-03	0.02	1.63e-03	81,84,94	0.0	0.0	0.0	0,0,0	-4.32e-04	-7.33e-04	-6.71e-04	83,89,96
	40.0	0.0	0.02	0.0	0,84,0	0.0	0.0	0.0	0,0,0				
437	0.0	0.0	0.06	0.0	0,84,0	0.0	0.0	0.0	0,0,0	-0.05	-0.03	-0.03	83,89,96
	310.3	0.0	0.07	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
438	0.0	0.02	0.16	0.02	84,83,97	0.0	0.0	0.0	0,0,0	6.14e-03	5.25e-03	4.90e-03	84,90,97
	45.0	0.09	0.25	0.09	84,83,97	0.0	0.0	0.0	0,0,0				
439	0.0	2.98e-04	1.95e-03	3.97e-04	81,84,94	0.0	0.0	0.0	0,0,0	-1.66e-03	-1.48e-03	-1.42e-03	84,90,97
	38.3	0.0	1.37e-03	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
440	0.0	0.0	3.92e-03	0.0	0,84,0	0.0	0.0	0.0	0,0,0	8.16e-04	8.16e-04	8.16e-04	81,87,94
	38.3	0.0	3.43e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
441	0.0	0.04	0.04	0.04	84,83,97	0.0	0.0	0.0	0,0,0	-5.39e-03	-4.95e-03	-4.77e-03	83,89,96
	54.5	0.03	0.02	0.03	84,81,97	0.0	0.0	0.0	0,0,0				
442	0.0	0.0	0.06	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.46e-03	-1.42e-03	-1.41e-03	83,89,96

	40.0	3.64e-03	0.01	4.85e-03	81,81,94	0.0	0.0	0.0	0,0,0				
445	0.0	0.13	0.25	0.15	83,83,96	0.0	0.0	0.0	0,0,0	1.58e-03	1.42e-03	1.36e-03	84,90,97
	29.9	0.10	0.22	0.12	83,83,96	0.0	0.0	0.0	0,0,0				
446	0.0	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.00e-03	-1.83e-03	-1.76e-03	83,89,96
	38.3	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
447	0.0	5.74e-03	3.29e-03	6.83e-03	83,83,96	0.0	0.0	0.0	0,0,0	1.82e-03	1.73e-03	1.69e-03	83,89,96
	38.3	4.13e-03	2.52e-03	4.94e-03	83,83,96	0.0	0.0	0.0	0,0,0				
448	0.0	0.0	0.01	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.87e-03	-1.60e-03	-1.49e-03	84,90,97
	38.3	0.0	0.01	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
449	0.0	0.13	0.23	0.15	83,83,96	0.0	0.0	0.0	0,0,0	1.93e-03	1.66e-03	1.55e-03	84,90,97
	45.0	0.09	0.18	0.11	83,83,96	0.0	0.0	0.0	0,0,0				
450	0.0	0.08	0.18	0.09	83,83,96	0.0	0.0	0.0	0,0,0	-1.36e-03	-1.25e-03	-1.21e-03	83,89,96
	31.3	0.09	0.19	0.10	83,84,96	0.0	0.0	0.0	0,0,0				
451	0.0	0.0	0.12	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.16e-03	-1.15e-03	-1.14e-03	83,89,96
	38.3	0.0	0.12	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
452	0.0	0.0	0.12	0.0	0,83,0	0.0	0.0	0.0	0,0,0	4.26e-04	4.26e-04	4.26e-04	81,87,94
	38.3	0.0	0.12	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
453	0.0	0.09	0.21	0.10	83,83,96	0.0	0.0	0.0	0,0,0	2.09e-04	1.85e-04	1.79e-04	84,90,97
	31.3	0.08	0.19	0.09	83,83,96	0.0	0.0	0.0	0,0,0				
454	0.0	0.0	0.14	0.0	0,84,0	0.0	0.0	0.0	0,0,0	-0.10	-0.09	-0.09	81,87,94
	374.9	0.23	0.49	0.22	84,84,97	0.14	0.0	0.0	84,0,0				
455	0.0	0.0	0.14	0.0	0,83,0	0.0	0.0	0.0	0,0,0	1.59e-03	1.32e-03	1.22e-03	84,90,97
	38.3	0.0	0.14	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
456	0.0	0.07	0.15	0.07	84,84,97	0.0	0.0	0.0	0,0,0	-4.32e-03	-3.68e-03	-3.43e-03	83,89,96
	39.6	0.09	0.18	0.09	84,84,97	0.0	0.0	0.0	0,0,0				
457	0.0	0.0	5.98e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-4.14e-03	-3.87e-03	-3.76e-03	83,89,96
	38.3	0.0	6.13e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
458	0.0	5.95e-03	3.43e-03	7.03e-03	83,83,96	0.0	0.0	0.0	0,0,0	-2.17e-03	-2.05e-03	-2.00e-03	83,89,96
	38.3	0.01	5.49e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
459	0.0	1.46e-03	4.63e-03	1.35e-03	83,83,96	0.0	0.0	0.0	0,0,0	-4.85e-03	-4.62e-03	-4.53e-03	83,89,96
	38.3	1.23e-03	4.32e-03	9.76e-04	83,83,96	0.0	0.0	0.0	0,0,0				
460	0.0	0.21	0.38	0.23	84,84,97	0.0	0.0	0.0	0,0,0	-0.05	-0.03	-0.03	84,90,97
	64.5	0.0	0.05	0.0	0,84,0	0.0	0.0	0.0	0,0,0				
461	0.0	0.0	0.12	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-8.62e-04	-8.62e-04	-8.62e-04	81,87,94
	38.3	0.0	0.13	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
462	0.0	0.0	0.09	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.68e-03	-2.55e-03	-2.50e-03	83,89,96
	38.3	0.0	0.08	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
463	0.0	0.07	0.13	0.07	83,83,96	0.0	0.0	0.0	0,0,0	7.53e-03	6.65e-03	6.29e-03	84,90,97
	39.6	0.13	0.22	0.14	83,83,96	0.0	0.0	0.0	0,0,0				
464	0.0	0.31	0.59	0.36	83,83,96	0.18	0.18	0.18	83,89,96	-0.10	-0.09	-0.09	83,89,96
	100.1	0.0	0.12	0.0	0,84,0	0.0	0.0	0.0	0,0,0				
465	0.0	0.03	0.09	0.04	83,83,96	0.0	0.0	0.0	0,0,0	-2.04e-04	-2.04e-04	-2.04e-04	81,87,94
	39.7	0.02	0.08	0.03	83,84,96	0.0	0.0	0.0	0,0,0				
466	0.0	0.01	0.20	8.91e-03	83,83,96	0.0	0.0	0.0	0,0,0	-3.17e-03	-2.83e-03	-2.69e-03	83,89,96
	39.7	0.05	0.24	0.06	83,83,96	0.0	0.0	0.0	0,0,0				
467	0.0	3.11e-03	0.01	3.86e-03	83,84,96	0.0	0.0	0.0	0,0,0	-8.61e-04	-4.07e-04	-3.75e-04	83,89,96
	40.0	1.50e-03	8.49e-03	2.01e-03	81,84,94	0.0	0.0	0.0	0,0,0				
468	0.0	0.07	0.21	0.08	83,83,96	0.0	0.0	0.0	0,0,0	-1.71e-03	-1.64e-03	-1.61e-03	83,89,96
	60.1	0.09	0.24	0.10	83,83,96	0.0	0.0	0.0	0,0,0				
469	0.0	7.55e-04	4.55e-04	1.01e-03	81,81,94	0.0	0.0	0.0	0,0,0	-1.67e-03	-1.50e-03	-1.43e-03	84,90,97
	38.3	1.01e-03	5.75e-04	1.34e-03	81,81,94	0.0	0.0	0.0	0,0,0				
470	0.0	0.0	6.06e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	4.08e-04	4.08e-04	4.08e-04	81,87,94
	38.3	0.0	6.69e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
471	0.0	1.26e-03	0.02	1.68e-03	81,81,94	0.0	0.0	0.0	0,0,0	-5.05e-04	-2.22e-04	-3.89e-04	83,89,96
	42.0	1.89e-03	0.02	2.52e-03	81,83,94	0.0	0.0	0.0	0,0,0				
472	0.0	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.20e-03	-2.00e-03	-1.93e-03	83,89,96
	38.3	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
473	0.0	2.26e-03	1.36e-03	2.73e-03	83,83,96	0.0	0.0	0.0	0,0,0	1.82e-03	1.73e-03	1.70e-03	83,89,96
	38.3	2.19e-03	1.32e-03	2.50e-03	83,83,96	0.0	0.0	0.0	0,0,0				
474	0.0	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.04e-03	-1.76e-03	-1.65e-03	84,90,97
	38.3	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
475	0.0	0.09	0.20	0.10	83,83,96	0.0	0.0	0.0	0,0,0	-1.45e-03	-1.35e-03	-1.32e-03	83,89,96
	60.1	0.08	0.19	0.09	84,83,97	0.0	0.0	0.0	0,0,0				
476	0.0	0.02	0.09	0.02	83,83,96	0.0	0.0	0.0	0,0,0	-8.61e-04	-8.28e-04	-8.15e-04	83,89,96
	39.7	8.82e-04	0.08	7.75e-04	83,83,96	0.0	0.0	0.0	0,0,0				
477	0.0	0.0	0.26	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-4.11e-03	-3.70e-03	-3.54e-03	83,89,96
	39.7	0.05	0.31	0.06	83,83,96	0.0	0.0	0.0	0,0,0				
478	0.0	0.04	0.12	0.05	84,83,97	0.0	0.0	0.0	0,0,0	-0.10	-0.06	-0.03	84,90,97
	100.1	0.25	0.41	0.27	83,83,96	0.11	0.0	0.0	83,0,0				
479	0.0	0.0	0.09	0.0	0,83,0	0.0	0.0	0.0	0,0,0	1.30e-03	9.68e-04	8.44e-04	84,90,97
	47.9	0.0	0.06	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
480	0.0	7.52e-03	0.07	8.42e-03	83,83,96	0.0	0.0	0.0	0,0,0	-1.32e-03	-1.24e-03	-1.22e-03	83,89,96
	39.7	0.0	0.06	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
481	0.0	0.04	0.10	0.05	84,84,97	0.0	0.0	0.0	0,0,0	-2.63e-03	-2.24e-03	-2.09e-03	83,89,96
	39.6	0.07	0.14	0.07	84,84,97	0.0	0.0	0.0	0,0,0				
482	0.0	0.0	5.57e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-4.12e-03	-3.85e-03	-3.74e-03	83,89,96
	38.3	0.0	5.22e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
483	0.0	3.80e-03	2.32e-03	4.54e-03	83,83,96	0.0	0.0	0.0	0,0,0	-2.30e-03	-2.17e-03	-2.12e-03	83,89,96
	38.3	5.39e-03	3.08e-03	6.38e-03	83,83,96	0.0	0.0	0.0	0,0,0				
484	0.0	1.79e-03	1.06e-03	1.96e-03	83,81,96	0.0	0.0	0.0	0,0,0	-4.73e-03	-4.51e-03	-4.42e-03	83,89,96
	38.3	2.01e-03	1.32e-03	2.19e-03	83,83,96	0.0	0.0	0.0	0,0,0				
485	0.0	0.07	0.19	0.08	84,83,97	0.0	0.0	0.0	0,0,0	-3.03e-03	-2.63e-03	-2.48e-03	83,89,96
	45.0	0.08	0.21	0.09	84,84,97	0.0	0.0	0.0	0,0,0				
486	0.0	0.0	0.10	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-3.36e-03	-3.27e-03	-3.24e-03	83,89,96
	38.3	0.0	0.10	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
487	0.0	0.0	0.11	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.46e-03	-1.24e-03	-1.16e-03	84,90,97
	38.3	0.0	0.11	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
488	0.0	0.11	0.27	0.13	83,83,96	0.0	0.0	0.0	0,0,0	-9.18e-03	-8.36e-03	-8.03e-03	83,89,96
	45.0	0.05	0.17	0.05	83,83,96	0.0	0.0	0.0	0,0,0				
489	0.0	0.09	0.23	0.10	84,83,97	0.0	0.0	0.0	0,0,0	1.46e-03	1.18e-03	1.07e-03	84,90,97
	45.0	0.07	0.21	0.08	83,83,96	0.0	0.0	0.0	0,0,0				
490	0.0	0.0	0.07	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-3.34e-03	-2.99e-03	-2.86e-03	83,89,96
	38.3	2.02e-03	0.11	0.0	84,83,0	0.0	0.0	0.0	0,0,0				
491	0.0	0.0	0.15	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-4.27e-04	-4.27e-04	-4.27e-04	81,87,94
	38.3	0.0	0.14	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
492	0.0	0.32	0.53	0.36	84,83,97	0.15	0.15	0.14	83,89,96	-0.10	-0.06	-0.0	

495	0.0	4.13e-03	0.04	4.85e-03	83,84,96	0.0	0.0	0.0	0.0,0	-2.29e-03	-2.15e-03	-2.09e-03	83,89,96
	55.2	0.0	0.03	0.0	0.84,0	0.0	0.0	0.0	0.0,0				
496	0.0	0.0	0.09	0.0	0.83,0	0.0	0.0	0.0	0.0,0	-6.30e-04	-3.36e-04	-2.35e-04	84,90,97
	54.8	0.0	0.09	0.0	0.83,0	0.0	0.0	0.0	0.0,0				
497	0.0	2.07e-03	6.81e-03	2.64e-03	83,84,96	0.0	0.0	0.0	0.0,0	-9.75e-04	-8.18e-04	-7.55e-04	83,89,96
	40.0	0.0	2.76e-03	0.0	0.84,0	0.0	0.0	0.0	0.0,0				
498	0.0	1.74e-03	1.04e-03	2.27e-03	83,83,96	0.0	0.0	0.0	0.0,0	-1.68e-03	-1.50e-03	-1.43e-03	84,90,97
	38.3	3.31e-03	1.79e-03	4.39e-03	83,83,96	0.0	0.0	0.0	0.0,0				
499	0.0	0.0	7.64e-03	0.0	0.83,0	0.0	0.0	0.0	0.0,0	3.81e-04	3.81e-04	3.81e-04	81,87,94
	38.3	0.0	8.04e-03	0.0	0.83,0	0.0	0.0	0.0	0.0,0				
500	0.0	0.0	0.04	0.0	0.83,0	0.0	0.0	0.0	0.0,0	-2.31e-03	-2.11e-03	-2.03e-03	83,89,96
	38.3	0.0	0.04	0.0	0.83,0	0.0	0.0	0.0	0.0,0				
501	0.0	2.24e-03	1.36e-03	2.56e-03	83,83,96	0.0	0.0	0.0	0.0,0	9.32e-04	8.89e-04	8.72e-04	83,89,96
	38.3	2.49e-03	1.47e-03	2.85e-03	83,83,96	0.0	0.0	0.0	0.0,0				
502	0.0	0.0	0.03	0.0	0.83,0	0.0	0.0	0.0	0.0,0	-2.31e-03	-2.01e-03	-1.88e-03	84,90,97
	38.3	0.0	0.03	0.0	0.83,0	0.0	0.0	0.0	0.0,0				
503	0.0	0.0	0.13	0.0	0.83,0	0.0	0.0	0.0	0.0,0	-1.22e-03	-9.51e-04	-8.53e-04	84,90,97
	38.3	0.0	0.13	0.0	0.83,0	0.0	0.0	0.0	0.0,0				
504	0.0	0.0	0.08	0.0	0.83,0	0.0	0.0	0.0	0.0,0	1.18e-03	1.16e-03	1.15e-03	83,89,96
	38.3	0.0	0.08	0.0	0.83,0	0.0	0.0	0.0	0.0,0				
505	0.0	0.09	0.19	0.10	83,83,96	0.0	0.0	0.0	0.0,0	1.57e-04	1.38e-04	1.31e-04	84,90,97
	30.0	0.08	0.19	0.09	83,83,96	0.0	0.0	0.0	0.0,0				
506	0.0	0.0	0.03	0.0	0.83,0	0.0	0.0	0.0	0.0,0	1.20e-03	9.16e-04	8.09e-04	84,90,97
	39.6	0.0	0.03	0.0	0.83,0	0.0	0.0	0.0	0.0,0				
507	0.0	0.0	0.10	0.0	0.83,0	0.0	0.0	0.0	0.0,0	8.15e-04	8.15e-04	8.15e-04	81,87,94
	38.3	0.0	0.10	0.0	0.83,0	0.0	0.0	0.0	0.0,0				
508	0.0	0.0	4.83e-03	0.0	0.83,0	0.0	0.0	0.0	0.0,0	-2.14e-03	-2.00e-03	-1.95e-03	83,89,96
	38.3	0.0	4.59e-03	0.0	0.83,0	0.0	0.0	0.0	0.0,0				
509	0.0	2.95e-03	1.79e-03	3.39e-03	83,83,96	0.0	0.0	0.0	0.0,0	-2.30e-03	-2.18e-03	-2.13e-03	83,89,96
	38.3	2.97e-03	1.80e-03	3.57e-03	83,83,96	0.0	0.0	0.0	0.0,0				
510	0.0	2.05e-03	1.14e-03	2.22e-03	83,83,96	0.0	0.0	0.0	0.0,0	-4.61e-03	-4.41e-03	-4.33e-03	83,89,96
	38.3	2.14e-03	1.18e-03	2.33e-03	83,83,96	0.0	0.0	0.0	0.0,0				
511	0.0	0.12	0.25	0.13	84,83,97	0.0	0.0	0.0	0.0,0	-8.07e-03	-7.08e-03	-6.68e-03	83,89,96
	39.6	0.06	0.17	0.06	84,83,97	0.0	0.0	0.0	0.0,0				
512	0.0	0.0	0.08	0.0	0.83,0	0.0	0.0	0.0	0.0,0	-3.16e-03	-2.99e-03	-2.92e-03	83,89,96
	38.3	0.0	0.08	0.0	0.83,0	0.0	0.0	0.0	0.0,0				
513	0.0	0.0	0.12	0.0	0.83,0	0.0	0.0	0.0	0.0,0	-2.48e-03	-2.48e-03	-2.48e-03	81,87,94
	38.3	0.0	0.12	0.0	0.83,0	0.0	0.0	0.0	0.0,0				
514	0.0	0.05	0.09	0.05	84,83,97	0.0	0.0	0.0	0.0,0	5.98e-03	5.17e-03	4.85e-03	84,90,97
	45.0	0.10	0.18	0.11	83,83,96	0.0	0.0	0.0	0.0,0				
515	0.0	0.08	0.21	0.09	84,84,97	0.0	0.0	0.0	0.0,0	-7.22e-03	-6.27e-03	-5.88e-03	83,89,96
	45.0	0.02	0.13	0.02	84,83,97	0.0	0.0	0.0	0.0,0				
516	0.0	5.25e-03	0.02	6.88e-03	83,84,96	0.0	0.0	0.0	0.0,0	-1.04e-03	-9.67e-04	-9.38e-04	83,89,96
	24.2	3.15e-03	0.02	4.21e-03	81,84,94	0.0	0.0	0.0	0.0,0				
517	0.0	0.0	0.06	0.0	0.83,0	0.0	0.0	0.0	0.0,0	-3.53e-03	-1.74e-03	-1.70e-03	83,89,96
	38.3	0.0	0.06	0.0	0.83,0	0.0	0.0	0.0	0.0,0				
518	0.0	0.09	0.26	0.09	84,84,97	0.0	0.0	0.0	0.0,0	3.65e-03	3.02e-03	2.78e-03	84,90,97
	39.6	0.05	0.21	0.05	84,83,97	0.0	0.0	0.0	0.0,0				
519	0.0	4.11e-03	0.02	5.49e-03	81,84,96	0.0	0.0	0.0	0.0,0	-1.88e-03	-1.74e-03	-1.69e-03	83,89,96
	39.7	0.0	7.57e-03	0.0	0.84,0	0.0	0.0	0.0	0.0,0				
520	0.0	0.0	0.10	0.0	0.83,0	0.0	0.0	0.0	0.0,0	-1.59e-03	-1.54e-03	-1.52e-03	83,89,96
	38.3	0.0	0.10	0.0	0.83,0	0.0	0.0	0.0	0.0,0				
521	0.0	4.32e-04	7.02e-04	5.77e-04	81,84,94	0.0	0.0	0.0	0.0,0	-1.03e-03	-8.67e-04	-8.02e-04	83,89,96
	40.0	3.99e-03	9.67e-03	4.01e-03	84,84,97	0.0	0.0	0.0	0.0,0				
522	0.0	4.45e-03	2.51e-03	5.85e-03	83,83,96	0.0	0.0	0.0	0.0,0	-1.59e-03	-1.40e-03	-1.33e-03	84,90,97
	38.3	0.01	6.52e-03	0.02	83,81,96	0.0	0.0	0.0	0.0,0				
523	0.0	0.0	4.96e-03	0.0	0.83,0	0.0	0.0	0.0	0.0,0	5.47e-04	5.47e-04	5.47e-04	81,87,94
	31.3	0.0	5.16e-03	0.0	0.83,0	0.0	0.0	0.0	0.0,0				
524	0.0	0.0	0.04	0.0	0.83,0	0.0	0.0	0.0	0.0,0	-2.41e-03	-2.20e-03	-2.12e-03	83,89,96
	38.3	0.0	0.04	0.0	0.83,0	0.0	0.0	0.0	0.0,0				
525	0.0	1.72e-03	9.98e-04	1.93e-03	83,83,96	0.0	0.0	0.0	0.0,0	1.71e-03	8.60e-04	8.44e-04	83,89,96
	38.3	1.81e-03	1.04e-03	2.04e-03	83,83,96	0.0	0.0	0.0	0.0,0				
526	0.0	0.0	0.04	0.0	0.83,0	0.0	0.0	0.0	0.0,0	-3.01e-03	-2.61e-03	-2.46e-03	84,90,97
	38.3	5.87e-03	0.05	2.46e-03	84,83,97	0.0	0.0	0.0	0.0,0				
527	0.0	6.58e-04	4.01e-04	8.77e-04	81,81,94	0.0	0.0	0.0	0.0,0	-1.76e-03	-1.65e-03	-1.61e-03	83,89,96
	39.7	2.39e-03	4.28e-03	2.71e-03	83,84,96	0.0	0.0	0.0	0.0,0				
528	0.0	0.0	0.12	0.0	0.83,0	0.0	0.0	0.0	0.0,0	2.35e-04	2.35e-04	2.35e-04	81,87,94
	38.3	0.0	0.13	0.0	0.83,0	0.0	0.0	0.0	0.0,0				
529	0.0	0.12	0.29	0.14	83,83,96	0.0	0.0	0.0	0.0,0	-0.07	-0.10	-0.09	84,90,97
	87.5	0.07	0.12	0.07	84,84,97	0.0	0.0	0.0	0.0,0				
530	0.0	0.0	4.30e-03	0.0	0.83,0	0.0	0.0	0.0	0.0,0	-2.12e-03	-1.98e-03	-1.93e-03	83,89,96
	38.3	0.0	4.14e-03	0.0	0.83,0	0.0	0.0	0.0	0.0,0				
531	0.0	3.93e-03	2.37e-03	4.54e-03	83,83,96	0.0	0.0	0.0	0.0,0	-1.18e-03	-1.12e-03	-1.10e-03	83,89,96
	38.3	3.68e-03	2.25e-03	4.25e-03	83,83,96	0.0	0.0	0.0	0.0,0				
532	0.0	1.98e-03	1.11e-03	2.10e-03	84,84,97	0.0	0.0	0.0	0.0,0	-4.51e-03	-4.32e-03	-4.24e-03	83,89,96
	38.3	2.04e-03	1.14e-03	2.17e-03	84,84,97	0.0	0.0	0.0	0.0,0				
533	0.0	0.09	0.21	0.10	84,83,97	0.0	0.0	0.0	0.0,0	-3.35e-03	-2.93e-03	-2.77e-03	83,89,96
	39.6	0.12	0.25	0.13	84,83,97	0.0	0.0	0.0	0.0,0				
534	0.0	2.63e-03	2.08e-03	2.98e-03	83,84,96	0.0	0.0	0.0	0.0,0	-1.67e-03	-1.58e-03	-1.54e-03	83,89,96
	39.7	3.86e-03	4.28e-03	4.45e-03	83,84,96	0.0	0.0	0.0	0.0,0				
535	0.0	0.0	0.09	0.0	0.83,0	0.0	0.0	0.0	0.0,0	-3.77e-03	-3.64e-03	-3.59e-03	83,89,96
	38.3	0.0	0.09	0.0	0.83,0	0.0	0.0	0.0	0.0,0				
536	0.0	0.35	0.57	0.41	83,83,96	0.17	0.18	0.17	83,89,96	-0.07	-0.10	-0.09	83,89,96
	374.8	0.12	0.30	0.13	83,83,96	0.0	0.0	0.0	0.0,0				
537	0.0	0.10	0.20	0.11	84,83,97	0.0	0.0	0.0	0.0,0	1.21e-03	1.04e-03	9.70e-04	84,90,97
	29.9	0.09	0.18	0.10	83,83,96	0.0	0.0	0.0	0.0,0				
538	0.0	4.23e-03	2.44e-03	5.02e-03	83,83,96	0.0	0.0	0.0	0.0,0	-1.55e-03	-1.47e-03	-1.43e-03	83,89,96
	39.7	4.28e-03	2.47e-03	5.19e-03	83,83,96	0.0	0.0	0.0	0.0,0				
539	0.0	0.0	0.10	0.0	0.83,0	0.0	0.0	0.0	0.0,0	-1.93e-03	-1.70e-03	-1.61e-03	84,90,97
	38.3	0.0	0.10	0.0	0.83,0	0.0	0.0	0.0	0.0,0				
540	0.0	0.05	0.20	0.05	84,83,97	0.0	0.0	0.0	0.0,0	1.84e-03	1.47e-03	1.33e-03	84,90,97
	39.6	3.79e-03	0.15	0.0	84,83,0	0.0	0.0	0.0	0.0,0				
541	0.0	0.0	0.13	0.0	0.83,0	0.0	0.0	0.0	0.0,0	-9.99e-04	-9.99e-04	-9.99e-04	81,87,94
	38.3	0.0	0.13	0.0	0.83,0	0.0	0.0	0.0	0.0,0				
542	0.0	0.0	0.10	0.0	0.83,0	0.0	0.0	0.0	0.0,0	-6.14e-04	-3.97e-04		

	45.3	0.0	8.70e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
546	0.0	0.0	0.05	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.54e-03	-2.31e-03	-2.22e-03	83,89,96
	38.3	0.0	0.05	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
547	0.0	9.27e-04	1.69e-03	9.37e-04	83,83,96	0.0	0.0	0.0	0,0,0	1.64e-03	1.58e-03	8.13e-04	83,89,96
	38.3	9.74e-04	1.77e-03	9.98e-04	83,83,96	0.0	0.0	0.0	0,0,0				
548	0.0	4.91e-03	0.05	2.61e-04	84,83,97	0.0	0.0	0.0	0,0,0	-3.08e-03	-2.69e-03	-2.53e-03	84,90,97
	38.3	0.03	0.08	0.04	84,83,97	0.0	0.0	0.0	0,0,0				
549	0.0	0.0	0.10	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-3.19e-03	-3.12e-03	-3.09e-03	83,89,96
	38.3	0.0	0.10	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
550	0.0	0.0	0.09	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.43e-03	-2.32e-03	-2.28e-03	83,89,96
	38.3	0.0	0.08	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
551	0.0	0.0	4.18e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.09e-03	-1.96e-03	-1.91e-03	83,89,96
	38.3	0.0	4.07e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
552	0.0	2.08e-03	1.20e-03	2.36e-03	83,83,96	0.0	0.0	0.0	0,0,0	-2.19e-03	-1.09e-03	-1.07e-03	83,89,96
	38.3	1.98e-03	1.15e-03	2.24e-03	83,83,96	0.0	0.0	0.0	0,0,0				
553	0.0	2.22e-03	1.26e-03	2.42e-03	83,83,96	0.0	0.0	0.0	0,0,0	-4.42e-03	-4.23e-03	-4.16e-03	83,89,96
	38.3	2.27e-03	1.28e-03	2.46e-03	83,83,96	0.0	0.0	0.0	0,0,0				
554	0.0	0.08	0.19	0.09	83,83,96	0.0	0.0	0.0	0,0,0	-1.14e-03	-9.99e-04	-9.41e-04	83,89,96
	39.6	0.09	0.22	0.10	84,83,97	0.0	0.0	0.0	0,0,0				
555	0.0	0.02	0.08	0.02	84,83,97	0.0	0.0	0.0	0,0,0	-8.91e-04	-8.04e-04	-7.70e-04	83,89,96
	14.8	0.02	0.08	0.02	84,83,97	0.0	0.0	0.0	0,0,0				
556	0.0	0.0	0.15	0.0	0,83,0	0.0	0.0	0.0	0,0,0	1.72e-04	-1.23e-04	-1.23e-04	84,87,94
	38.3	0.0	0.15	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
557	0.0	0.13	0.26	0.15	83,83,96	0.0	0.0	0.0	0,0,0	-1.00e-02	-9.00e-03	-8.60e-03	83,89,96
	45.0	0.06	0.15	0.07	83,83,96	0.0	0.0	0.0	0,0,0				
558	0.0	0.0	0.15	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-6.08e-04	-4.96e-04	-4.54e-04	84,90,97
	14.8	0.0	0.15	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
559	0.0	0.0	0.08	0.0	0,83,0	0.0	0.0	0.0	0,0,0	1.08e-03	1.08e-03	1.08e-03	83,89,96
	38.3	0.0	0.08	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
560	0.0	0.01	0.13	9.62e-03	84,83,97	0.0	0.0	0.0	0,0,0	9.24e-04	7.03e-04	6.20e-04	84,90,97
	31.3	0.0	0.10	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
561	0.0	0.0	0.11	0.0	0,83,0	0.0	0.0	0.0	0,0,0	7.02e-04	7.02e-04	7.02e-04	81,87,94
	38.3	0.0	0.11	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
562	0.0	0.0	0.07	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-3.47e-03	-3.26e-03	-3.18e-03	83,89,96
	38.3	0.0	0.07	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
563	0.0	0.01	0.01	0.01	84,84,97	0.0	0.0	0.0	0,0,0	-5.11e-04	-4.50e-04	-4.26e-04	83,89,96
	40.0	0.02	0.02	0.02	84,84,97	0.0	0.0	0.0	0,0,0				
564	0.0	0.03	0.02	0.04	83,83,96	0.0	0.0	0.0	0,0,0	1.08e-03	1.08e-03	1.08e-03	81,87,94
	38.3	0.01	8.24e-03	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
565	0.0	0.0	7.63e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	5.14e-04	5.14e-04	5.14e-04	81,87,94
	38.3	0.0	7.80e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
566	0.0	3.50e-04	3.69e-03	0.0	84,83,0	0.0	0.0	0.0	0,0,0	1.57e-03	1.51e-03	1.49e-03	83,89,96
	38.3	3.70e-04	3.71e-03	0.0	84,83,0	0.0	0.0	0.0	0,0,0				
567	0.0	4.47e-03	2.60e-03	5.46e-03	83,83,96	0.0	0.0	0.0	0,0,0	-1.40e-03	-1.33e-03	-1.31e-03	83,89,96
	39.7	3.17e-03	1.90e-03	4.23e-03	81,81,94	0.0	0.0	0.0	0,0,0				
568	0.0	0.0	0.13	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.17e-03	-2.17e-03	-2.17e-03	81,87,94
	38.3	0.0	0.12	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
569	0.0	0.0	3.92e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.07e-03	-1.94e-03	-1.88e-03	83,89,96
	38.3	0.0	3.85e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
570	0.0	1.90e-03	1.09e-03	2.15e-03	83,84,96	0.0	0.0	0.0	0,0,0	-2.12e-03	-2.02e-03	-1.97e-03	83,89,96
	38.3	1.86e-03	1.07e-03	2.09e-03	83,84,96	0.0	0.0	0.0	0,0,0				
571	0.0	2.45e-03	1.40e-03	2.67e-03	83,83,96	0.0	0.0	0.0	0,0,0	-4.32e-03	-4.15e-03	-4.08e-03	83,89,96
	38.3	2.48e-03	1.42e-03	2.69e-03	83,83,96	0.0	0.0	0.0	0,0,0				
572	0.0	0.09	0.21	0.11	83,83,96	0.0	0.0	0.0	0,0,0	-3.80e-03	-3.40e-03	-3.24e-03	83,89,96
	45.0	0.13	0.26	0.15	83,83,96	0.0	0.0	0.0	0,0,0				
573	0.0	0.0	0.08	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-3.03e-03	-2.87e-03	-2.81e-03	83,89,96
	38.3	0.0	0.08	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
574	0.0	0.0	0.13	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.75e-04	-1.63e-04	-1.23e-04	84,90,97
	38.3	0.0	0.13	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
575	0.0	0.21	0.32	0.28	82,84,95	0.09	0.09	0.09	84,93,97	-0.29	-0.29	-0.29	83,89,96
	459.0	0.14	0.20	0.18	82,82,95	0.0	0.0	0.0	0,0,0				
576	918.0	0.28	0.41	0.37	83,83,96	0.12	0.13	0.13	83,89,96	-1.46e-03	-1.42e-03	-1.41e-03	83,89,96
	0.0	0.0	0.11	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
577	0.0	0.01	5.80e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0	1.34e-03	1.34e-03	1.34e-03	81,87,94
	38.3	6.80e-03	4.12e-03	8.70e-03	83,83,96	0.0	0.0	0.0	0,0,0				
578	0.0	0.0	7.30e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	4.31e-04	4.31e-04	4.31e-04	81,87,94
	38.3	0.0	7.42e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
579	0.0	7.17e-04	2.96e-03	3.81e-04	84,85,97	0.0	0.0	0.0	0,0,0	1.50e-03	1.45e-03	1.43e-03	83,89,96
	38.3	7.24e-04	2.98e-03	3.99e-04	84,81,97	0.0	0.0	0.0	0,0,0				
580	0.0	0.0	0.13	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-8.43e-04	-8.43e-04	-8.43e-04	81,87,94
	38.3	0.0	0.13	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
581	0.0	0.0	0.10	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-3.65e-03	-3.53e-03	-3.49e-03	83,89,96
	38.3	0.0	0.10	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
582	0.0	0.0	3.80e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.04e-03	-1.91e-03	-1.86e-03	83,89,96
	38.3	0.0	3.74e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
583	0.0	1.71e-03	9.72e-04	1.91e-03	84,84,97	0.0	0.0	0.0	0,0,0	-2.04e-03	-1.95e-03	-1.91e-03	83,89,96
	38.3	1.68e-03	9.58e-04	1.88e-03	84,84,97	0.0	0.0	0.0	0,0,0				
584	0.0	2.59e-03	1.50e-03	2.82e-03	83,83,96	0.0	0.0	0.0	0,0,0	-4.23e-03	-4.07e-03	-4.00e-03	83,89,96
	38.3	2.61e-03	1.51e-03	2.84e-03	83,83,96	0.0	0.0	0.0	0,0,0				
585	0.0	0.08	0.19	0.09	83,83,96	0.0	0.0	0.0	0,0,0	-9.56e-04	-8.58e-04	-8.19e-04	83,89,96
	30.1	0.09	0.21	0.11	83,83,96	0.0	0.0	0.0	0,0,0				
586	0.0	0.07	0.09	0.09	81,82,94	0.0	0.0	0.0	0,0,0	0.01	0.01	0.01	81,87,94
	175.0	0.02	0.02	0.02	81,81,94	0.0	0.0	0.0	0,0,0				
587	350.0	0.08	0.11	0.11	83,83,96	0.0	0.0	0.0	0,0,0				
	0.0	0.0	0.09	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.28e-03	-2.04e-03	-1.94e-03	84,90,97
588	0.0	0.0	0.09	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
	38.3	0.0	0.11	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.99e-03	-2.94e-03	-2.92e-03	83,89,96
589	0.0	0.0	0.11	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-7.71e-04	-5.41e-04	-4.60e-04	84,90,97
	38.3	0.0	0.11	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
590	0.0	1.60e-03	8.93e-04	1.57e-03	84,84,97	0.0	0.0	0.0	0,0,0	1.31e-03	1.31e-03	1.31e-03	81,87,94
	38.3	0.01	0.02	0.02	83,81,96	0.0	0.0	0.0	0,0,0				
591	0.0	0.0	7.19e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	3.44e-04	3.44e-04	3.44e-04	81,87,94
	38.3	0.0	7.30e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
592	0.0	0.0	7.28e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	1.42e-03	1.38e-03	1.36e-03	83,89,96
	38.3	0.0	7.30e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
593	0.0	0.0	0.11	0.0	0,83,0</								

595	0.0	0.0	3.80e-03	0.0	0.81,0	0.0	0.0	0.0	0.0,0	-2.01e-03	-1.88e-03	-1.83e-03	83,89,96
	38.3	0.0	3.75e-03	0.0	0.81,0	0.0	0.0	0.0	0.0,0				
596	0.0	1.49e-03	8.26e-04	1.63e-03	84,84,97	0.0	0.0	0.0	0.0,0	-1.96e-03	-1.88e-03	-1.84e-03	83,89,96
	38.3	1.45e-03	8.10e-04	1.59e-03	84,84,97	0.0	0.0	0.0	0.0,0				
597	0.0	2.68e-03	1.55e-03	2.90e-03	83,83,96	0.0	0.0	0.0	0.0,0	-4.14e-03	-3.99e-03	-3.92e-03	83,89,96
	38.3	2.69e-03	1.56e-03	2.91e-03	83,83,96	0.0	0.0	0.0	0.0,0				
598	0.0	0.27	0.41	0.36	83,83,96	0.12	0.12	0.12	83,89,96	-0.29	-0.28	-0.29	83,89,96
	459.0	0.14	0.20	0.18	82,82,95	0.0	0.0	0.0	0.0,0				
	918.0	0.22	0.32	0.29	84,84,97	0.09	0.09	0.09	84,93,97				
599	0.0	0.0	0.09	0.0	0.83,0	0.0	0.0	0.0	0.0,0	1.00e-03	1.00e-03	1.00e-03	81,87,94
	38.3	0.0	0.09	0.0	0.83,0	0.0	0.0	0.0	0.0,0				
600	0.0	0.0	0.09	0.0	0.83,0	0.0	0.0	0.0	0.0,0	-2.87e-03	-2.73e-03	-2.67e-03	83,89,96
	38.3	0.0	0.09	0.0	0.83,0	0.0	0.0	0.0	0.0,0				
601	0.0	0.0	0.07	0.0	0.83,0	0.0	0.0	0.0	0.0,0	-3.37e-03	-3.18e-03	-3.10e-03	83,89,96
	38.3	0.0	0.07	0.0	0.83,0	0.0	0.0	0.0	0.0,0				
602	0.0	0.0	0.05	0.0	0.83,0	0.0	0.0	0.0	0.0,0	6.43e-04	6.43e-04	6.43e-04	81,87,94
	38.3	0.02	0.07	0.03	83,83,96	0.0	0.0	0.0	0.0,0				
603	0.0	0.0	6.76e-03	0.0	0.83,0	0.0	0.0	0.0	0.0,0	2.54e-04	2.54e-04	2.54e-04	81,87,94
	38.3	0.0	6.92e-03	0.0	0.83,0	0.0	0.0	0.0	0.0,0				
604	0.0	0.0	6.08e-03	0.0	0.83,0	0.0	0.0	0.0	0.0,0	1.35e-03	1.31e-03	1.30e-03	83,89,96
	38.3	0.0	6.10e-03	0.0	0.83,0	0.0	0.0	0.0	0.0,0				
605	0.0	0.0	5.20e-03	0.0	0.81,0	0.0	0.0	0.0	0.0,0	-3.76e-03	-1.86e-03	-1.81e-03	83,89,96
	38.3	0.0	5.15e-03	0.0	0.81,0	0.0	0.0	0.0	0.0,0				
606	0.0	1.34e-03	6.64e-04	1.47e-03	83,83,96	0.0	0.0	0.0	0.0,0	-1.88e-03	-1.80e-03	-1.77e-03	83,89,96
	38.3	1.26e-03	6.34e-04	1.37e-03	83,84,96	0.0	0.0	0.0	0.0,0				
607	0.0	1.90e-03	1.08e-03	1.98e-03	84,84,97	0.0	0.0	0.0	0.0,0	-4.06e-03	-3.91e-03	-3.85e-03	83,89,96
	38.3	1.90e-03	1.08e-03	1.97e-03	84,84,97	0.0	0.0	0.0	0.0,0				
608	0.0	0.0	0.15	0.0	0.83,0	0.0	0.0	0.0	0.0,0	-6.57e-04	-6.57e-04	-6.57e-04	81,87,94
	38.3	0.0	0.14	0.0	0.83,0	0.0	0.0	0.0	0.0,0				
609	0.0	0.0	0.12	0.0	0.83,0	0.0	0.0	0.0	0.0,0	-1.31e-03	-1.29e-03	-1.28e-03	83,89,96
	38.3	0.0	0.12	0.0	0.83,0	0.0	0.0	0.0	0.0,0				
610	0.0	0.0	0.11	0.0	0.83,0	0.0	0.0	0.0	0.0,0	-1.54e-03	-1.31e-03	-1.22e-03	84,90,97
	38.3	0.0	0.08	0.0	0.81,0	0.0	0.0	0.0	0.0,0				
611	0.0	0.0	8.92e-03	0.0	0.83,0	0.0	0.0	0.0	0.0,0	-1.67e-04	1.02e-04	1.02e-04	84,87,94
	21.8	0.0	8.90e-03	0.0	0.83,0	0.0	0.0	0.0	0.0,0				
612	0.0	1.14e-03	5.99e-04	1.22e-03	83,83,96	0.0	0.0	0.0	0.0,0	1.27e-03	1.25e-03	1.24e-03	83,89,96
	38.3	1.16e-03	6.08e-04	1.25e-03	83,83,96	0.0	0.0	0.0	0.0,0				
613	0.0	0.0	6.83e-03	0.0	0.83,0	0.0	0.0	0.0	0.0,0	-3.70e-03	-1.83e-03	-1.78e-03	83,89,96
	38.3	0.0	6.77e-03	0.0	0.83,0	0.0	0.0	0.0	0.0,0				
614	0.0	1.24e-03	2.85e-03	1.28e-03	84,83,97	0.0	0.0	0.0	0.0,0	-1.79e-03	-1.72e-03	-1.70e-03	83,89,96
	38.3	1.14e-03	2.70e-03	1.16e-03	84,83,97	0.0	0.0	0.0	0.0,0				
615	0.0	2.86e-03	1.68e-03	3.02e-03	84,84,97	0.0	0.0	0.0	0.0,0	-3.97e-03	-3.83e-03	-3.77e-03	83,89,96
	38.3	2.85e-03	1.67e-03	3.00e-03	84,84,97	0.0	0.0	0.0	0.0,0				
616	0.0	0.0	0.12	0.0	0.83,0	0.0	0.0	0.0	0.0,0	-2.76e-03	-2.73e-03	-2.72e-03	83,89,96
	38.3	0.0	0.12	0.0	0.83,0	0.0	0.0	0.0	0.0,0				
617	0.0	0.0	0.10	0.0	0.83,0	0.0	0.0	0.0	0.0,0	-3.51e-03	-3.41e-03	-3.37e-03	83,89,96
	38.3	0.0	0.10	0.0	0.83,0	0.0	0.0	0.0	0.0,0				
618	0.0	0.0	0.07	0.0	0.83,0	0.0	0.0	0.0	0.0,0	-1.99e-03	-1.78e-03	-1.69e-03	84,90,97
	38.3	0.0	0.06	0.0	0.83,0	0.0	0.0	0.0	0.0,0				
619	0.0	1.21e-03	4.79e-03	1.57e-03	84,83,97	0.0	0.0	0.0	0.0,0	-5.73e-04	-2.88e-04	-1.91e-04	84,90,97
	54.8	1.22e-03	4.82e-03	1.61e-03	84,83,97	0.0	0.0	0.0	0.0,0				
620	0.0	3.49e-03	2.08e-03	4.03e-03	83,83,96	0.0	0.0	0.0	0.0,0	1.20e-03	1.18e-03	1.17e-03	83,89,96
	38.3	3.51e-03	2.08e-03	4.05e-03	83,83,96	0.0	0.0	0.0	0.0,0				
621	0.0	0.0	0.01	0.0	0.83,0	0.0	0.0	0.0	0.0,0	-3.64e-03	-1.80e-03	-1.75e-03	83,89,96
	38.3	0.0	0.01	0.0	0.83,0	0.0	0.0	0.0	0.0,0				
622	0.0	1.51e-03	2.14e-03	1.61e-03	83,81,96	0.0	0.0	0.0	0.0,0	-1.70e-03	-1.64e-03	-1.62e-03	83,89,96
	38.3	1.38e-03	1.97e-03	1.45e-03	83,81,96	0.0	0.0	0.0	0.0,0				
623	0.0	1.92e-03	1.08e-03	1.94e-03	84,84,97	0.0	0.0	0.0	0.0,0	-3.88e-03	-3.75e-03	-3.69e-03	83,89,96
	38.3	1.89e-03	1.07e-03	1.90e-03	84,84,97	0.0	0.0	0.0	0.0,0				
624	0.0	0.0	0.04	0.0	0.83,0	0.0	0.0	0.0	0.0,0	-2.17e-03	-1.95e-03	-1.86e-03	83,89,96
	38.3	0.0	0.04	0.0	0.83,0	0.0	0.0	0.0	0.0,0				
625	0.0	0.0	0.01	0.0	0.83,0	0.0	0.0	0.0	0.0,0	-5.31e-04	-3.23e-04	-2.51e-04	84,90,97
	38.3	0.0	0.01	0.0	0.83,0	0.0	0.0	0.0	0.0,0				
626	0.0	9.36e-04	2.88e-03	7.70e-04	84,81,97	0.0	0.0	0.0	0.0,0	1.12e-03	1.11e-03	1.10e-03	83,89,96
	38.3	9.60e-04	2.91e-03	8.06e-04	84,81,97	0.0	0.0	0.0	0.0,0				
627	0.0	0.0	0.01	0.0	0.83,0	0.0	0.0	0.0	0.0,0	-3.57e-03	-3.36e-03	-1.72e-03	83,89,96
	38.3	0.0	0.01	0.0	0.83,0	0.0	0.0	0.0	0.0,0				
628	0.0	1.15e-03	4.63e-03	9.66e-04	84,83,97	0.0	0.0	0.0	0.0,0	-1.60e-03	-1.55e-03	-1.53e-03	83,89,96
	38.3	9.74e-04	4.40e-03	7.09e-04	84,83,97	0.0	0.0	0.0	0.0,0				
629	0.0	2.70e-03	1.56e-03	2.89e-03	83,84,96	0.0	0.0	0.0	0.0,0	-3.79e-03	-3.66e-03	-3.61e-03	83,89,96
	38.3	2.66e-03	1.54e-03	2.84e-03	84,84,97	0.0	0.0	0.0	0.0,0				
630	0.0	0.0	0.03	0.0	0.83,0	0.0	0.0	0.0	0.0,0	-2.30e-03	-2.07e-03	-1.97e-03	83,89,96
	38.3	0.0	0.03	0.0	0.83,0	0.0	0.0	0.0	0.0,0				
631	0.0	0.0	0.01	0.0	0.83,0	0.0	0.0	0.0	0.0,0	-6.41e-04	-4.26e-04	-3.50e-04	84,90,97
	38.3	0.0	0.01	0.0	0.83,0	0.0	0.0	0.0	0.0,0				
632	0.0	2.87e-04	4.29e-03	0.0	84,83,0	0.0	0.0	0.0	0.0,0	1.04e-03	1.04e-03	1.04e-03	83,89,96
	38.3	3.19e-04	4.32e-03	0.0	84,83,0	0.0	0.0	0.0	0.0,0				
633	0.0	6.34e-04	3.77e-03	0.0	84,81,0	0.0	0.0	0.0	0.0,0	-3.50e-03	-3.30e-03	-3.22e-03	83,89,96
	38.3	5.13e-04	3.62e-03	0.0	84,81,0	0.0	0.0	0.0	0.0,0				
634	0.0	0.0	7.93e-03	0.0	0.83,0	0.0	0.0	0.0	0.0,0	-1.49e-03	-1.45e-03	-1.44e-03	83,89,96
	38.3	0.0	7.64e-03	0.0	0.83,0	0.0	0.0	0.0	0.0,0				
635	0.0	2.41e-03	1.37e-03	2.54e-03	84,84,97	0.0	0.0	0.0	0.0,0	-3.69e-03	-3.57e-03	-3.52e-03	83,89,96
	38.3	2.35e-03	1.35e-03	2.47e-03	84,84,97	0.0	0.0	0.0	0.0,0				
636	0.0	0.0	0.03	0.0	0.83,0	0.0	0.0	0.0	0.0,0	-2.49e-03	-2.23e-03	-2.13e-03	83,89,96
	38.3	0.0	0.03	0.0	0.83,0	0.0	0.0	0.0	0.0,0				
637	0.0	0.0	0.01	0.0	0.83,0	0.0	0.0	0.0	0.0,0	-7.50e-04	-5.28e-04	-4.49e-04	84,90,97
	38.3	0.0	0.02	0.0	0.83,0	0.0	0.0	0.0	0.0,0				
638	0.0	0.0	7.33e-03	0.0	0.83,0	0.0	0.0	0.0	0.0,0	9.69e-04	9.69e-04	9.69e-04	81,87,94
	38.3	0.0	7.33e-03	0.0	0.83,0	0.0	0.0	0.0	0.0,0				
639	0.0	0.0	6.57e-03	0.0	0.83,0	0.0	0.0	0.0	0.0,0	-3.42e-03	-3.23e-03	-3.15e-03	83,89,96
	38.3	0.0	6.37e-03	0.0	0.83,0	0.0	0.0	0.0	0.0,0				
640	0.0	0.0	0.01	0.0	0.83,0	0.0	0.0	0.0	0.0,0	-1.37e-03	-1.34e-03	-1.33e-03	83,89,96
	38.3	0.0	0.01	0.0	0.83,0	0.0	0.0	0.0	0.0,0				
641	0.0	2.29e-03	1.29e-03	2.41e-03	84,84,97	0.0	0.0	0.0	0.0,0	-3.59e-03	-3.48e-03	-3.43e-03	83,89,96
	38.3	2.22e-03	1.26e-03	2.32e-03	84,84,97	0.0	0.0	0.0	0.0,0				
642	0.0	0											

645	0.0	0.0	9.41e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-3.34e-03	-3.15e-03	-3.08e-03	83,89,96
	38.3	0.0	9.14e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
646	0.0	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.24e-03	-1.22e-03	-1.22e-03	83,89,96
	38.3	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
647	0.0	0.0	8.00e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-3.48e-03	-3.38e-03	-3.34e-03	83,89,96
	38.3	0.0	7.82e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
648	0.0	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-8.69e-04	-4.36e-04	-4.19e-04	83,89,96
	14.8	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
649	0.0	0.0	0.01	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.44e-04	-1.97e-04	-1.80e-04	84,90,97
	14.8	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
650	0.0	0.0	0.01	0.0	0,83,0	0.0	0.0	0.0	0,0,0	4.42e-04	4.42e-04	4.42e-04	81,87,94
	38.3	0.0	0.01	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
651	0.0	0.0	0.01	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-3.25e-03	-3.07e-03	-2.99e-03	83,89,96
	38.3	0.0	0.01	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
652	0.0	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.09e-03	-1.09e-03	-1.09e-03	83,89,96
	38.3	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
653	0.0	1.59e-03	5.74e-03	1.18e-03	84,81,97	0.0	0.0	0.0	0,0,0	-3.37e-03	-3.27e-03	-3.23e-03	83,89,96
	38.3	1.39e-03	5.52e-03	9.00e-04	84,81,97	0.0	0.0	0.0	0,0,0				
654	0.0	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0	4.11e-04	4.11e-04	4.11e-04	81,87,94
	38.3	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
655	0.0	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-3.14e-03	-2.97e-03	-2.90e-03	83,89,96
	38.3	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
656	0.0	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-9.51e-04	-9.51e-04	-9.51e-04	81,87,94
	38.3	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
657	0.0	0.0	0.01	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-3.24e-03	-3.16e-03	-3.12e-03	83,89,96
	38.3	0.0	0.01	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
658	0.0	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0	3.87e-04	3.87e-04	3.87e-04	81,87,94
	38.3	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
659	0.0	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-3.01e-03	-2.85e-03	-2.79e-03	83,89,96
	38.3	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
660	0.0	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-7.95e-04	-7.95e-04	-7.95e-04	81,87,94
	38.3	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
661	0.0	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-3.10e-03	-3.03e-03	-3.00e-03	83,89,96
	38.3	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
662	0.0	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	7.08e-04	7.08e-04	7.08e-04	81,87,94
	38.3	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
663	0.0	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.86e-03	-2.71e-03	-2.65e-03	83,89,96
	38.3	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
664	0.0	0.0	0.04	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-6.07e-04	-6.07e-04	-6.07e-04	81,87,94
	38.3	0.0	0.04	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
665	0.0	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.93e-03	-2.87e-03	-2.85e-03	83,89,96
	38.3	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
666	0.0	0.0	0.05	0.0	0,83,0	0.0	0.0	0.0	0,0,0	7.08e-04	7.08e-04	7.08e-04	81,87,94
	38.3	0.0	0.05	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
667	0.0	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.61e-03	-2.50e-03	-2.45e-03	83,89,96
	38.3	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
668	0.0	0.0	0.05	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-3.46e-04	-3.46e-04	-3.46e-04	81,87,94
	38.3	0.0	0.05	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
669	0.0	0.0	0.04	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.66e-03	-2.64e-03	-2.63e-03	83,89,96
	38.3	0.0	0.04	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
670	0.0	0.0	0.08	0.0	0,83,0	0.0	0.0	0.0	0,0,0	6.35e-04	6.35e-04	6.35e-04	81,87,94
	38.3	0.0	0.10	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
671	0.0	0.02	0.05	0.02	84,83,97	0.0	0.0	0.0	0,0,0	-2.12e-03	-2.07e-03	-2.05e-03	83,89,96
	38.3	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
672	0.0	4.01e-03	0.08	0.0	84,83,0	0.0	0.0	0.0	0,0,0	5.75e-04	3.90e-04	3.22e-04	84,90,97
	38.3	0.0	0.05	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
673	0.0	0.0	0.05	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.15e-03	-2.15e-03	-2.15e-03	81,87,94
	38.3	0.0	0.05	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
674	0.0	1.93e-03	0.01	2.58e-03	81,83,94	0.0	0.0	0.0	0,0,0	2.64e-03	2.54e-03	2.45e-03	83,89,96
	25.8	3.61e-03	0.02	4.07e-03	84,84,97	0.0	0.0	0.0	0,0,0				
675	0.0	0.03	0.08	0.04	83,83,96	0.0	0.0	0.0	0,0,0	-1.06e-03	-1.03e-03	-1.01e-03	83,89,96
	39.7	0.02	0.06	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
676	0.0	0.0	0.02	0.0	0,84,0	0.0	0.0	0.0	0,0,0	5.60e-03	5.12e-03	4.99e-03	83,89,96
	39.7	6.62e-03	0.03	7.78e-03	84,84,97	0.0	0.0	0.0	0,0,0				
677	0.0	0.02	0.06	0.02	83,83,96	0.0	0.0	0.0	0,0,0	-1.57e-03	-1.48e-03	-1.45e-03	83,89,96
	39.7	7.37e-03	0.05	8.11e-03	83,83,96	0.0	0.0	0.0	0,0,0				
678	0.0	0.0	0.03	0.0	0,84,0	0.0	0.0	0.0	0,0,0	-5.05e-03	-4.67e-03	-4.52e-03	83,89,96
	39.7	6.45e-03	0.04	7.71e-03	83,84,96	0.0	0.0	0.0	0,0,0				
679	0.0	0.0	0.06	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.87e-03	-1.76e-03	-1.71e-03	83,89,96
	39.7	0.0	0.05	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
680	0.0	2.16e-03	0.04	2.20e-03	84,84,97	0.0	0.0	0.0	0,0,0	-4.88e-03	-4.52e-03	-4.38e-03	83,89,96
	39.7	3.97e-03	0.04	4.86e-03	83,83,96	0.0	0.0	0.0	0,0,0				
681	0.0	0.0	0.04	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.05e-03	-1.92e-03	-1.87e-03	83,89,96
	39.7	0.0	0.04	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
682	0.0	2.06e-03	0.04	2.08e-03	84,83,97	0.0	0.0	0.0	0,0,0	-4.83e-03	-4.48e-03	-4.35e-03	83,89,96
	39.7	7.00e-04	0.04	9.34e-04	81,83,94	0.0	0.0	0.0	0,0,0				
683	0.0	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.20e-03	-2.05e-03	-2.00e-03	83,89,96
	39.7	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
684	0.0	5.66e-04	0.04	2.54e-04	84,83,97	0.0	0.0	0.0	0,0,0	5.01e-03	4.68e-03	4.55e-03	83,89,96
	39.7	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
685	0.0	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.33e-03	-2.18e-03	-2.12e-03	83,89,96
	39.7	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
686	0.0	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	6.01e-03	5.71e-03	5.59e-03	83,89,96
	39.7	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
687	0.0	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.56e-03	-2.40e-03	-2.33e-03	83,89,96
	39.7	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
688	0.0	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	1.88e-03	1.75e-03	1.70e-03	83,89,96
	39.7	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
689	0.0	0.0	0.01	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.21e-03	-1.13e-03	-1.10e-03	83,89,96
	39.7	0.0	0.01	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
690	0.0	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	1.89e-03	1.76e-03	1.71e-03	83,89,96
	39.7	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
691	0.0	0.0	9.17e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.15e-03	-2.00e-03	-1.94e-03	83,89,96
	39.7	0.0	9.51e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
692	0.0	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0	2.02e-03	1.78e-03	1.72e-03	83,89,96
	39.7	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
693	0.0	0.0	6.34e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-2.19e-03	-2.04e-03	-1.98e-03	83,89,96
	39.7	1.11e-03	9.41e-03	7.17e-04	84,81,97	0.0							

	459.0	0.14	0.22	0.19	83,83,96	0.0	0.0	0.0	0,0,0				
	918.0	0.29	0.45	0.39	83,83,96	0.13	0.15	0.15	83,89,96				
696	0.0	0.06	0.08	0.07	82,81,95	0.0	0.0	0.0	0,0,0	0.01	0.01	0.01	83,89,96
	175.0	0.02	0.02	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
	350.0	0.09	0.13	0.11	83,83,96	0.0	0.0	0.0	0,0,0				
697	0.0	0.28	0.44	0.38	83,83,96	0.13	0.14	0.14	83,89,96	-0.32	-0.32	-0.32	83,89,96
	459.0	0.14	0.22	0.19	83,83,96	0.0	0.0	0.0	0,0,0				
	918.0	0.19	0.30	0.25	82,82,95	0.0	0.0	0.0	0,0,0				
698	0.0	8.67e-04	2.05e-03	1.00e-03	83,83,96	0.0	0.0	0.0	0,0,0	-3.82e-03	-3.41e-03	-3.24e-03	83,89,96
	39.3	1.44e-03	4.01e-03	1.85e-03	84,84,97	0.0	0.0	0.0	0,0,0				
699	0.0	2.79e-03	8.32e-03	3.35e-03	84,84,97	0.0	0.0	0.0	0,0,0	-1.08e-03	-9.56e-04	-9.09e-04	84,90,97
	38.3	9.19e-04	6.04e-03	9.54e-04	84,83,97	0.0	0.0	0.0	0,0,0				
700	0.0	6.29e-04	3.32e-03	7.90e-04	83,83,96	0.0	0.0	0.0	0,0,0	-4.39e-03	-4.06e-03	-3.92e-03	83,89,96
	39.3	0.0	2.09e-03	0.0	84,0	0.0	0.0	0.0	0,0,0				
701	0.0	5.06e-03	2.75e-03	5.69e-03	83,83,96	0.0	0.0	0.0	0,0,0	-5.04e-04	-4.10e-04	-3.72e-04	83,89,96
	38.3	0.03	0.03	0.03	83,83,96	0.0	0.0	0.0	0,0,0				
702	0.0	0.02	0.02	0.02	84,84,97	0.0	0.0	0.0	0,0,0	-0.02	-0.02	-0.02	83,89,96
	78.5	0.06	0.12	0.07	84,84,97	0.0	0.0	0.0	0,0,0				
703	0.0	0.07	0.12	0.08	83,83,96	0.0	0.0	0.0	0,0,0	0.04	0.04	0.04	83,89,96
	111.3	3.93e-03	0.03	4.94e-03	82,83,95	0.0	0.0	0.0	0,0,0				
	222.5	0.09	0.16	0.12	83,83,96	0.0	0.0	0.0	0,0,0				
704	0.0	0.06	0.12	0.07	83,83,96	0.0	0.0	0.0	0,0,0	3.62e-04	3.62e-04	3.62e-04	81,87,94
	50.0	0.0	0.04	0.0	83,0	0.0	0.0	0.0	0,0,0				
705	0.0	0.05	0.13	0.05	84,83,97	0.0	0.0	0.0	0,0,0	-0.04	-0.03	-0.03	83,89,96
	111.3	0.0	0.06	0.0	83,0	0.0	0.0	0.0	0,0,0				
	222.5	0.02	0.09	0.01	84,83,97	0.0	0.0	0.0	0,0,0				
706	0.0	0.0	0.02	0.0	83,0	0.0	0.0	0.0	0,0,0	-1.27e-03	-1.16e-03	-1.12e-03	83,89,96
	40.0	0.0	0.03	0.0	83,0	0.0	0.0	0.0	0,0,0				
707	0.0	0.0	0.04	0.0	83,0	0.0	0.0	0.0	0,0,0	-4.91e-04	-3.43e-04	-2.93e-04	84,90,97
	50.0	0.0	0.05	0.0	83,0	0.0	0.0	0.0	0,0,0				
708	0.0	2.45e-04	0.02	3.27e-04	81,83,94	0.0	0.0	0.0	0,0,0	-1.18e-03	-1.04e-03	-9.79e-04	83,89,96
	40.0	0.0	0.02	0.0	83,0	0.0	0.0	0.0	0,0,0				
709	0.0	0.04	0.03	0.05	83,83,96	0.0	0.0	0.0	0,0,0	1.76e-03	1.76e-03	1.76e-03	81,87,94
	38.3	8.56e-03	5.27e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
710	0.0	0.03	0.03	0.03	84,84,97	0.0	0.0	0.0	0,0,0	-0.04	-0.03	-0.03	84,90,97
	78.5	0.08	0.16	0.08	84,84,97	0.0	0.0	0.0	0,0,0				
711	0.0	0.05	0.03	0.05	84,84,97	0.0	0.0	0.0	0,0,0	-0.14	-0.12	-0.10	84,90,97
	87.5	0.12	0.21	0.13	83,84,96	0.0	0.0	0.0	0,0,0				
712	0.0	0.06	0.15	0.06	84,84,97	0.0	0.0	0.0	0,0,0	9.45e-04	8.53e-04	8.21e-04	84,90,97
	39.6	0.07	0.17	0.07	84,84,97	0.0	0.0	0.0	0,0,0				
713	0.0	0.06	0.31	0.06	84,83,97	0.0	0.0	0.0	0,0,0	9.36e-03	8.35e-03	7.94e-03	84,90,97
	39.6	0.13	0.40	0.14	84,83,97	0.0	0.0	0.0	0,0,0				
714	0.0	5.57e-03	3.25e-03	6.85e-03	83,83,96	0.0	0.0	0.0	0,0,0	-3.80e-03	-3.38e-03	-3.21e-03	83,89,96
	40.2	9.84e-03	8.24e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
715	0.0	0.0	0.15	0.0	83,0	0.0	0.0	0.0	0,0,0	-6.20e-03	-5.65e-03	-5.43e-03	83,89,96
	54.5	0.0	0.16	0.0	83,0	0.0	0.0	0.0	0,0,0				
716	0.0	4.40e-03	4.57e-03	5.26e-03	84,84,97	0.0	0.0	0.0	0,0,0	-4.61e-03	-4.26e-03	-4.12e-03	83,89,96
	40.2	0.01	0.02	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
717	0.0	0.0	0.16	0.0	81,0	0.0	0.0	0.0	0,0,0	-1.55e-03	-1.55e-03	-1.55e-03	83,89,96
	54.5	0.0	0.15	0.0	81,0	0.0	0.0	0.0	0,0,0				
718	0.0	0.06	0.12	0.07	84,84,97	0.0	0.0	0.0	0,0,0	-0.02	-0.02	-0.02	83,89,96
	120.5	0.07	0.15	0.08	84,84,97	0.0	0.0	0.0	0,0,0				
	241.0	0.05	0.07	0.06	83,83,96	0.0	0.0	0.0	0,0,0				
719	0.0	0.0	0.04	0.0	83,0	0.0	0.0	0.0	0,0,0	-2.93e-03	-2.33e-03	-2.11e-03	84,90,97
	120.0	0.01	0.06	0.01	84,83,97	0.0	0.0	0.0	0,0,0				
720	0.0	0.0	2.60e-03	0.0	83,0	0.0	0.0	0.0	0,0,0	-1.81e-03	-1.67e-03	-1.62e-03	83,89,96
	40.0	3.45e-03	7.46e-03	4.44e-03	83,83,96	0.0	0.0	0.0	0,0,0				
721	0.0	0.0	0.06	0.0	83,0	0.0	0.0	0.0	0,0,0	-1.15e-03	-9.86e-04	-9.25e-04	84,90,97
	40.0	0.0	0.05	0.0	83,0	0.0	0.0	0.0	0,0,0				
722	0.0	0.0	0.02	0.0	83,0	0.0	0.0	0.0	0,0,0	-1.92e-03	-1.76e-03	-1.69e-03	83,89,96
	40.0	0.0	0.01	0.0	83,0	0.0	0.0	0.0	0,0,0				
723	0.0	0.08	0.25	0.08	84,83,97	0.0	0.0	0.0	0,0,0	-3.86e-03	-3.66e-03	-3.58e-03	83,89,96
	54.5	0.03	0.18	4.85e-05	84,83,97	0.0	0.0	0.0	0,0,0				
724	0.0	0.08	0.16	0.08	84,84,97	0.0	0.0	0.0	0,0,0	-0.04	-0.03	-0.03	84,90,97
	119.0	0.06	0.12	0.06	84,84,97	0.0	0.0	0.0	0,0,0				
725	0.0	0.09	0.27	0.11	84,83,97	0.0	0.0	0.0	0,0,0	-2.85e-03	-2.52e-03	-2.38e-03	83,89,96
	29.9	0.09	0.27	0.10	84,83,97	0.0	0.0	0.0	0,0,0				
726	0.0	0.03	0.03	0.03	84,84,97	0.0	0.0	0.0	0,0,0	-0.03	-0.03	-0.03	83,89,96
	100.1	0.25	0.33	0.30	83,83,96	0.0	0.0	0.0	0,0,0				
727	0.0	0.11	0.28	0.12	84,83,97	0.0	0.0	0.0	0,0,0	-5.46e-03	-4.94e-03	-4.74e-03	83,89,96
	47.9	0.12	0.30	0.14	84,83,97	0.0	0.0	0.0	0,0,0				
728	0.0	2.05e-03	1.19e-03	2.60e-03	84,84,97	0.0	0.0	0.0	0,0,0	-3.81e-03	-3.39e-03	-3.23e-03	83,89,96
	39.3	4.87e-03	5.91e-03	6.04e-03	83,83,96	0.0	0.0	0.0	0,0,0				
729	0.0	2.47e-03	0.08	0.0	84,83,0	0.0	0.0	0.0	0,0,0	-1.05e-03	-9.52e-04	-9.14e-04	83,89,96
	23.5	0.0	0.07	0.0	83,0	0.0	0.0	0.0	0,0,0				
730	0.0	6.98e-04	4.18e-04	7.73e-04	84,84,97	0.0	0.0	0.0	0,0,0	-4.52e-03	-4.18e-03	-4.04e-03	83,89,96
	39.3	4.12e-03	6.34e-03	4.90e-03	84,84,97	0.0	0.0	0.0	0,0,0				
731	0.0	0.03	0.01	0.03	83,83,96	0.0	0.0	0.0	0,0,0	1.21e-03	1.17e-03	1.15e-03	83,89,96
	38.3	0.01	7.21e-03	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
732	0.0	0.0	8.08e-03	0.0	83,0	0.0	0.0	0.0	0,0,0	-1.81e-03	-1.67e-03	-1.61e-03	83,89,96
	40.0	0.0	6.26e-03	0.0	83,0	0.0	0.0	0.0	0,0,0				
733	0.0	0.0	0.01	0.0	83,0	0.0	0.0	0.0	0,0,0	-1.65e-03	-1.49e-03	-1.43e-03	83,89,96
	40.0	0.0	0.02	0.0	83,0	0.0	0.0	0.0	0,0,0				
734	0.0	0.0	0.13	0.0	83,0	0.0	0.0	0.0	0,0,0	-9.59e-04	-8.19e-04	-7.61e-04	84,90,97
	23.5	0.0	0.13	0.0	83,0	0.0	0.0	0.0	0,0,0				
735	0.0	0.12	0.20	0.13	83,84,96	0.0	0.0	0.0	0,0,0	-0.14	-0.12	-0.10	84,90,97
	374.8	0.22	0.27	0.26	83,83,96	0.0	0.0	0.0	0,0,0				
736	0.0	0.06	0.13	0.06	84,84,97	0.0	0.0	0.0	0,0,0	-2.05e-03	-1.76e-03	-1.64e-03	83,89,96
	31.3	0.06	0.14	0.06	84,84,97	0.0	0.0	0.0	0,0,0				
737	0.0	0.15	0.31	0.17	83,83,96	0.0	0.0	0.0	0,0,0	3.98e-03	3.53e-03	3.35e-03	84,90,97
	39.6	0.13	0.28	0.14	83,83,96	0.0	0.0	0.0	0,0,0				
738	0.0	0.01	6.84e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0	-1.94e-03	-1.63e-03	-1.51e-03	83,89,96
	39.7	0.01	6.68e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
739	0.0	0.03	0.08	0.03	84,81,97	0.0	0.0	0.0	0,0,0	-2.22e-03	-2.06e-03	-2.00e-03	83,89,96
	38.3	0.02	0.07	9.02e-03	84,81,97	0.0	0.0	0.0	0,0,0				
740	0.0	7.53e-03	4.36e-03	9.62e-03	83,83,96	0.0	0.0	0.0	0,0,0	-1.54e-03	-1.33e-03	-1.25e-03	83,89,96
	53.5	5.70e-03	3.42e-03	6.90e-03	83,83,96	0.0	0.0	0.0	0,0,0				
741	0.0	0.0	0.16	0.0	83,0</								

743	0.0	0.01	0.06	0.02	84,83,97	0.0	0.0	0.0	0,0,0	-3.77e-03	-3.32e-03	-3.14e-03	84,90,97
	50.0	0.03	0.09	0.04	84,83,97	0.0	0.0	0.0	0,0,0				
744	0.0	0.0	0.07	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.67e-03	-2.37e-03	-2.26e-03	84,90,97
	50.0	0.0	0.06	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
745	0.0	0.01	0.15	0.0	84,83,0	0.0	0.0	0.0	0,0,0	5.83e-04	3.67e-04	2.88e-04	84,90,97
	38.3	0.0	0.11	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
746	0.0	3.62e-03	2.17e-03	4.49e-03	84,84,94	0.0	0.0	0.0	0,0,0	-8.69e-04	-7.70e-04	-3.39e-04	83,89,96
	38.0	3.96e-03	2.35e-03	5.29e-03	81,81,94	0.0	0.0	0.0	0,0,0				
747	0.0	0.07	0.12	0.07	83,83,96	0.0	0.0	0.0	0,0,0	-0.05	-0.04	-0.04	84,90,97
	214.6	0.10	0.20	0.11	84,84,97	0.0	0.0	0.0	0,0,0				
748	0.0	0.13	0.27	0.15	83,83,96	0.0	0.0	0.0	0,0,0	8.19e-04	7.44e-04	7.14e-04	84,90,97
	60.1	0.10	0.24	0.11	83,83,96	0.0	0.0	0.0	0,0,0				
749	0.0	0.02	0.02	0.02	84,81,97	0.0	0.0	0.0	0,0,0	-0.06	-0.06	-0.05	83,89,96
	374.8	0.16	0.22	0.18	84,83,97	0.0	0.0	0.0	0,0,0				
750	0.0	0.0	0.01	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.26e-03	-1.11e-03	-1.06e-03	84,90,97
	38.3	0.0	0.01	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
751	0.0	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.72e-03	-1.58e-03	-1.53e-03	83,89,96
	40.0	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
752	0.0	0.0	0.01	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.59e-03	-1.43e-03	-1.36e-03	83,89,96
	40.0	0.0	0.01	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
753	0.0	2.74e-03	1.62e-03	3.65e-03	81,81,94	0.0	0.0	0.0	0,0,0	1.52e-03	1.52e-03	1.52e-03	81,87,94
	38.3	4.33e-03	2.35e-03	5.54e-03	83,83,96	0.0	0.0	0.0	0,0,0				
754	0.0	0.07	0.17	0.07	84,84,97	0.0	0.0	0.0	0,0,0	-1.71e-03	-1.44e-03	-1.34e-03	83,89,96
	47.9	0.05	0.15	0.06	83,84,96	0.0	0.0	0.0	0,0,0				
755	0.0	0.01	6.24e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0	-2.31e-03	-1.97e-03	-1.84e-03	83,89,96
	40.2	0.01	6.81e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
756	0.0	0.0	0.20	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-6.01e-03	-5.42e-03	-5.19e-03	83,89,96
	40.2	0.0	0.19	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
757	0.0	0.0	0.11	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.01e-03	-1.01e-03	-1.01e-03	81,87,94
	40.2	0.0	0.11	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
758	0.0	0.0	0.05	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.38e-03	-1.20e-03	-1.13e-03	84,90,97
	40.0	0.0	0.06	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
759	0.0	0.0	0.17	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-0.05	-0.04	-0.04	84,90,97
	120.5	0.0	0.19	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
760	0.0	0.03	0.04	0.03	84,84,97	0.0	0.0	0.0	0,0,0	-1.69e-03	-1.14e-03	-9.19e-04	84,90,97
	40.0	0.02	0.02	0.02	84,84,97	0.0	0.0	0.0	0,0,0				
761	0.0	0.16	0.21	0.18	84,84,97	0.0	0.0	0.0	0,0,0	-0.05	-0.04	-0.04	84,90,97
	100.1	0.07	0.12	0.07	83,83,96	0.0	0.0	0.0	0,0,0				
762	0.0	0.08	0.18	0.10	83,83,96	0.0	0.0	0.0	0,0,0	9.91e-03	9.16e-03	8.86e-03	83,89,96
	45.0	0.15	0.28	0.17	83,83,96	0.0	0.0	0.0	0,0,0				
763	0.0	0.21	0.29	0.24	84,83,97	0.0	0.0	0.0	0,0,0	-0.06	-0.06	-0.05	83,89,96
	87.5	0.02	0.02	0.02	84,83,97	0.0	0.0	0.0	0,0,0				
764	0.0	0.0	0.08	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.19e-03	-1.11e-03	-1.07e-03	83,89,96
	38.3	0.0	0.07	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
765	0.0	0.01	0.02	0.02	83,83,96	0.0	0.0	0.0	0,0,0	1.94e-03	1.84e-03	1.80e-03	83,89,96
	38.3	4.27e-03	6.73e-03	5.10e-03	83,83,96	0.0	0.0	0.0	0,0,0				
766	0.0	0.0	0.12	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.82e-03	-1.56e-03	-1.46e-03	84,90,97
	38.3	0.0	0.13	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
767	0.0	0.05	0.21	0.07	83,83,96	0.0	0.0	0.0	0,0,0	9.18e-03	8.50e-03	8.23e-03	83,89,96
	45.0	0.12	0.31	0.15	83,83,96	0.0	0.0	0.0	0,0,0				
768	0.0	0.15	0.17	0.15	84,84,97	0.0	0.0	0.0	0,0,0	-0.03	-0.03	-0.03	84,90,97
	374.9	0.03	0.02	0.03	84,84,97	0.0	0.0	0.0	0,0,0				
769	0.0	0.13	0.29	0.14	83,83,96	0.0	0.0	0.0	0,0,0	7.71e-04	6.54e-04	6.10e-04	84,90,97
	39.6	0.11	0.27	0.12	83,83,96	0.0	0.0	0.0	0,0,0				
770	0.0	0.04	0.27	0.04	83,83,96	0.0	0.0	0.0	0,0,0	-6.42e-03	-5.87e-03	-5.65e-03	83,89,96
	43.8	0.05	0.28	0.06	83,83,96	0.0	0.0	0.0	0,0,0				
771	0.0	0.0	0.01	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-4.70e-03	-4.39e-03	-4.26e-03	83,89,96
	38.3	0.01	0.03	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
772	0.0	0.03	0.36	0.03	83,83,96	0.0	0.0	0.0	0,0,0	-7.89e-03	-7.21e-03	-6.94e-03	83,89,96
	43.8	0.07	0.39	0.08	83,83,96	0.0	0.0	0.0	0,0,0				
773	0.0	0.03	0.01	0.03	83,83,96	0.0	0.0	0.0	0,0,0	-1.55e-04	-1.54e-04	-1.53e-04	82,91,95
	38.3	9.43e-03	5.34e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
774	0.0	0.03	0.09	0.03	83,83,96	0.0	0.0	0.0	0,0,0	6.55e-04	5.67e-04	5.39e-04	84,90,97
	25.8	0.03	0.09	0.04	83,83,96	0.0	0.0	0.0	0,0,0				
775	0.0	0.0	6.32e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-6.33e-03	-5.99e-03	-5.85e-03	83,89,96
	38.3	0.05	0.08	0.06	83,83,96	0.0	0.0	0.0	0,0,0				
776	0.0	0.05	0.10	0.06	84,84,97	0.0	0.0	0.0	0,0,0	0.02	0.01	0.01	84,90,97
	198.0	0.17	0.24	0.18	84,84,97	0.0	0.0	0.0	0,0,0				
777	0.0	0.10	0.21	0.11	84,83,97	0.0	0.0	0.0	0,0,0	-0.05	-0.04	-0.04	83,89,96
	160.3	0.24	0.37	0.28	83,83,96	0.0	0.0	0.0	0,0,0				
778	0.0	0.01	7.84e-03	0.01	84,84,97	0.0	0.0	0.0	0,0,0	-0.03	-0.03	-0.03	83,89,96
	87.5	0.23	0.32	0.26	83,83,96	0.0	0.0	0.0	0,0,0				
779	0.0	0.12	0.29	0.14	83,83,96	0.0	0.0	0.0	0,0,0	-3.22e-03	-3.01e-03	-2.93e-03	83,89,96
	29.9	0.13	0.31	0.16	83,83,96	0.0	0.0	0.0	0,0,0				
780	0.0	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.61e-03	-1.48e-03	-1.43e-03	83,89,96
	40.0	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
781	0.0	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.48e-03	-1.32e-03	-1.25e-03	83,89,96
	40.0	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
782	0.0	9.98e-03	5.86e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0	-2.56e-03	-2.22e-03	-2.09e-03	83,89,96
	40.2	0.01	6.14e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
783	0.0	0.01	6.74e-03	0.01	84,84,97	0.0	0.0	0.0	0,0,0	-5.94e-03	-5.29e-03	-5.03e-03	83,89,96
	40.2	0.04	0.03	0.04	84,83,97	0.0	0.0	0.0	0,0,0				
784	0.0	0.0	0.15	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.62e-03	-1.62e-03	-1.62e-03	81,87,94
	40.2	0.0	0.14	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
785	0.0	0.0	0.05	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.28e-03	-1.11e-03	-1.05e-03	84,90,97
	40.0	0.0	0.05	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
786	0.0	2.38e-03	0.23	0.0	84,83,0	0.0	0.0	0.0	0,0,0	-0.05	-0.04	-0.04	84,90,97
	120.5	0.0	0.17	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
787	0.0	0.10	0.25	0.11	84,84,97	0.0	0.0	0.0	0,0,0	-8.34e-03	-7.39e-03	-7.01e-03	83,89,96
	45.0	0.04	0.16	0.04	84,84,97	0.0	0.0	0.0	0,0,0				
788	0.0	0.12	0.31	0.14	84,83,97	0.0	0.0	0.0	0,0,0	-9.58e-03	-8.64e-03	-8.26e-03	83,89,96
	39.6	0.06	0.22	0.06	84,83,97	0.0	0.0	0.0	0,0,0				
789	0.0	0.09	0.20	0.09	84,84,97	0.0	0.0	0.0	0,0,0	-9.22e-03	-7.88e-03	-7.36e-03	84,90,97
	39.6	0.04	0.13	0.04	84,84,97	0.0	0.0	0.0	0,0,0				
790	0.0	0.01	6.47e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0	-1.64e-03	-1.36e-03	-1.24e-03	83,89,96
	39.7	0.01	6.18e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
791	0.0	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-4.53e-03	-4.23e-03	-4.10e-03	83,89,96
	38.3	0.0	0										

	38.3	0.02	0.03	0.03	83,83,96	0.0	0.0	0.0	0,0,0				
794	0.0	0.0	0.05	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-5.96e-03	-5.65e-03	-5.52e-03	83,89,96
	38.3	0.0	0.04	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
795	0.0	3.40e-03	1.97e-03	4.53e-03	81,81,94	0.0	0.0	0.0	0,0,0	-1.04e-03	-4.40e-04	-4.09e-04	83,89,96
	40.0	3.18e-03	1.85e-03	4.24e-03	81,81,94	0.0	0.0	0.0	0,0,0				
796	0.0	0.02	0.03	0.02	83,81,96	0.0	0.0	0.0	0,0,0	-0.03	-0.03	-0.03	83,89,96
	310.3	0.01	0.02	0.01	84,82,97	0.0	0.0	0.0	0,0,0				
797	0.0	0.02	0.22	0.01	84,83,97	0.0	0.0	0.0	0,0,0	7.80e-03	6.87e-03	6.50e-03	84,90,97
	45.0	0.09	0.30	0.10	84,83,97	0.0	0.0	0.0	0,0,0				
798	0.0	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.36e-03	-1.21e-03	-1.15e-03	84,90,97
	38.3	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
799	0.0	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0	1.30e-03	1.30e-03	1.30e-03	81,87,94
	38.3	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
800	0.0	0.03	0.06	0.02	84,81,97	0.0	0.0	0.0	0,0,0	-5.01e-03	-4.48e-03	-4.27e-03	83,89,96
	54.5	0.03	0.06	0.02	84,81,97	0.0	0.0	0.0	0,0,0				
801	0.0	0.0	0.13	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-3.87e-04	-3.42e-04	-3.25e-04	83,89,96
	54.5	0.0	0.16	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
802	0.0	0.0	0.19	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-4.46e-03	-3.84e-03	-3.60e-03	84,90,97
	54.5	0.10	0.33	0.09	84,83,97	0.0	0.0	0.0	0,0,0				
803	0.0	0.02	0.03	0.02	84,84,97	0.0	0.0	0.0	0,0,0	-9.46e-04	-6.65e-04	-5.53e-04	83,89,96
	40.0	0.01	6.04e-03	6.63e-03	84,84,97	0.0	0.0	0.0	0,0,0				
804	0.0	0.14	0.32	0.16	83,83,96	0.0	0.0	0.0	0,0,0	2.78e-03	2.59e-03	2.51e-03	83,89,96
	29.9	0.12	0.30	0.14	83,83,96	0.0	0.0	0.0	0,0,0				
805	0.0	0.0	0.09	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.77e-03	-1.62e-03	-1.56e-03	83,89,96
	38.3	0.0	0.09	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
806	0.0	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	2.14e-03	2.03e-03	1.98e-03	83,89,96
	38.3	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
807	0.0	0.0	0.13	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.12e-03	-1.83e-03	-1.72e-03	84,90,97
	38.3	0.0	0.13	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
808	0.0	0.13	0.27	0.16	83,83,96	0.0	0.0	0.0	0,0,0	3.18e-03	2.96e-03	2.87e-03	84,90,97
	45.0	0.11	0.24	0.13	83,83,96	0.0	0.0	0.0	0,0,0				
809	0.0	0.11	0.26	0.12	83,83,96	0.0	0.0	0.0	0,0,0	-1.22e-03	-1.12e-03	-1.08e-03	83,89,96
	31.3	0.11	0.27	0.13	83,83,96	0.0	0.0	0.0	0,0,0				
810	0.0	0.02	9.83e-03	0.02	84,84,97	0.0	0.0	0.0	0,0,0	2.46e-04	2.14e-04	1.82e-04	82,91,95
	43.8	0.04	0.03	0.04	84,82,97	0.0	0.0	0.0	0,0,0				
811	0.0	0.04	0.02	0.04	83,83,96	0.0	0.0	0.0	0,0,0	-3.74e-03	-3.33e-03	-3.16e-03	83,89,96
	43.8	0.02	0.01	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
812	0.0	0.12	0.28	0.13	83,83,96	0.0	0.0	0.0	0,0,0	5.54e-04	5.10e-04	4.95e-04	84,90,97
	31.3	0.11	0.27	0.12	83,83,96	0.0	0.0	0.0	0,0,0				
813	0.0	0.04	0.03	0.03	84,84,97	0.0	0.0	0.0	0,0,0	-0.07	-0.06	-0.06	81,87,94
	374.9	0.16	0.17	0.16	84,84,97	0.0	0.0	0.0	0,0,0				
814	0.0	0.01	6.47e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0	-2.76e-03	-2.41e-03	-2.27e-03	83,89,96
	40.2	9.81e-03	5.74e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
815	0.0	0.08	0.16	0.08	84,84,97	0.0	0.0	0.0	0,0,0	-5.72e-03	-4.92e-03	-4.60e-03	84,90,97
	39.6	0.09	0.18	0.10	84,84,97	0.0	0.0	0.0	0,0,0				
816	0.0	0.0	0.04	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-4.40e-03	-4.10e-03	-3.98e-03	83,89,96
	38.3	0.0	0.04	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
817	0.0	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.46e-03	-2.32e-03	-2.27e-03	83,89,96
	38.3	7.54e-04	0.05	2.57e-04	83,83,96	0.0	0.0	0.0	0,0,0				
818	0.0	0.0	0.06	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-5.58e-03	-5.30e-03	-5.19e-03	83,89,96
	38.3	0.0	0.06	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
819	0.0	0.15	0.21	0.17	84,84,97	0.0	0.0	0.0	0,0,0	-0.03	-0.03	-0.03	84,90,97
	64.5	0.02	0.02	0.02	83,81,96	0.0	0.0	0.0	0,0,0				
820	0.0	0.05	0.27	0.05	83,83,96	0.0	0.0	0.0	0,0,0	-0.01	-0.01	-0.01	83,89,96
	47.7	0.0	0.22	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
821	0.0	0.06	0.43	0.07	83,83,96	0.0	0.0	0.0	0,0,0	-0.02	-0.02	-0.02	83,89,96
	47.7	0.0	0.39	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
822	0.0	0.07	0.20	0.08	83,83,96	0.0	0.0	0.0	0,0,0	9.14e-03	8.22e-03	7.86e-03	83,89,96
	39.6	0.14	0.30	0.15	83,83,96	0.0	0.0	0.0	0,0,0				
823	0.0	0.24	0.31	0.29	83,83,96	0.0	0.0	0.0	0,0,0	-0.07	-0.06	-0.06	83,89,96
	100.1	0.04	0.03	0.03	84,84,97	0.0	0.0	0.0	0,0,0				
824	0.0	0.01	6.38e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0	-1.38e-03	-1.11e-03	-1.01e-03	83,89,96
	39.7	0.01	6.26e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
825	0.0	0.0	0.02	0.0	0,84,0	0.0	0.0	0.0	0,0,0	-1.34e-03	-1.16e-03	-1.09e-03	83,89,96
	39.7	0.0	0.02	0.0	0,84,0	0.0	0.0	0.0	0,0,0				
826	0.0	3.17e-03	1.84e-03	4.23e-03	81,81,94	0.0	0.0	0.0	0,0,0	-1.13e-03	-4.94e-04	-4.63e-04	83,89,96
	40.0	2.04e-03	1.21e-03	2.72e-03	81,81,94	0.0	0.0	0.0	0,0,0				
827	0.0	0.11	0.23	0.12	83,83,96	0.0	0.0	0.0	0,0,0	-1.36e-03	-1.36e-03	-1.36e-03	81,87,94
	60.1	0.13	0.26	0.15	83,83,96	0.0	0.0	0.0	0,0,0				
828	0.0	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-7.55e-04	-6.69e-04	-6.37e-04	84,90,97
	38.3	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
829	0.0	0.0	0.05	0.0	0,83,0	0.0	0.0	0.0	0,0,0	1.11e-03	1.11e-03	1.11e-03	81,87,94
	38.3	0.0	0.05	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
830	0.0	0.01	9.32e-03	5.69e-03	84,84,97	0.0	0.0	0.0	0,0,0	-8.81e-04	-6.91e-04	-6.15e-04	83,89,96
	42.0	3.41e-03	2.04e-03	3.71e-03	84,84,94	0.0	0.0	0.0	0,0,0				
831	0.0	0.0	0.10	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.11e-03	-1.94e-03	-1.87e-03	83,89,96
	38.3	0.0	0.10	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
832	0.0	0.0	0.05	0.0	0,83,0	0.0	0.0	0.0	0,0,0	2.13e-03	2.04e-03	1.04e-03	83,89,96
	38.3	0.0	0.05	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
833	0.0	0.0	0.13	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.45e-03	-2.14e-03	-2.02e-03	84,90,97
	38.3	0.0	0.13	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
834	0.0	0.11	0.24	0.13	83,83,96	0.0	0.0	0.0	0,0,0	-1.26e-03	-1.06e-03	-9.78e-04	83,89,96
	60.1	0.10	0.23	0.12	84,84,97	0.0	0.0	0.0	0,0,0				
835	0.0	0.03	0.07	0.03	83,84,96	0.0	0.0	0.0	0,0,0	-7.25e-03	-6.76e-03	-6.56e-03	83,89,96
	53.7	0.0	0.02	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
836	0.0	0.04	0.07	0.05	83,84,96	0.0	0.0	0.0	0,0,0	-0.01	-9.45e-03	-9.13e-03	83,89,96
	53.7	7.86e-03	0.02	8.79e-03	83,82,96	0.0	0.0	0.0	0,0,0				
837	0.0	0.06	0.12	0.06	84,83,97	0.0	0.0	0.0	0,0,0	-0.06	-0.03	-0.03	84,90,97
	100.1	0.17	0.25	0.19	83,83,96	0.0	0.0	0.0	0,0,0				
838	0.0	0.02	0.04	0.03	84,84,97	0.0	0.0	0.0	0,0,0	3.21e-03	2.71e-03	2.52e-03	84,90,97
	47.9	4.91e-03	0.01	5.12e-03	83,84,96	0.0	0.0	0.0	0,0,0				
839	0.0	0.01	7.40e-03	0.02	83,83,96	0.0	0.0	0.0	0,0,0	-3.06e-03	-2.69e-03	-2.54e-03	83,89,96
	40.2	0.01	6.74e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
840	0.0	0.06	0.13	0.06	84,84,97	0.0	0.0	0.0	0,0,0	-3.73e-03	-3.21e-03	-3.00e-03	83,89,96
	39.6	0.08	0.16	0.08	84,84,97	0.0	0.0	0.0	0,0,0				
841	0.0	0.0	0.04	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-4.30e-03	-4.01e-03	-3.90e-03	83,89,96
	38.3	0.0	0.04	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
842	0.0	0.0	0										

844	0.0	0.10	0.24	0.11	83,83,96	0.0	0.0	0.0	0,0,0	-3.55e-03	-3.11e-03	-2.93e-03	83,89,96
	45.0	0.10	0.24	0.11	84,84,97	0.0	0.0	0.0	0,0,0				
845	0.0	0.05	0.28	0.06	83,83,96	0.0	0.0	0.0	0,0,0	-9.61e-03	-8.85e-03	-8.54e-03	83,89,96
	43.8	0.04	0.27	0.05	83,83,96	0.0	0.0	0.0	0,0,0				
846	0.0	0.06	0.40	0.07	83,83,96	0.0	0.0	0.0	0,0,0	-0.01	-0.01	-0.01	83,89,96
	43.8	0.07	0.41	0.08	83,83,96	0.0	0.0	0.0	0,0,0				
847	0.0	0.13	0.30	0.16	83,83,96	0.0	0.0	0.0	0,0,0	-0.01	-9.61e-03	-9.32e-03	83,89,96
	45.0	0.07	0.21	0.08	83,83,96	0.0	0.0	0.0	0,0,0				
848	0.0	0.11	0.22	0.13	83,83,96	0.0	0.0	0.0	0,0,0	2.93e-03	2.53e-03	2.37e-03	84,90,97
	45.0	0.11	0.22	0.12	83,83,96	0.0	0.0	0.0	0,0,0				
849	0.0	0.03	0.06	0.04	84,84,97	0.0	0.0	0.0	0,0,0	-1.43e-03	-1.27e-03	-1.21e-03	83,89,96
	43.8	0.04	0.08	0.05	83,84,96	0.0	0.0	0.0	0,0,0				
850	0.0	0.01	8.44e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0	-3.43e-03	-3.10e-03	-2.97e-03	83,89,96
	43.8	0.03	0.02	0.04	83,83,96	0.0	0.0	0.0	0,0,0				
851	0.0	0.23	0.34	0.26	84,83,97	0.0	0.0	0.0	0,0,0	-0.06	-0.03	-0.03	83,89,96
	374.9	0.06	0.12	0.07	84,83,97	0.0	0.0	0.0	0,0,0				
852	0.0	0.05	0.09	0.05	84,84,97	0.0	0.0	0.0	0,0,0	9.52e-03	8.09e-03	7.54e-03	84,90,97
	39.6	0.10	0.15	0.10	84,84,97	0.0	0.0	0.0	0,0,0				
853	0.0	0.13	0.31	0.15	83,83,96	0.0	0.0	0.0	0,0,0	4.57e-03	4.13e-03	3.95e-03	84,90,97
	47.9	0.12	0.29	0.13	83,83,96	0.0	0.0	0.0	0,0,0				
854	0.0	0.01	6.11e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0	-1.08e-03	-8.28e-04	-7.28e-04	83,89,96
	39.7	8.84e-03	5.23e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
855	0.0	0.0	0.03	0.0	84,0	0.0	0.0	0.0	0,0,0	-1.46e-03	-1.26e-03	-1.18e-03	83,89,96
	39.7	0.0	0.03	0.0	84,0	0.0	0.0	0.0	0,0,0				
856	0.0	2.63e-03	1.60e-03	3.51e-03	83,83,96	0.0	0.0	0.0	0,0,0	-1.17e-03	-1.03e-03	-9.68e-04	83,89,96
	40.0	3.47e-03	2.05e-03	3.31e-03	83,83,96	0.0	0.0	0.0	0,0,0				
857	0.0	0.0	0.02	0.0	83,0	0.0	0.0	0.0	0,0,0	-1.47e-03	-1.29e-03	-1.23e-03	84,90,97
	38.3	0.0	0.02	0.0	83,0	0.0	0.0	0.0	0,0,0				
858	0.0	0.0	0.05	0.0	83,0	0.0	0.0	0.0	0,0,0	9.38e-04	9.38e-04	9.38e-04	81,87,94
	38.3	0.0	0.05	0.0	83,0	0.0	0.0	0.0	0,0,0				
859	0.0	0.0	0.11	0.0	83,0	0.0	0.0	0.0	0,0,0	-2.41e-03	-2.21e-03	-2.13e-03	83,89,96
	38.3	0.0	0.11	0.0	83,0	0.0	0.0	0.0	0,0,0				
860	0.0	0.0	0.08	0.0	83,0	0.0	0.0	0.0	0,0,0	2.00e-03	1.90e-03	1.86e-03	83,89,96
	38.3	0.0	0.08	0.0	83,0	0.0	0.0	0.0	0,0,0				
861	0.0	0.0	0.14	0.0	83,0	0.0	0.0	0.0	0,0,0	-2.96e-03	-2.61e-03	-2.47e-03	84,90,97
	38.3	0.0	0.15	0.0	83,0	0.0	0.0	0.0	0,0,0				
862	0.0	0.07	0.14	0.08	83,84,96	0.0	0.0	0.0	0,0,0	3.69e-03	3.44e-03	3.34e-03	83,89,96
	43.8	0.08	0.15	0.10	83,83,96	0.0	0.0	0.0	0,0,0				
863	0.0	0.06	0.07	0.07	83,84,96	0.0	0.0	0.0	0,0,0	2.84e-03	2.67e-03	2.60e-03	83,89,96
	43.8	0.07	0.09	0.09	83,84,96	0.0	0.0	0.0	0,0,0				
864	0.0	0.11	0.26	0.12	83,83,96	0.0	0.0	0.0	0,0,0	6.27e-04	5.14e-04	4.73e-04	84,90,97
	30.0	0.11	0.26	0.12	83,83,96	0.0	0.0	0.0	0,0,0				
865	0.0	6.02e-03	8.35e-03	6.67e-03	83,84,96	0.0	0.0	0.0	0,0,0	2.66e-03	2.24e-03	2.08e-03	84,90,97
	39.6	2.98e-04	1.70e-04	3.97e-04	81,81,94	0.0	0.0	0.0	0,0,0				
866	0.0	0.01	6.12e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0	-3.48e-03	-3.07e-03	-2.91e-03	83,89,96
	40.2	0.01	7.13e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
867	0.0	0.0	0.05	0.0	83,0	0.0	0.0	0.0	0,0,0	-4.21e-03	-3.94e-03	-3.82e-03	83,89,96
	38.3	0.0	0.05	0.0	83,0	0.0	0.0	0.0	0,0,0				
868	0.0	0.0	0.08	0.0	83,0	0.0	0.0	0.0	0,0,0	-2.63e-03	-2.51e-03	-2.42e-03	83,89,96
	38.3	0.0	0.07	0.0	83,0	0.0	0.0	0.0	0,0,0				
869	0.0	0.0	0.08	0.0	83,0	0.0	0.0	0.0	0,0,0	-5.08e-03	-4.84e-03	-4.74e-03	83,89,96
	38.3	0.0	0.08	0.0	83,0	0.0	0.0	0.0	0,0,0				
870	0.0	0.10	0.45	0.11	84,83,97	0.0	0.0	0.0	0,0,0	-0.01	-8.93e-03	-8.50e-03	83,89,96
	39.6	0.02	0.36	0.01	84,83,97	0.0	0.0	0.0	0,0,0				
871	0.0	0.07	0.04	0.08	83,83,96	0.0	0.0	0.0	0,0,0	1.30e-03	1.11e-03	1.05e-03	84,90,97
	51.7	0.07	0.04	0.08	83,83,96	0.0	0.0	0.0	0,0,0				
872	0.0	0.07	0.04	0.08	83,83,96	0.0	0.0	0.0	0,0,0	-2.79e-03	-2.53e-03	-2.43e-03	83,89,96
	51.7	0.07	0.04	0.09	83,83,96	0.0	0.0	0.0	0,0,0				
873	0.0	0.05	0.16	0.05	84,83,97	0.0	0.0	0.0	0,0,0	7.72e-03	6.81e-03	6.46e-03	84,90,97
	45.0	0.11	0.25	0.12	84,83,97	0.0	0.0	0.0	0,0,0				
874	0.0	0.09	0.28	0.10	84,83,97	0.0	0.0	0.0	0,0,0	-8.04e-03	-7.10e-03	-6.73e-03	84,90,97
	45.0	0.02	0.19	0.01	84,83,97	0.0	0.0	0.0	0,0,0				
875	0.0	0.04	0.06	0.05	83,84,96	0.0	0.0	0.0	0,0,0	-2.91e-03	-2.66e-03	-2.57e-03	83,89,96
	43.8	0.05	0.06	0.06	83,84,96	0.0	0.0	0.0	0,0,0				
876	0.0	0.03	0.02	0.04	84,82,97	0.0	0.0	0.0	0,0,0	-4.58e-03	-4.18e-03	-4.02e-03	83,89,96
	43.8	0.05	0.04	0.06	83,84,96	0.0	0.0	0.0	0,0,0				
877	0.0	0.10	0.16	0.10	84,84,97	0.0	0.0	0.0	0,0,0	5.87e-03	5.01e-03	4.68e-03	84,90,97
	39.6	0.07	0.13	0.08	84,84,97	0.0	0.0	0.0	0,0,0				
878	0.0	8.13e-03	4.75e-03	9.35e-03	83,83,96	0.0	0.0	0.0	0,0,0	-8.33e-04	-6.03e-04	-5.11e-04	83,89,96
	39.7	5.53e-03	3.32e-03	5.87e-03	83,83,96	0.0	0.0	0.0	0,0,0				
879	0.0	0.0	0.03	0.0	84,0	0.0	0.0	0.0	0,0,0	-1.56e-03	-1.36e-03	-1.27e-03	83,89,96
	39.7	0.0	0.04	0.0	84,0	0.0	0.0	0.0	0,0,0				
880	0.0	3.29e-03	1.93e-03	3.26e-03	83,83,96	0.0	0.0	0.0	0,0,0	-1.16e-03	-1.02e-03	-9.65e-04	83,89,96
	40.0	9.84e-03	0.01	9.89e-03	84,84,97	0.0	0.0	0.0	0,0,0				
881	0.0	0.0	0.02	0.0	83,0	0.0	0.0	0.0	0,0,0	-1.36e-03	-1.17e-03	-1.11e-03	84,90,97
	38.3	1.25e-03	0.03	1.67e-03	81,83,94	0.0	0.0	0.0	0,0,0				
882	0.0	0.0	0.07	0.0	83,0	0.0	0.0	0.0	0,0,0	6.47e-04	6.47e-04	6.47e-04	81,87,94
	31.3	0.0	0.07	0.0	83,0	0.0	0.0	0.0	0,0,0				
883	0.0	0.0	0.11	0.0	83,0	0.0	0.0	0.0	0,0,0	-2.75e-03	-2.53e-03	-2.43e-03	83,89,96
	38.3	0.0	0.12	0.0	83,0	0.0	0.0	0.0	0,0,0				
884	0.0	0.0	0.05	0.0	83,0	0.0	0.0	0.0	0,0,0	1.86e-03	1.78e-03	1.74e-03	83,89,96
	38.3	0.0	0.05	0.0	83,0	0.0	0.0	0.0	0,0,0				
885	0.0	0.0	0.15	0.0	83,0	0.0	0.0	0.0	0,0,0	-3.95e-03	-3.50e-03	-3.32e-03	84,90,97
	38.3	0.0	0.13	0.0	81,0	0.0	0.0	0.0	0,0,0				
886	0.0	0.04	0.17	0.05	83,84,96	0.0	0.0	0.0	0,0,0	-6.67e-03	-6.21e-03	-6.02e-03	83,89,96
	47.7	0.0	0.12	0.0	84,0	0.0	0.0	0.0	0,0,0				
887	0.0	0.05	0.16	0.06	83,84,96	0.0	0.0	0.0	0,0,0	-7.22e-03	-6.69e-03	-6.47e-03	83,89,96
	47.7	0.01	0.12	0.01	83,84,96	0.0	0.0	0.0	0,0,0				
888	0.0	0.11	0.22	0.13	83,84,96	0.0	0.0	0.0	0,0,0	-0.05	-0.04	-0.04	84,90,97
	87.5	0.05	0.04	0.05	84,84,97	0.0	0.0	0.0	0,0,0				
889	0.0	0.0	0.06	0.0	83,0	0.0	0.0	0.0	0,0,0	-4.13e-03	-3.86e-03	-3.75e-03	83,89,96
	38.3	0.0	0.06	0.0	83,0	0.0	0.0	0.0	0,0,0				
890	0.0	0.0	0.12	0.0	83,0	0.0	0.0	0.0	0,0,0	-2.48e-03	-2.35e-03	-2.30e-03	83,89,96
	38.3	0.0	0.11	0.0	83,0	0.0	0.0	0.0	0,0,0				
891	0.0	0.0	0.11	0.0	83,0	0.0	0.0	0.0	0,0,0	-4.85e-03	-4.63e-03	-4.54e-03	83,89,96
	38.3	0.0	0.11	0.0	83,0	0.0	0.0	0.0	0,0,0				
892	0.0	0.12	0.29	0.14	83,83,96	0.0	0.0	0.0	0,0,0	-4.78e-03	-4.25e-03	-4.05e-03	83,89,96
	39.6	0.14											

	43.8	0.07	0.15	0.09	83,84,96	0.0	0.0	0.0	0,0,0				
895	0.0	0.23	0.31	0.28	83,83,96	0.0	0.0	0.0	0,0,0	-0.05	-0.04	-0.04	83,89,96
	374.8	0.11	0.21	0.13	83,84,96	0.0	0.0	0.0	0,0,0				
896	0.0	0.10	0.30	0.11	84,83,97	0.0	0.0	0.0	0,0,0	2.25e-03	1.97e-03	1.86e-03	84,90,97
	29.9	0.10	0.30	0.11	84,83,97	0.0	0.0	0.0	0,0,0				
897	0.0	0.05	0.06	0.06	83,84,96	0.0	0.0	0.0	0,0,0	-4.54e-03	-4.20e-03	-4.07e-03	83,89,96
	43.8	0.03	0.05	0.04	83,82,96	0.0	0.0	0.0	0,0,0				
898	0.0	0.05	0.05	0.06	83,84,96	0.0	0.0	0.0	0,0,0	-6.45e-03	-5.92e-03	-5.71e-03	83,89,96
	43.8	0.05	0.05	0.05	83,84,96	0.0	0.0	0.0	0,0,0				
899	0.0	0.07	0.13	0.08	84,84,97	0.0	0.0	0.0	0,0,0	3.90e-03	3.32e-03	3.10e-03	84,90,97
	39.6	0.04	0.08	0.05	84,84,97	0.0	0.0	0.0	0,0,0				
900	0.0	3.93e-03	2.31e-03	4.03e-03	83,83,96	0.0	0.0	0.0	0,0,0	-7.66e-04	-5.48e-04	-4.62e-04	83,89,96
	39.7	2.34e-03	1.43e-03	1.98e-03	83,83,96	0.0	0.0	0.0	0,0,0				
901	0.0	0.0	0.04	0.0	0.84,0	0.0	0.0	0.0	0,0,0	-2.41e-03	-2.10e-03	-1.97e-03	83,89,96
	55.2	0.0	0.04	0.0	0.83,0	0.0	0.0	0.0	0,0,0				
902	0.0	0.01	8.39e-03	0.01	84,84,97	0.0	0.0	0.0	0,0,0	-9.70e-04	-8.74e-04	-8.35e-04	83,89,96
	40.0	0.02	0.03	0.02	84,84,97	0.0	0.0	0.0	0,0,0				
903	0.0	5.79e-03	0.02	7.73e-03	81,83,94	0.0	0.0	0.0	0,0,0	-1.03e-03	-8.20e-04	-7.45e-04	84,90,97
	38.3	8.92e-03	0.03	0.01	81,83,94	0.0	0.0	0.0	0,0,0				
904	0.0	0.0	0.05	0.0	0.83,0	0.0	0.0	0.0	0,0,0	7.89e-04	7.89e-04	7.89e-04	81,87,94
	45.3	0.0	0.05	0.0	0.83,0	0.0	0.0	0.0	0,0,0				
905	0.0	0.0	0.13	0.0	0.83,0	0.0	0.0	0.0	0,0,0	-3.27e-03	-3.00e-03	-2.89e-03	83,89,96
	38.3	0.0	0.14	0.0	0.83,0	0.0	0.0	0.0	0,0,0				
906	0.0	0.0	0.06	0.0	0.83,0	0.0	0.0	0.0	0,0,0	1.77e-03	1.69e-03	1.66e-03	83,89,96
	38.3	0.0	0.06	0.0	0.83,0	0.0	0.0	0.0	0,0,0				
907	0.0	0.0	0.13	0.0	0.81,0	0.0	0.0	0.0	0,0,0	-5.01e-03	-4.55e-03	-4.36e-03	83,89,96
	38.3	0.0	0.17	0.0	0.83,0	0.0	0.0	0.0	0,0,0				
908	0.0	0.04	0.06	0.05	83,84,96	0.0	0.0	0.0	0,0,0	4.55e-03	4.22e-03	4.09e-03	83,89,96
	43.7	0.05	0.07	0.06	83,84,96	0.0	0.0	0.0	0,0,0				
909	0.0	0.04	0.02	0.05	83,83,96	0.0	0.0	0.0	0,0,0	4.65e-03	4.32e-03	4.19e-03	83,89,96
	43.7	0.05	0.03	0.06	83,83,96	0.0	0.0	0.0	0,0,0				
910	0.0	0.0	0.06	0.0	0.83,0	0.0	0.0	0.0	0,0,0	-4.05e-03	-3.79e-03	-3.68e-03	83,89,96
	38.3	0.0	0.06	0.0	0.83,0	0.0	0.0	0.0	0,0,0				
911	0.0	0.0	0.08	0.0	0.83,0	0.0	0.0	0.0	0,0,0	-2.33e-03	-2.21e-03	-2.16e-03	83,89,96
	38.3	0.0	0.08	0.0	0.83,0	0.0	0.0	0.0	0,0,0				
912	0.0	0.0	0.09	0.0	0.83,0	0.0	0.0	0.0	0,0,0	-4.65e-03	-4.44e-03	-4.36e-03	83,89,96
	38.3	0.0	0.09	0.0	0.83,0	0.0	0.0	0.0	0,0,0				
913	0.0	0.11	0.27	0.12	83,83,96	0.0	0.0	0.0	0,0,0	-1.63e-03	-1.44e-03	-1.36e-03	83,89,96
	39.6	0.12	0.29	0.14	83,83,96	0.0	0.0	0.0	0,0,0				
914	0.0	0.07	0.19	0.08	83,83,96	0.0	0.0	0.0	0,0,0	4.89e-04	4.79e-04	4.73e-04	83,90,97
	43.8	0.05	0.17	0.06	83,84,96	0.0	0.0	0.0	0,0,0				
915	0.0	0.07	0.11	0.09	83,84,96	0.0	0.0	0.0	0,0,0	2.38e-04	2.22e-04	2.15e-04	83,89,96
	43.8	0.06	0.09	0.07	83,84,96	0.0	0.0	0.0	0,0,0				
916	0.0	0.11	0.40	0.14	83,83,96	0.0	0.0	0.0	0,0,0	-0.01	-0.01	-9.85e-03	83,89,96
	45.0	0.03	0.30	0.04	83,83,96	0.0	0.0	0.0	0,0,0				
917	0.0	0.07	0.15	0.09	83,84,96	0.0	0.0	0.0	0,0,0	-3.80e-03	-3.52e-03	-3.41e-03	83,89,96
	43.8	0.06	0.13	0.07	83,84,96	0.0	0.0	0.0	0,0,0				
918	0.0	0.07	0.15	0.09	83,84,96	0.0	0.0	0.0	0,0,0	-4.10e-03	-3.79e-03	-3.66e-03	83,89,96
	43.8	0.06	0.14	0.07	83,84,96	0.0	0.0	0.0	0,0,0				
919	0.0	0.04	0.08	0.05	84,84,97	0.0	0.0	0.0	0,0,0	2.38e-03	2.02e-03	1.88e-03	84,90,97
	31.3	0.02	0.05	0.03	83,84,96	0.0	0.0	0.0	0,0,0				
920	0.0	0.0	7.12e-03	0.0	0.82,0	0.0	0.0	0.0	0,0,0	-7.47e-04	-5.36e-04	-4.53e-04	83,89,96
	39.7	0.0	8.52e-03	0.0	0.82,0	0.0	0.0	0.0	0,0,0				
921	0.0	0.0	0.05	0.0	0.83,0	0.0	0.0	0.0	0,0,0	-5.97e-04	-5.20e-04	-4.90e-04	83,89,96
	24.2	0.0	0.05	0.0	0.83,0	0.0	0.0	0.0	0,0,0				
922	0.0	0.02	0.02	0.02	84,84,97	0.0	0.0	0.0	0,0,0	-2.77e-04	-2.77e-04	-2.77e-04	81,87,94
	40.0	0.02	0.03	0.03	84,84,97	0.0	0.0	0.0	0,0,0				
923	0.0	7.91e-03	0.03	0.01	81,83,94	0.0	0.0	0.0	0,0,0	-5.15e-04	-2.80e-04	-2.00e-04	84,90,97
	38.3	5.64e-03	0.03	7.52e-03	81,83,94	0.0	0.0	0.0	0,0,0				
924	0.0	0.0	0.06	0.0	0.83,0	0.0	0.0	0.0	0,0,0	5.52e-04	5.52e-04	5.52e-04	81,87,94
	38.3	0.0	0.06	0.0	0.83,0	0.0	0.0	0.0	0,0,0				
925	0.0	0.0	0.07	0.0	0.83,0	0.0	0.0	0.0	0,0,0	1.66e-03	1.60e-03	1.57e-03	83,89,96
	38.3	0.0	0.07	0.0	0.83,0	0.0	0.0	0.0	0,0,0				
926	0.0	0.01	6.21e-03	0.01	83,83,97	0.0	0.0	0.0	0,0,0	-4.88e-04	-4.42e-04	-3.95e-04	82,91,95
	47.7	0.03	0.02	0.04	83,83,96	0.0	0.0	0.0	0,0,0				
927	0.0	0.01	6.16e-03	0.01	84,84,97	0.0	0.0	0.0	0,0,0	6.82e-04	5.25e-04	4.62e-04	83,89,96
	47.7	0.03	0.02	0.03	83,83,96	0.0	0.0	0.0	0,0,0				
928	0.0	0.0	0.07	0.0	0.83,0	0.0	0.0	0.0	0,0,0	-3.97e-03	-3.72e-03	-3.62e-03	83,89,96
	38.3	0.0	0.07	0.0	0.83,0	0.0	0.0	0.0	0,0,0				
929	0.0	0.0	0.09	0.0	0.83,0	0.0	0.0	0.0	0,0,0	-2.22e-03	-2.11e-03	-2.07e-03	83,89,96
	38.3	0.0	0.09	0.0	0.83,0	0.0	0.0	0.0	0,0,0				
930	0.0	0.0	0.09	0.0	0.83,0	0.0	0.0	0.0	0,0,0	-4.51e-03	-4.32e-03	-4.24e-03	83,89,96
	38.3	0.0	0.09	0.0	0.83,0	0.0	0.0	0.0	0,0,0				
931	0.0	0.11	0.28	0.13	83,83,96	0.0	0.0	0.0	0,0,0	-4.59e-03	-4.25e-03	-4.11e-03	83,89,96
	45.0	0.14	0.31	0.16	83,83,96	0.0	0.0	0.0	0,0,0				
932	0.0	0.05	0.08	0.06	83,84,96	0.0	0.0	0.0	0,0,0	2.66e-03	2.46e-03	2.38e-03	83,89,96
	43.8	0.04	0.07	0.05	83,84,96	0.0	0.0	0.0	0,0,0				
933	0.0	0.05	0.04	0.06	83,84,96	0.0	0.0	0.0	0,0,0	2.96e-03	2.74e-03	2.65e-03	83,89,96
	43.8	0.04	0.03	0.05	84,84,97	0.0	0.0	0.0	0,0,0				
934	0.0	0.0	0.01	0.0	0.82,0	0.0	0.0	0.0	0,0,0	-7.10e-04	-5.06e-04	-4.24e-04	83,89,96
	39.7	5.08e-03	0.02	4.31e-03	83,81,96	0.0	0.0	0.0	0,0,0				
935	0.0	0.0	0.06	0.0	0.83,0	0.0	0.0	0.0	0,0,0	-1.98e-03	-1.73e-03	-1.63e-03	83,89,96
	39.7	0.0	0.07	0.0	0.83,0	0.0	0.0	0.0	0,0,0				
936	0.0	0.0	0.04	0.0	0.83,0	0.0	0.0	0.0	0,0,0	5.49e-04	5.49e-04	5.49e-04	81,87,94
	38.3	0.0	0.03	0.0	0.83,0	0.0	0.0	0.0	0,0,0				
937	0.0	0.0	0.07	0.0	0.83,0	0.0	0.0	0.0	0,0,0	4.50e-04	4.50e-04	4.50e-04	81,87,94
	38.3	0.0	0.07	0.0	0.83,0	0.0	0.0	0.0	0,0,0				
938	0.0	0.0	0.07	0.0	0.83,0	0.0	0.0	0.0	0,0,0	1.56e-03	1.51e-03	1.48e-03	83,89,96
	38.3	0.0	0.07	0.0	0.83,0	0.0	0.0	0.0	0,0,0				
939	0.0	0.05	0.14	0.06	83,83,96	0.0	0.0	0.0	0,0,0	0.02	0.01	0.01	83,89,96
	43.7	0.02	0.11	0.03	83,83,96	0.0	0.0	0.0	0,0,0				
940	0.0	0.05	0.14	0.06	83,83,96	0.0	0.0	0.0	0,0,0	0.02	0.02	0.01	83,89,96
	43.7	0.02	0.10	0.03	83,83,96	0.0	0.0	0.0	0,0,0				
941	0.0	0.0	0.07	0.0	0.83,0	0.0	0.0	0.0	0,0,0	-3.89e-03	-3.65e-03	-3.55e-03	83,89,96
	38.3	0.0	0.07	0.0	0.83,0	0.0	0.0	0.0	0,0,0				
942	0.0	0.0	0.09	0.0	0.83,0	0.0	0.0	0.0	0,0,0	-2.10e-03	-2.00e-03	-1.96e-03	83,89,96
	38.3	0.0	0.09	0.0	0.83,0	0.0	0.0	0.0	0,0,0				
943	0.0	0.0	0.09	0.0	0.83,0	0.0	0.0</						

945	0.0	0.04	0.05	0.05	83,84,96	0.0	0.0	0.0	0,0,0	1.18e-03	1.06e-03	1.02e-03	83,89,96
	43.8	0.03	0.03	0.04	84,82,97	0.0	0.0	0.0	0,0,0				
946	0.0	0.04	0.05	0.05	83,84,96	0.0	0.0	0.0	0,0,0	1.57e-03	1.43e-03	1.38e-03	83,89,96
	43.8	0.03	0.03	0.03	84,82,97	0.0	0.0	0.0	0,0,0				
947	0.0	0.0	0.03	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-7.21e-04	-5.09e-04	-4.24e-04	83,89,96
	39.7	0.01	0.05	0.01	83,81,96	0.0	0.0	0.0	0,0,0				
948	0.0	0.0	0.08	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.88e-03	-1.63e-03	-1.53e-03	83,89,96
	39.7	0.0	0.10	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
949	0.0	0.0	0.05	0.0	0,83,0	0.0	0.0	0.0	0,0,0	6.79e-04	6.79e-04	6.79e-04	81,87,94
	38.3	0.0	0.05	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
950	0.0	0.0	0.07	0.0	0,83,0	0.0	0.0	0.0	0,0,0	3.46e-04	3.46e-04	3.46e-04	81,87,94
	38.3	0.0	0.07	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
951	0.0	0.0	0.08	0.0	0,83,0	0.0	0.0	0.0	0,0,0	1.46e-03	1.41e-03	1.39e-03	83,89,96
	38.3	0.0	0.08	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
952	0.0	0.03	0.10	0.03	83,83,96	0.0	0.0	0.0	0,0,0	0.01	0.01	0.01	83,89,96
	43.8	0.0	0.05	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
953	0.0	0.03	0.09	0.03	83,83,96	0.0	0.0	0.0	0,0,0	0.01	0.01	0.01	83,89,96
	43.8	0.0	0.04	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
954	0.0	0.0	0.08	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-3.81e-03	-3.58e-03	-3.48e-03	83,89,96
	38.3	0.0	0.08	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
955	0.0	0.0	0.10	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.97e-03	-1.88e-03	-1.85e-03	83,89,96
	38.3	0.0	0.10	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
956	0.0	0.0	0.10	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-4.23e-03	-4.06e-03	-4.00e-03	83,89,96
	38.3	0.0	0.10	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
957	0.0	0.03	0.02	0.04	84,82,97	0.0	0.0	0.0	0,0,0	3.01e-04	2.09e-04	1.71e-04	83,89,96
	43.8	7.36e-03	4.39e-03	9.41e-03	82,82,95	0.0	0.0	0.0	0,0,0				
958	0.0	0.03	0.02	0.03	84,84,97	0.0	0.0	0.0	0,0,0	6.65e-04	5.65e-04	5.25e-04	83,89,96
	43.8	9.76e-03	5.96e-03	0.01	84,84,97	0.0	0.0	0.0	0,0,0				
959	0.0	0.0	0.08	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.05e-03	-8.22e-04	-7.30e-04	83,89,96
	39.7	0.02	0.10	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
960	0.0	0.0	0.12	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.09e-03	-1.83e-03	-1.73e-03	83,89,96
	39.7	0.0	0.14	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
961	0.0	0.0	0.07	0.0	0,83,0	0.0	0.0	0.0	0,0,0	3.83e-04	3.83e-04	3.83e-04	81,87,94
	38.3	0.0	0.08	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
962	0.0	0.0	0.07	0.0	0,83,0	0.0	0.0	0.0	0,0,0	2.50e-04	2.50e-04	2.50e-04	81,87,94
	38.3	0.0	0.07	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
963	0.0	0.0	0.08	0.0	0,83,0	0.0	0.0	0.0	0,0,0	1.35e-03	1.32e-03	1.31e-03	83,89,96
	38.3	0.0	0.08	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
964	0.0	0.0	0.11	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-3.68e-03	-3.45e-03	-3.36e-03	83,89,96
	38.3	0.0	0.11	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
965	0.0	0.0	0.10	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.84e-03	-1.77e-03	-1.74e-03	83,89,96
	38.3	0.0	0.10	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
966	0.0	0.0	0.09	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-4.11e-03	-3.96e-03	-3.89e-03	83,89,96
	38.3	0.0	0.09	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
967	0.0	0.0	0.13	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.84e-03	-1.57e-03	-1.46e-03	83,89,96
	39.7	0.03	0.17	0.04	83,83,96	0.0	0.0	0.0	0,0,0				
968	0.0	0.0	0.18	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.72e-03	-2.42e-03	-2.29e-03	83,89,96
	39.7	0.02	0.22	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
969	0.0	0.0	9.77e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-4.00e-03	-3.65e-03	-3.51e-03	83,89,96
	39.3	4.32e-03	0.02	5.39e-03	83,83,96	0.0	0.0	0.0	0,0,0				
970	0.0	2.02e-05	6.46e-03	0.0	83,83,0	0.0	0.0	0.0	0,0,0	-3.37e-03	-2.99e-03	-2.84e-03	83,89,96
	39.3	0.0	5.97e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
971	0.0	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-4.68e-03	-4.29e-03	-4.13e-03	83,89,96
	40.2	6.26e-03	0.03	6.35e-03	84,83,97	0.0	0.0	0.0	0,0,0				
972	0.0	4.58e-04	0.01	6.11e-04	81,83,94	0.0	0.0	0.0	0,0,0	-3.34e-03	-2.95e-03	-2.79e-03	83,89,96
	40.2	4.85e-03	0.02	5.84e-03	83,83,96	0.0	0.0	0.0	0,0,0				
973	0.0	6.94e-04	0.02	3.47e-04	83,83,96	0.0	0.0	0.0	0,0,0	-4.29e-03	-3.92e-03	-3.77e-03	83,89,96
	39.3	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
974	0.0	0.0	9.17e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-3.34e-03	-2.96e-03	-2.80e-03	83,89,96
	39.3	0.0	0.01	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
975	0.0	5.83e-04	6.48e-03	7.77e-04	81,81,94	0.0	0.0	0.0	0,0,0	-1.74e-03	-1.55e-03	-1.48e-03	83,89,96
	53.5	5.79e-03	0.01	6.14e-03	83,84,96	0.0	0.0	0.0	0,0,0				
976	0.0	1.69e-03	0.03	2.00e-03	83,83,96	0.0	0.0	0.0	0,0,0	-1.91e-03	-1.61e-03	-1.49e-03	83,89,96
	39.7	1.28e-03	0.03	1.15e-03	83,83,96	0.0	0.0	0.0	0,0,0				
977	0.0	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.21e-03	-1.90e-03	-1.77e-03	83,89,96
	40.2	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
978	0.0	0.04	0.29	0.05	83,83,96	0.0	0.0	0.0	0,0,0	-5.58e-03	-5.03e-03	-4.81e-03	83,89,96
	43.8	0.10	0.36	0.12	83,83,96	0.0	0.0	0.0	0,0,0				
979	0.0	0.05	0.22	0.06	83,83,96	0.0	0.0	0.0	0,0,0	-4.25e-03	-3.80e-03	-3.62e-03	83,89,96
	43.8	0.08	0.26	0.09	83,83,96	0.0	0.0	0.0	0,0,0				
980	0.0	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.35e-03	-2.03e-03	-1.90e-03	83,89,96
	40.2	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
981	0.0	0.0	0.01	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-5.18e-04	-4.60e-04	-4.37e-04	83,89,96
	25.8	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
982	0.0	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.67e-03	-1.38e-03	-1.27e-03	83,89,96
	39.7	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
983	0.0	0.04	0.05	0.04	83,83,96	0.0	0.0	0.0	0,0,0	-2.14e-03	-1.93e-03	-1.85e-03	83,89,96
	43.8	0.01	7.46e-03	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
984	0.0	0.0	0.08	0.0	0,84,0	0.0	0.0	0.0	0,0,0	1.60e-04	1.58e-04	1.51e-04	84,93,97
	43.8	0.01	0.09	0.01	83,84,96	0.0	0.0	0.0	0,0,0				
985	0.0	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.44e-03	-2.12e-03	-1.99e-03	83,89,96
	40.2	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
986	0.0	0.07	0.61	0.08	83,83,96	0.17	0.17	0.0	83,89,0	-0.02	-0.02	-0.02	83,89,96
	46.6	0.0	0.42	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
987	0.0	0.04	0.42	0.05	83,83,96	0.0	0.0	0.0	0,0,0	-0.01	-0.01	-0.01	83,89,96
	47.7	0.0	0.35	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
988	0.0	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.60e-03	-1.44e-03	-1.38e-03	83,89,96
	39.7	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
989	0.0	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.51e-03	-1.24e-03	-1.13e-03	83,89,96
	39.7	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
990	0.0	0.02	0.25	0.02	83,83,96	0.0	0.0	0.0	0,0,0	-9.56e-03	-8.66e-03	-8.30e-03	83,89,96
	53.7	0.0	0.18	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
991	0.0	0.0	0.20	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-6.83e-03	-6.20e-03	-5.95e-03	83,89,96
	53.7	0.0	0.15	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
992	0.0	2.68e-03	0.03	2.70e-03	83,83,96	0.0	0.0	0.0	0,0,0	-2.66e-03	-2.32e-03	-2.19e-03	83,89,96
	40.2	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
993	0.0	0.07	0.43	0.08	83,83,96	0.0	0.0	0.0	0,0,0	-0.01	-9.14e-03	-8.77e-03	83,89,96
	43.8	0.13	0.50	0.15	83,83,96								

	43.8	0.02	0.06	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
996	0.0	0.0	0.12	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-7.40e-04	-6.33e-04	-5.89e-04	83,89,96
	43.8	0.0	0.13	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
997	0.0	0.06	0.07	0.07	83,83,96	0.0	0.0	0.0	0,0,0	-5.48e-03	-4.98e-03	-4.78e-03	83,89,96
	60.1	0.04	0.03	0.05	83,83,96	0.0	0.0	0.0	0,0,0				
998	0.0	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.72e-03	-1.53e-03	-1.46e-03	83,89,96
	39.7	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
999	0.0	1.83e-03	0.02	2.11e-03	83,83,96	0.0	0.0	0.0	0,0,0	-1.31e-03	-1.05e-03	-9.49e-04	83,89,96
	39.7	1.26e-03	0.02	1.07e-03	83,83,96	0.0	0.0	0.0	0,0,0				
1000	0.0	0.04	0.20	0.04	83,83,96	0.0	0.0	0.0	0,0,0	1.72e-03	1.58e-03	1.52e-03	83,89,96
	43.8	0.03	0.19	0.03	83,83,96	0.0	0.0	0.0	0,0,0				
1001	0.0	0.06	0.25	0.07	83,83,96	0.0	0.0	0.0	0,0,0	2.53e-03	2.32e-03	2.23e-03	83,89,96
	43.8	0.04	0.23	0.05	83,83,96	0.0	0.0	0.0	0,0,0				
1002	0.0	4.73e-03	0.02	5.60e-03	83,83,96	0.0	0.0	0.0	0,0,0	-3.03e-03	-2.66e-03	-2.52e-03	83,89,96
	40.2	5.94e-03	0.02	6.92e-03	83,83,96	0.0	0.0	0.0	0,0,0				
1003	0.0	0.08	0.09	0.10	83,83,96	0.0	0.0	0.0	0,0,0	-6.63e-03	-6.03e-03	-5.78e-03	83,89,96
	45.0	0.07	0.05	0.08	83,83,96	0.0	0.0	0.0	0,0,0				
1004	0.0	0.07	0.08	0.08	83,83,96	0.0	0.0	0.0	0,0,0	-2.62e-03	-2.37e-03	-2.27e-03	83,89,96
	40.1	0.07	0.08	0.08	83,83,96	0.0	0.0	0.0	0,0,0				
1005	0.0	0.07	0.06	0.08	83,83,96	0.0	0.0	0.0	0,0,0	1.30e-03	1.12e-03	1.06e-03	84,90,97
	51.7	0.07	0.07	0.08	83,83,96	0.0	0.0	0.0	0,0,0				
1006	0.0	0.0	0.08	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.35e-03	-2.11e-03	-2.01e-03	83,89,96
	43.8	0.04	0.13	0.05	83,83,96	0.0	0.0	0.0	0,0,0				
1007	0.0	0.0	0.14	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.76e-03	-1.56e-03	-1.47e-03	83,89,96
	43.8	0.01	0.15	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
1008	0.0	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.85e-03	-1.66e-03	-1.58e-03	83,89,96
	39.7	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1009	0.0	3.71e-03	0.02	4.19e-03	83,83,96	0.0	0.0	0.0	0,0,0	-1.09e-03	-8.51e-04	-7.55e-04	83,89,96
	39.7	1.29e-03	0.01	9.33e-04	83,83,96	0.0	0.0	0.0	0,0,0				
1010	0.0	0.0	0.30	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-6.94e-03	-6.30e-03	-6.04e-03	83,89,96
	46.8	0.0	0.25	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1011	0.0	0.0	0.29	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-6.46e-03	-5.87e-03	-5.64e-03	83,89,96
	47.7	0.0	0.24	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1012	0.0	0.0	0.18	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-9.45e-04	-8.30e-04	-7.84e-04	83,89,96
	43.8	0.03	0.21	0.03	83,83,96	0.0	0.0	0.0	0,0,0				
1013	0.0	0.0	0.19	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-6.76e-04	-5.78e-04	-5.39e-04	83,89,96
	43.8	0.02	0.21	0.03	83,83,96	0.0	0.0	0.0	0,0,0				
1014	0.0	0.04	0.05	0.05	83,83,96	0.0	0.0	0.0	0,0,0	4.67e-03	4.29e-03	4.13e-03	83,89,96
	39.6	0.02	0.01	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
1015	0.0	0.02	0.18	0.02	83,83,96	0.0	0.0	0.0	0,0,0	-4.32e-03	-3.89e-03	-3.72e-03	83,89,96
	43.8	0.05	0.20	0.05	83,83,96	0.0	0.0	0.0	0,0,0				
1016	0.0	7.50e-03	0.15	6.74e-03	83,83,96	0.0	0.0	0.0	0,0,0	-3.16e-03	-2.83e-03	-2.70e-03	83,89,96
	43.8	0.02	0.16	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
1017	0.0	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.05e-03	-8.50e-04	-8.03e-04	83,89,96
	39.7	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1018	0.0	0.0	0.01	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-9.89e-04	-7.67e-04	-6.79e-04	83,89,96
	39.7	0.0	0.01	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1019	0.0	0.03	0.19	0.04	83,83,96	0.0	0.0	0.0	0,0,0	2.38e-03	2.17e-03	2.09e-03	83,89,96
	43.7	0.01	0.17	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
1020	0.0	0.02	0.23	0.02	83,83,96	0.0	0.0	0.0	0,0,0	2.46e-03	2.24e-03	2.15e-03	83,89,96
	43.7	0.0	0.21	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1021	0.0	0.02	0.20	0.02	83,83,96	0.0	0.0	0.0	0,0,0	-3.45e-04	-2.89e-04	-2.67e-04	84,90,97
	43.8	0.0	0.17	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1022	0.0	0.03	0.25	0.03	83,83,96	0.0	0.0	0.0	0,0,0	2.34e-04	2.11e-04	2.02e-04	83,89,96
	43.8	0.0	0.21	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1023	0.0	0.02	0.02	0.02	83,83,96	0.0	0.0	0.0	0,0,0	7.47e-03	6.95e-03	6.74e-03	83,89,96
	52.6	0.03	0.02	0.03	83,83,96	0.0	0.0	0.0	0,0,0				
1024	0.0	0.02	0.23	0.02	83,83,96	0.0	0.0	0.0	0,0,0	-3.23e-03	-2.90e-03	-2.78e-03	83,89,96
	43.8	0.03	0.25	0.04	83,83,96	0.0	0.0	0.0	0,0,0				
1025	0.0	0.02	0.21	0.02	83,83,96	0.0	0.0	0.0	0,0,0	-2.87e-03	-2.57e-03	-2.46e-03	83,89,96
	43.8	0.03	0.23	0.04	83,83,96	0.0	0.0	0.0	0,0,0				
1026	0.0	0.01	0.03	0.01	83,84,96	0.0	0.0	0.0	0,0,0	4.61e-03	4.22e-03	4.06e-03	83,89,96
	35.4	0.05	0.08	0.05	83,83,96	0.0	0.0	0.0	0,0,0				
1027	0.0	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-9.76e-04	-8.56e-04	-8.07e-04	83,89,96
	39.7	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1028	0.0	0.0	0.01	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-9.62e-04	-7.49e-04	-6.64e-04	83,89,96
	39.7	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1029	0.0	0.0	0.07	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-7.03e-04	-5.82e-04	-5.44e-04	84,90,97
	46.9	0.0	0.12	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1030	0.0	0.0	0.07	0.0	0,84,0	0.0	0.0	0.0	0,0,0	-9.21e-04	-8.30e-04	-8.00e-04	84,90,97
	47.7	0.0	0.11	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1031	0.0	0.04	0.05	0.05	83,83,96	0.0	0.0	0.0	0,0,0	5.75e-03	5.24e-03	5.03e-03	83,89,96
	45.0	0.02	0.01	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
1032	0.0	0.02	0.02	0.02	83,83,96	0.0	0.0	0.0	0,0,0	5.42e-03	4.96e-03	4.78e-03	83,89,96
	39.6	0.01	7.88e-03	0.02	84,83,97	0.0	0.0	0.0	0,0,0				
1033	0.0	7.74e-03	0.18	5.74e-03	83,83,96	0.0	0.0	0.0	0,0,0	7.44e-04	7.00e-04	6.83e-04	83,89,96
	43.8	0.0	0.15	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1034	0.0	5.85e-03	0.20	2.55e-03	83,83,96	0.0	0.0	0.0	0,0,0	6.79e-04	6.44e-04	6.30e-04	83,89,96
	43.8	0.0	0.17	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1035	0.0	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.13e-03	-1.97e-03	-8.00e-04	83,89,96
	39.7	0.0	0.04	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1036	0.0	0.0	0.01	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-8.76e-04	-6.65e-04	-5.81e-04	83,89,96
	39.7	0.0	0.01	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1037	0.0	0.08	0.39	0.09	83,83,96	0.0	0.0	0.0	0,0,0	0.01	0.01	0.01	83,89,96
	43.7	0.0	0.31	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1038	0.0	0.08	0.39	0.09	83,83,96	0.0	0.0	0.0	0,0,0	0.01	0.01	0.01	83,89,96
	43.7	0.0	0.31	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1039	0.0	0.0	0.19	0.0	0,83,0	0.0	0.0	0.0	0,0,0	0.03	0.03	0.03	83,89,96
	70.8	0.11	0.33	0.12	83,83,96	0.0	0.0	0.0	0,0,0				
1040	0.0	0.0	0.13	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.51e-04	-1.96e-04	-1.76e-04	84,90,97
	43.8	0.0	0.11	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1041	0.0	0.0	0.14	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-3.47e-04	-2.85e-04	-2.61e-04	84,90,97
	43.8	0.0	0.12	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1042	0.0	0.0	0.05	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.87e-03	-1.64e-03	-1.54e-03	83,89,96
	39.7	0.0	0.05	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1043	0.0	0.0	0.01	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-6.82e-04	-4.84e-04	-4.05e-04	83,89,96
	39.7	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1044	0.0	0.05											

1046	0.0	0.0	0.05	0.0	0,83,0	0.0	0.0	0.0	0,0,0	0.02	0.02	0.02	83,89,96
	39.6	0.03	0.11	0.03	83,83,96	0.0	0.0	0.0	0,0,0				
1047	0.0	0.0	0.09	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-6.76e-04	-5.81e-04	-5.42e-04	84,90,97
	43.8	0.0	0.07	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1048	0.0	0.0	0.10	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-7.78e-04	-6.78e-04	-6.39e-04	84,90,97
	43.8	0.0	0.07	0.0	0,84,0	0.0	0.0	0.0	0,0,0				
1049	0.0	0.0	0.07	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.84e-03	-1.60e-03	-1.50e-03	83,89,96
	39.7	0.0	0.09	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1050	0.0	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-6.74e-04	-4.68e-04	-3.86e-04	83,89,96
	39.7	0.01	0.05	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
1051	0.0	0.03	0.07	0.04	83,83,96	0.0	0.0	0.0	0,0,0	0.02	0.02	0.02	83,89,96
	39.6	4.56e-03	8.91e-03	5.12e-03	84,82,97	0.0	0.0	0.0	0,0,0				
1052	0.0	0.0	0.11	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.03e-03	-1.77e-03	-1.66e-03	83,89,96
	39.7	0.02	0.14	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
1053	0.0	6.36e-04	0.07	8.49e-04	81,83,94	0.0	0.0	0.0	0,0,0	-9.56e-04	-7.40e-04	-6.53e-04	83,89,96
	39.7	0.03	0.10	0.04	83,83,96	0.0	0.0	0.0	0,0,0				
1054	0.0	0.0	0.18	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.77e-03	-2.45e-03	-2.32e-03	83,89,96
	39.7	0.06	0.24	0.07	83,83,96	0.0	0.0	0.0	0,0,0				
1055	0.0	0.02	0.13	0.02	83,83,96	0.0	0.0	0.0	0,0,0	-1.72e-03	-1.46e-03	-1.35e-03	83,89,96
	39.7	0.06	0.18	0.07	83,83,96	0.0	0.0	0.0	0,0,0				
1056	0.0	0.08	0.13	0.09	83,83,96	0.0	0.0	0.0	0,0,0	0.04	0.04	0.04	83,89,96
	111.3	0.0	0.02	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
	222.5	0.12	0.20	0.14	83,83,96	0.0	0.0	0.0	0,0,0				
1057	0.0	0.06	0.17	0.06	84,83,97	0.0	0.0	0.0	0,0,0	-0.03	-0.03	-0.03	83,89,96
	111.3	0.0	0.07	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
	222.5	0.01	0.12	0.0	84,83,0	0.0	0.0	0.0	0,0,0				
1058	0.0	0.0	0.12	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-6.37e-03	-5.66e-03	-5.38e-03	83,89,96
	40.2	0.0	0.10	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1059	0.0	0.0	0.05	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-6.68e-03	-5.92e-03	-5.63e-03	83,89,96
	40.2	0.0	0.04	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1060	0.0	0.0	0.05	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-6.58e-03	-5.82e-03	-5.52e-03	83,89,96
	40.2	0.0	0.05	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1061	0.0	6.14e-03	0.01	5.35e-03	84,81,97	0.0	0.0	0.0	0,0,0	-6.23e-03	-5.52e-03	-5.23e-03	83,89,96
	40.2	9.62e-03	0.02	8.36e-03	84,81,97	0.0	0.0	0.0	0,0,0				
1062	0.0	0.0	0.14	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-6.79e-03	-6.08e-03	-5.80e-03	83,89,96
	40.2	0.0	0.13	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1063	0.0	0.0	0.08	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-6.89e-03	-6.13e-03	-5.83e-03	83,89,96
	40.2	0.0	0.08	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1064	0.0	0.0	0.09	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-6.58e-03	-5.83e-03	-5.52e-03	83,89,96
	40.2	0.0	0.10	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1065	0.0	0.0	0.06	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-5.96e-03	-5.26e-03	-4.97e-03	83,89,96
	40.2	1.87e-03	0.07	0.0	84,81,0	0.0	0.0	0.0	0,0,0				
1066	0.0	0.02	0.04	0.01	84,81,97	0.0	0.0	0.0	0,0,0	-5.07e-03	-4.46e-03	-4.22e-03	83,89,96
	40.2	0.03	0.05	0.03	84,81,97	0.0	0.0	0.0	0,0,0				
1067	0.0	0.01	8.68e-03	0.02	83,84,96	0.0	0.0	0.0	0,0,0	-4.26e-03	-3.93e-03	-3.80e-03	83,89,96
	40.2	0.02	0.02	0.03	83,83,96	0.0	0.0	0.0	0,0,0				
1068	0.0	0.02	0.01	0.03	83,83,96	0.0	0.0	0.0	0,0,0	-3.54e-03	-3.26e-03	-3.15e-03	83,89,96
	40.2	0.03	0.02	0.03	83,83,96	0.0	0.0	0.0	0,0,0				
1069	0.0	0.03	0.02	0.03	83,83,96	0.0	0.0	0.0	0,0,0	-2.68e-03	-2.45e-03	-2.36e-03	83,89,96
	40.2	0.03	0.02	0.03	83,83,96	0.0	0.0	0.0	0,0,0				
1070	0.0	0.02	0.02	0.03	83,83,96	0.0	0.0	0.0	0,0,0	-1.87e-03	-1.68e-03	-1.61e-03	83,89,96
	40.2	0.02	0.01	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
1071	0.0	0.02	0.01	0.02	83,83,96	0.0	0.0	0.0	0,0,0	-1.30e-03	-1.14e-03	-1.08e-03	83,89,96
	40.2	9.02e-03	5.36e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
1072	0.0	0.01	0.02	0.01	83,83,96	0.0	0.0	0.0	0,0,0	-4.29e-03	-3.94e-03	-3.80e-03	83,89,96
	40.2	0.02	0.04	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
1073	0.0	0.02	0.03	0.03	83,83,96	0.0	0.0	0.0	0,0,0	-3.48e-03	-3.20e-03	-3.09e-03	83,89,96
	40.2	0.03	0.03	0.03	83,83,96	0.0	0.0	0.0	0,0,0				
1074	0.0	0.03	0.03	0.03	83,83,96	0.0	0.0	0.0	0,0,0	-2.55e-03	-2.34e-03	-2.25e-03	83,89,96
	40.2	0.02	0.03	0.03	83,83,96	0.0	0.0	0.0	0,0,0				
1075	0.0	0.02	0.03	0.03	83,83,96	0.0	0.0	0.0	0,0,0	-1.72e-03	-1.56e-03	-1.50e-03	83,89,96
	40.2	0.01	0.01	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
1076	0.0	0.01	0.02	0.02	83,83,96	0.0	0.0	0.0	0,0,0	-1.22e-03	-1.10e-03	-1.05e-03	83,89,96
	40.2	2.23e-03	1.27e-03	2.98e-03	81,81,94	0.0	0.0	0.0	0,0,0				
1077	0.0	0.0	0.16	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-8.77e-03	-7.99e-03	-7.67e-03	83,89,96
	46.8	0.0	0.10	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1078	0.0	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-8.13e-03	-7.42e-03	-7.13e-03	83,89,96
	46.9	0.02	0.09	0.03	83,83,96	0.0	0.0	0.0	0,0,0				
1079	0.0	0.03	0.04	0.04	83,83,96	0.0	0.0	0.0	0,0,0	-6.61e-03	-6.04e-03	-5.81e-03	83,89,96
	46.8	0.05	0.08	0.06	83,83,96	0.0	0.0	0.0	0,0,0				
1080	0.0	0.06	0.06	0.06	83,83,96	0.0	0.0	0.0	0,0,0	-4.23e-03	-3.87e-03	-3.73e-03	83,89,96
	46.8	0.07	0.08	0.08	83,83,96	0.0	0.0	0.0	0,0,0				
1081	0.0	0.07	0.07	0.08	83,83,96	0.0	0.0	0.0	0,0,0	-1.52e-03	-1.39e-03	-1.34e-03	84,90,97
	46.9	0.07	0.07	0.08	83,83,96	0.0	0.0	0.0	0,0,0				
1082	0.0	0.07	0.07	0.08	83,83,96	0.0	0.0	0.0	0,0,0	1.46e-03	1.32e-03	1.26e-03	83,89,96
	46.8	0.06	0.06	0.07	83,83,96	0.0	0.0	0.0	0,0,0				
1083	0.0	0.06	0.07	0.07	83,83,96	0.0	0.0	0.0	0,0,0	4.06e-03	3.69e-03	3.54e-03	83,89,96
	46.8	0.04	0.04	0.05	83,83,96	0.0	0.0	0.0	0,0,0				
1084	0.0	0.03	0.06	0.03	83,83,96	0.0	0.0	0.0	0,0,0	6.47e-04	6.27e-04	6.19e-04	83,89,96
	46.9	0.05	0.12	0.06	83,83,96	0.0	0.0	0.0	0,0,0				
1085	0.0	0.06	0.08	0.07	83,83,96	0.0	0.0	0.0	0,0,0	3.35e-03	3.09e-03	2.99e-03	83,89,96
	46.9	0.08	0.12	0.09	83,83,96	0.0	0.0	0.0	0,0,0				
1086	0.0	0.08	0.10	0.10	83,83,96	0.0	0.0	0.0	0,0,0	6.84e-03	6.28e-03	6.06e-03	83,89,96
	46.9	0.09	0.12	0.11	83,83,96	0.0	0.0	0.0	0,0,0				
1087	0.0	0.09	0.11	0.11	83,83,96	0.0	0.0	0.0	0,0,0	0.01	9.79e-03	9.43e-03	83,89,96
	46.9	0.09	0.11	0.11	83,83,96	0.0	0.0	0.0	0,0,0				
1088	0.0	0.09	0.11	0.11	83,83,96	0.0	0.0	0.0	0,0,0	0.01	0.01	0.01	83,89,96
	46.9	0.08	0.10	0.10	83,83,96	0.0	0.0	0.0	0,0,0				
1089	0.0	0.08	0.11	0.09	83,83,96	0.0	0.0	0.0	0,0,0	0.02	0.02	0.02	83,89,96
	46.9	0.06	0.08	0.07	83,83,96	0.0	0.0	0.0	0,0,0				
1090	0.0	0.06	0.10	0.07	83,83,96	0.0	0.0	0.0	0,0,0	0.02	0.02	0.02	83,89,96
	46.9	0.03	0.05	0.04	83,83,96	0.0	0.0	0.0	0,0,0				
1091	0.0	0.0	0.10	0.0	0,83,0	0.0	0.0	0.0	0,0,0	6.33e-03	5.76e-03	5.53e-03	83,89,96
	52.6	0.05	0.15	0.06	83,83,96	0.0	0.0	0.0	0,0,0				
1092	0.0	0.02	0.15	0.02	83,83,96	0.0	0.0	0.0	0,0,0	3.43e-03	3.14e-03	3.02e-03	83,89,96
	35.4	0.05	0.18	0.05	83,83,96	0.0	0.0	0.0	0,0,0				
1093	0.0	0.01	0.09	0.01	83,83,96	0.0	0.0	0.0	0,0,0	-0.01	-0.01	-9.91e-03	83,89,96
	53.7	0.0	0.08										

	53.7	0.07	0.07	0.08	83,83,96	0.0	0.0	0.0	0,0,0				
1096	0.0	0.07	0.08	0.08	83,83,96	0.0	0.0	0.0	0,0,0	-4.99e-04	-4.30e-04	-4.02e-04	83,89,96
	40.1	0.07	0.07	0.08	83,83,96	0.0	0.0	0.0	0,0,0				
1097	0.0	0.07	0.08	0.08	83,83,96	0.0	0.0	0.0	0,0,0	1.56e-03	1.45e-03	1.40e-03	83,89,96
	40.1	0.06	0.06	0.07	83,83,96	0.0	0.0	0.0	0,0,0				
1098	0.0	0.06	0.07	0.07	83,83,96	0.0	0.0	0.0	0,0,0	3.36e-03	3.09e-03	2.98e-03	83,89,96
	40.1	0.04	0.04	0.05	83,83,96	0.0	0.0	0.0	0,0,0				
1099	0.0	0.04	0.42	0.05	83,83,96	0.0	0.0	0.0	0,0,0	-0.02	-0.02	-0.02	83,89,96
	46.6	0.0	0.33	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1100	0.0	0.01	0.21	0.01	83,83,96	0.0	0.0	0.0	0,0,0	-0.03	-0.02	-0.02	83,89,96
	46.6	0.0	0.14	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1101	0.0	0.0	0.04	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-0.02	-0.02	-0.02	83,89,96
	46.6	0.02	0.09	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
1102	0.0	0.03	0.03	0.04	83,83,96	0.0	0.0	0.0	0,0,0	-0.02	-0.02	-0.02	83,89,96
	46.6	0.06	0.09	0.07	83,83,96	0.0	0.0	0.0	0,0,0				
1103	0.0	0.06	0.06	0.07	83,83,96	0.0	0.0	0.0	0,0,0	-0.02	-0.02	-0.02	83,89,96
	46.6	0.08	0.09	0.09	83,83,96	0.0	0.0	0.0	0,0,0				
1104	0.0	0.08	0.07	0.10	83,83,96	0.0	0.0	0.0	0,0,0	-0.02	-0.02	-0.02	83,89,96
	46.6	0.09	0.09	0.11	83,83,96	0.0	0.0	0.0	0,0,0				
1105	0.0	0.09	0.08	0.11	83,83,96	0.0	0.0	0.0	0,0,0	-0.01	-0.01	-0.01	83,89,96
	46.6	0.09	0.08	0.11	83,83,96	0.0	0.0	0.0	0,0,0				
1106	0.0	0.10	0.08	0.11	83,83,96	0.0	0.0	0.0	0,0,0	-0.01	-9.34e-03	-8.97e-03	83,89,96
	46.6	0.09	0.06	0.10	83,83,96	0.0	0.0	0.0	0,0,0				
1107	0.0	0.04	0.02	0.04	83,83,96	0.0	0.0	0.0	0,0,0	1.93e-03	1.65e-03	1.53e-03	83,89,96
	47.7	0.06	0.03	0.07	83,83,96	0.0	0.0	0.0	0,0,0				
1108	0.0	0.06	0.04	0.07	83,83,96	0.0	0.0	0.0	0,0,0	4.35e-03	3.87e-03	3.67e-03	83,89,96
	47.7	0.08	0.04	0.09	83,83,96	0.0	0.0	0.0	0,0,0				
1109	0.0	0.08	0.05	0.09	83,83,96	0.0	0.0	0.0	0,0,0	7.51e-03	6.78e-03	6.49e-03	83,89,96
	47.7	0.09	0.05	0.10	83,83,96	0.0	0.0	0.0	0,0,0				
1110	0.0	0.09	0.05	0.11	83,83,96	0.0	0.0	0.0	0,0,0	0.01	0.01	9.65e-03	83,89,96
	47.7	0.09	0.05	0.11	83,83,96	0.0	0.0	0.0	0,0,0				
1111	0.0	0.09	0.05	0.11	83,83,96	0.0	0.0	0.0	0,0,0	0.01	0.01	0.01	83,89,96
	47.7	0.08	0.05	0.10	83,83,96	0.0	0.0	0.0	0,0,0				
1112	0.0	0.08	0.05	0.10	83,83,96	0.0	0.0	0.0	0,0,0	0.02	0.02	0.02	83,89,96
	47.7	0.07	0.04	0.08	83,83,96	0.0	0.0	0.0	0,0,0				
1113	0.0	0.07	0.04	0.08	83,83,96	0.0	0.0	0.0	0,0,0	0.02	0.02	0.02	83,89,96
	47.7	0.05	0.03	0.06	83,83,96	0.0	0.0	0.0	0,0,0				
1114	0.0	0.04	0.02	0.05	84,83,97	0.0	0.0	0.0	0,0,0	0.02	0.02	0.02	83,89,96
	47.7	0.02	0.01	0.03	84,84,97	0.0	0.0	0.0	0,0,0				
1115	0.0	0.01	7.16e-03	0.02	84,84,97	0.0	0.0	0.0	0,0,0	0.02	0.02	0.02	83,89,96
	47.7	0.04	0.02	0.04	83,83,96	0.0	0.0	0.0	0,0,0				
1116	0.0	0.03	0.09	0.03	83,83,96	0.0	0.0	0.0	0,0,0	0.02	0.02	0.02	83,89,96
	47.7	0.05	0.12	0.06	83,83,96	0.0	0.0	0.0	0,0,0				
1117	0.0	0.04	0.04	0.04	83,84,96	0.0	0.0	0.0	0,0,0	-8.46e-03	-7.84e-03	-7.60e-03	83,89,96
	47.7	4.68e-03	4.13e-03	5.44e-03	83,82,96	0.0	0.0	0.0	0,0,0				
1118	0.0	0.01	9.09e-03	0.02	83,83,96	0.0	0.0	0.0	0,0,0	-8.35e-03	-7.73e-03	-7.48e-03	83,89,96
	47.7	0.03	0.02	0.04	83,83,96	0.0	0.0	0.0	0,0,0				
1119	0.0	0.04	0.02	0.05	83,83,96	0.0	0.0	0.0	0,0,0	-6.79e-03	-6.28e-03	-6.08e-03	83,89,96
	47.7	0.06	0.03	0.07	83,83,96	0.0	0.0	0.0	0,0,0				
1120	0.0	0.06	0.03	0.07	83,83,96	0.0	0.0	0.0	0,0,0	-4.48e-03	-4.14e-03	-4.01e-03	83,89,96
	47.7	0.07	0.04	0.08	83,83,96	0.0	0.0	0.0	0,0,0				
1121	0.0	0.07	0.04	0.08	83,83,96	0.0	0.0	0.0	0,0,0	-1.83e-03	-1.66e-03	-1.61e-03	84,90,97
	47.7	0.07	0.04	0.09	83,83,96	0.0	0.0	0.0	0,0,0				
1122	0.0	0.07	0.04	0.09	83,83,96	0.0	0.0	0.0	0,0,0	1.12e-03	1.06e-03	1.04e-03	83,89,96
	47.7	0.07	0.04	0.08	83,83,96	0.0	0.0	0.0	0,0,0				
1123	0.0	0.07	0.04	0.08	83,83,96	0.0	0.0	0.0	0,0,0	3.79e-03	3.54e-03	3.44e-03	83,89,96
	47.7	0.06	0.03	0.07	83,83,96	0.0	0.0	0.0	0,0,0				
1124	0.0	0.05	0.03	0.06	83,83,96	0.0	0.0	0.0	0,0,0	5.94e-03	5.54e-03	5.37e-03	83,89,96
	47.7	0.04	0.02	0.04	83,83,96	0.0	0.0	0.0	0,0,0				
1125	0.0	0.03	0.02	0.04	83,83,96	0.0	0.0	0.0	0,0,0	7.29e-03	6.79e-03	6.59e-03	83,89,96
	47.7	0.02	0.01	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
1126	0.0	0.01	6.24e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0	6.63e-03	6.17e-03	5.99e-03	83,89,96
	47.7	0.04	0.02	0.05	83,83,96	0.0	0.0	0.0	0,0,0				
1127	0.0	0.07	0.29	0.08	83,83,96	0.0	0.0	0.0	0,0,0	-0.02	-0.02	-0.02	83,89,96
	47.7	0.0	0.21	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1128	0.0	0.04	0.11	0.05	83,83,96	0.0	0.0	0.0	0,0,0	-0.02	-0.02	-0.02	83,89,96
	47.7	0.0	0.04	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1129	0.0	9.50e-03	5.78e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0	-0.03	-0.02	-0.02	83,89,96
	47.7	0.03	0.03	0.04	84,83,97	0.0	0.0	0.0	0,0,0				
1130	0.0	0.03	0.02	0.04	83,83,96	0.0	0.0	0.0	0,0,0	-0.02	-0.02	-0.02	83,89,96
	47.7	0.06	0.04	0.07	83,83,96	0.0	0.0	0.0	0,0,0				
1131	0.0	0.06	0.03	0.07	83,83,96	0.0	0.0	0.0	0,0,0	-0.02	-0.02	-0.02	83,89,96
	47.7	0.08	0.04	0.09	83,83,96	0.0	0.0	0.0	0,0,0				
1132	0.0	0.08	0.04	0.09	83,83,96	0.0	0.0	0.0	0,0,0	-0.02	-0.02	-0.02	83,89,96
	47.7	0.09	0.05	0.10	83,83,96	0.0	0.0	0.0	0,0,0				
1133	0.0	0.09	0.05	0.10	83,83,96	0.0	0.0	0.0	0,0,0	-0.01	-0.01	-0.01	83,89,96
	47.7	0.09	0.05	0.10	83,83,96	0.0	0.0	0.0	0,0,0				
1134	0.0	0.09	0.05	0.10	83,83,96	0.0	0.0	0.0	0,0,0	-0.01	-0.01	-9.57e-03	83,89,96
	47.7	0.08	0.05	0.09	83,83,96	0.0	0.0	0.0	0,0,0				
1135	0.0	0.08	0.05	0.09	83,83,96	0.0	0.0	0.0	0,0,0	-7.95e-03	-7.09e-03	-6.75e-03	83,89,96
	47.7	0.06	0.04	0.07	83,83,96	0.0	0.0	0.0	0,0,0				
1136	0.0	0.06	0.04	0.07	83,83,96	0.0	0.0	0.0	0,0,0	-5.42e-03	-4.80e-03	-4.55e-03	83,89,96
	47.7	0.04	0.03	0.05	83,83,96	0.0	0.0	0.0	0,0,0				
1137	0.0	0.07	0.04	0.09	83,83,96	0.0	0.0	0.0	0,0,0	7.19e-04	7.09e-04	7.00e-04	82,91,95
	51.7	0.07	0.04	0.08	83,83,96	0.0	0.0	0.0	0,0,0				
1138	0.0	0.07	0.04	0.08	83,83,96	0.0	0.0	0.0	0,0,0	3.65e-03	3.45e-03	3.37e-03	83,89,96
	51.7	0.05	0.03	0.06	83,83,96	0.0	0.0	0.0	0,0,0				
1139	0.0	0.05	0.03	0.06	83,83,96	0.0	0.0	0.0	0,0,0	5.97e-03	5.60e-03	5.45e-03	83,89,96
	51.7	0.03	0.02	0.04	83,83,96	0.0	0.0	0.0	0,0,0				
1140	0.0	0.02	0.01	0.03	83,83,96	0.0	0.0	0.0	0,0,0	7.44e-03	7.00e-03	6.83e-03	83,89,96
	51.7	0.03	0.02	0.03	83,83,96	0.0	0.0	0.0	0,0,0				
1141	0.0	0.02	0.03	0.03	83,82,96	0.0	0.0	0.0	0,0,0	5.87e-03	5.51e-03	5.36e-03	83,89,96
	51.7	0.06	0.08	0.07	83,84,96	0.0	0.0	0.0	0,0,0				
1142	0.0	0.02	9.99e-03	0.02	83,83,96	0.0	0.0	0.0	0,0,0	-0.01	-0.01	-9.81e-03	83,89,96
	53.7	0.03	0.02	0.03	83,83,96	0.0	0.0	0.0	0,0,0				
1143	0.0	0.04	0.02	0.04	83,83,96	0.0	0.0	0.0	0,0,0	-9.26e-03	-8.54e-03	-8.25e-03	83,89,96
	53.7	0.06	0.03	0.07	83,83,96	0.0	0.0	0.0	0,0,0				
1144	0.0	0.06	0.03	0.07	83,83,96	0.0	0.0	0.0	0,0,0	-6.35e-03	-5.84e-03	-5.63e-03	

1146	0.0	0.0	0.08	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.51e-03	-1.51e-03	-1.51e-03	81,87,94
	40.2	0.0	0.07	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1147	0.0	0.0	0.09	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-7.99e-04	-7.99e-04	-7.99e-04	81,87,94
	40.2	0.0	0.08	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1148	0.0	0.0	0.08	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-8.68e-04	-8.68e-04	-8.68e-04	81,87,94
	40.2	0.0	0.07	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1149	0.0	0.0	0.10	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-5.91e-04	-5.91e-04	-5.91e-04	81,87,94
	40.2	0.0	0.10	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1150	0.0	0.0	0.10	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.54e-04	-2.54e-04	-2.54e-04	81,87,94
	40.2	0.0	0.11	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1151	0.0	0.0	0.12	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.65e-03	-1.65e-03	-1.65e-03	81,87,94
	40.2	0.0	0.12	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
1152	0.0	0.0	0.10	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.40e-03	-1.40e-03	-1.40e-03	81,87,94
	40.2	0.0	0.11	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
1153	0.0	0.04	0.14	0.05	83,83,96	0.0	0.0	0.0	0,0,0	-0.02	-0.02	-0.01	83,89,96
	47.7	0.0	0.08	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1154	0.0	0.01	6.99e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0	-0.02	-0.02	-0.01	83,89,96
	47.7	0.02	0.03	0.03	84,84,97	0.0	0.0	0.0	0,0,0				
1155	0.0	0.03	0.02	0.03	84,84,97	0.0	0.0	0.0	0,0,0	-0.02	-0.01	-0.01	83,89,96
	47.7	0.05	0.04	0.06	83,83,96	0.0	0.0	0.0	0,0,0				
1156	0.0	0.05	0.03	0.06	83,83,96	0.0	0.0	0.0	0,0,0	-0.01	-0.01	-0.01	83,89,96
	47.7	0.06	0.04	0.08	83,83,96	0.0	0.0	0.0	0,0,0				
1157	0.0	0.07	0.04	0.08	83,83,96	0.0	0.0	0.0	0,0,0	-0.01	-9.89e-03	-9.55e-03	83,89,96
	47.7	0.07	0.04	0.09	83,83,96	0.0	0.0	0.0	0,0,0				
1158	0.0	0.07	0.04	0.09	83,83,96	0.0	0.0	0.0	0,0,0	-7.77e-03	-7.12e-03	-6.87e-03	83,89,96
	47.7	0.07	0.04	0.09	83,83,96	0.0	0.0	0.0	0,0,0				
1159	0.0	0.07	0.04	0.09	83,83,96	0.0	0.0	0.0	0,0,0	-4.82e-03	-4.39e-03	-4.21e-03	83,89,96
	47.7	0.06	0.04	0.08	83,83,96	0.0	0.0	0.0	0,0,0				
1160	0.0	0.06	0.04	0.08	83,83,96	0.0	0.0	0.0	0,0,0	-2.22e-03	-1.98e-03	-1.88e-03	83,89,96
	47.7	0.05	0.03	0.06	83,83,96	0.0	0.0	0.0	0,0,0				
1161	0.0	0.04	0.03	0.05	83,83,96	0.0	0.0	0.0	0,0,0	5.20e-04	4.54e-04	3.89e-04	82,91,95
	47.7	0.03	0.01	0.03	83,83,96	0.0	0.0	0.0	0,0,0				
1162	0.0	0.02	0.01	0.02	83,83,96	0.0	0.0	0.0	0,0,0	8.71e-04	9.35e-04	8.77e-04	82,91,95
	47.7	0.02	0.01	0.02	84,84,97	0.0	0.0	0.0	0,0,0				
1163	0.0	0.03	0.05	0.03	83,84,96	0.0	0.0	0.0	0,0,0	-7.76e-03	-7.24e-03	-7.03e-03	83,89,96
	47.7	4.91e-03	0.02	4.15e-03	83,84,96	0.0	0.0	0.0	0,0,0				
1164	0.0	0.01	8.32e-03	0.02	83,83,96	0.0	0.0	0.0	0,0,0	-7.41e-03	-6.91e-03	-6.71e-03	83,89,96
	47.7	0.04	0.03	0.04	83,84,96	0.0	0.0	0.0	0,0,0				
1165	0.0	0.04	0.02	0.05	83,83,96	0.0	0.0	0.0	0,0,0	-5.82e-03	-5.44e-03	-5.29e-03	83,89,96
	47.7	0.05	0.03	0.07	83,84,96	0.0	0.0	0.0	0,0,0				
1166	0.0	0.06	0.03	0.07	83,83,96	0.0	0.0	0.0	0,0,0	-3.50e-03	-3.29e-03	-3.21e-03	83,89,96
	47.7	0.07	0.04	0.08	83,83,96	0.0	0.0	0.0	0,0,0				
1167	0.0	0.07	0.04	0.08	83,83,96	0.0	0.0	0.0	0,0,0	-8.89e-04	-8.51e-04	-8.43e-04	84,90,97
	47.7	0.07	0.04	0.08	83,83,96	0.0	0.0	0.0	0,0,0				
1168	0.0	0.07	0.04	0.08	83,83,96	0.0	0.0	0.0	0,0,0	1.99e-03	1.82e-03	1.74e-03	83,89,96
	47.7	0.06	0.04	0.08	83,83,96	0.0	0.0	0.0	0,0,0				
1169	0.0	0.06	0.04	0.07	83,83,96	0.0	0.0	0.0	0,0,0	4.54e-03	4.19e-03	4.04e-03	83,89,96
	47.7	0.05	0.03	0.06	83,83,96	0.0	0.0	0.0	0,0,0				
1170	0.0	0.05	0.03	0.06	83,83,96	0.0	0.0	0.0	0,0,0	6.53e-03	6.04e-03	5.84e-03	83,89,96
	47.7	0.03	0.02	0.04	83,83,96	0.0	0.0	0.0	0,0,0				
1171	0.0	0.02	0.01	0.03	83,83,96	0.0	0.0	0.0	0,0,0	7.74e-03	7.16e-03	6.92e-03	83,89,96
	47.7	0.02	0.01	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
1172	0.0	0.01	0.01	0.02	83,82,96	0.0	0.0	0.0	0,0,0	6.84e-03	6.33e-03	6.13e-03	83,89,96
	47.7	0.04	0.06	0.05	83,84,96	0.0	0.0	0.0	0,0,0				
1173	0.0	0.04	0.02	0.04	83,83,96	0.0	0.0	0.0	0,0,0	1.65e-03	1.32e-03	1.19e-03	83,89,96
	47.7	0.06	0.04	0.07	83,83,96	0.0	0.0	0.0	0,0,0				
1174	0.0	0.06	0.04	0.07	83,83,96	0.0	0.0	0.0	0,0,0	4.12e-03	3.58e-03	3.36e-03	83,89,96
	47.7	0.08	0.04	0.09	83,83,96	0.0	0.0	0.0	0,0,0				
1175	0.0	0.08	0.05	0.09	83,83,96	0.0	0.0	0.0	0,0,0	7.30e-03	6.51e-03	6.19e-03	83,89,96
	47.7	0.09	0.05	0.10	83,83,96	0.0	0.0	0.0	0,0,0				
1176	0.0	0.09	0.05	0.11	83,83,96	0.0	0.0	0.0	0,0,0	0.01	9.78e-03	9.35e-03	83,89,96
	47.7	0.09	0.05	0.11	83,83,96	0.0	0.0	0.0	0,0,0				
1177	0.0	0.09	0.05	0.11	83,83,96	0.0	0.0	0.0	0,0,0	0.01	0.01	0.01	83,89,96
	47.7	0.08	0.05	0.10	83,83,96	0.0	0.0	0.0	0,0,0				
1178	0.0	0.08	0.05	0.10	83,83,96	0.0	0.0	0.0	0,0,0	0.02	0.02	0.02	83,89,96
	47.7	0.07	0.04	0.08	83,83,96	0.0	0.0	0.0	0,0,0				
1179	0.0	0.06	0.04	0.08	83,83,96	0.0	0.0	0.0	0,0,0	0.02	0.02	0.02	83,89,96
	47.7	0.05	0.03	0.06	83,83,96	0.0	0.0	0.0	0,0,0				
1180	0.0	0.04	0.02	0.05	84,83,97	0.0	0.0	0.0	0,0,0	0.02	0.02	0.02	83,89,96
	47.7	0.02	0.01	0.02	84,84,97	0.0	0.0	0.0	0,0,0				
1181	0.0	9.48e-03	5.67e-03	0.01	82,82,95	0.0	0.0	0.0	0,0,0	0.02	0.02	0.02	83,89,96
	47.7	0.04	0.02	0.05	83,83,96	0.0	0.0	0.0	0,0,0				
1182	0.0	0.03	0.10	0.03	83,83,96	0.0	0.0	0.0	0,0,0	0.02	0.02	0.02	83,89,96
	47.7	0.05	0.14	0.06	83,83,96	0.0	0.0	0.0	0,0,0				
1183	0.0	0.01	0.25	0.02	83,83,96	0.0	0.0	0.0	0,0,0	-0.02	-0.02	-0.01	83,89,96
	47.7	0.0	0.17	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1184	0.0	0.0	0.08	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-0.02	-0.01	-0.01	83,89,96
	47.7	0.0	0.09	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1185	0.0	0.02	0.03	0.02	83,83,96	0.0	0.0	0.0	0,0,0	-0.02	-0.01	-0.01	83,89,96
	47.7	0.05	0.09	0.05	83,83,96	0.0	0.0	0.0	0,0,0				
1186	0.0	0.05	0.05	0.06	83,83,96	0.0	0.0	0.0	0,0,0	-0.01	-0.01	-0.01	83,89,96
	47.7	0.07	0.09	0.08	83,83,96	0.0	0.0	0.0	0,0,0				
1187	0.0	0.07	0.07	0.08	83,83,96	0.0	0.0	0.0	0,0,0	-0.01	-9.66e-03	-9.34e-03	83,89,96
	47.7	0.08	0.08	0.09	83,83,96	0.0	0.0	0.0	0,0,0				
1188	0.0	0.08	0.07	0.09	83,83,96	0.0	0.0	0.0	0,0,0	-7.12e-03	-6.60e-03	-6.40e-03	83,89,96
	47.7	0.08	0.07	0.09	83,83,96	0.0	0.0	0.0	0,0,0				
1189	0.0	0.08	0.08	0.09	83,83,96	0.0	0.0	0.0	0,0,0	-3.81e-03	-3.58e-03	-3.48e-03	83,89,96
	47.7	0.07	0.06	0.08	83,83,96	0.0	0.0	0.0	0,0,0				
1190	0.0	0.06	0.07	0.08	83,83,96	0.0	0.0	0.0	0,0,0	-9.53e-04	-9.52e-04	-9.51e-04	83,89,96
	47.7	0.04	0.03	0.05	83,83,96	0.0	0.0	0.0	0,0,0				
1191	0.0	0.04	0.05	0.05	83,83,96	0.0	0.0	0.0	0,0,0	1.23e-03	1.04e-03	9.78e-04	84,90,97
	47.7	0.01	6.68e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
1192	0.0	0.0	0.04	0.0	0,83,0	0.0	0.0	0.0	0,0,0	1.35e-03	1.18e-03	1.13e-03	84,90,97
	47.7	0.01	0.06	0.01	83,84,96	0.0	0.0	0.0	0,0,0				
1193	0.0	0.0	0.15	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-8.30e-03	-7.58e-03	-7.29e-03	83,89,96
	47.7	0.0	0.09	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1194	0.0	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-7.59e-03	-6.96e-03	-6.71e-03	83,89,96
	47.7	0.03	0.08	0.03	83,83,96	0.0	0.0	0.0					

	47.7	0.07	0.08	0.08	83,83,96	0.0	0.0	0.0	0,0,0				
1197	0.0	0.07	0.07	0.08	83,83,96	0.0	0.0	0.0	0,0,0	-5.42e-04	-5.69e-04	-5.55e-04	84,93,97
	47.7	0.07	0.07	0.08	83,83,96	0.0	0.0	0.0	0,0,0				
1198	0.0	0.07	0.07	0.08	83,83,96	0.0	0.0	0.0	0,0,0	2.57e-03	2.28e-03	2.16e-03	83,89,96
	47.7	0.06	0.05	0.07	83,83,96	0.0	0.0	0.0	0,0,0				
1199	0.0	0.06	0.06	0.07	83,83,96	0.0	0.0	0.0	0,0,0	5.18e-03	4.67e-03	4.46e-03	83,89,96
	47.7	0.04	0.03	0.05	83,83,96	0.0	0.0	0.0	0,0,0				
1200	0.0	0.04	0.05	0.04	83,83,96	0.0	0.0	0.0	0,0,0	7.03e-03	6.36e-03	6.09e-03	83,89,96
	47.7	9.82e-03	5.79e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0				
1201	0.0	0.0	0.04	0.0	83,83,96	0.0	0.0	0.0	0,0,0	7.62e-03	6.91e-03	6.63e-03	83,89,96
	47.7	0.03	0.08	0.04	83,83,96	0.0	0.0	0.0	0,0,0				
1202	0.0	0.0	0.16	0.0	83,83,96	0.0	0.0	0.0	0,0,0	6.05e-03	5.48e-03	5.25e-03	83,89,96
	47.7	0.04	0.21	0.04	83,83,96	0.0	0.0	0.0	0,0,0				
1203	0.0	0.03	0.05	0.03	83,83,96	0.0	0.0	0.0	0,0,0	2.92e-04	2.34e-04	-2.12e-04	83,89,96
	47.7	0.05	0.11	0.06	83,83,96	0.0	0.0	0.0	0,0,0				
1204	0.0	0.06	0.08	0.07	83,83,96	0.0	0.0	0.0	0,0,0	3.04e-03	2.72e-03	2.59e-03	83,89,96
	47.7	0.08	0.11	0.09	83,83,96	0.0	0.0	0.0	0,0,0				
1205	0.0	0.08	0.09	0.10	83,83,96	0.0	0.0	0.0	0,0,0	6.65e-03	6.00e-03	5.75e-03	83,89,96
	47.7	0.09	0.11	0.11	83,83,96	0.0	0.0	0.0	0,0,0				
1206	0.0	0.09	0.10	0.11	83,83,96	0.0	0.0	0.0	0,0,0	0.01	9.64e-03	9.24e-03	83,89,96
	47.7	0.09	0.10	0.11	83,83,96	0.0	0.0	0.0	0,0,0				
1207	0.0	0.09	0.11	0.11	83,83,96	0.0	0.0	0.0	0,0,0	0.01	0.01	0.01	83,89,96
	47.7	0.08	0.09	0.10	83,83,96	0.0	0.0	0.0	0,0,0				
1208	0.0	0.08	0.10	0.10	83,83,96	0.0	0.0	0.0	0,0,0	0.02	0.02	0.02	83,89,96
	47.7	0.06	0.07	0.07	83,83,96	0.0	0.0	0.0	0,0,0				
1209	0.0	0.06	0.09	0.07	83,83,96	0.0	0.0	0.0	0,0,0	0.02	0.02	0.02	83,89,96
	47.7	0.03	0.04	0.04	83,83,96	0.0	0.0	0.0	0,0,0				
1210	0.0	0.02	0.08	0.03	83,83,96	0.0	0.0	0.0	0,0,0	0.02	0.02	0.02	83,89,96
	47.7	1.95e-03	0.03	0.0	83,83,96	0.0	0.0	0.0	0,0,0				
1211	0.0	0.0	0.11	0.0	83,83,96	0.0	0.0	0.0	0,0,0	0.02	0.02	0.02	83,89,96
	47.7	0.04	0.20	0.05	83,83,96	0.0	0.0	0.0	0,0,0				
1212	0.0	0.0	0.29	0.0	83,83,96	0.0	0.0	0.0	0,0,0	0.02	0.02	0.02	83,89,96
	47.7	0.08	0.39	0.09	83,83,96	0.0	0.0	0.0	0,0,0				
1213	0.0	0.07	0.04	0.08	83,83,96	0.0	0.0	0.0	0,0,0	4.43e-03	4.04e-03	3.89e-03	84,90,97
	51.7	0.06	0.03	0.07	83,83,96	0.0	0.0	0.0	0,0,0				
1214	0.0	0.06	0.03	0.07	83,83,96	0.0	0.0	0.0	0,0,0	7.22e-03	6.64e-03	6.41e-03	83,89,96
	51.7	0.04	0.02	0.05	83,83,96	0.0	0.0	0.0	0,0,0				
1215	0.0	0.04	0.02	0.05	83,83,96	0.0	0.0	0.0	0,0,0	9.16e-03	8.46e-03	8.18e-03	83,89,96
	51.7	0.02	0.01	0.02	83,83,96	0.0	0.0	0.0	0,0,0				
1216	0.0	8.58e-03	5.17e-03	0.01	83,83,96	0.0	0.0	0.0	0,0,0	9.22e-03	8.53e-03	8.27e-03	83,89,96
	51.7	0.04	0.03	0.05	83,84,96	0.0	0.0	0.0	0,0,0				
1217	0.0	0.03	0.10	0.03	83,84,96	0.0	0.0	0.0	0,0,0	7.70e-03	7.15e-03	6.93e-03	83,89,96
	51.7	0.07	0.15	0.08	83,84,96	0.0	0.0	0.0	0,0,0				
1218	0.0	0.07	0.07	0.08	83,83,96	0.0	0.0	0.0	0,0,0	4.64e-03	4.19e-03	4.00e-03	83,89,96
	51.7	0.06	0.05	0.07	83,83,96	0.0	0.0	0.0	0,0,0				
1219	0.0	0.06	0.06	0.07	83,83,96	0.0	0.0	0.0	0,0,0	7.71e-03	6.99e-03	6.70e-03	83,89,96
	51.7	0.04	0.02	0.05	83,83,96	0.0	0.0	0.0	0,0,0				
1220	0.0	0.04	0.05	0.04	83,83,96	0.0	0.0	0.0	0,0,0	9.73e-03	8.84e-03	8.48e-03	83,89,96
	51.7	5.27e-03	3.23e-03	6.40e-03	83,83,96	0.0	0.0	0.0	0,0,0				
1221	0.0	0.0	0.04	0.0	83,84,96	0.0	0.0	0.0	0,0,0	0.01	9.17e-03	8.80e-03	83,89,96
	51.7	0.04	0.12	0.05	83,83,96	0.0	0.0	0.0	0,0,0				
1222	0.0	0.0	0.21	0.0	83,83,96	0.0	0.0	0.0	0,0,0	7.64e-03	6.95e-03	6.67e-03	83,89,96
	51.7	0.05	0.27	0.06	83,83,96	0.0	0.0	0.0	0,0,0				
1223	0.0	9.38e-03	5.75e-03	9.83e-03	83,83,96	0.0	0.0	0.0	0,0,0	-7.18e-03	-6.71e-03	-6.53e-03	83,89,96
	53.7	0.03	0.03	0.04	83,84,96	0.0	0.0	0.0	0,0,0				
1224	0.0	0.04	0.02	0.04	83,83,96	0.0	0.0	0.0	0,0,0	-5.24e-03	-4.93e-03	-4.81e-03	83,89,96
	53.7	0.06	0.04	0.07	83,84,96	0.0	0.0	0.0	0,0,0				
1225	0.0	0.06	0.03	0.07	83,83,96	0.0	0.0	0.0	0,0,0	-2.24e-03	-2.16e-03	-2.12e-03	83,89,96
	53.7	0.07	0.04	0.08	83,83,96	0.0	0.0	0.0	0,0,0				
1226	0.0	0.0	0.06	0.0	83,83,96	0.0	0.0	0.0	0,0,0	-7.31e-03	-6.67e-03	-6.41e-03	83,89,96
	53.7	0.01	0.09	9.68e-03	84,83,97	0.0	0.0	0.0	0,0,0				
1227	0.0	0.03	0.03	0.03	83,83,96	0.0	0.0	0.0	0,0,0	-5.71e-03	-5.24e-03	-5.05e-03	83,89,96
	53.7	0.05	0.08	0.06	83,83,96	0.0	0.0	0.0	0,0,0				
1228	0.0	0.06	0.06	0.06	83,83,96	0.0	0.0	0.0	0,0,0	-2.59e-03	-2.41e-03	-2.33e-03	83,89,96
	53.7	0.07	0.08	0.08	83,83,96	0.0	0.0	0.0	0,0,0				
Trave	rRfck	rRfyk	rPfck	wR	wF	wP	dR	dF	dP				
	0.35	0.61	0.41	0.19	0.18	0.18	0.21	0.53	0.52				

VERIFICHE ELEMENTI PARETE E/O GUSCIO IN C.A.

Per le pareti in c.a., in ottemperanza al cap. 7 del DM 17-01-18, viene effettuata una doppia progettazione: sia come *Singolo Elemento* sia come *Parete Sismica* o *Parete Debolmente Armata*.

Per la progettazione come *Singolo Elemento* di ogni elemento vengono riportati il codice dello stato di verifica con le sigle **Ok** e **NV**, il rapporto x/d , la verifica per sollecitazioni ultime (verifica a compressione media gli sforzi membranali, verifica a presso-flessionale e verifica a sollecitazioni taglianti), gli sforzi membranali e flessionali, il quantitativo di armatura nella direzione principale e secondaria sia inferiore che superiore e il quantitativo di armatura a taglio.

Per la progettazione come *Parete Sismica* o *Parete Debolmente Armata* vengono riportate invece le caratteristiche geometriche della parete e delle zone dissipative (quest'ultime solo nel caso di parete sismica), i coefficienti di verifica a compressione assiale, pressoflessione e sollecitazioni taglianti.

Inoltre vengono riportate per ogni quota significativa l'armatura principale e secondaria, l'armatura in zona confinata (solo per parete sismica) e non confinata, l'armatura concentrata all'estremità (per

pareti debolmente armate), lo sforzo assiale aggiuntivo per q superiore a 2 e i valori di involuppo di taglio e momento. Per le pareti debolmente armate viene riportato anche lo stato di verifica relativo alla snellezza.

Le azioni derivate dall'analisi, in ogni combinazione di calcolo, sono elaborate come previsto al punto 7.4.4.5.1: traslazione del momento, incremento e variazione diagramma taglio, incremento e decremento sforzo assiale

La progettazione nel caso dei gusci viene effettuata una progettazione come *Singolo Elemento*, riportando in tabella il rapporto x/d , la verifica per sollecitazioni ultime, (verifica a compressione media gli sforzi membranali, verifica a presso-flessionale e verifica a sollecitazioni taglianti) di ogni elemento.

Per ogni elemento, viene riportata inoltre la maglia di armatura necessaria in relazione alle risultanze della progettazione dei nodi dell'elemento stesso. Le quantità di armature necessarie sono armature (disposte rispettivamente in direzione principale e secondaria, inferiore e superiore) distribuite nell'elemento ed espresse in centimetri quadri per sviluppo lineare pari ad un metro.

Nel caso dei gusci viene effettuata, inoltre, la verifica a punzonamento, riportando in tabella il codice dello stato di verifica, il coefficiente di verifica per piastre prive di armature a taglio lungo il perimetro resistente e lungo il perimetro del pilastro, coefficiente di incremento dovuto ai momenti flettenti, fattore di amplificazione per le fondazioni, il fattore di amplificazione dell'altezza utile per individuare il perimetro di verifica lungo il quale l'armatura a taglio non è richiesta, il quantitativo di armatura a punzonamento, il numero di serie di armature, il numero di braccia di armatura ed il riferimento alla combinazione più gravosa.

Simbologia adottata nelle tabelle di verifica

Per gli elementi con progettazione “Singolo Elemento ...” è presente una tabella con i simboli di seguito descritti:

Macro Guscio	Numero del macroelemento di tipo guscio (elementi non verticali contigui ed analoghi per proprietà)
Macro Setto	Numero del macroelemento di tipo setto (elementi verticali contigui ed analoghi per proprietà)
Spessore	Spessore della parete
Id Materiale	Codice del materiale assegnato all'elemento
Id Criterio	Codice del criterio di progetto assegnato all'elemento
Progettazione	Sigla tipo di Elemento: - Singolo Elemento; - Singolo Elemento FONDAZIONE; - Singolo Elemento NON DISSIPATIVO

Per gli elementi con progettazione “Parete Sismica o Parete Debolmente Armata” è presente una tabella con i simboli di seguito descritti:

Parete	Numero della PARETE SISMICA
Parete PDA	Numero della PARETE DEBOLMENTE ARMATA
H totale	Altezza complessiva della parete
Spessore	Spessore della parete
H critica	Altezza come da punto 7.4.4.5.1 per traslazione momento (solo in Parete Sismica)
H critica V	Altezza della zona dissipativa (solo in Parete Sismica)
L totale	Larghezza di base della parete
L confinata	Lunghezza della zona dissipativa (solo in Parete Sismica)
Verif. N	Verifica di cui al punto 7.4.4.5.1 compressione semplice
Verif. N-M	Verifica di cui al punto 7.4.4.5.1 pressoflessione
Fattore V	Fattore di amplificazione del taglio di cui al punto 7.4.4.5.1
Diagramma V	Diagramma elaborato per effetto modi superiori come da fig. 7.4.4
Verif. V	Verifica di cui al punto 7.4.4.5.1 taglio (compressione cls, trazione acciaio, scorrimento in zona critica) (solo in Parete Sismica)
Verifica Snellezza	Verifica di cui al punto 7.4.4.5.1 limitazione compressione per prevenire l'instabilità (solo in Parete Debolmente Armata)

Prog. composta	Sigla per la progettazione composta
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Per le verifiche degli elementi con progettazione “Singolo Elemento ...” e Progettazione Composta è presente una tabella con i simboli di seguito descritti:

Nodo	numero del nodo
Stato	codice di verifica dell'elemento ok o NV
x/d	rapporto tra posizione dell'asse neutro e altezza utile alla rottura della sezione (per sola flessione)
V N/M	Verifica delle sollecitazioni Normali (momento e sforzo normale)
Ver. rid	Rapporto Nd/Nu (Nu ottenuto con riduzione del 25% di fcd)
Af pr+	quantità di armatura richiesta in direzione principale relativa alla faccia positiva (estradosso piastre) (valore derivante da calcolo o minimo normativo)
Af pr-	quantità di armatura richiesta in direzione principale relativa alla faccia negativa (intradosso piastre) (valore derivante da calcolo o minimo normativo)
Af sec+	quantità di armatura richiesta in direzione secondaria relativa alla faccia positiva (estradosso piastre) (valore derivante da calcolo o minimo normativo)
Af sec-	quantità di armatura richiesta in direzione secondaria relativa alla faccia negativa (intradosso piastre) (valore derivante da calcolo o minimo normativo)
Nz No Nzo	Sforzi membranali per pareti e/o setti verticali
Mz Mo Mzo	Sforzi flessionali per pareti e/o setti verticali
Nx Ny Nxy	Sforzi membranali per gusci orizzontali
Mx Mx Mxy	Sforzi flessionali per gusci orizzontali

Nodo	numero del nodo
Stato	codice di verifica dell'elemento ok o NV
Max tau	Tensione tangenziale Massima
Ver V pr	Verifica a taglio nella direzione principale lato calcestruzzo
Ver V sec	Verifica a taglio nella direzione secondaria lato calcestruzzo
Af V pr	Armatura nella direzione principale
V pr-	Verifica dell'armatura nella direzione principale
Af V sec	Armatura nella direzione secondaria
V sec-	Verifica dell'armatura nella direzione secondaria

Per le verifiche degli elementi con progettazione “Parete Sismica o Parete Debolmente Armata”, oltre alla tabella con le verifiche per gli elementi con progettazione “Singolo Elemento ...”, è presente una tabella con i simboli di seguito descritti:

Quota	Ascissa verticale di riferimento
Af conf.	Numero e diametro armatura presente in una zona confinata
Af std	Diametro e passo armatura in zona non confinata (doppia maglia)
Af estremi	Diametro dei ferri di estremità del pannello; se posto uguale 0, viene utilizzato il diametro standard
Af V (ori)	Diametro e passo armatura orizzontale (doppia maglia)
Ver. N	Rapporto tra azione di calcolo e resistenza a compressione (normalizzato a 1 in quanto da confrontare con 40% in CDB e 35 % in CDA)
Ver. N/M	Rapporto tra azione di calcolo e resistenza a pressoflessione
Ver. V acc(7)	Rapporto tra azione di calcolo e resistenza a taglio-trazione secondo paragrafo 7.4.4.5.1
Ver. V cls	Rapporto tra azione di calcolo e resistenza a taglio-compressione
Ver. V acc	Rapporto tra azione di calcolo e resistenza a taglio-trazione
Ver. V scorr.	Rapporto tra azione di calcolo e resistenza a taglio scorrimento
N add	Sforzo assiale di cui al punto 7.4.4.5.1 da sommare e sottrarre nelle verifiche quando q supera 2
N invil M invil	Inviluppo del Momento e Sforzo Normale come al punto 7.4.4.5.1 (informativo) (solo in Parete Sismica)

Quota	Ascissa verticale di riferimento
N v.N	Valore dello sforzo assiale per cui Ver. N attinge il massimo valore
N v.M/N, M v.M/N	Valore dello sforzo assiale e momento per cui Ver. N/M attinge il massimo valore
N v.M/N, M v.M/N Mo v.M/N	Valore dello sforzo assiale e dei momenti per cui Ver. N/M attinge il massimo valore (per le pareti estese debolmente armate)
N v.Vcls, V v.Vcls,	Valore dello sforzo assiale e taglio per cui Ver. V. cls attinge il massimo valore
N v.Vacc, M v.Vacc, V v.Vacc,	Valore dello sforzo assiale, momento e taglio per cui Ver. V. acc attinge il massimo valore
N v.Vscorr, M v.Vscorr, V v.Vscorr,	Valore dello sforzo assiale, momento e taglio per cui Ver. V. scorr.e
N v.N	Valore dello sforzo assiale per cui Ver. N attinge il massimo valore
N v.M/N, M v.M/N	Valore dello sforzo assiale e momento per cui Ver. N/M attinge il massimo valore
N v.M/N, M v.M/N Mo v.M/N	Valore dello sforzo assiale e dei momenti per cui Ver. N/M attinge il massimo valore (per le pareti estese debolmente armate)
N v.Vcls, V v.Vcls,	Valore dello sforzo assiale e taglio per cui Ver. V. cls attinge il massimo valore

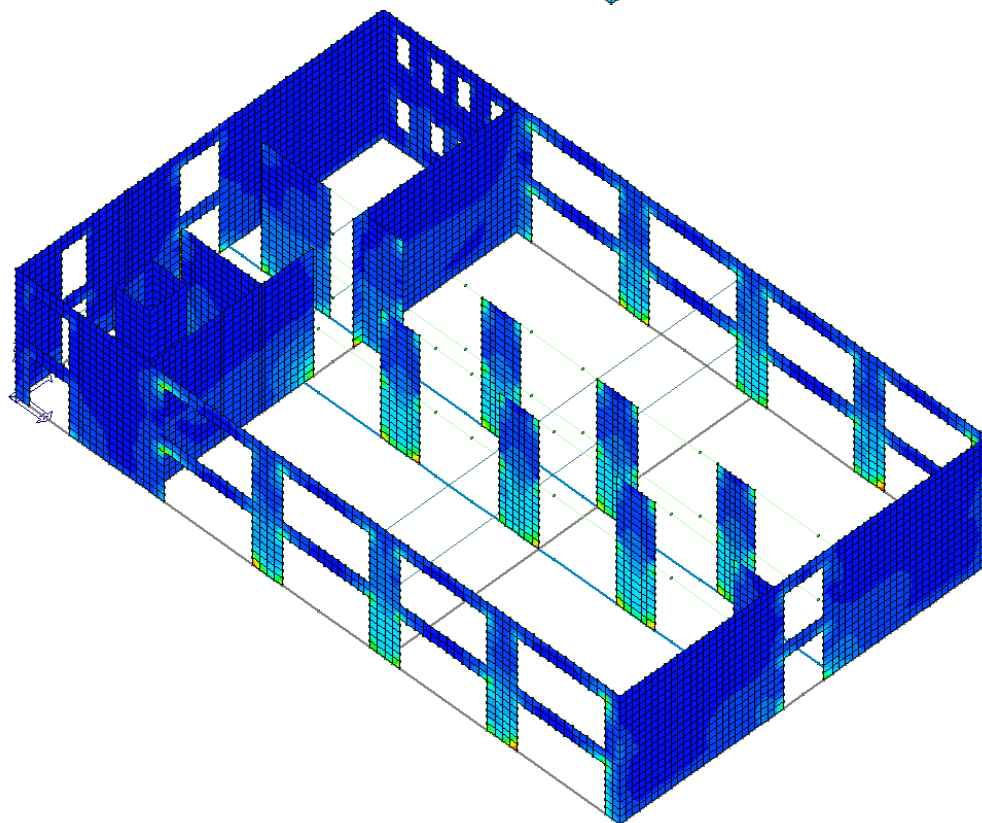
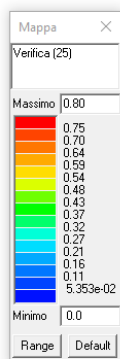
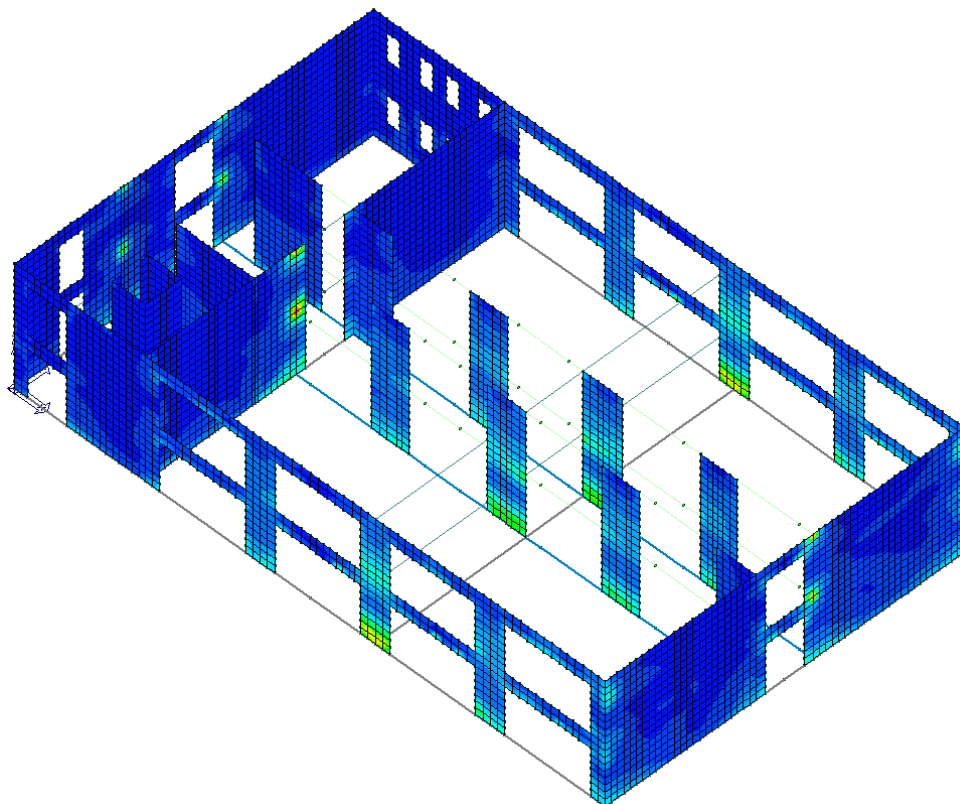
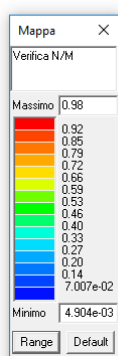
Quota	Ascissa verticale di riferimento
CtgT Vcls	Valore di ctg(teta) adottato nella verifica V compressione cls
Vrsd Vcls	Valore della resistenza a taglio trazione (armatura di calcolo)
Vrcd Vcls	Valore della resistenza a taglio compressione
CtgT Vacc	Valore di ctg(teta) adottato nella verifica V trazione armatura
Vrsd Vacc	Valore della resistenza a taglio trazione (armatura presente)
Vrcd Vacc	Valore della resistenza a taglio compressione
Vdd	Valore del contributo alla resistenza allo scorrimento come da [7.4.20]
Vid	Valore del contributo alla resistenza allo scorrimento come da [7.4.21]
A s.i.	Somma delle aree di armature
Incli.	Angolo di inclinazione delle armature
Dist.	Distanza alla base tra le armature inclinate

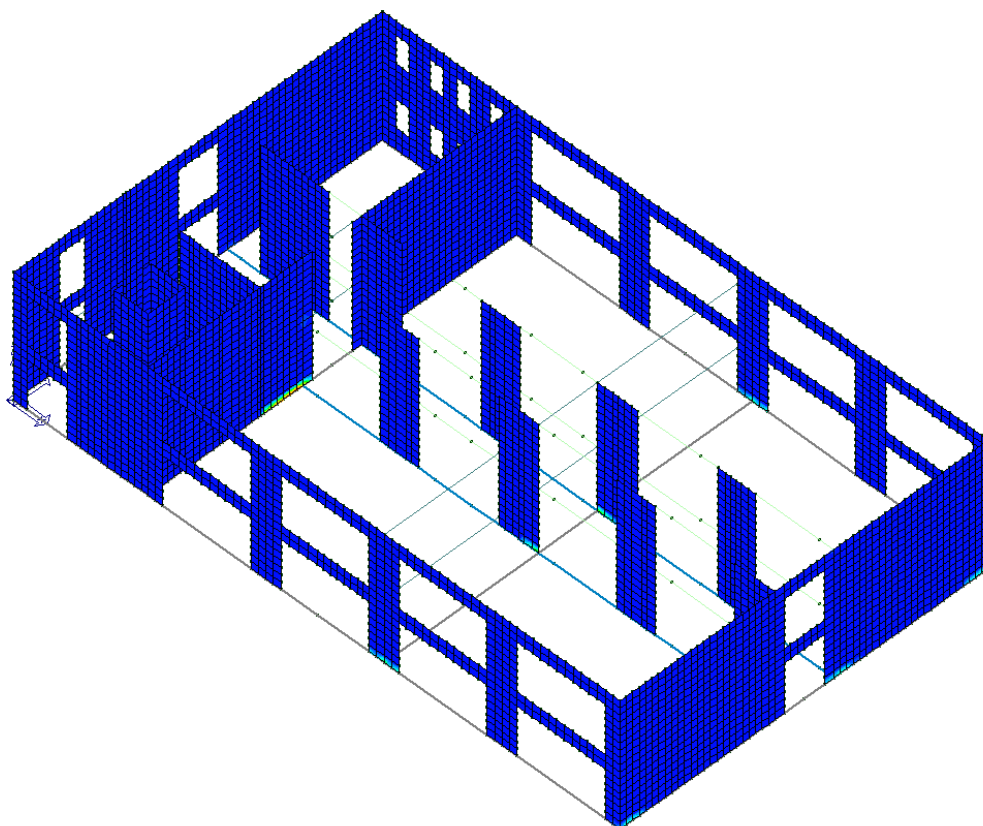
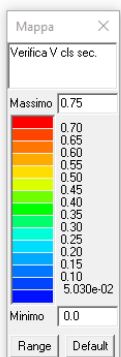
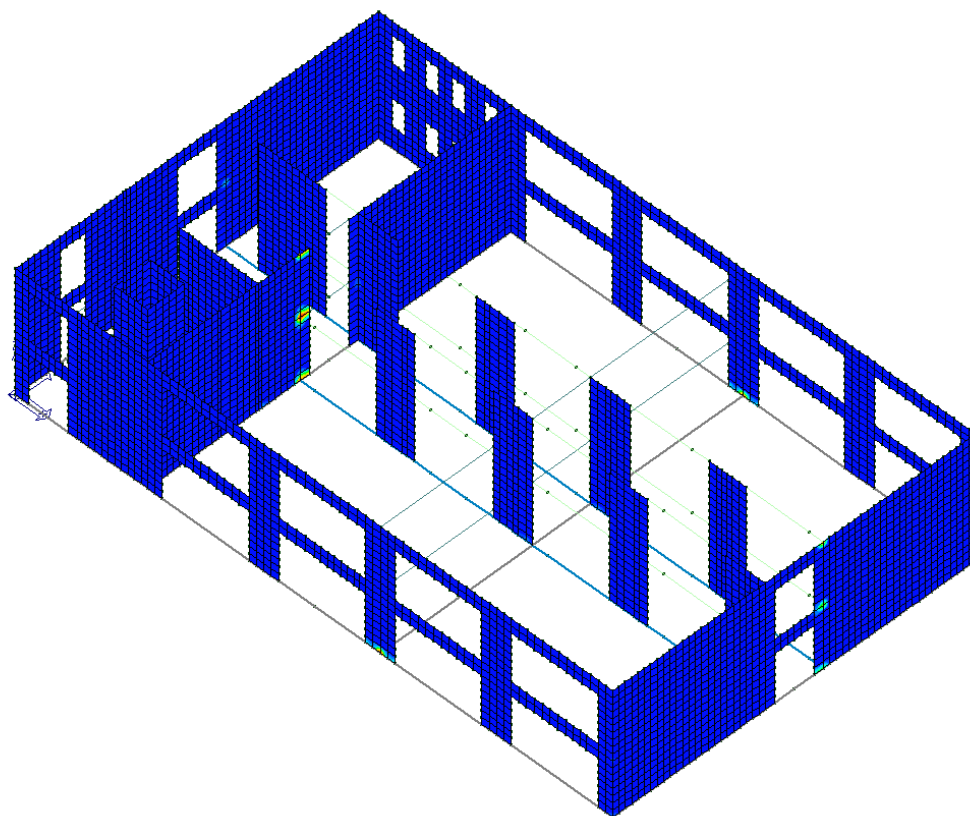
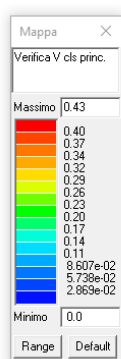
Quota	Ascissa verticale di riferimento
V[7.4.16]	Verifica a taglio-trazione dell'armatura dell'anima (7.4.16)
N M V	Sollecitazioni di calcolo della condizione più gravosa
Alfas	Rapporto di Taglio
Vrd,c	Resistenza a taglio degli elementi non armati
VRd,s	Resistenza a taglio nei confronti dello scorrimento
V[7.4.17]	Verifica a taglio-trazione dell'armatura dell'anima (7.4.17)
roH	Rapporto tra l'armatura orizzontale e l'area della sezione relativa di calcestruzzo
roV	Rapporto tra l'armatura verticale e l'area della sezione relativa di calcestruzzo
roN	Sforzo normale adimensionalizzato Ned/(bw fyd)

Per la verifica a Punzonamento è presente una tabella con i simboli di seguito descritti:

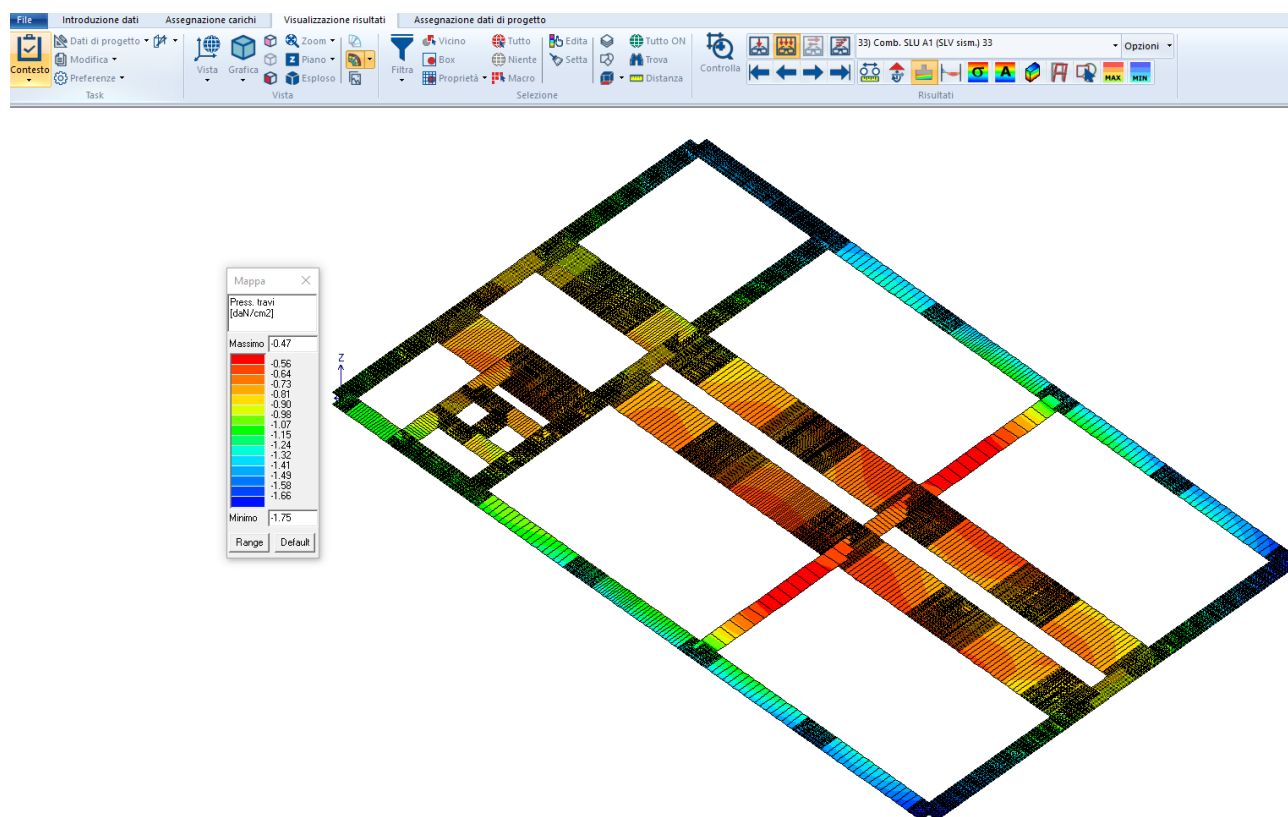
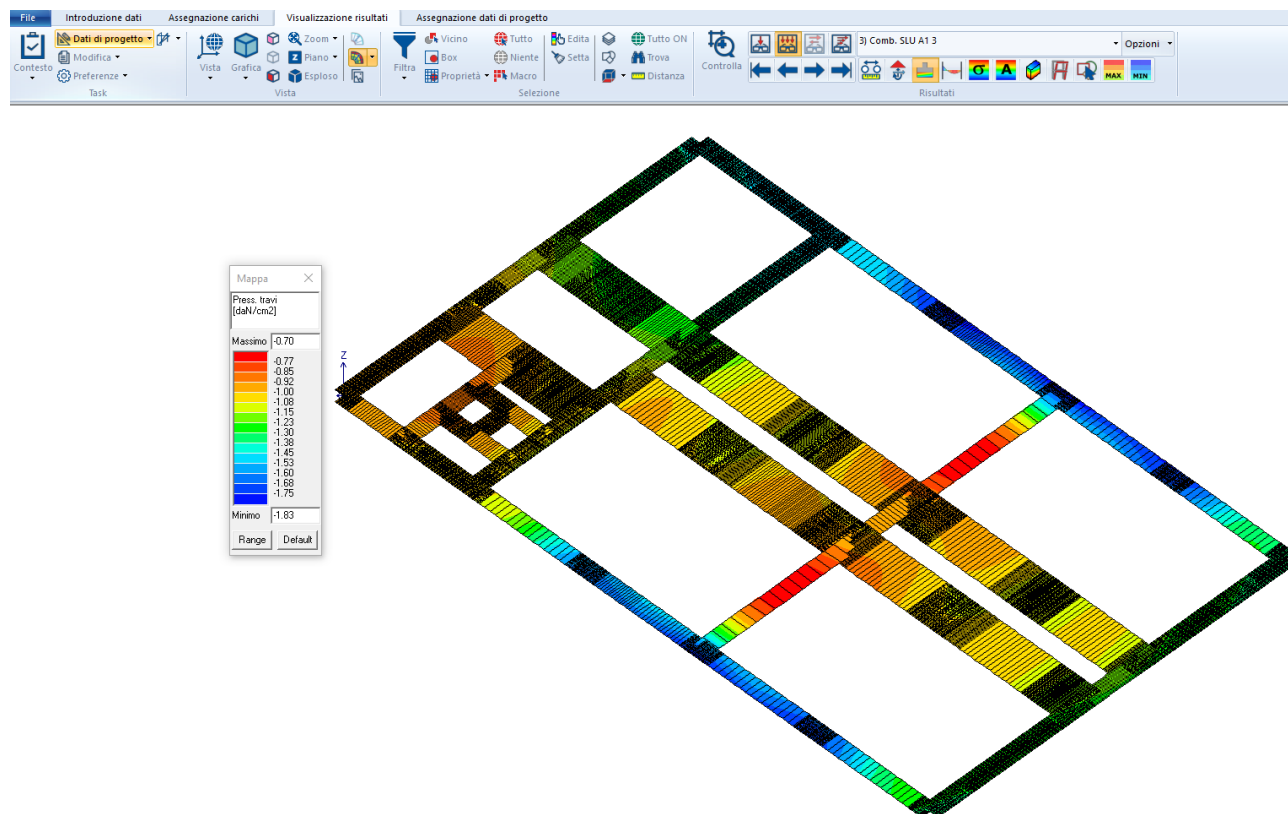
Nodo	numero del nodo
Stato	codice di verifica dell'elemento ok o NV
V. 6.47	Fattore di sicurezza per la verifica per piastre prive di armature a taglio lungo il perimetro resistente U1
V. 6.53	Fattore di sicurezza per la verifica per piastre prive di armature a taglio lungo il perimetro del pilastro U0
Beta	Fattore di incremento dovuto ai momenti flettenti
f. a fon	fattore di amplificazione per le fondazioni (solo per gusci di fondazione)
f. Uout	fattore di amplificazione dell'altezza utile per individuare il perimetro di verifica lungo il quale l'armatura a taglio non è richiesta
Aw tot	Quantitativo di armatura per la verifica di piastre munite di armatura (formula 6.52 dell'EC2)

Asw,min	Quantitativo minimo di armatura previsto dai dettagli costruttivi (formula 9.11 dell'EC2)
n. x serie	Numero di serie di armature
n.ser 0(R)	Numero di braccia delle armatura in direzione 0 (o numero di braccia radiale)
n.ser 90	Numero di braccia delle armatura in direzione 90 (solo se armatura cruciforme)
Rif. cmb	Riferimento combinazioni da cui si generano le verifiche più gravose



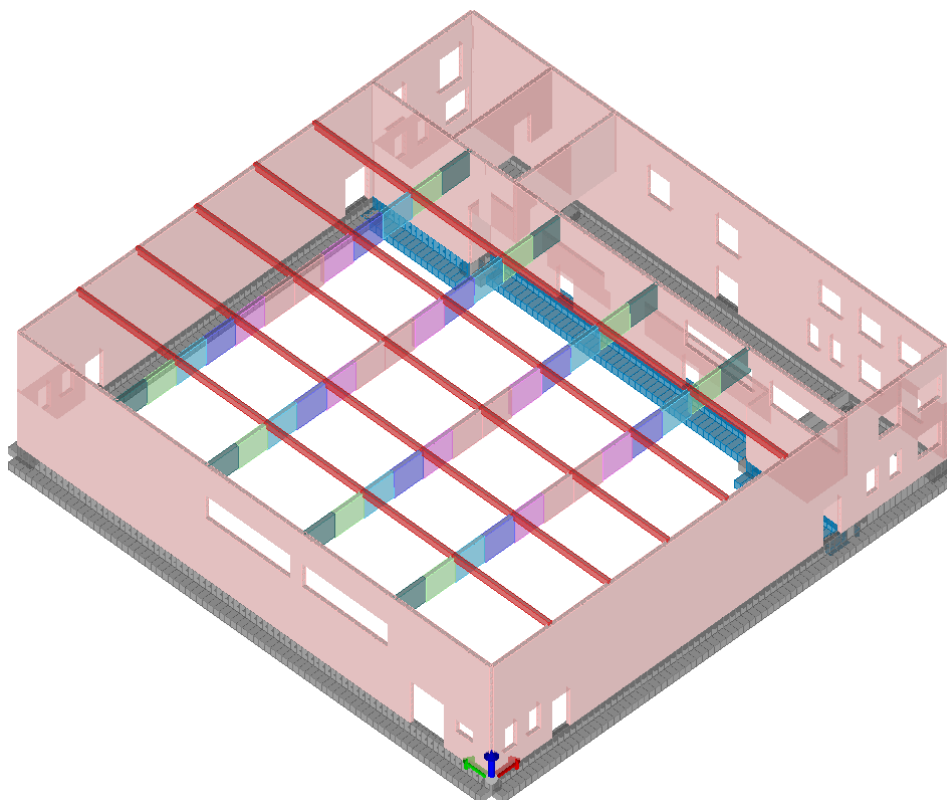


RELAZIONE SULLE FONDAZIONI

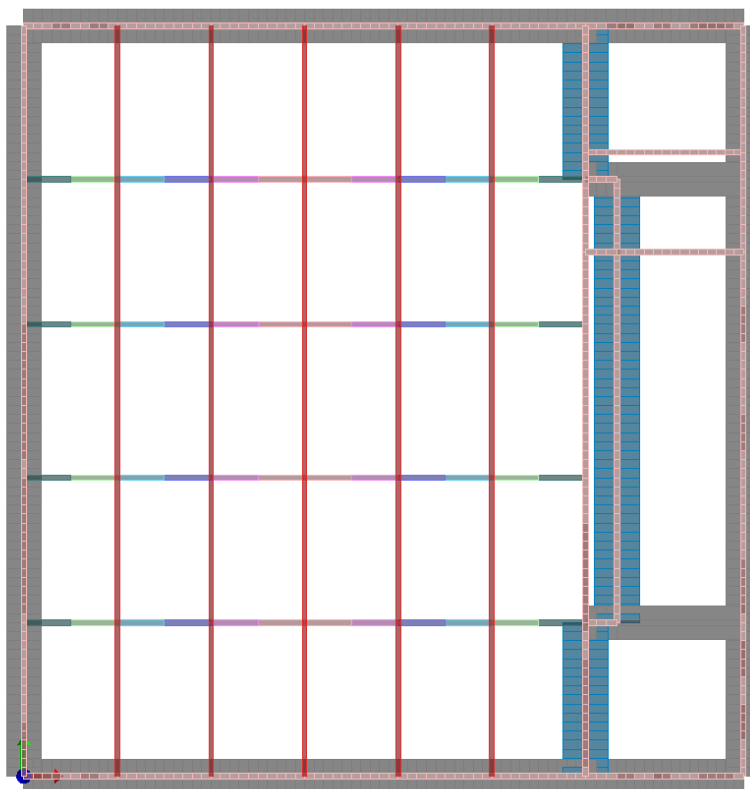


La tensione massima sul terreno, 0.185 Mpa è comunque inferiore a quella di riferimento 0.25 MPa

7 VERIFICA DELLE STRUTTURE DELLA PALESTRA



Vista tridimensionale dello scheletro delle strutture



Vista dall'alto dello scheletro delle strutture

CARATTERISTICHE MATERIALI UTILIZZATI

Il programma consente l'uso di materiali diversi. Sono previsti i seguenti tipi di materiale:

1	materiale tipo cemento armato
2	materiale tipo acciaio
3	materiale tipo muratura
4	materiale tipo legno
5	materiale tipo generico

I materiali utilizzati nella modellazione sono individuati da una sigla identificativa ed un codice numerico (gli elementi strutturali richiamano quest'ultimo nella propria descrizione). Per ogni materiale vengono riportati in tabella i seguenti dati:

Young	modulo di elasticità normale
Poisson	coefficiente di contrazione trasversale
G	modulo di elasticità tangenziale
Gamma	peso specifico
Alfa	coefficiente di dilatazione termica

I dati soprariportati vengono utilizzati per la modellazione dello schema statico e per la determinazione dei carichi inerziali e termici. In relazione al tipo di materiale vengono riportati inoltre:

1	cemento armato	Rck Fctm	resistenza caratteristica cubica resistenza media a trazione semplice
2	acciaio	Ft Fy Fd Fdt Sadm Sadmt	tensione di rottura a trazione tensione di snervamento resistenza di calcolo resistenza di calcolo per spess. $t > 40$ mm tensione ammissibile tensione ammissibile per spess. $t > 40$ mm
3	muratura	Resist. Fk Resist. Fvko	resistenza caratteristica a compressione resistenza caratteristica a taglio
4	legno	Resist. fc0k Resist. ft0k Resist. fmk Resist. fvk Modulo E0,05 Lamellare	Resistenza caratteristica (tensione amm. per REGLES) per compressione Resistenza caratteristica (tensione amm. per REGLES) per trazione Resistenza caratteristica (tensione amm. per REGLES) per flessione Resistenza caratteristica (tensione amm. per REGLES) per taglio Modulo elastico parallelo caratteristico lamellare o massiccio

Vengono inoltre riportate le tabelle contenenti il riassunto delle informazioni assegnate nei criteri di progetto in uso.

Id	Tipo / Note	V. caratt.	V. medio	Young	Poisson	G	Gamma	Alfa	Altri
		daN/cm ²	daN/cm ²	daN/cm ²		daN/cm ²	daN/cm ³		
1	Calcestruzzo Classe C25/30			3.145e+05	0.20	1.310e+05	2.50e-03	1.00e-05	
	Resistenza Rc	300.0							
	Resistenza fctm		25.6						
	Rapporto Rfessurata								1.00
	Coefficiente ksb								0.85
	Rapporto HRDb								1.00e-05
	Rapporto HRDv								1.00e-05
58	Legno lamellare omogeneo GL28h E = 1.260e+05			1.260e+05	0.0	6500.0	4.60e-04	0.0	
	Modulo E0,05			1.050e+05					
	Lamellare : Si								

Id	Tipo / Note	V. caratt.	V. medio	Young	Poisson	G	Gamma	Alfa	Altri
	Resistenza f_{c0}	280.0							
	Resistenza f_{t0}	223.0							
	Resistenza f_m	280.0							
	Resistenza f_v	35.0							
	Rapporto HRDb								1.00e-05
	Rapporto HRDv								1.00e-05

MODELLAZIONE DELLE SEZIONI

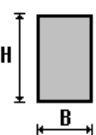
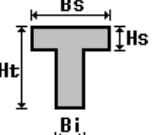
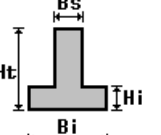
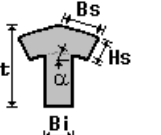
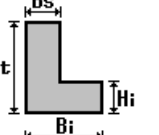
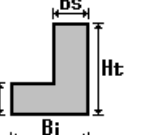
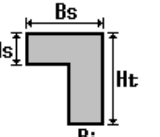
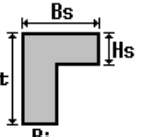
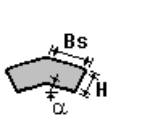
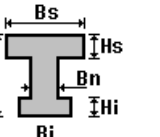
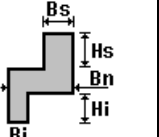
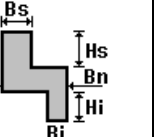
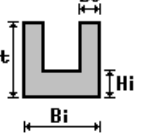
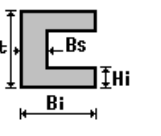
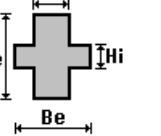
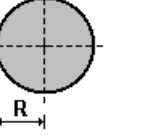
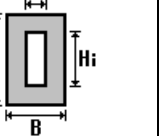
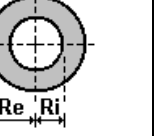
Il programma consente l'uso di sezioni diverse. Sono previsti i seguenti tipi di sezione:

4. sezione di tipo generico
5. profilati semplici
6. profilati accoppiati e speciali

Le sezioni utilizzate nella modellazione sono individuate da una sigla identificativa ed un codice numerico (gli elementi strutturali richiamano quest'ultimo nella propria descrizione). Per ogni sezione vengono riportati in tabella i seguenti dati:

Area	area della sezione
A V2	area della sezione/fattore di taglio (per il taglio in direzione 2)
A V3	area della sezione/fattore di taglio (per il taglio in direzione 3)
Jt	fattore torsionale di rigidezza
J2-2	momento d'inerzia della sezione riferito all'asse 2
J3-3	momento d'inerzia della sezione riferito all'asse 3
W2-2	modulo di resistenza della sezione riferito all'asse 2
W3-3	modulo di resistenza della sezione riferito all'asse 3
Wp2-2	modulo di resistenza plastico della sezione riferito all'asse 2
Wp3-3	modulo di resistenza plastico della sezione riferito all'asse 3

I dati sopra riportati vengono utilizzati per la determinazione dei carichi inerziali e per la definizione delle rigidezze degli elementi strutturali; qualora il valore di Area V2 (e/o Area V3) sia nullo la deformabilità per taglio V2 (e/o V3) è trascurata. La valutazione delle caratteristiche inerziali delle sezioni è condotta nel riferimento 2-3 dell'elemento.

					
rettangolare	a T	a T rovescia	a T di colmo	a L	a L specchiata
					
a L specchiata rovescia	a L rovescia	a L di colmo	a doppio T	a quattro specchiata	a quattro
					
a U	a C	a croce	circolare	rettangolare cava	circolare cava

Per quanto concerne i profilati semplici ed accoppiati l'asse 2 del riferimento coincide con l'asse x riportato nei più diffusi profilati.

Per quanto concerne le sezioni di tipo generico (tipo 1.):

i valori dimensionali con prefisso B sono riferiti all'asse 2

i valori dimensionali con prefisso H sono riferiti all'asse 3

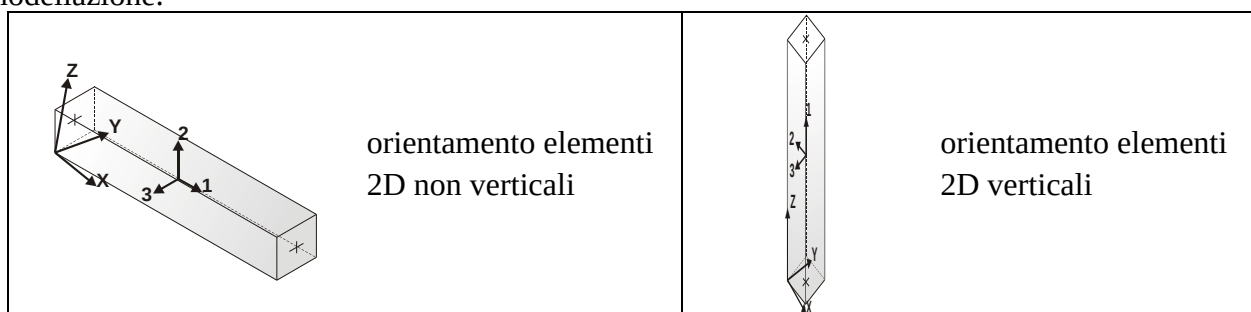
Id	Tipo	Area	A V2	A V3	Jt	J 2-2	J 3-3	W 2-2	W 3-3	Wp 2-2	Wp 3-3
1	T rovescia: bi=150 ht=125 bs=25 hi=50	9375.00	0.0	0.0	5.507e+06	1.416e+07	8.301e+06	1.888e+05	9.487e+04	2.930e+05	2.051e+05
2	T rovescia: bi=200 ht=125 bs=25 hi=50	1.188e+04	0.0	0.0	7.590e+06	3.343e+07	9.130e+06	3.343e+05	1.013e+05	5.117e+05	2.378e+05
3	Rettangolare: b=24 h=160	3840.00	3200.00	3200.00	6.676e+05	1.843e+05	8.192e+06	1.536e+04	1.024e+05	2.304e+04	1.536e+05
4	Rettangolare: b=24 h=168	4032.00	3360.00	3360.00	7.045e+05	1.935e+05	9.483e+06	1.613e+04	1.129e+05	2.419e+04	1.693e+05
5	Rettangolare: b=24 h=176	4224.00	3520.00	3520.00	7.413e+05	2.028e+05	1.090e+07	1.690e+04	1.239e+05	2.534e+04	1.859e+05
6	Rettangolare: b=24 h=184	4416.00	3680.00	3680.00	7.782e+05	2.120e+05	1.246e+07	1.766e+04	1.354e+05	2.650e+04	2.031e+05
7	Rettangolare: b=24 h=192	4608.00	3840.00	3840.00	8.151e+05	2.212e+05	1.416e+07	1.843e+04	1.475e+05	2.765e+04	2.212e+05
8	Rettangolare: b=24 h=200	4800.00	4000.00	4000.00	8.519e+05	2.304e+05	1.600e+07	1.920e+04	1.600e+05	2.880e+04	2.400e+05
9	Rettangolare: b=20 h=40	800.00	666.67	666.67	7.307e+04	2.667e+04	1.067e+05	2666.67	5333.33	4000.00	8000.00
10	Rettangolare: b=100 h=10	1000.00	833.33	833.33	3.123e+04	8.333e+05	8333.33	1.667e+04	1666.67	2.500e+04	2500.00
11	Rettangolare: b=25 h=50	1250.00	1041.67	1041.67	1.784e+05	6.510e+04	2.604e+05	5208.33	1.042e+04	7812.50	1.563e+04
12	Rettangolare: b=25 h=36	900.00	750.00	750.00	1.071e+05	4.688e+04	9.720e+04	3750.00	5400.00	5625.00	8100.00
13	Rettangolare: b=25 h=120	3000.00	2500.00	2500.00	5.430e+05	1.563e+05	3.600e+06	1.250e+04	6.000e+04	1.875e+04	9.000e+04

MODELLAZIONE STRUTTURA: ELEMENTI TRAVE

Il programma utilizza per la modellazione elementi a due nodi denominati in generale travi.

Ogni elemento trave è individuato dal nodo iniziale e dal nodo finale.

Ogni elemento è caratterizzato da un insieme di proprietà riportate in tabella che ne completano la modellazione.



In particolare per ogni elemento viene indicato in tabella:

Elem.	numero dell'elemento
Note	codice di comportamento: trave, trave di fondazione, pilastro, asta, asta tesa, asta compressa,
Nodo I (J)	numero del nodo iniziale (finale)
Mat.	codice del materiale assegnato all'elemento
Sez.	codice della sezione assegnata all'elemento
Rotaz.	valore della rotazione dell'elemento, attorno al proprio asse, nel caso in cui l'orientamento di default non sia adottabile; l'orientamento di default prevede per gli elementi non verticali l'asse 2 contenuto nel piano verticale e l'asse 3 orizzontale, per

	gli elementi verticali l'asse 2 diretto secondo X negativo e l'asse 3 diretto secondo Y negativo
Svincolo I (J)	codici di svincolo per le azioni interne; i primi sei codici si riferiscono al nodo iniziale, i restanti sei al nodo finale (il valore 1 indica che la relativa azione interna non è attiva)
Wink V	costante di sottofondo (coefficiente di Winkler) per la modellazione della trave su suolo elastico
Wink O	costante di sottofondo (coefficiente di Winkler) per la modellazione del suolo elastico orizzontale

Elem.	Note	Nodo I	Nodo J	Mat.	Sez.	Rotaz. gradi	Svincolo I	Svincolo J	Wink V daN/cm3	Wink O daN/cm3
1	Trave f.	1	29	1	1				4.00	1.00
2	Trave f.	1	2050	1	1				4.00	1.00
3	Trave f.	2	2886	1	1				4.00	1.00
4	Trave f.	3	1452	1	1				4.00	1.00
5	Trave f.	5	3305	1	1				4.00	1.00
6	Trave f.	6	3334	1	1				4.00	1.00
7	Trave f.	5	3218	1	2				4.00	1.00
8	Trave f.	7	3276	1	1				4.00	1.00
9	Trave f.	9	4144	1	2				4.00	1.00
10	Trave f.	8	3248	1	1				4.00	1.00
11	Trave f.	8	2893	1	2				4.00	1.00
12	Trave f.	10	11	1	1				4.00	1.00
13	Trave f.	9	12	1	1				4.00	1.00
14	Trave f.	11	2226	1	1				4.00	1.00
15	Trave f.	12	2716	1	1				4.00	1.00
16	Trave f.	29	46	1	1				4.00	1.00
17	Trave f.	1463	5	1	1				4.00	1.00
18	Trave f.	2736	12	1	1				4.00	1.00
19	Trave f.	865	6	1	1				4.00	1.00
20	Trave f.	2076	4	1	1				4.00	1.00
21	Trave f.	2246	11	1	1				4.00	1.00
22	Trave f.	1480	1463	1	1				4.00	1.00
23	Trave f.	2746	2736	1	1				4.00	1.00
24	Trave f.	882	865	1	1				4.00	1.00
25	Trave f.	2086	2076	1	1				4.00	1.00
26	Trave f.	2256	2246	1	1				4.00	1.00
27	Trave f.	46	56	1	1				4.00	1.00
28	Trave f.	1490	1480	1	1				4.00	1.00
29	Trave f.	2756	2746	1	1				4.00	1.00
30	Trave f.	892	882	1	1				4.00	1.00
31	Trave f.	2096	2086	1	1				4.00	1.00
32	Trave f.	2266	2256	1	1				4.00	1.00
33	Trave f.	56	66	1	1				4.00	1.00
34	Trave f.	1500	1490	1	1				4.00	1.00
35	Trave f.	2766	2756	1	1				4.00	1.00
36	Trave f.	902	892	1	1				4.00	1.00
37	Trave f.	2106	2096	1	1				4.00	1.00
38	Trave f.	2276	2266	1	1				4.00	1.00
39	Trave f.	66	76	1	1				4.00	1.00
40	Trave f.	1510	1500	1	1				4.00	1.00
41	Trave f.	2776	2766	1	1				4.00	1.00
42	Trave f.	912	902	1	1				4.00	1.00
43	Trave f.	2116	2106	1	1				4.00	1.00
44	Trave f.	2286	2276	1	1				4.00	1.00
45	Trave f.	76	86	1	1				4.00	1.00
46	Trave f.	1520	1510	1	1				4.00	1.00
47	Trave f.	2786	2776	1	1				4.00	1.00
48	Trave f.	922	912	1	1				4.00	1.00
49	Trave f.	2126	2116	1	1				4.00	1.00
50	Trave f.	2296	2286	1	1				4.00	1.00
51	Trave f.	86	96	1	1				4.00	1.00
52	Trave f.	1530	1520	1	1				4.00	1.00
53	Trave f.	2796	2786	1	1				4.00	1.00
54	Trave f.	932	922	1	1				4.00	1.00
55	Trave f.	2136	2126	1	1				4.00	1.00
56	Trave f.	2306	2296	1	1				4.00	1.00
57	Trave f.	96	106	1	1				4.00	1.00
58	Trave f.	1540	1530	1	1				4.00	1.00
59	Trave f.	2806	2796	1	1				4.00	1.00
60	Trave f.	942	932	1	1				4.00	1.00
61	Trave f.	2146	2136	1	1				4.00	1.00
62	Trave f.	2316	2306	1	1				4.00	1.00
63	Trave f.	106	116	1	1				4.00	1.00
64	Trave f.	1550	1540	1	1				4.00	1.00
65	Trave f.	2816	2806	1	1				4.00	1.00
66	Trave f.	952	942	1	1				4.00	1.00
67	Trave f.	2156	2146	1	1				4.00	1.00
68	Trave f.	2326	2316	1	1				4.00	1.00
69	Trave f.	116	126	1	1				4.00	1.00
70	Trave f.	1560	1550	1	1				4.00	1.00
71	Trave f.	2826	2816	1	1				4.00	1.00
72	Trave f.	962	952	1	1				4.00	1.00
73	Trave f.	2166	2156	1	1				4.00	1.00
74	Trave f.	2336	2326	1	1				4.00	1.00
75	Trave f.	126	136	1	1				4.00	1.00
76	Trave f.	1570	1560	1	1				4.00	1.00
77	Trave f.	2836	2826	1	1				4.00	1.00
78	Trave f.	972	962	1	1				4.00	1.00
79	Trave f.	2176	2166	1	1				4.00	1.00

80	Trave f.	2346	2336	1	1	4.00	1.00
81	Trave f.	136	146	1	1	4.00	1.00
82	Trave f.	1580	1570	1	1	4.00	1.00
83	Trave f.	2846	2836	1	1	4.00	1.00
84	Trave f.	982	972	1	1	4.00	1.00
85	Trave f.	2186	2176	1	1	4.00	1.00
86	Trave f.	2356	2346	1	1	4.00	1.00
87	Trave f.	146	156	1	1	4.00	1.00
88	Trave f.	1590	1580	1	1	4.00	1.00
89	Trave f.	2856	2846	1	1	4.00	1.00
90	Trave f.	992	982	1	1	4.00	1.00
91	Trave f.	2196	2186	1	1	4.00	1.00
92	Trave f.	2366	2356	1	1	4.00	1.00
93	Trave f.	156	166	1	1	4.00	1.00
94	Trave f.	1600	1590	1	1	4.00	1.00
95	Trave f.	2866	2856	1	1	4.00	1.00
96	Trave f.	1002	992	1	1	4.00	1.00
97	Trave f.	2206	2196	1	1	4.00	1.00
98	Trave f.	2376	2366	1	1	4.00	1.00
99	Trave f.	166	176	1	1	4.00	1.00
100	Trave f.	1610	1600	1	1	4.00	1.00
101	Trave f.	2876	2866	1	1	4.00	1.00
102	Trave f.	1012	1002	1	1	4.00	1.00
103	Trave f.	2216	2206	1	1	4.00	1.00
104	Trave f.	2386	2376	1	1	4.00	1.00
105	Trave f.	176	186	1	1	4.00	1.00
106	Trave f.	1620	1610	1	1	4.00	1.00
107	Trave f.	2886	2876	1	1	4.00	1.00
108	Trave f.	1022	1012	1	1	4.00	1.00
109	Trave f.	2226	2216	1	1	4.00	1.00
110	Trave f.	2396	2386	1	1	4.00	1.00
111	Trave f.	186	196	1	1	4.00	1.00
112	Trave f.	1630	1620	1	1	4.00	1.00
113	Trave f.	1032	1022	1	1	4.00	1.00
114	Trave f.	2406	2396	1	1	4.00	1.00
115	Trave f.	196	206	1	1	4.00	1.00
116	Trave f.	1640	1630	1	1	4.00	1.00
117	Trave f.	1042	1032	1	1	4.00	1.00
118	Trave f.	2416	2406	1	1	4.00	1.00
119	Trave f.	206	216	1	1	4.00	1.00
120	Trave f.	1650	1640	1	1	4.00	1.00
121	Trave f.	1052	1042	1	1	4.00	1.00
122	Trave f.	2426	2416	1	1	4.00	1.00
123	Trave f.	216	226	1	1	4.00	1.00
124	Trave f.	1660	1650	1	1	4.00	1.00
125	Trave f.	1062	1052	1	1	4.00	1.00
126	Trave f.	2436	2426	1	1	4.00	1.00
127	Trave f.	226	236	1	1	4.00	1.00
128	Trave f.	1670	1660	1	1	4.00	1.00
129	Trave f.	1072	1062	1	1	4.00	1.00
130	Trave f.	2446	2436	1	1	4.00	1.00
131	Trave f.	236	246	1	1	4.00	1.00
132	Trave f.	1680	1670	1	1	4.00	1.00
133	Trave f.	1082	1072	1	1	4.00	1.00
134	Trave f.	2456	2446	1	1	4.00	1.00
135	Trave f.	246	256	1	1	4.00	1.00
136	Trave f.	1690	1680	1	1	4.00	1.00
137	Trave f.	1092	1082	1	1	4.00	1.00
138	Trave f.	2466	2456	1	1	4.00	1.00
139	Trave f.	256	266	1	1	4.00	1.00
140	Trave f.	1700	1690	1	1	4.00	1.00
141	Trave f.	1102	1092	1	1	4.00	1.00
142	Trave f.	2476	2466	1	1	4.00	1.00
143	Trave f.	266	276	1	1	4.00	1.00
144	Trave f.	1710	1700	1	1	4.00	1.00
145	Trave f.	1112	1102	1	1	4.00	1.00
146	Trave f.	2486	2476	1	1	4.00	1.00
147	Trave f.	276	286	1	1	4.00	1.00
148	Trave f.	1720	1710	1	1	4.00	1.00
149	Trave f.	1122	1112	1	1	4.00	1.00
150	Trave f.	2496	2486	1	1	4.00	1.00
151	Trave f.	286	296	1	1	4.00	1.00
152	Trave f.	1730	1720	1	1	4.00	1.00
153	Trave f.	1132	1122	1	1	4.00	1.00
154	Trave f.	2506	2496	1	1	4.00	1.00
155	Trave f.	296	306	1	1	4.00	1.00
156	Trave f.	1740	1730	1	1	4.00	1.00
157	Trave f.	1142	1132	1	1	4.00	1.00
158	Trave f.	2516	2506	1	1	4.00	1.00
159	Trave f.	306	316	1	1	4.00	1.00
160	Trave f.	1750	1740	1	1	4.00	1.00
161	Trave f.	1152	1142	1	1	4.00	1.00
162	Trave f.	2526	2516	1	1	4.00	1.00
163	Trave f.	316	326	1	1	4.00	1.00
164	Trave f.	1760	1750	1	1	4.00	1.00
165	Trave f.	1162	1152	1	1	4.00	1.00
166	Trave f.	2536	2526	1	1	4.00	1.00
167	Trave f.	326	336	1	1	4.00	1.00
168	Trave f.	1770	1760	1	1	4.00	1.00
169	Trave f.	1172	1162	1	1	4.00	1.00
170	Trave f.	2546	2536	1	1	4.00	1.00
171	Trave f.	336	346	1	1	4.00	1.00
172	Trave f.	1780	1770	1	1	4.00	1.00
173	Trave f.	1182	1172	1	1	4.00	1.00
174	Trave f.	2556	2546	1	1	4.00	1.00
175	Trave f.	346	356	1	1	4.00	1.00
176	Trave f.	1790	1780	1	1	4.00	1.00
177	Trave f.	1192	1182	1	1	4.00	1.00
178	Trave f.	2566	2556	1	1	4.00	1.00
179	Trave f.	356	366	1	1	4.00	1.00
180	Trave f.	1800	1790	1	1	4.00	1.00

181	Trave f.	1202	1192	1	1	4.00	1.00
182	Trave f.	2576	2566	1	1	4.00	1.00
183	Trave f.	366	376	1	1	4.00	1.00
184	Trave f.	1810	1800	1	1	4.00	1.00
185	Trave f.	1212	1202	1	1	4.00	1.00
186	Trave f.	2586	2576	1	1	4.00	1.00
187	Trave f.	376	386	1	1	4.00	1.00
188	Trave f.	1820	1810	1	1	4.00	1.00
189	Trave f.	1222	1212	1	1	4.00	1.00
190	Trave f.	2596	2586	1	1	4.00	1.00
191	Trave f.	386	396	1	1	4.00	1.00
192	Trave f.	1830	1820	1	1	4.00	1.00
193	Trave f.	1232	1222	1	1	4.00	1.00
194	Trave f.	2606	2596	1	1	4.00	1.00
195	Trave f.	396	406	1	1	4.00	1.00
196	Trave f.	1840	1830	1	1	4.00	1.00
197	Trave f.	1242	1232	1	1	4.00	1.00
198	Trave f.	2616	2606	1	1	4.00	1.00
199	Trave f.	406	416	1	1	4.00	1.00
200	Trave f.	1850	1840	1	1	4.00	1.00
201	Trave f.	1252	1242	1	1	4.00	1.00
202	Trave f.	2626	2616	1	1	4.00	1.00
203	Trave f.	416	426	1	1	4.00	1.00
204	Trave f.	1860	1850	1	1	4.00	1.00
205	Trave f.	1262	1252	1	1	4.00	1.00
206	Trave f.	2636	2626	1	1	4.00	1.00
207	Trave f.	426	436	1	1	4.00	1.00
208	Trave f.	1870	1860	1	1	4.00	1.00
209	Trave f.	1272	1262	1	1	4.00	1.00
210	Trave f.	2646	2636	1	1	4.00	1.00
211	Trave f.	436	446	1	1	4.00	1.00
212	Trave f.	1880	1870	1	1	4.00	1.00
213	Trave f.	1282	1272	1	1	4.00	1.00
214	Trave f.	2656	2646	1	1	4.00	1.00
215	Trave f.	446	456	1	1	4.00	1.00
216	Trave f.	1890	1880	1	1	4.00	1.00
217	Trave f.	1292	1282	1	1	4.00	1.00
218	Trave f.	2666	2656	1	1	4.00	1.00
219	Trave f.	456	466	1	1	4.00	1.00
220	Trave f.	1900	1890	1	1	4.00	1.00
221	Trave f.	1302	1292	1	1	4.00	1.00
222	Trave f.	2676	2666	1	1	4.00	1.00
223	Trave f.	466	476	1	1	4.00	1.00
224	Trave f.	1910	1900	1	1	4.00	1.00
225	Trave f.	1312	1302	1	1	4.00	1.00
226	Trave f.	2686	2676	1	1	4.00	1.00
227	Trave f.	476	486	1	1	4.00	1.00
228	Trave f.	1920	1910	1	1	4.00	1.00
229	Trave f.	1322	1312	1	1	4.00	1.00
230	Trave f.	2696	2686	1	1	4.00	1.00
231	Trave f.	486	496	1	1	4.00	1.00
232	Trave f.	1930	1920	1	1	4.00	1.00
233	Trave f.	1332	1322	1	1	4.00	1.00
234	Trave f.	2706	2696	1	1	4.00	1.00
235	Trave f.	496	506	1	1	4.00	1.00
236	Trave f.	1940	1930	1	1	4.00	1.00
237	Trave f.	1342	1332	1	1	4.00	1.00
238	Trave f.	2716	2706	1	1	4.00	1.00
239	Trave f.	506	516	1	1	4.00	1.00
240	Trave f.	1950	1940	1	1	4.00	1.00
241	Trave f.	1352	1342	1	1	4.00	1.00
242	Trave f.	516	526	1	1	4.00	1.00
243	Trave f.	1960	1950	1	1	4.00	1.00
244	Trave f.	1362	1352	1	1	4.00	1.00
245	Trave f.	526	536	1	1	4.00	1.00
246	Trave f.	1970	1960	1	1	4.00	1.00
247	Trave f.	1372	1362	1	1	4.00	1.00
248	Trave f.	536	546	1	1	4.00	1.00
249	Trave f.	1980	1970	1	1	4.00	1.00
250	Trave f.	1382	1372	1	1	4.00	1.00
251	Trave f.	546	556	1	1	4.00	1.00
252	Trave f.	1990	1980	1	1	4.00	1.00
253	Trave f.	1392	1382	1	1	4.00	1.00
254	Trave f.	556	566	1	1	4.00	1.00
255	Trave f.	2000	1990	1	1	4.00	1.00
256	Trave f.	1402	1392	1	1	4.00	1.00
257	Trave f.	566	576	1	1	4.00	1.00
258	Trave f.	2010	2000	1	1	4.00	1.00
259	Trave f.	1412	1402	1	1	4.00	1.00
260	Trave f.	576	586	1	1	4.00	1.00
261	Trave f.	2020	2010	1	1	4.00	1.00
262	Trave f.	1422	1412	1	1	4.00	1.00
263	Trave f.	586	596	1	1	4.00	1.00
264	Trave f.	2030	2020	1	1	4.00	1.00
265	Trave f.	1432	1422	1	1	4.00	1.00
266	Trave f.	596	606	1	1	4.00	1.00
267	Trave f.	2040	2030	1	1	4.00	1.00
268	Trave f.	1442	1432	1	1	4.00	1.00
269	Trave f.	606	616	1	1	4.00	1.00
270	Trave f.	2050	2040	1	1	4.00	1.00
271	Trave f.	1452	1442	1	1	4.00	1.00
272	Trave f.	616	626	1	1	4.00	1.00
273	Trave f.	626	636	1	1	4.00	1.00
274	Trave f.	636	646	1	1	4.00	1.00
275	Trave f.	646	656	1	1	4.00	1.00
276	Trave f.	656	666	1	1	4.00	1.00
277	Trave f.	666	676	1	1	4.00	1.00
278	Trave f.	676	686	1	1	4.00	1.00
279	Trave f.	686	696	1	1	4.00	1.00
280	Trave f.	696	706	1	1	4.00	1.00
281	Trave f.	706	716	1	1	4.00	1.00

282	Trave f.	716	726	1	1	4.00	1.00
283	Trave f.	726	736	1	1	4.00	1.00
284	Trave f.	736	746	1	1	4.00	1.00
285	Trave f.	746	756	1	1	4.00	1.00
286	Trave f.	756	766	1	1	4.00	1.00
287	Trave f.	766	776	1	1	4.00	1.00
288	Trave f.	776	786	1	1	4.00	1.00
289	Trave f.	786	796	1	1	4.00	1.00
290	Trave f.	796	806	1	1	4.00	1.00
291	Trave f.	806	816	1	1	4.00	1.00
292	Trave f.	816	826	1	1	4.00	1.00
293	Trave f.	826	836	1	1	4.00	1.00
294	Trave f.	836	846	1	1	4.00	1.00
295	Trave f.	846	3	1	1	4.00	1.00
296	Trave f.	3228	3344	1	1	4.00	1.00
297	Trave f.	3227	3474	1	1	4.00	1.00
298	Trave f.	3061	7	1	2	4.00	1.00
299	Trave f.	2893	2910	1	2	4.00	1.00
300	Trave f.	3078	3061	1	2	4.00	1.00
301	Trave f.	2910	2920	1	2	4.00	1.00
302	Trave f.	3088	3078	1	2	4.00	1.00
303	Trave f.	2920	2930	1	2	4.00	1.00
304	Trave f.	3098	3088	1	2	4.00	1.00
305	Trave f.	2930	2940	1	2	4.00	1.00
306	Trave f.	3108	3098	1	2	4.00	1.00
307	Trave f.	2940	2950	1	2	4.00	1.00
308	Trave f.	3118	3108	1	2	4.00	1.00
309	Trave f.	2950	2960	1	2	4.00	1.00
310	Trave f.	3128	3118	1	2	4.00	1.00
311	Trave f.	2960	2970	1	2	4.00	1.00
312	Trave f.	3138	3128	1	2	4.00	1.00
313	Trave f.	2970	2980	1	2	4.00	1.00
314	Trave f.	3148	3138	1	2	4.00	1.00
315	Trave f.	2980	2990	1	2	4.00	1.00
316	Trave f.	3158	3148	1	2	4.00	1.00
317	Trave f.	2990	3000	1	2	4.00	1.00
318	Trave f.	3168	3158	1	2	4.00	1.00
319	Trave f.	3000	3010	1	2	4.00	1.00
320	Trave f.	3178	3168	1	2	4.00	1.00
321	Trave f.	3010	3020	1	2	4.00	1.00
322	Trave f.	3188	3178	1	2	4.00	1.00
323	Trave f.	3020	3030	1	2	4.00	1.00
324	Trave f.	3198	3188	1	2	4.00	1.00
325	Trave f.	3030	3040	1	2	4.00	1.00
326	Trave f.	3208	3198	1	2	4.00	1.00
327	Trave f.	3040	3050	1	2	4.00	1.00
328	Trave f.	3218	3208	1	2	4.00	1.00
329	Trave f.	3050	6	1	2	4.00	1.00
330	Trave f.	3287	3228	1	1	4.00	1.00
331	Trave f.	3316	3227	1	1	4.00	1.00
332	Trave f.	3259	9	1	1	4.00	1.00
333	Trave f.	3231	10	1	1	4.00	1.00
334	Trave f.	3344	3354	1	1	4.00	1.00
335	Trave f.	3474	3484	1	1	4.00	1.00
336	Trave f.	3305	3287	1	1	4.00	1.00
337	Trave f.	3334	3316	1	1	4.00	1.00
338	Trave f.	3276	3259	1	1	4.00	1.00
339	Trave f.	3248	3231	1	1	4.00	1.00
340	Trave f.	3354	3364	1	1	4.00	1.00
341	Trave f.	3484	3494	1	1	4.00	1.00
342	Trave f.	3364	3374	1	1	4.00	1.00
343	Trave f.	3494	3504	1	1	4.00	1.00
344	Trave f.	3374	3384	1	1	4.00	1.00
345	Trave f.	3504	3514	1	1	4.00	1.00
346	Trave f.	3384	3394	1	1	4.00	1.00
347	Trave f.	3514	3524	1	1	4.00	1.00
348	Trave f.	3394	3404	1	1	4.00	1.00
349	Trave f.	3524	3534	1	1	4.00	1.00
350	Trave f.	3404	3414	1	1	4.00	1.00
351	Trave f.	3534	3544	1	1	4.00	1.00
352	Trave f.	3414	3424	1	1	4.00	1.00
353	Trave f.	3544	3554	1	1	4.00	1.00
354	Trave f.	3424	3434	1	1	4.00	1.00
355	Trave f.	3554	3564	1	1	4.00	1.00
356	Trave f.	3434	3444	1	1	4.00	1.00
357	Trave f.	3564	3574	1	1	4.00	1.00
358	Trave f.	3444	3454	1	1	4.00	1.00
359	Trave f.	3574	3584	1	1	4.00	1.00
360	Trave f.	3454	3464	1	1	4.00	1.00
361	Trave f.	3584	3594	1	1	4.00	1.00
362	Trave f.	3464	2	1	1	4.00	1.00
363	Trave f.	3594	4	1	1	4.00	1.00
364	Trave f.	6874	10	1	2	4.00	1.00
365	Trave f.	6884	6874	1	2	4.00	1.00
366	Trave f.	6894	6884	1	2	4.00	1.00
367	Trave f.	6904	6894	1	2	4.00	1.00
368	Trave f.	6914	6904	1	2	4.00	1.00
369	Trave f.	6924	6914	1	2	4.00	1.00
370	Trave f.	6934	6924	1	2	4.00	1.00
371	Trave f.	6944	6934	1	2	4.00	1.00
372	Trave f.	6954	6944	1	2	4.00	1.00
373	Trave f.	6964	6954	1	2	4.00	1.00
374	Trave f.	6974	6964	1	2	4.00	1.00
375	Trave f.	6984	6974	1	2	4.00	1.00
376	Trave f.	6994	6984	1	2	4.00	1.00
377	Trave f.	7004	6994	1	2	4.00	1.00
378	Trave f.	7014	7004	1	2	4.00	1.00
379	Trave f.	7024	7014	1	2	4.00	1.00
380	Trave f.	7034	7024	1	2	4.00	1.00
381	Trave f.	7044	7034	1	2	4.00	1.00
382	Trave f.	7054	7044	1	2	4.00	1.00

383	Trave f.	7064	7054	1	2			4.00	1.00
384	Trave f.	7074	7064	1	2			4.00	1.00
385	Trave f.	7084	7074	1	2			4.00	1.00
386	Trave f.	7094	7084	1	2			4.00	1.00
387	Trave f.	7104	7094	1	2			4.00	1.00
388	Trave f.	7114	7104	1	2			4.00	1.00
389	Trave f.	7124	7114	1	2			4.00	1.00
390	Trave f.	7134	7124	1	2			4.00	1.00
391	Trave f.	3624	7134	1	2			4.00	1.00
392	Trave f.	3644	3624	1	2			4.00	1.00
393	Trave f.	3664	3644	1	2			4.00	1.00
394	Trave f.	3694	3664	1	2			4.00	1.00
395	Trave f.	3724	3694	1	2			4.00	1.00
396	Trave f.	3744	3724	1	2			4.00	1.00
397	Trave f.	3774	3744	1	2			4.00	1.00
398	Trave f.	3804	3774	1	2			4.00	1.00
399	Trave f.	3824	3804	1	2			4.00	1.00
400	Trave f.	3854	3824	1	2			4.00	1.00
401	Trave f.	3884	3854	1	2			4.00	1.00
402	Trave f.	3904	3884	1	2			4.00	1.00
403	Trave f.	3934	3904	1	2			4.00	1.00
404	Trave f.	3964	3934	1	2			4.00	1.00
405	Trave f.	3984	3964	1	2			4.00	1.00
406	Trave f.	4014	3984	1	2			4.00	1.00
407	Trave f.	4044	4014	1	2			4.00	1.00
408	Trave f.	4064	4044	1	2			4.00	1.00
409	Trave f.	4094	4064	1	2			4.00	1.00
410	Trave f.	4124	4094	1	2			4.00	1.00
411	Trave f.	4144	4124	1	2			4.00	1.00
412	Trave	894	895	58	8				
413	Trave	4667	906	58	3	000011			
414	Trave	896	5613	58	4				
415	Trave	5613	4193	58	3		000011		
416	Trave	906	886	58	4				
417	Trave	891	893	58	7				
418	Trave	893	903	58	6				
419	Trave	903	904	58	5				
420	Trave	886	883	58	5				
421	Trave	883	884	58	6				
422	Trave	884	885	58	7				
423	Trave	885	881	58	8				
424	Trave	881	891	58	8				
425	Trave	904	905	58	4				
426	Trave	905	5579	58	3				000011
427	Trave	4411	5615	58	3	000011			
428	Trave	5615	5627	58	4				
429	Trave	6287	6288	58	7				
430	Trave	6288	6299	58	6				
431	Trave	6299	3477	58	5				
432	Trave	5627	3478	58	5				
433	Trave	3478	3479	58	6				
434	Trave	3479	3517	58	7				
435	Trave	3517	3518	58	8				
436	Trave	3518	6287	58	8				
437	Trave	3477	3519	58	4				
438	Trave	3519	7730	58	3				000011
439	Trave	4139	5867	58	3	000011			
440	Trave	5867	5868	58	4				
441	Trave	5869	5903	58	7				
442	Trave	5903	5904	58	6				
443	Trave	5904	5925	58	5				
444	Trave	5868	5949	58	5				
445	Trave	5949	5950	58	6				
446	Trave	5950	5951	58	7				
447	Trave	5951	3569	58	8				
448	Trave	3569	5869	58	8				
449	Trave	5925	3579	58	4				
450	Trave	3579	7935	58	3				000011
451	Trave	3883	3589	58	3	000011			
452	Trave	3589	3567	58	4				
453	Trave	895	3568	58	7				
454	Trave	3568	3577	58	6				
455	Trave	3577	896	58	5				
456	Trave	3567	3578	58	5				
457	Trave	3578	3587	58	6				
458	Trave	3587	3588	58	7				
459	Trave	3588	894	58	8				
460	Trave	3518	881	58	9	000001	000001		
461	Trave	3569	3518	58	9	000001	000001		
462	Trave	894	3569	58	9	000001	000001		
463	Trave	6394	894	58	9	000001	000001		
464	Trave	881	5434	58	9	000001	000001		
465	Trave	3479	884	58	9	000001	000001		
466	Trave	5950	3479	58	9	000001	000001		
467	Trave	3587	5950	58	9	000001	000001		
468	Trave	6554	3587	58	9	000001	000001		
469	Trave	884	5594	58	9	000001	000001		
470	Trave	5627	886	58	9	000001	000001		
471	Trave	5868	5627	58	9	000001	000001		
472	Trave	3567	5868	58	9	000001	000001		
473	Trave	6714	3567	58	9	000001	000001		
474	Trave	886	5754	58	9	000001	000001		
475	Trave	6288	893	58	9	000001	000001		
476	Trave	5903	6288	58	9	000001	000001		
477	Trave	3568	5903	58	9	000001	000001		
478	Trave	6234	3568	58	9	000001	000001		
479	Trave	893	5274	58	9	000001	000001		
480	Trave	3477	904	58	9	000001	000001		
481	Trave	5925	3477	58	9	000001	000001		
482	Trave	896	5925	58	9	000001	000001		
483	Trave	6074	896	58	9	000001	000001		

484	Trave	904	5114	58	9	000001	000001
485	Trave	4939	5898	1	11		
486	Trave	4573	6508	1	11		
487	Trave	5923	4860	1	11		
488	Trave	3621	3622	1	11		
489	Trave	3621	6858	1	11		
490	Trave	5451	8023	1	11		
491	Trave	7680	3349	1	11		
492	Trave	4963	5710	1	11		
493	Trave	4220	5056	1	11		
494	Trave	1943	7919	1	11		
495	Trave	3622	3643	1	11		
496	Trave	4225	4351	1	11		
497	Trave	7957	7958	1	11		
498	Trave	127	159	1	11		
499	Trave	4964	4963	1	11		
500	Trave	4432	4828	1	11		
501	Trave	2035	7929	1	11		
502	Trave	5923	6347	1	11		
503	Trave	8023	8024	1	11		
504	Trave	141	127	1	11		
505	Trave	5647	6304	1	11		
506	Trave	5056	5792	1	11		
507	Trave	2512	7700	1	11		
508	Trave	3643	3659	1	11		
509	Trave	4351	4477	1	11		
510	Trave	7958	8092	1	11		
511	Trave	159	4357	1	11		
512	Trave	4986	4964	1	11		
513	Trave	4781	7620	1	11		
514	Trave	4193	7939	1	11		
515	Trave	5924	5923	1	11		
516	Trave	1333	141	1	11		
517	Trave	5648	5647	1	11		
518	Trave	2701	7760	1	11		
519	Trave	4828	5054	1	11		
520	Trave	7929	1943	1	11		
521	Trave	6347	6383	1	11		
522	Trave	8024	8041	1	11		
523	Trave	5776	5775	1	11		
524	Trave	5792	6718	1	11		
525	Trave	4893	4963	1	11		
526	Trave	3659	3675	1	11		
527	Trave	4477	4573	1	11		
528	Trave	7981	7982	1	11		
529	Trave	3457	7220	1	11		
530	Trave	5002	4986	1	11		
531	Trave	4782	4781	1	11		
532	Trave	4204	4193	1	11		
533	Trave	5946	5924	1	11		
534	Trave	3349	4206	1	11		
535	Trave	5710	5648	1	11		
536	Trave	2822	7780	1	11		
537	Trave	5838	5776	1	11		
538	Trave	4929	4893	1	11		
539	Trave	8092	7981	1	11		
540	Trave	3940	3457	1	11		
541	Trave	6683	6684	1	11		
542	Trave	7939	2035	1	11		
543	Trave	5805	7740	1	11		
544	Trave	5054	5390	1	11		
545	Trave	6383	6429	1	11		
546	Trave	8041	8114	1	11		
547	Trave	6014	6720	1	11		
548	Trave	3675	3691	1	11		
549	Trave	7982	8057	1	11		
550	Trave	5018	5002	1	11		
551	Trave	4924	4782	1	11		
552	Trave	4256	4204	1	11		
553	Trave	5962	5946	1	11		
554	Trave	3821	7900	1	11		
555	Trave	5884	5838	1	11		
556	Trave	4975	4929	1	11		
557	Trave	3989	3940	1	11		
558	Trave	7150	6683	1	11		
559	Trave	7750	5805	1	11		
560	Trave	6718	6014	1	11		
561	Trave	4205	1333	1	11		
562	Trave	7770	2701	1	11		
563	Trave	6684	6846	1	11		
564	Trave	7595	7720	1	11		
565	Trave	5390	5676	1	11		
566	Trave	6429	6475	1	11		
567	Trave	8114	7957	1	11		
568	Trave	6720	5775	1	11		
569	Trave	3691	3707	1	11		
570	Trave	7997	7998	1	11		
571	Trave	5034	5018	1	11		
572	Trave	5020	4924	1	11		
573	Trave	4302	4256	1	11		
574	Trave	5978	5962	1	11		
575	Trave	3823	3821	1	11		
576	Trave	5930	5884	1	11		
577	Trave	5021	4975	1	11		
578	Trave	4051	3989	1	11		
579	Trave	7160	7150	1	11		
580	Trave	7760	7750	1	11		
581	Trave	4206	4205	1	11		
582	Trave	7780	7770	1	11		
583	Trave	7730	7595	1	11		
584	Trave	8057	8058	1	11		

585	Trave	4173	7800	1	11
586	Trave	6846	4432	1	11
587	Trave	7710	2512	1	11
588	Trave	5676	5982	1	11
589	Trave	6475	6511	1	11
590	Trave	3707	3723	1	11
591	Trave	7998	4432	1	11
592	Trave	5050	5034	1	11
593	Trave	5136	5020	1	11
594	Trave	4348	4302	1	11
595	Trave	5994	5978	1	11
596	Trave	7919	3823	1	11
597	Trave	5966	5930	1	11
598	Trave	5067	5021	1	11
599	Trave	4100	4051	1	11
600	Trave	7170	7160	1	11
601	Trave	7740	7730	1	11
602	Trave	4542	7860	1	11
603	Trave	7720	7710	1	11
604	Trave	8058	8069	1	11
605	Trave	7790	2822	1	11
606	Trave	5982	6318	1	11
607	Trave	6511	6557	1	11
608	Trave	3723	3739	1	11
609	Trave	5066	5050	1	11
610	Trave	5262	5136	1	11
611	Trave	4384	4348	1	11
612	Trave	6010	5994	1	11
613	Trave	6012	5966	1	11
614	Trave	5103	5067	1	11
615	Trave	4197	4100	1	11
616	Trave	7180	7170	1	11
617	Trave	4717	7880	1	11
618	Trave	7800	7790	1	11
619	Trave	7810	4173	1	11
620	Trave	8069	8089	1	11
621	Trave	6318	6544	1	11
622	Trave	6557	6603	1	11
623	Trave	3739	3755	1	11
624	Trave	5082	5066	1	11
625	Trave	5358	5262	1	11
626	Trave	4430	4384	1	11
627	Trave	6026	6010	1	11
628	Trave	6048	6012	1	11
629	Trave	5149	5103	1	11
630	Trave	4259	4197	1	11
631	Trave	7190	7180	1	11
632	Trave	7890	4717	1	11
633	Trave	7820	7810	1	11
634	Trave	7870	4542	1	11
635	Trave	8078	7997	1	11
636	Trave	6544	4220	1	11
637	Trave	6603	6639	1	11
638	Trave	3755	3771	1	11
639	Trave	5098	5082	1	11
640	Trave	5484	5358	1	11
641	Trave	4476	4430	1	11
642	Trave	6042	6026	1	11
643	Trave	6094	6048	1	11
644	Trave	5195	5149	1	11
645	Trave	4308	4259	1	11
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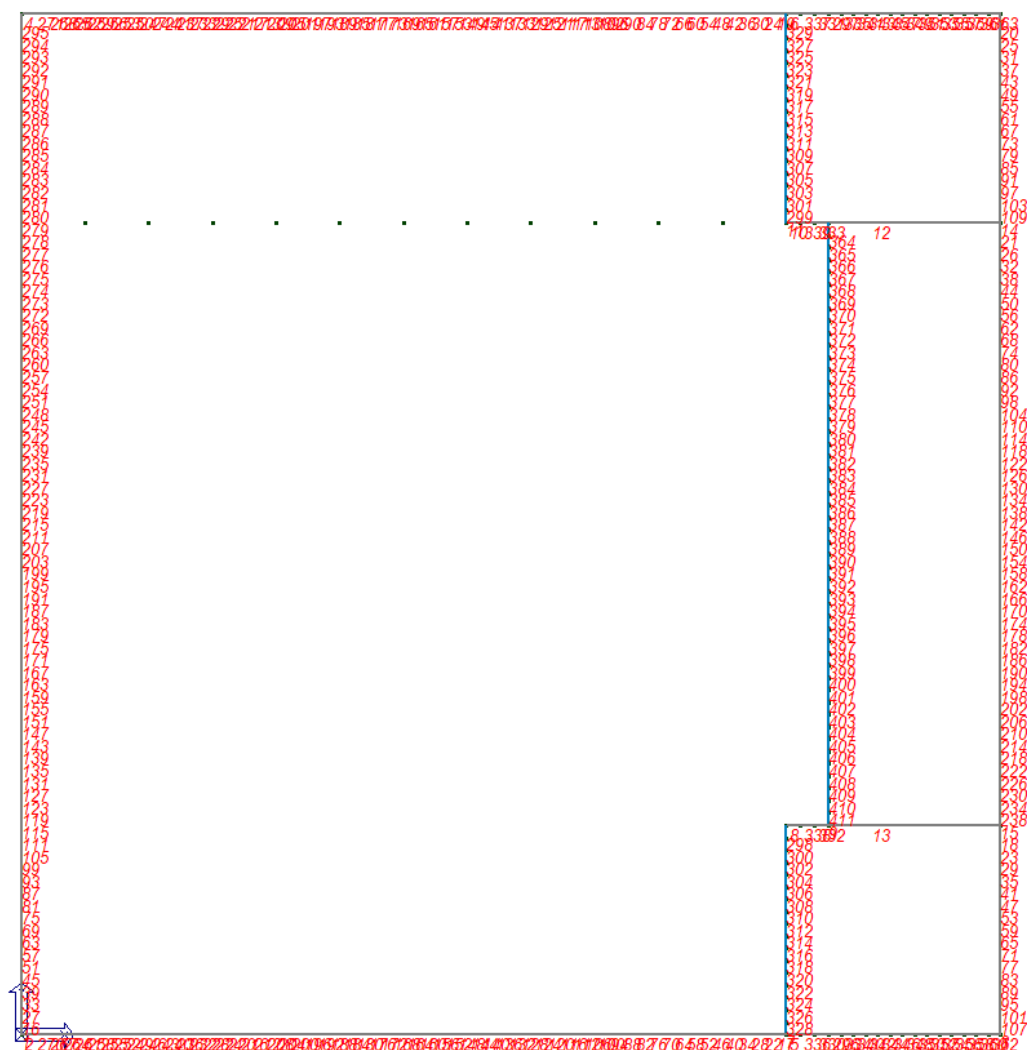
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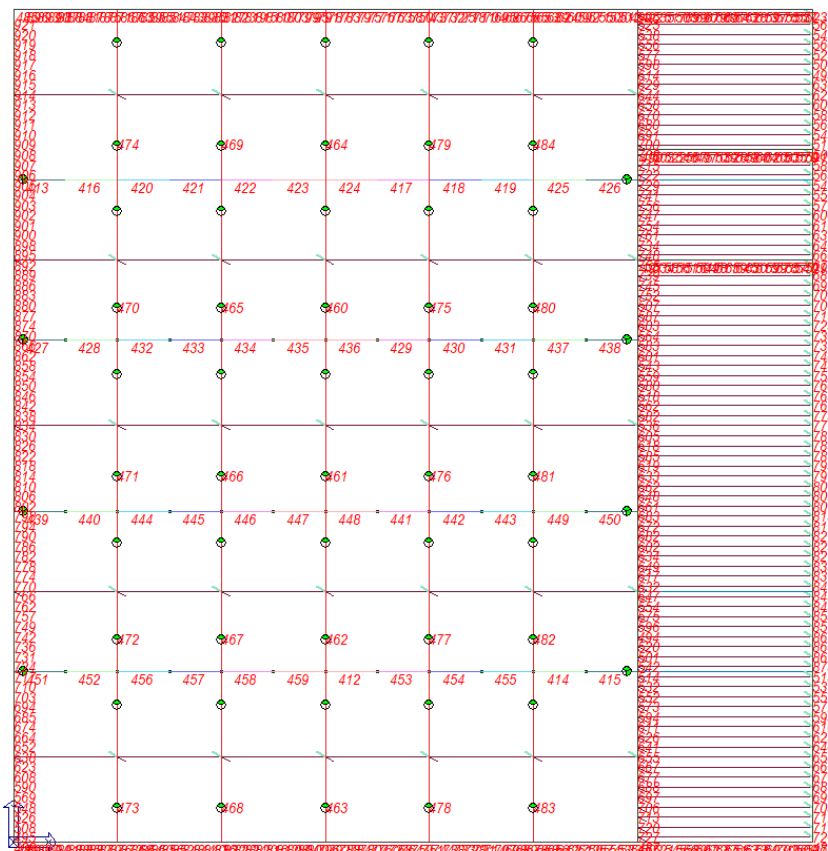
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1134	Trave	224	234	1	12
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1136	Trave	1648	1638	1	12
1137	Trave	5855	5611	1	13
1138	Trave	2388	2378	1	12
1139	Trave	234	244	1	12
1140	Trave	1070	1060	1	12
1141	Trave	1658	1648	1	12
1142	Trave	7292	7291	1	13
1143	Trave	2398	2388	1	12
1144	Trave	7940	22	1	13
1145	Trave	244	254	1	12
1146	Trave	1080	1070	1	12
1147	Trave	1668	1658	1	12
1148	Trave	7411	7292	1	13
1149	Trave	2408	2398	1	12
1150	Trave	7952	7941	1	13
1151	Trave	7284	5855	1	13
1152	Trave	254	264	1	12
1153	Trave	1090	1080	1	12
1154	Trave	1678	1668	1	12
1155	Trave	7412	7411	1	13
1156	Trave	2418	2408	1	12
1157	Trave	5599	7952	1	13
1158	Trave	7291	7284	1	13
1159	Trave	7941	7940	1	13
1160	Trave	264	274	1	12
1161	Trave	1100	1090	1	12
1162	Trave	1688	1678	1	12
1163	Trave	2428	2418	1	12
1164	Trave	5611	5599	1	13
1165	Trave	274	284	1	12
1166	Trave	1110	1100	1	12
1167	Trave	1698	1688	1	12
1168	Trave	2438	2428	1	12
1169	Trave	284	294	1	12
1170	Trave	1120	1110	1	12
1171	Trave	1708	1698	1	12
1172	Trave	2448	2438	1	12
1173	Trave	294	304	1	12
1174	Trave	1130	1120	1	12
1175	Trave	1718	1708	1	12
1176	Trave	2458	2448	1	12
1177	Trave	304	314	1	12
1178	Trave	1140	1130	1	12
1179	Trave	1728	1718	1	12
1180	Trave	2468	2458	1	12
1181	Trave	314	324	1	12
1182	Trave	1150	1140	1	12
1183	Trave	1738	1728	1	12
1184	Trave	2478	2468	1	12
1185	Trave	324	334	1	12
1186	Trave	1160	1150	1	12
1187	Trave	1748	1738	1	12
1188	Trave	2488	2478	1	12
1189	Trave	334	344	1	12
1190	Trave	1170	1160	1	12

1191	Trave	1758	1748	1	12
1192	Trave	2498	2488	1	12
1193	Trave	344	354	1	12
1194	Trave	1180	1170	1	12
1195	Trave	1768	1758	1	12
1196	Trave	2508	2498	1	12
1197	Trave	354	364	1	12
1198	Trave	1190	1180	1	12
1199	Trave	1778	1768	1	12
1200	Trave	2518	2508	1	12
1201	Trave	364	374	1	12
1202	Trave	1200	1190	1	12
1203	Trave	1788	1778	1	12
1204	Trave	2528	2518	1	12
1205	Trave	374	384	1	12
1206	Trave	1210	1200	1	12
1207	Trave	1798	1788	1	12
1208	Trave	2538	2528	1	12
1209	Trave	384	394	1	12
1210	Trave	1220	1210	1	12
1211	Trave	1808	1798	1	12
1212	Trave	2548	2538	1	12
1213	Trave	394	404	1	12
1214	Trave	1230	1220	1	12
1215	Trave	1818	1808	1	12
1216	Trave	2558	2548	1	12
1217	Trave	404	414	1	12
1218	Trave	1240	1230	1	12
1219	Trave	1828	1818	1	12
1220	Trave	2568	2558	1	12
1221	Trave	414	424	1	12
1222	Trave	1250	1240	1	12
1223	Trave	1838	1828	1	12
1224	Trave	2578	2568	1	12
1225	Trave	424	434	1	12
1226	Trave	1260	1250	1	12
1227	Trave	1848	1838	1	12
1228	Trave	2588	2578	1	12
1229	Trave	434	444	1	12
1230	Trave	1270	1260	1	12
1231	Trave	1858	1848	1	12
1232	Trave	2598	2588	1	12
1233	Trave	444	454	1	12
1234	Trave	1280	1270	1	12
1235	Trave	1868	1858	1	12
1236	Trave	2608	2598	1	12
1237	Trave	454	464	1	12
1238	Trave	1290	1280	1	12
1239	Trave	1878	1868	1	12
1240	Trave	2618	2608	1	12
1241	Trave	464	474	1	12
1242	Trave	1300	1290	1	12
1243	Trave	1888	1878	1	12
1244	Trave	2628	2618	1	12
1245	Trave	474	484	1	12
1246	Trave	1310	1300	1	12
1247	Trave	1898	1888	1	12
1248	Trave	2638	2628	1	12
1249	Trave	484	494	1	12
1250	Trave	1320	1310	1	12
1251	Trave	1908	1898	1	12
1252	Trave	2648	2638	1	12
1253	Trave	494	504	1	12
1254	Trave	1330	1320	1	12
1255	Trave	1918	1908	1	12
1256	Trave	2658	2648	1	12
1257	Trave	504	514	1	12
1258	Trave	1340	1330	1	12
1259	Trave	1928	1918	1	12
1260	Trave	2668	2658	1	12
1261	Trave	514	524	1	12
1262	Trave	1350	1340	1	12
1263	Trave	1938	1928	1	12
1264	Trave	2678	2668	1	12
1265	Trave	524	534	1	12
1266	Trave	1360	1350	1	12
1267	Trave	1948	1938	1	12
1268	Trave	2688	2678	1	12
1269	Trave	534	544	1	12
1270	Trave	1370	1360	1	12
1271	Trave	1958	1948	1	12
1272	Trave	2698	2688	1	12
1273	Trave	544	554	1	12
1274	Trave	1380	1370	1	12
1275	Trave	1968	1958	1	12
1276	Trave	2708	2698	1	12
1277	Trave	554	564	1	12
1278	Trave	1390	1380	1	12
1279	Trave	1978	1968	1	12
1280	Trave	564	574	1	12
1281	Trave	1400	1390	1	12
1282	Trave	1988	1978	1	12
1283	Trave	574	584	1	12
1284	Trave	1410	1400	1	12
1285	Trave	1998	1988	1	12
1286	Trave	584	594	1	12
1287	Trave	1420	1410	1	12
1288	Trave	2008	1998	1	12
1289	Trave	594	604	1	12
1290	Trave	1430	1420	1	12
1291	Trave	2018	2008	1	12

1292	Trave	604	614	1	12
1293	Trave	1440	1430	1	12
1294	Trave	2028	2018	1	12
1295	Trave	614	624	1	12
1296	Trave	1450	1440	1	12
1297	Trave	2038	2028	1	12
1298	Trave	624	634	1	12
1299	Trave	1460	1450	1	12
1300	Trave	2048	2038	1	12
1301	Trave	634	644	1	12
1302	Trave	2058	2048	1	12
1303	Trave	644	654	1	12
1304	Trave	654	664	1	12
1305	Trave	664	674	1	12
1306	Trave	674	684	1	12
1307	Trave	684	694	1	12
1308	Trave	694	704	1	12
1309	Trave	704	714	1	12
1310	Trave	714	724	1	12
1311	Trave	724	734	1	12
1312	Trave	734	744	1	12
1313	Trave	744	754	1	12
1314	Trave	754	764	1	12
1315	Trave	764	774	1	12
1316	Trave	774	784	1	12
1317	Trave	784	794	1	12
1318	Trave	794	804	1	12
1319	Trave	804	814	1	12
1320	Trave	814	824	1	12
1321	Trave	824	834	1	12
1322	Trave	834	844	1	12
1323	Trave	844	854	1	12
1324	Trave	854	17	1	12

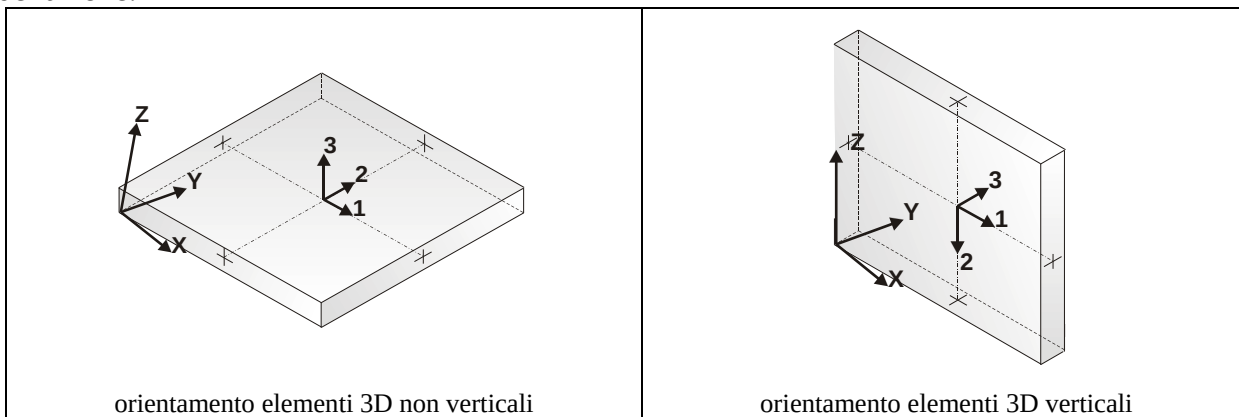


Fondazioni

*Solaio di piano**Copertura*

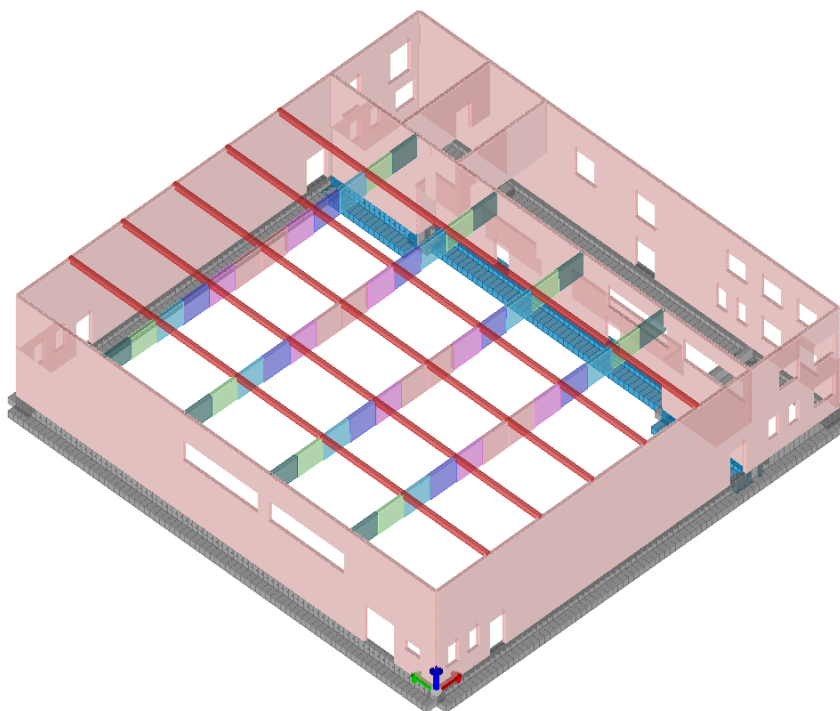
MODELLAZIONE STRUTTURA: ELEMENTI SHELL

Il programma utilizza per la modellazione elementi a tre o quattro nodi denominati in generale shell. Ogni elemento shell è individuato dai nodi I, J, K, L ($L=I$ per gli elementi a tre nodi). Ogni elemento è caratterizzato da un insieme di proprietà riportate in tabella che ne completano la modellazione.



In particolare per ogni elemento viene indicato in tabella:

Elem.	numero dell'elemento
Note	codice di comportamento: <i>Guscio</i> (elemento guscio in elevazione non verticale) <i>Guscio fond.</i> (elemento guscio su suolo elastico) <i>Setto</i> (elemento guscio in elevazione verticale) <i>Membrana</i> (elemento guscio con comportamento membranale)
Nodo I (J, K, L)	numero del nodo I (J, K, L)
Mat.	codice del materiale assegnato all'elemento
Spessore	spessore dell'elemento (costante)
Wink V	costante di sottofondo (coefficiente di Winkler) per la modellazione del suolo elastico verticale
Wink O	costante di sottofondo (coefficiente di Winkler) per la modellazione del suolo elastico orizzontale



MODELLAZIONE DELLA STRUTTURA: ELEMENTI SOLAIO-PANNELLO

Il programma utilizza per la modellazione elementi a tre o più nodi denominati in generale solaio o pannello.

Ogni elemento solaio-pannello è individuato da una poligonale di nodi 1,2, ..., N.

L'elemento solaio è utilizzato in primo luogo per la modellazione dei carichi agenti sugli elementi strutturali. In secondo luogo può essere utilizzato per la corretta ripartizione delle forze orizzontali agenti nel proprio piano. L'elemento balcone è derivato dall'elemento solaio.

I carichi agenti sugli elementi solaio, raccolti in un archivio, sono direttamente assegnati agli elementi utilizzando le informazioni raccolte nell'archivio (es. i coefficienti combinatori). La tabella seguente riporta i dati utilizzati per la definizione dei carichi e delle masse.

L'elemento pannello è utilizzato solo per l'applicazione dei carichi, quali pesi delle tamponature o spinte dovute al vento o terre. In questo caso i carichi sono applicati in analogia agli altri elementi strutturali (si veda il cap. SCHEMATIZZAZIONE DEI CASI DI CARICO).

Id.Arch.	Identificativo dell'archivio
Tipo	Tipo di carico Variab. Carico variabile generico Var. rid. Carico variabile generico con riduzione in funzione dell'area (c.5.5. ...) Neve Carico
G1k	carico permanente (comprensivo del peso proprio)
G2k	carico permanente non strutturale e non compiutamente definito
Qk	carico variabile
Fatt. A	fattore di riduzione del carico variabile (0.5 o 0.75) per tipo "Var.rid."
S sis.	fattore di riduzione del carico variabile per la definizione delle masse sismiche per D.M. 96 (vedi NOTA sul capitolo "normativa di riferimento")
Psi 0	Coefficiente combinatorio dei valori caratteristici delle azioni variabili: per valore raro
Psi 1	Coefficiente combinatorio dei valori caratteristici delle azioni variabili: per valore frequente
Psi 2	Coefficiente combinatorio dei valori caratteristici delle azioni variabili: per valore quasi permanente
Psi S 2	Coefficiente di combinazione che fornisce il valore quasi-permanente dell'azione variabile: per la definizione delle masse sismiche
Fatt. Fi	Coefficiente di correlazione dei carichi per edifici

Ogni elemento è caratterizzato da un insieme di proprietà riportate in tabella che ne completano la modellazione. In particolare per ogni elemento viene indicato in tabella:

Elem	numero dell'elemento
Tipo	codice di comportamento S elemento utilizzato solo per scarico C elemento utilizzato per scarico e per modellazione piano rigido P elemento utilizzato come pannello M scarico monodirezionale B scarico bidirezionale
Id.Arch.	Identificativo dell'archivio
Mat	codice del materiale assegnato all'elemento
Spessore	spessore dell'elemento (costante)
Orditura	angolo (rispetto all'asse X) della direzione dei travetti principali
Gk	carico permanente solaio (comprensivo del peso proprio)
Qk	carico variabile solaio
Nodi	numero dei nodi che definiscono l'elemento (5 per riga)

Nel caso in cui si sia proceduto alla progettazione dei solai con le tensioni ammissibili vengono riportate le massime tensioni nell'elemento (massima compressione nel calcestruzzo, massima tensione nell'acciaio, massima tensione tangenziale); nel caso in cui si sia proceduto alla

progettazione con il metodo degli stati limite vengono riportati il rapporto x/d e le verifiche per sollecitazioni proporzionali nonché le verifiche in esercizio.

In particolare i simboli utilizzati in tabella assumono il seguente significato:

Elem.	numero identificativo dell'elemento
Stato	Codici di verifica relativi alle tensioni normali e alle tensioni tangenziali
Note	Viene riportato il codice relativo alla sezione(s) e relativo al materiale(m);
Pos.	Ascissa del punto di verifica
F ist, F infi	Frecce istantanee e a tempo infinito
Momento	Momento flettente
Taglio	Sollecitazione di taglio
Af inf.	Area di armatura longitudinale posta all'intradosso della trave
Af sup.	Area di armatura longitudinale posta all'estradosso della trave
AfV	Area dell'armatura atta ad assorbire le azioni di taglio
Beff	Base della sezione di cls per l'assorbimento del taglio
simboli utilizzati con il metodo delle tensioni ammissibili:	
sc max	Massima tensione di compressione del calcestruzzo
sf max	Massima tensione nell'acciaio
tau max	Massima tensione tangenziale nel cls
simboli utilizzati con il metodo degli stati limite:	
x/d	rapporto tra posizione dell'asse neutro e altezza utile alla rottura della sezione (per sola flessione)
verif.	rapporto S_d/S_u con sollecitazioni ultime proporzionali: valore minore o uguale a 1 per verifica positiva
Verif.V	rapporto S_d/S_u con sollecitazioni taglianti proporzionali: valore minore o uguale a 1 per verifica positiva
rRfck	rapporto tra la massima compressione nel calcestruzzo e la tensione f_{ck} in combinazioni rare [normalizzato a 1]
rFfck	rapporto tra la massima compressione nel calcestruzzo e la tensione f_{ck} in combinazioni frequenti [normalizzato a 1]
rPfck	rapporto tra la massima compressione nel calcestruzzo e la tensione f_{ck} in combinazioni quasi permanenti [normalizzato a 1]
rRfyk	rapporto tra la massima tensione nell'acciaio e la tensione f_{yk} in combinazioni frequenti [normalizzato a 1]
rFyk	rapporto tra la massima tensione nell'acciaio e la tensione f_{yk} in combinazioni rare [normalizzato a 1]
rPfyk	rapporto tra la massima tensione nell'acciaio e la tensione f_{yk} in combinazioni quasi permanenti [normalizzato a 1]
wR	apertura caratteristica delle fessure in combinazioni rare
wF	apertura caratteristica delle fessure in combinazioni frequenti [mm]
wP	apertura caratteristica delle fessure in combinazioni quasi permanenti [mm]

Nel caso in cui si sia proceduto alla verifica delle tamponature secondo il D.M. 17.01.2018 - §7.2.3 viene riportata una tabella riassuntiva delle verifiche degli elementi pannello. La verifica confronta i momenti sollecitanti indotti dal sisma con i momenti resistenti, secondo tre ipotesi, due basate sulla resistenza a pressoflessione della tamponatura ed una basata sul cinematismo a seguito della formazione di tre cerniere plastiche sulla tamponatura (rif. Ufficio di Vigilanza sulle Costruzioni, Provincia di Terni).

Qualora la tamponatura sia di tipo antiespulsione (nelle due possibili varianti ordinaria o armata) viene condotta una verifica con meccanismo ad arco con degrado di resistenza. La verifica confronta le pressioni sollecitanti indotte dal sisma con le pressioni resistenti che la tamponatura

sviluppa attraverso il meccanismo ad arco. La verifica considera anche il degrado di resistenza dovuto al danneggiamento nel piano della tamponatura.

Per quest'ultima tamponatura sono disponibili, in funzione del materiale impiegato (materiale [52] o materiale [53]):

- **Tamponatura Antiespulsione ordinaria Poroton® Cis Edil** sp.30 cm; con metodo di verifica per meccanismo ad arco con degrado di resistenza, sviluppato attraverso i risultati di un progetto di ricerca sperimentale condotto dall'Università degli Studi di Padova.
Utilizzabile per il materiale [52].
- **Tamponatura Antiespulsione armata Poroton® Cis Edil** sp.30 cm; con metodo di verifica per meccanismo ad arco con degrado di resistenza, sviluppato attraverso i risultati di un progetto di ricerca sperimentale condotto dall'Università degli Studi di Padova.
Utilizzabile per il materiale [53].

La verifica è stata calibrata sulla base di prove sperimentali sul sistema di Tamponatura Antiespulsione anche in presenza di aperture.

(rif. Rapporti di Prova redatti dal Dipartimento ICEA - Università degli Studi di Padova di test sperimentali condotti sul sistema Tamponatura Antiespulsione di Cis Edil)

In particolare i simboli utilizzati in tabella assumono il seguente significato:

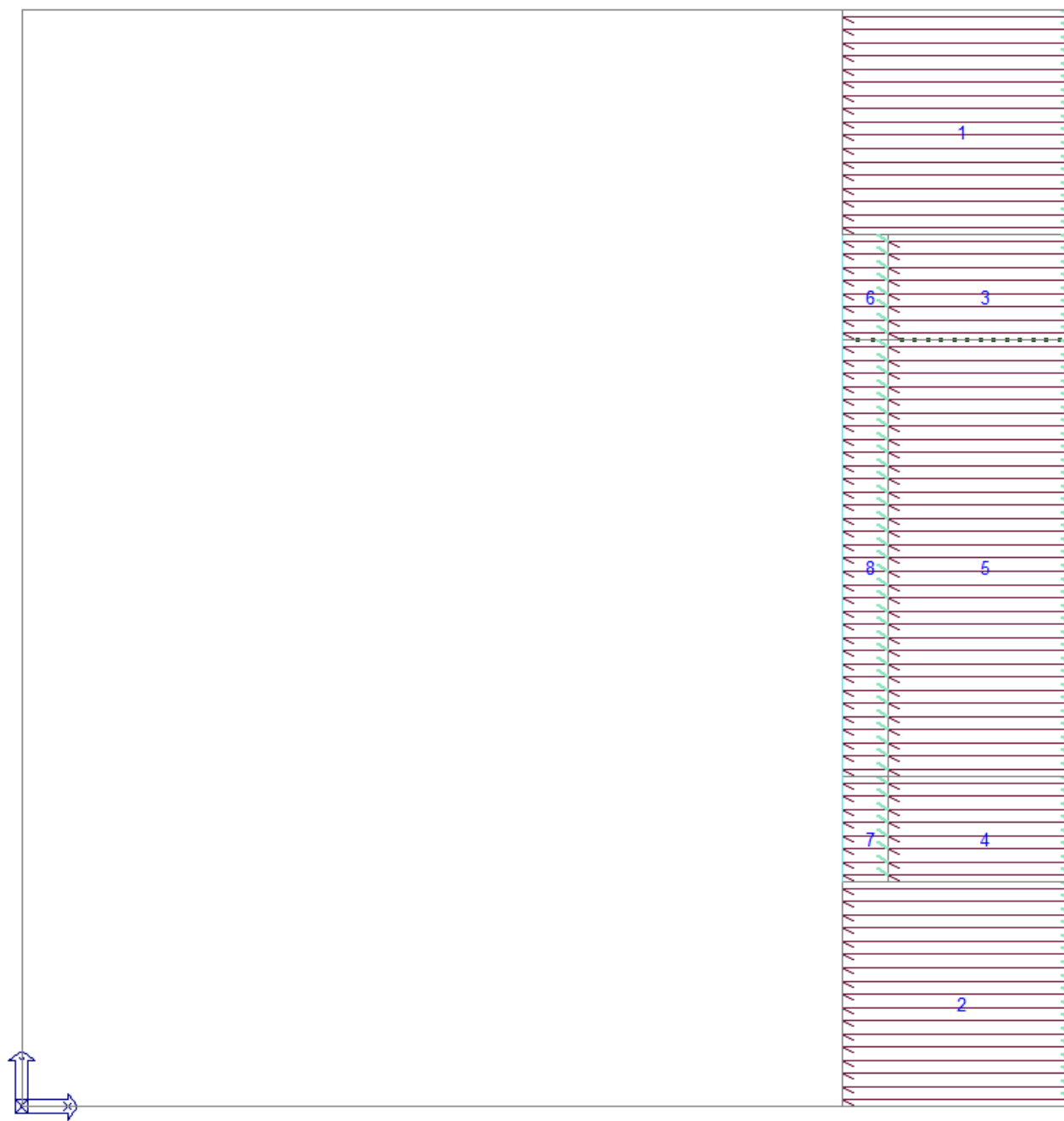
Elem.	Numero identificativo dell'elemento
Stato	Codice di verifica
Ver. c.c.	Verifica nell'ipotesi di trave appoggiata con carico concentrato in mezzzeria
Ver. c.d.	Verifica nell'ipotesi di trave appoggiata con carico distribuito
Ver. c.cin.	Verifica nell'ipotesi di cinematismo con formazione di cerniere plastiche in appoggio e mezzzeria
Ver. CIS	Rapporto p_a/p_r (valore minore o uguale a 1 per verifica positiva)
Z	Quota del baricentro dell'elemento
T1	Periodo proprio dell'edificio nella direzione di interesse (ortogonale al pannello)
Ta	Periodo proprio della parete
Sa	Accelerazione massima, adimensionalizzata allo SLV
p_a	Pressione sulla parete causata dall'azione sismica
p_r	Pressione resistente del meccanismo ad arco
Drift	Spostamento relativo interpiano allo SLV valutato secondo il D.M. 14.01.2018 - § 7.3.3.3
Beta a	Coef. riduttivo per tener conto del danneggiamento del piano dipendente dallo spostamento, ottenuto sperimentalmente

ID Arch.	Tipo	G1k	G2k	Qk	Fatt. A	s sis.	Psi 0	Psi 1	Psi 2	Psi S 2	Fatt. Fi
1	Variab.	daN/cm2 5.00e-02	daN/cm2 2.80e-02	daN/cm2 3.00e-02		1.00	0.70	0.50	0.30	0.30	1.00
2	Variab.	5.00e-02	3.00e-02	2.00e-02		1.00	0.70	0.50	0.30	0.30	1.00
3	Neve	5.00e-03		1.20e-02		1.00	0.50	0.20	0.0	0.0	1.00

Elem.	Tipo	ID Arch.	Mat.	Spessore	Orditura	G1k	G2k	Qk	Nodo 1/6..	Nodo 2/7..	Nodo 3/8..	Nodo..	Nodo..
1	CM	1	m=1	6.0	0.0	daN/cm2 5.00e-02	daN/cm2 2.80e-02	daN/cm2 3.00e-02	3058	3048	3038	3028	3018
									3008	2998	2988	2978	2968
									2958	2948	2938	2928	2918
									2908	22	3256	3246	24
									2228	2218	2208	2198	2188
									2178	2168	2158	2148	2138
									2128	2118	2108	2098	2088
									2078	2061	18	3602	3592
									3582	3572	3562	3552	3542
									3532	3522	3512	3502	3492
									3482	3331	3332	3342	20
2	CM	1	m=1	6.0	0.0	5.00e-02	2.80e-02	3.00e-02	3076	3086	3096	3106	3116
									3126	3136	3146	3156	3166
									3176	3186	3196	3206	3216
									3226	19	3313	3303	3302
									3352	3362	3372	3382	3392

									3402	3412	3422	3432	3442
									3452	3462	3472	16	2878
									2868	2858	2848	2838	2828
									2818	2808	2798	2788	2778
									2768	2758	2748	2738	2728
									2718	23	3274	3284	21
3	CM	1	m=1	6.0	0.0	5.00e-02	2.80e-02	3.00e-02	6866	6876	6886	6896	6906
									6916	6926	6936	2308	2298
									2288	2278	2268	2258	2248
									2238	2228	24		
4	CM	1	m=1	6.0	0.0	5.00e-02	2.80e-02	3.00e-02	3966	3996	4016	4046	4076
									4096	4126	23	2718	2708
									2698	2688	2678	2668	2658
									2648	2638	3936		
5	CM	1	m=1	6.0	0.0	5.00e-02	2.80e-02	3.00e-02	6946	6956	6966	6976	6986
									6996	7006	7016	7026	7036
									7046	7056	7066	7076	7086
									7096	7106	7116	7126	7136
									3626	3646	3676	3696	3726
									3756	3776	3806	3836	3856
									3886	3916	3936	2638	2628
									2618	2608	2598	2588	2578
									2568	2558	2548	2538	2528
									2518	2508	2498	2488	2478
									2468	2458	2448	2438	2428
									2418	2408	2398	2388	2378
									2368	2358	2348	2338	2328
									2318	2308	6936		
6	CM	1	m=1	6.0	0.0	5.00e-02	2.80e-02	3.00e-02	7940	7941	7952	5599	5611
									5855	7284	7291	6936	6926
									6916	6906	6896	6886	6876
									6866	24	3246	3256	22
7	CM	1	m=1	6.0	0.0	5.00e-02	2.80e-02	3.00e-02	4753	3822	6990	6991	1944
									1949	1479	21	3284	3274
									23	4126	4096	4076	4046
									4016	3996	3966	3936	4752
8	CM	1	m=1	6.0	0.0	5.00e-02	2.80e-02	3.00e-02	7291	7292	7411	7412	7413
									2513	2514	2515	7603	7604
									7605	5806	5807	5931	2702
									2750	2751	2830	2831	2832
									4175	4625	4636	7896	7904
									7905	4368	4369	4380	4543
									4544	4588	4718	4752	3936
									3916	3886	3856	3836	3806
									3776	3756	3726	3696	3676
									3646	3626	7136	7126	7116
									7106	7096	7086	7076	7066
									7056	7046	7036	7026	7016
									7006	6996	6986	6976	6966
									6956	6946	6936		
9	CM	2	m=1	6.0	0.0	5.00e-02	3.00e-02	2.00e-02	3821	3823	7919	1943	7929
									2035	7939	4193	4781	7620
									7610	7600	7590	7580	7570
									7560	7550	7900		
10	CM	2	m=1	6.0	0.0	5.00e-02	3.00e-02	2.00e-02	7628	7949	7638	7648	7658
									7281	7668	7678	3347	6654
									6620	80	139	121	157
									4355	4293	4244	4195	4085
									4036	3987	3925	3437	7218
									7208	7198	7188	7178	7168
									7158	7148	6669	5581	
11	CM	2	m=1	6.0	0.0	5.00e-02	3.00e-02	2.00e-02	4204	4256	4302	4348	4384
									4430	4476	4512	4558	4604
									4640	4686	4732	4768	4814
									4860	5923	6347	6383	6429
									6475	6511	6557	6603	6639
									6685	6731	6767	6813	6859
									4225	4351	4477	4573	6508
									6382	6316	6190	6064	5968
									5852	5726	5660	5484	5358
									5262	5136	5020	4924	4782
									4781	4193			
12	CM	2	m=1	6.0	0.0	5.00e-02	3.00e-02	2.00e-02	7404	7690	7700	2512	7710
									7720	7595	7730	7740	5805
									7750	7760	7701	7770	7780
									2822	7790	7800	4173	7810

									7820	7895	7830	7840	7935
									7850	7860	4542	7870	7880
									4717	7890	7900	7550	7540
									7530	7520	7510	7500	7490
									7480	7470	7460	7450	7440
									7430	7420	7410	7400	7390
									7380	7370	7360	7350	7340
									7330	7320	7310	7300	7290
									7280	7270	7260	7250	7240
									7230	7220	3457	3940	3989
									4051	4100	4197	4259	4308
									4357	159	127	141	1333
									4205	4206	3349	7680	
13	CM	2	m=1	6.0	0.0	5.00e-02	3.00e-02	2.00e-02	4895	4941	4987	5023	5069
									5115	5151	5197	5243	5279
									5325	5371	5407	5453	5499
									5535	5581	6669	6670	6844
									4350	4816	5052	5308	5664
									5980	6236	6542	6848	4864
									5790	6716	5392	6108	5771
									5772	5836	5872	5928	5964
									6000	6046	6092	6128	6174
									6220	6256	6302	5643	5644
									5708	4959			
14	SM	3	m=58	20.0	0.0	5.00e-03		1.20e-02	3479	3517	3518	881	885
									884				
15	SM	3	m=58	20.0	0.0	5.00e-03		1.20e-02	5627	3478	3479	884	883
									886				
16	SM	3	m=58	20.0	0.0	5.00e-03		1.20e-02	4411	5615	5627	886	906
									4667				
17	SM	3	m=58	20.0	0.0	5.00e-03		1.20e-02	3518	6287	6288	893	891
									881				
18	SM	3	m=58	20.0	0.0	5.00e-03		1.20e-02	6288	6299	3477	904	903
									893				
19	SM	3	m=58	20.0	0.0	5.00e-03		1.20e-02	3477	3519	7730	5579	905
									904				
20	SM	3	m=58	20.0	0.0	5.00e-03		1.20e-02	3569	5869	5903	6288	6287
									3518				
21	SM	3	m=58	20.0	0.0	5.00e-03		1.20e-02	5950	5951	3569	3518	3517
									3479				
22	SM	3	m=58	20.0	0.0	5.00e-03		1.20e-02	5868	5949	5950	3479	3478
									5627				
23	SM	3	m=58	20.0	0.0	5.00e-03		1.20e-02	4139	5867	5868	5627	5615
									4411				
24	SM	3	m=58	20.0	0.0	5.00e-03		1.20e-02	5903	5904	5925	3477	6299
									6288				
25	SM	3	m=58	20.0	0.0	5.00e-03		1.20e-02	5925	3579	7935	7730	3519
									3477				
26	SM	3	m=58	20.0	0.0	5.00e-03		1.20e-02	894	895	3568	5903	5869
									3569				
27	SM	3	m=58	20.0	0.0	5.00e-03		1.20e-02	3587	3588	894	3569	5951
									5950				
28	SM	3	m=58	20.0	0.0	5.00e-03		1.20e-02	3567	3578	3587	5950	5949
									5868				
29	SM	3	m=58	20.0	0.0	5.00e-03		1.20e-02	3883	3589	3567	5868	5867
									4139				
30	SM	3	m=58	20.0	0.0	5.00e-03		1.20e-02	3568	3577	896	5925	5904
									5903				
31	SM	3	m=58	20.0	0.0	5.00e-03		1.20e-02	896	5613	4193	7935	3579
									5925				
32	SM	3	m=58	20.0	0.0	5.00e-03		1.20e-02	6394	6234	3568	895	894
33	SM	3	m=58	20.0	0.0	5.00e-03		1.20e-02	6554	6394	894	3588	3587
34	SM	3	m=58	20.0	0.0	5.00e-03		1.20e-02	6714	6554	3587	3578	3567
35	SM	3	m=58	20.0	0.0	5.00e-03		1.20e-02	3621	6714	3567	3589	3883
36	SM	3	m=58	20.0	0.0	5.00e-03		1.20e-02	6234	6074	896	3577	3568
37	SM	3	m=58	20.0	0.0	5.00e-03		1.20e-02	6074	5923	4193	5613	896
38	SM	3	m=58	20.0	0.0	5.00e-03		1.20e-02	884	885	881	5434	5594
39	SM	3	m=58	20.0	0.0	5.00e-03		1.20e-02	886	883	884	5594	5754
40	SM	3	m=58	20.0	0.0	5.00e-03		1.20e-02	4667	906	886	5754	4939
41	SM	3	m=58	20.0	0.0	5.00e-03		1.20e-02	881	891	893	5274	5434
42	SM	3	m=58	20.0	0.0	5.00e-03		1.20e-02	893	903	904	5114	5274
43	SM	3	m=58	20.0	0.0	5.00e-03		1.20e-02	904	905	5579	4963	5114

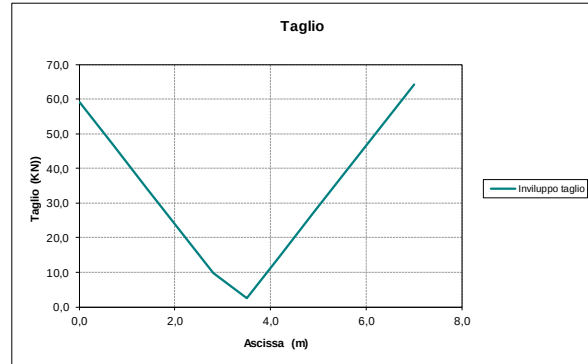
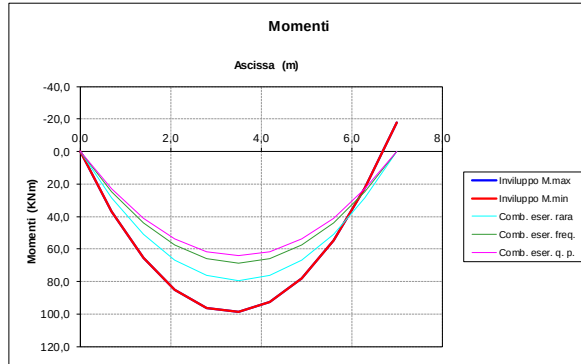
*Solaio di piano*

Solaio primo 1 e 2 ($G=5.0+2.8 \text{ kN/mq}$; $Q=3.0 \text{ kN/mq}$)**Titolo** SOLAIO PRIMO 1 campata

L 7 m
 g 9,4 kN/m
 q 3,6 kN/m

Sezioni di verifica

		0,00	0,70	1,40	2,10	2,80	3,50	4,20	4,90	5,60	6,30	7,00	comb. carico
Involuppo M.max	Msin=-1/ 0 $*(1.3g+1.5q)*L^2$	0,00	37,05	65,47	85,26	96,41	98,93	92,81	78,06	54,68	22,66	-17,99	Mdes=1/ 48 $*(1.3g+1.5q)*L^2$ 17,62
Involuppo M.min	Msin=-1/ 0 $*(1.3g+1.5q)*L^2$	0,00	37,05	65,47	85,26	96,41	98,93	92,81	78,06	54,68	22,66	-17,99	Mdes=1/ 48 $*(1.3g+1.5q)*L^2$ 17,62
Involuppo taglio		59,10	46,77	34,43	22,10	9,76	2,57	14,90	27,24	39,57	51,91	64,24	
Comb. eser. rara	Msin=-1/ 0 $*(g+q)*L^2$	0,00	28,67	50,96	66,89	76,44	79,63	76,44	66,89	50,96	28,67	0,00	Mdes=1/ 0 $*(g+q)*L^2$ 13
Comb. eser. freq.	Msin=-1/ 0 $*(g+0.5q)*L^2$	0,00	24,70	43,90	57,62	65,86	68,60	65,86	57,62	43,90	24,70	0,00	Mdes=1/ 0 $*(g+0.5q)*L^2$ 11,2
Comb. eser. q. p.	Msin=-1/ 0 $*(g+0.3q)*L^2$	0,00	23,11	41,08	53,92	61,62	64,19	61,62	53,92	41,08	23,11	0,00	Mdes=1/ 0 $*(g+0.3q)*L^2$ 10,48

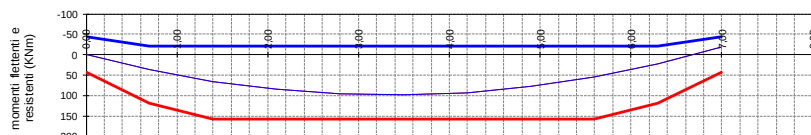


SOLAIO PRIMO 1 campata

Rck	Ec	fcd	fctd	Acciaio tipo	fyd	Bsup	Binf	Sp_ala	h	c	d
MPa	(MPa)	MPa			MPa	cm			cm	cm	cm
30	31220	14,11	1,19	B450C	391	120	40	6	36	2	34

Luce di calcolo (m) **7,00****Verifica agli stati limite ultimi**

Involuppo Momento max											
	0,00	37,05	65,47	85,26	96,41	98,93	92,81	78,06	54,68	22,66	-17,99
Involuppo Momento min											
	0,00	37,05	65,47	85,26	96,41	98,93	92,81	78,06	54,68	22,66	-17,99
As,sup,app	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	150
As,inf,app	0,00	3,30	5,47	7,33	8,06	8,27	7,76	6,52	4,57	189	0,00
X	0,00	0,70	1,40	2,10	2,80	3,50	4,20	4,90	5,60	6,30	7,00
Armatura (cmq)											
φ6		6	6	6	6	6	6	6	6	6	
φ8											
φ10											
φ12	3										3
As,sup	3,39	1,70	1,70	1,70	1,70	1,70	1,70	1,70	1,70	1,70	3,39
As,inf	3,39	9,42	12,57	12,57	12,57	12,57	12,57	12,57	12,57	9,42	3,39
φ5											
φ8											
φ12	3										3
φ20		3	4	4	4	4	4	4	4	3	
Momenti positivi											
b	120,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00
psi	0,07	0,13	0,15	0,15	0,15	0,15	0,15	0,15	0,15	0,13	0,07
M+res	43,84	119,46	157,84	157,84	157,84	157,84	157,84	157,84	157,83	119,46	43,84
Momenti negativi											
b	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00
psi	0,11	0,07	0,07	0,07	0,07	0,07	0,07	0,07	0,07	0,07	0,11
M-res	-43,04	-21,68	-21,66	-21,66	-21,66	-21,66	-21,66	-21,66	-21,66	-21,68	-43,04



VERIFICA ALLO S.L.U. DI TAGLIO											
Vsd	59,10	46,77	34,43	22,10	9,76	2,57	14,90	27,24	39,57	51,91	64,24
ρ ₁	0,0025	0,0069	0,0092	0,0092	0,0092	0,0092	0,0092	0,0092	0,0092	0,0069	0,0025
Bmin	42,37	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	46,06

VERIFICA AGLI S.L. DI ESERCIZIO**Caratteristiche geometriche sezioni**

Per gruppo di esigenze cond. ambientali poco aggressive e armatura poco sensibile:

Beta,1 1,00 K2 0,40 Diam.min. 16 copr.netto 1,20											
Beta,2 0,50 K3 0,13 Sig.SR 101,38 n 15											
As (cmq)	3,39	9,42	12,57	12,57	12,57	12,57	12,57	12,57	12,57	9,42	3,39
A's (cmq)	3,39	1,70	1,70	1,70	1,70	1,70	1,70	1,70	1,70	1,70	3,39
b resistente	40,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	40,00
Y	7,36	7,71	8,75	8,75	8,75	8,75	8,75	8,75	8,75	7,71	7,36
Wc	5829	15150	16939	16939	16939	16939	16939	16939	16939	15150	5829
Ws	1610	4446	5866	5866	5866	5866	5866	5866	5866	4446	1610
N barre	3	3	4	4	4	4	4	4	4	3	3
dist. barre	18,00	22,40	22,40	22,40	22,40	22,40	22,40	22,40	22,40	22,40	18,00
Beff (cm)	40	49	71	71	71	71	71	71	71	49	40
Deff (cm)	13,20	13,20	13,20	13,20	13,20	13,20	13,20	13,20	13,20	13,20	13,20
Aeff	528,00	644,16	939,84	939,84	939,84	939,84	939,84	939,84	939,84	644,16	528,00
RO,r	0,64%	1,46%	1,34%	1,34%	1,34%	1,34%	1,34%	1,34%	1,34%	1,46%	0,64%

Combinazioni di carico											
Rara	0,00	28,67	50,96	66,89	76,44	79,63	76,44	66,89	50,96	28,67	0,00
Frequente	0,00	24,70	43,90	57,62	65,86	68,60	65,86	57,62	43,90	24,70	0,00
Quasi perm.	0,00	23,11	41,08	53,92	61,62	64,19	61,62	53,92	41,08	23,11	0,00

Verifica allo stato limite di tensione in esercizio

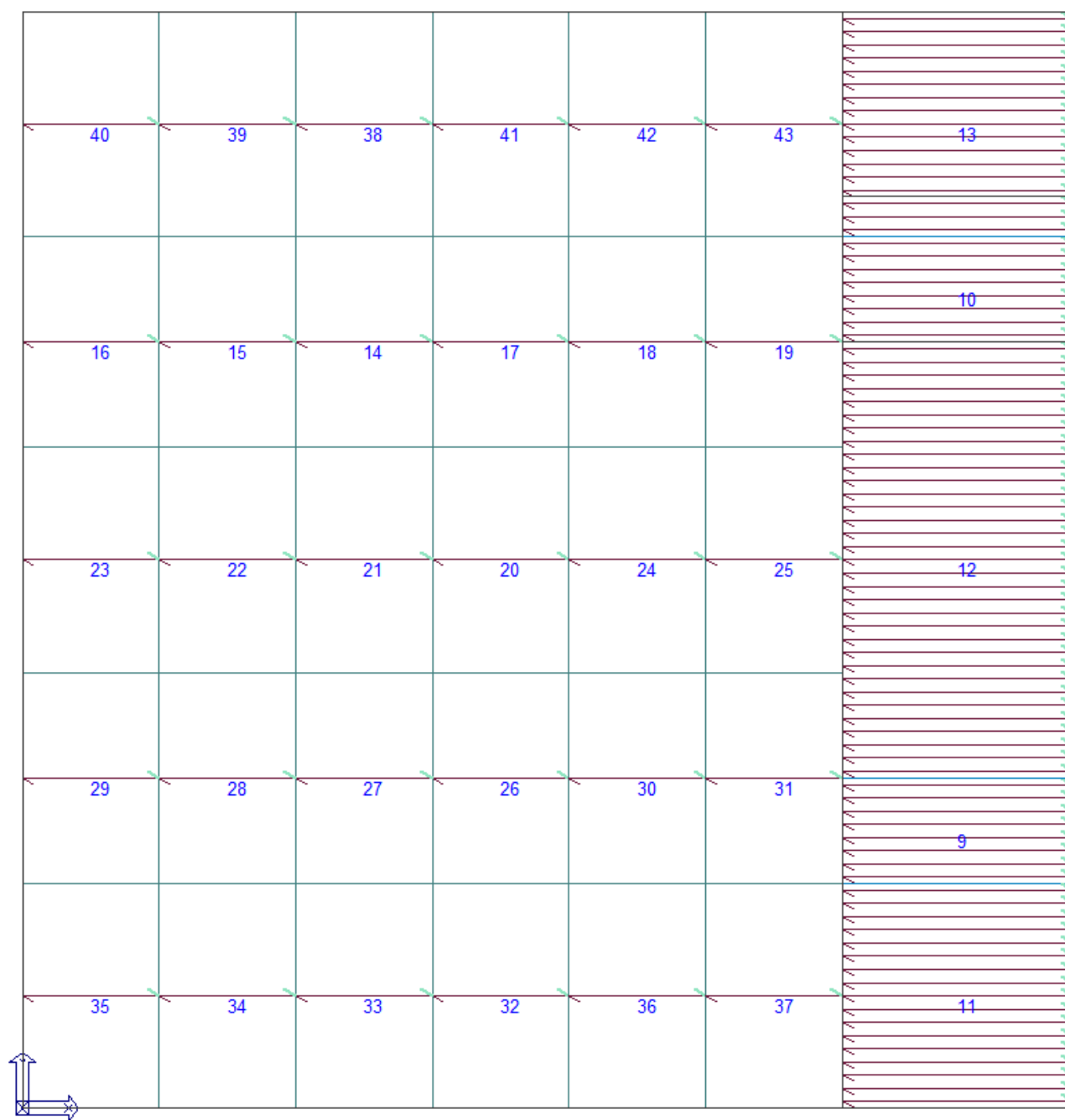
Combinazione rara Sigma,C,amm = 0.60*fck = 14,94 MPa Sigma,S,amm = 0.70*fyk = 315 MPa											
Sigma,C	-0,01	-1,89	-3,01	-3,95	-4,51	-4,70	-4,51	-3,95	-3,01	-1,89	-0,01
Sigma,S	0,01	96,70	130,32	171,04	195,48	203,62	195,48	171,04	130,32	96,70	0,01
Combinazione quasi permanente Sigma,C,amm = 0.45*fck = 11,21 MPa											
Sigma,C	-0,01	-1,53	-2,43	-3,18	-3,64	-3,79	-3,64	-3,18	-2,43	-1,53	-0,01

Verifica allo stato limite di apertura fessure

S _{rm} (mm)	184,49	123,48	128,63	128,63	128,63	128,63	128,63	128,63	128,63	123,48	184,49
Combinazione frequente Apertura limite-W3= 0,20 mm											
Sigma,S	0,10	83,31	112,28	147,36	168,41	175,43	168,41	147,36	112,28	83,31	0,10
Eps,sm	0,000%	0,000%	0,022%	0,039%	0,053%	0,057%	0,053%	0,039%	0,022%	0,000%	0,000%
Wk (mm)	0,000	0,000	0,048	0,084	0,116	0,126	0,116	0,084	0,048	0,000	0,000
Combinazione quasi permanente Apertura limite-W2= 0,20 mm											
Sigma,S	0,10	77,96	105,06	137,89	157,59	164,15	157,59	137,89	105,06	77,96	0,10
Eps,sm	0,000%	0,000%	0,020%	0,032%	0,046%	0,050%	0,046%	0,032%	0,020%	0,000%	0,000%
Wk (mm)	0,000	0,000	0,045	0,069	0,100	0,110	0,100	0,069	0,045	0,000	0,000

Verifica allo stato limite di deformazione**Verifica esatta: combinazione quasi permanente**

EpsCm	0,000%	-0,005%	-0,008%	-0,010%	-0,012%	-0,012%	-0,012%	-0,010%	-0,008%	-0,005%	0,000%
EpsSm	0,000%	0,036%	0,049%	0,066%	0,075%	0,079%	0,075%	0,066%	0,049%	0,036%	0,000%
l/r	0,0000%	-0,0012%	-0,0017%	-0,0022%	-0,0026%	-0,0027%	-0,0026%	-0,0022%	-0,0017%	-0,0012%	0,0000%
rot.	0,0000	-0,0004	-0,0014	-0,0028	-0,0045	-0,0063	-0,0081	-0,0098	-0,0112	-0,0122	-0,0126
frecchia	0,00	-0,01	-0,08	-0,23	-0,48	-0,86	-1,36	-1,99	-2,72	-3,54	-4,41
frecchia	0,000	0,426	0,803	1,096	1,283	1,347	1,283	1,096	0,803	0,426	0,000
frecchia massima:	1,35 cm pari a L/520										
verifica sommaria:	Rapporto di snellezza effettivo l/h = 19,44 < 26,00 Rapporto limite										

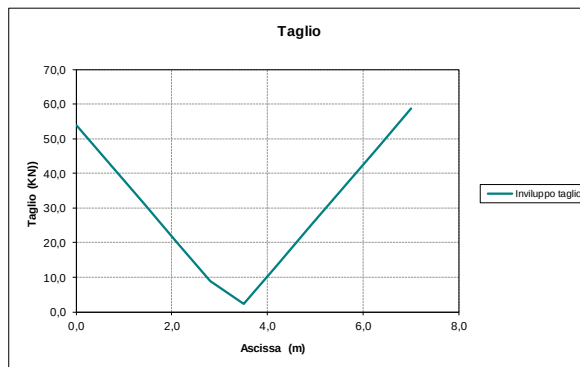
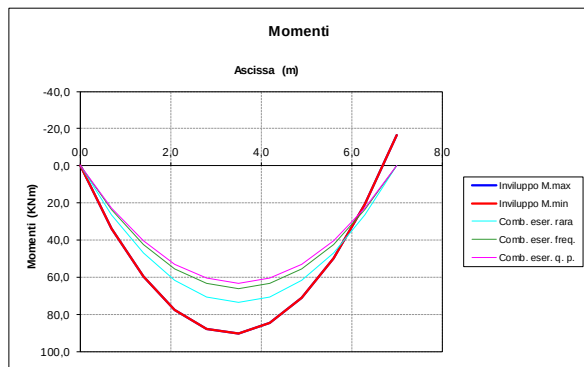
*Solaio di copertura*

Solaio copertura 9 ; 10 ; 11 ; 12 ; 13 ($G=5.0+3.0 \text{ kN/mq}$; $Q=2.0 \text{ kN/mq}$)**Titolo** SOLAIO COPERTURA 1 campata

L 7 m
 g 9,6 kN/m
 q 2,4 kN/m

Sezioni di verifica

		0,00	0,70	1,40	2,10	2,80	3,50	4,20	4,90	5,60	6,30	7,00	comb. carico
Involuppo M.max	Msin=-1/ 0 $*(1.3g+1.5q)*L^2$	0,00	33,81	59,75	77,81	87,98	90,28	84,70	71,24	49,90	20,68	-16,42	Mdes=1/ 48 $*(1.3g+1.5q)*L^2$ 16,08
Involuppo M.min	Msin=-1/ 0 $*(1.3g+1.5q)*L^2$	0,00	33,81	59,75	77,81	87,98	90,28	84,70	71,24	49,90	20,68	-16,42	Mdes=1/ 48 $*(1.3g+1.5q)*L^2$ 16,08
Involuppo taglio		53,94	42,68	31,42	20,17	8,91	2,35	13,60	24,86	36,11	47,37	58,63	
Comb. eser. rara	Msin=-1/ 0 $*(g+q)*L^2$	0,00	26,46	47,04	61,74	70,56	73,50	70,56	61,74	47,04	26,46	0,00	Mdes=1/ 0 $*(g+q)*L^2$ 12
Comb. eser. freq.	Msin=-1/ 0 $*(g+0.5q)*L^2$	0,00	23,81	42,34	55,57	63,50	66,15	63,50	55,57	42,34	23,81	0,00	Mdes=1/ 0 $*(g+0.5q)*L^2$ 10,8
Comb. eser. q. p.	Msin=-1/ 0 $*(g+0.3q)*L^2$	0,00	22,76	40,45	53,10	60,68	63,21	60,68	53,10	40,45	22,76	0,00	Mdes=1/ 0 $*(g+0.3q)*L^2$ 10,32

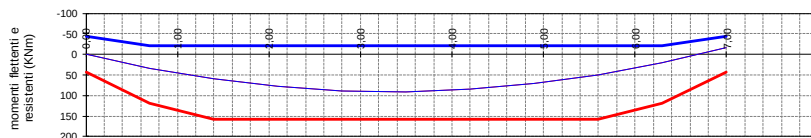


SOLAIO COPERTURA 1 campata

Rck	Ec	fcd	fctd	Acciaio tipo	fyd	Bsup	Binf	Sp_ala	h	c	d
MPa	(MPa)	MPa			MPa	cm			cm	cm	cm
30	31220	14,11	1,19	B450C	391	120	40	6	36	2	34

Luce di calcolo (m) **7,00****Verifica agli stati limite ultimi**

Involuppo Momento max	0,00	33,81	59,75	77,81	87,98	90,28	84,70	71,24	49,90	20,68	-16,42
Involuppo Momento min	0,00	33,81	59,75	77,81	87,98	90,28	84,70	71,24	49,90	20,68	-16,42
As,sup.app	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	137
As,inf.app	0,00	2,83	4,99	6,50	7,35	7,55	7,08	5,95	4,17	1,73	0,00
X	0,00	0,70	1,40	2,10	2,80	3,50	4,20	4,90	5,60	6,30	7,00
Armatura (cmq)											
φ6		6	6	6	6	6	6	6	6	6	
φ8											
φ10											
φ12	3										3
As,sup	3,39	1,70	1,70	1,70	1,70	1,70	1,70	1,70	1,70	1,70	3,39
As,inf	3,39	9,42	12,57	12,57	12,57	12,57	12,57	12,57	12,57	9,42	3,39
φ5											
φ8											
φ12	3										3
φ20		3	4	4	4	4	4	4	4	3	
Momenti positivi											
b	120,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00
psi	0,07	0,13	0,15	0,15	0,15	0,15	0,15	0,15	0,15	0,13	0,07
M+res	43,84	119,46	157,84	157,84	157,84	157,84	157,84	157,84	157,83	119,46	43,84
Momenti negativi											
b	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00
psi	0,11	0,07	0,07	0,07	0,07	0,07	0,07	0,07	0,07	0,07	0,11
M-res	-43,04	-21,68	-21,66	-21,66	-21,66	-21,66	-21,66	-21,66	-21,66	-21,68	-43,04



VERIFICA ALLO S.L.U. DI TAGLIO											
Vsd	53,94	42,68	31,42	20,17	8,91	2,35	13,60	24,86	36,11	47,37	58,63
ρ ₁	0,0025	0,0069	0,0092	0,0092	0,0092	0,0092	0,0092	0,0092	0,0092	0,0069	0,0025
Bmin	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	40,00	42,03

VERIFICA AGLI S.L. DI ESERCIZIO**Caratteristiche geometriche sezioni**

Per gruppo di esigenze cond. ambientali poco aggressive e armatura poco sensibile:

Gruppo di calcolo della resistenza a trazione per barre di acciaio											
		Beta,1 1,00		K2 0,40		Diam.min. 16		copr.netto 1,20			
		Beta,2 0,50		K3 0,13		Sig,SR 101,38		n 15			
As (cmq)	3,39	9,42	12,57	12,57	12,57	12,57	12,57	12,57	12,57	9,42	3,39
A's (cmq)	3,39	1,70	1,70	1,70	1,70	1,70	1,70	1,70	1,70	1,70	3,39
b resistente	40,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	120,00	40,00
Y	7,36	7,71	8,75	8,75	8,75	8,75	8,75	8,75	8,75	7,71	7,36
Wc	5829	15150	16939	16939	16939	16939	16939	16939	16939	15150	5829
Ws	1610	4446	5866	5866	5866	5866	5866	5866	5866	4446	1610
N. barre	3	3	4	4	4	4	4	4	4	3	3
dist. barre	18,00	22,40	22,40	22,40	22,40	22,40	22,40	22,40	22,40	22,40	18,00
Beff (cm)	40	49	71	71	71	71	71	71	71	49	40
Deff (cm)	13,20	13,20	13,20	13,20	13,20	13,20	13,20	13,20	13,20	13,20	13,20
Aeff	528,00	644,16	939,84	939,84	939,84	939,84	939,84	939,84	939,84	644,16	528,00
RO,r	0,64%	1,46%	1,34%	1,34%	1,34%	1,34%	1,34%	1,34%	1,34%	1,46%	0,64%

Combinazioni di carico

Rara	0,00	26,46	47,04	61,74	70,56	73,50	70,56	61,74	47,04	26,46	0,00
Frequente	0,00	23,81	42,34	55,57	63,50	66,15	63,50	55,57	42,34	23,81	0,00
Quasi perm.	0,00	22,76	40,45	53,10	60,68	63,21	60,68	53,10	40,45	22,76	0,00

Verifica allo stato limite di tensione in esercizio

Combinazione rara	Sigma,C,amm = 0.60*fck = 14,94 MPa					Sigma,S,amm = 0.70*fyk = 315 MPa				
Sigma,C	-0,01	-1,75	-2,78	-3,64	-4,17	-4,17	-3,64	-2,78	-1,75	-0,01
Sigma,S	0,01	89,27	120,29	157,89	180,44	187,96	180,44	157,89	120,29	89,27
Combinazione quasi permanente	Sigma,C,amm = 0.45*fck = 11,21 MPa					Sigma,S,amm = 0.45*fck = 11,21 MPa				
Sigma,C	-0,01	-1,50	-2,39	-3,13	-3,58	-3,73	-3,58	-3,13	-2,39	-1,50

Verifica allo stato limite di apertura fessure

Srm (mm)	184,49	123,48	128,63	128,63	128,63	128,63	128,63	128,63	128,63	123,48	184,49
Combinazione frequente	Apertura limite=W3= 0,20 mm					Apertura limite=W2= 0,20 mm					
Sigma,S	0,10	80,34	108,27	142,10	162,40	169,16	162,40	142,10	108,27	80,34	0,10
Eps,sm	0,000%	0,000%	0,021%	0,035%	0,049%	0,053%	0,049%	0,035%	0,021%	0,000%	0,000%
Wk (mm)	0,000	0,000	0,046	0,076	0,107	0,117	0,107	0,076	0,046	0,000	0,000
Combinazione quasi permanente	Apertura limite=W2= 0,20 mm					Apertura limite=W2= 0,20 mm					
Sigma,S	0,10	76,77	103,45	135,78	155,18	161,65	155,18	135,78	103,45	76,77	0,10
Eps,sm	0,000%	0,000%	0,020%	0,030%	0,044%	0,048%	0,044%	0,030%	0,020%	0,000%	0,000%
Wk (mm)	0,000	0,000	0,044	0,066	0,096	0,106	0,096	0,066	0,044	0,000	0,000

Verifica allo stato limite di deformazione**Verifica esatta: combinazione quasi permanente**

EpsCm	0,000%	-0,005%	-0,008%	-0,010%	-0,011%	-0,012%	-0,011%	-0,010%	-0,008%	-0,005%	0,000%
EpsSm	0,000%	0,035%	0,048%	0,065%	0,074%	0,077%	0,074%	0,065%	0,048%	0,035%	0,000%
1/r	0,0000%	-0,0012%	-0,0017%	-0,0022%	-0,0025%	-0,0026%	-0,0025%	-0,0022%	-0,0017%	-0,0012%	0,0000%
rot.	0,0000	-0,0004	-0,0014	-0,0027	-0,0044	-0,0062	-0,0080	-0,0096	-0,0110	-0,0120	-0,0124
frecchia	0,00	-0,01	-0,08	-0,22	-0,47	-0,84	-1,34	-1,96	-2,68	-3,48	-4,33
frecchia	0,000	0,419	0,789	1,078	1,262	1,325	1,262	1,078	0,789	0,419	0,000
frecchia massima:	1,32 cm					528					
verifica sommaria:	Rapporto di snellezza effettivo l/h =					19,44	<	26,00 Rapporto limite			

SCHEMATIZZAZIONE DEI CASI DI CARICO

Il programma consente l'applicazione di diverse tipologie di casi di carico.

Sono previsti i seguenti 11 tipi di casi di carico:

	Sigla	Tipo	Descrizione
1	Ggk	A	caso di carico comprensivo del peso proprio struttura
2	Gk	NA	caso di carico con azioni permanenti
3	Qk	NA	caso di carico con azioni variabili
4	Gsk	A	caso di carico comprensivo dei carichi permanenti sui solai e sulle coperture
5	Qsk	A	caso di carico comprensivo dei carichi variabili sui solai
6	Qnk	A	caso di carico comprensivo dei carichi di neve sulle coperture
7	Qtk	SA	caso di carico comprensivo di una variazione termica agente sulla struttura
8	Qvk	NA	caso di carico comprensivo di azioni da vento sulla struttura
9	Esk	SA	caso di carico sismico con analisi statica equivalente
10	Edk	SA	caso di carico sismico con analisi dinamica
11	Etk	NA	caso di carico comprensivo di azioni derivanti dall' incremento di spinta delle terre in condizione sismica
12	Pk	NA	caso di carico comprensivo di azioni derivanti da coazioni, cedimenti e precompressioni

Sono di tipo automatico A (ossia non prevedono introduzione dati da parte dell'utente) i seguenti casi di carico: 1-Ggk; 4-Gsk; 5-Qsk; 6-Qnk.

Sono di tipo semi-automatico SA (ossia prevedono una minima introduzione dati da parte dell'utente) i seguenti casi di carico:

7-Qtk, in quanto richiede solo il valore della variazione termica;

9-Esk e 10-Edk, in quanto richiedono il valore dell'angolo di ingresso del sisma e l'individuazione dei casi di carico partecipanti alla definizione delle masse.

Sono di tipo non automatico NA ossia prevedono la diretta applicazione di carichi generici agli elementi strutturali (si veda il precedente punto Modellazione delle Azioni) i restanti casi di carico.

Nella tabella successiva vengono riportati i casi di carico agenti sulla struttura, con l'indicazione dei dati relativi al caso di carico stesso:

Numero Tipo e Sigla identificativa, Valore di riferimento del caso di carico (se previsto).

In successione, per i casi di carico non automatici, viene riportato l'elenco di nodi ed elementi direttamente caricati con la sigla identificativa del carico.

Per i casi di carico di tipo sismico (9-Esk e 10-Edk), viene riportata la tabella di definizione delle masse: per ogni caso di carico partecipante alla definizione delle masse viene indicata la relativa aliquota (partecipazione) considerata. Si precisa che per i caso di carico 5-Qsk e 6-Qnk la partecipazione è prevista localmente per ogni elemento solaio o copertura presente nel modello (si confronti il valore Sksol nel capitolo relativo agli elementi solaio) e pertanto la loro partecipazione è di norma pari a uno.

CDC	Tipo	Sigla Id	Note
1	Ggk	CDC=Ggk (peso proprio della struttura)	
2	Gsk	CDC=G1sk (permanente solai-coperture)	
3	Gsk	CDC=G2sk (permanente solai-coperture n.c.d.)	
4	Qsk	CDC=Qsk (variabile solai)	
5	Qnk	CDC=Qnk (carico da neve)	
6	Edk	CDC=Ed (dinamico SLU) alfa=0.0 (ecc. +)	partecipazione:1.00 per 1 CDC=Ggk (peso proprio della struttura)
			partecipazione:1.00 per 2 CDC=G1sk (permanente solai-coperture)
			partecipazione:1.00 per 3 CDC=G2sk (permanente solai-coperture n.c.d.)
			partecipazione:1.00 per 4 CDC=Qsk (variabile solai)
			partecipazione:1.00 per 5 CDC=Qnk (carico da neve)
7	Edk	CDC=Ed (dinamico SLU) alfa=0.0 (ecc. -)	come precedente CDC sismico
8	Edk	CDC=Ed (dinamico SLU) alfa=90.00 (ecc. +)	come precedente CDC sismico
9	Edk	CDC=Ed (dinamico SLU) alfa=90.00 (ecc. -)	come precedente CDC sismico
10	Edk	CDC=Ed (dinamico SLD) alfa=0.0 (ecc. +)	come precedente CDC sismico
11	Edk	CDC=Ed (dinamico SLD) alfa=0.0 (ecc. -)	come precedente CDC sismico
12	Edk	CDC=Ed (dinamico SLD) alfa=90.00 (ecc. +)	come precedente CDC sismico
13	Edk	CDC=Ed (dinamico SLD) alfa=90.00 (ecc. -)	come precedente CDC sismico

DEFINIZIONE DELLE COMBINAZIONI

Il programma combina i diversi tipi di casi di carico (CDC) secondo le regole previste dalla normativa vigente.

Le combinazioni previste sono destinate al controllo di sicurezza della struttura ed alla verifica degli spostamenti e delle sollecitazioni.

La prima tabella delle combinazioni riportata di seguito comprende le seguenti informazioni: Numero, Tipo, Sigla identificativa. Una seconda tabella riporta il peso nella combinazione assunto per ogni caso di carico.

Ai fini delle verifiche degli stati limite si definiscono le seguenti combinazioni delle azioni:

Combinazione fondamentale SLU

$$\gamma G_1 \cdot G_1 + \gamma G_2 \cdot G_2 + \gamma P \cdot P + \gamma Q_1 \cdot Q_{k1} + \gamma Q_2 \cdot \psi_{02} \cdot Q_{k2} + \gamma Q_3 \cdot \psi_{03} \cdot Q_{k3} + \dots$$

Combinazione caratteristica (rara) SLE

$$G_1 + G_2 + P + Q_{k1} + \psi_{02} \cdot Q_{k2} + \psi_{03} \cdot Q_{k3} + \dots$$

Combinazione frequente SLE

$$G_1 + G_2 + P + \psi_{11} \cdot Q_{k1} + \psi_{22} \cdot Q_{k2} + \psi_{23} \cdot Q_{k3} + \dots$$

Combinazione quasi permanente SLE

$$G_1 + G_2 + P + \psi_{21} \cdot Q_{k1} + \psi_{22} \cdot Q_{k2} + \psi_{23} \cdot Q_{k3} + \dots$$

Combinazione sismica, impiegata per gli stati limite ultimi e di esercizio connessi all'azione sismica E

$$E + G_1 + G_2 + P + \psi_{21} \cdot Q_{k1} + \psi_{22} \cdot Q_{k2} + \dots$$

Combinazione eccezionale, impiegata per gli stati limite connessi alle azioni eccezionali

$$G_1 + G_2 + A_d + P + \psi_{21} \cdot Q_{k1} + \psi_{22} \cdot Q_{k2} + \dots$$

Dove:

NTC 2018 Tabella 2.5.I

Destinazione d'uso/azione	ψ_0	ψ_1	ψ_2
Categoria A residenziali	0,70	0,50	0,30
Categoria B uffici	0,70	0,50	0,30
Categoria C ambienti suscettibili di affollamento	0,70	0,70	0,60
Categoria D ambienti ad uso commerciale	0,70	0,70	0,60
Categoria E biblioteche, archivi, magazzini, ...	1,00	0,90	0,80
Categoria F Rimesse e parcheggi (autoveicoli $\leq 30kN$)	0,70	0,70	0,60
Categoria G Rimesse e parcheggi (autoveicoli $> 30kN$)	0,70	0,50	0,30
Categoria H Coperture	0,00	0,00	0,00
Vento	0,60	0,20	0,00
Neve a quota ≤ 1000 m	0,50	0,20	0,00
Neve a quota > 1000 m	0,70	0,50	0,20
Variazioni Termiche	0,60	0,50	0,00

Nelle verifiche possono essere adottati in alternativa due diversi approcci progettuali:

- per l'approccio 1 si considerano due diverse combinazioni di gruppi di coefficienti di sicurezza parziali per le azioni, per i materiali e per la resistenza globale (combinazione 1 con coefficienti A1 e combinazione 2 con coefficienti A2),
- per l'approccio 2 si definisce un'unica combinazione per le azioni, per la resistenza dei materiali e per la resistenza globale (con coefficienti A1).

NTC 2018 Tabella 2.6.I

		Coefficiente γ_f	EQU	A1	A2
Carichi permanenti	Favorevoli	γ_{G1}	0,9	1,0	1,0
	Sfavorevoli		1,1	1,3	1,0
Carichi permanenti non strutturali (Non compiutamente definiti)	Favorevoli	γ_{G2}	0,8	0,8	0,8
	Sfavorevoli		1,5	1,5	1,3
Carichi variabili	Favorevoli	γ_{Qi}	0,0	0,0	0,0
	Sfavorevoli		1,5	1,5	1,3

Cmb	Tipo	Sigla Id	effetto P-delta
1	SLU	Comb. SLU A1 1	
2	SLU	Comb. SLU A1 2	
3	SLU	Comb. SLU A1 3	
4	SLU	Comb. SLU A1 4	
5	SLU	Comb. SLU A1 5	
6	SLU	Comb. SLU A1 6	
7	SLU	Comb. SLU A1 7	
8	SLU	Comb. SLU A1 8	
9	SLU	Comb. SLU A1 9	
10	SLU	Comb. SLU A1 10	
11	SLU	Comb. SLU A1 11	
12	SLU	Comb. SLU A1 12	
13	SLU	Comb. SLU A1 13	
14	SLU	Comb. SLU A1 14	
15	SLU	Comb. SLU A1 (SLV sism.) 15	
16	SLU	Comb. SLU A1 (SLV sism.) 16	
17	SLU	Comb. SLU A1 (SLV sism.) 17	
18	SLU	Comb. SLU A1 (SLV sism.) 18	
19	SLU	Comb. SLU A1 (SLV sism.) 19	
20	SLU	Comb. SLU A1 (SLV sism.) 20	
21	SLU	Comb. SLU A1 (SLV sism.) 21	
22	SLU	Comb. SLU A1 (SLV sism.) 22	
23	SLU	Comb. SLU A1 (SLV sism.) 23	
24	SLU	Comb. SLU A1 (SLV sism.) 24	
25	SLU	Comb. SLU A1 (SLV sism.) 25	
26	SLU	Comb. SLU A1 (SLV sism.) 26	
27	SLU	Comb. SLU A1 (SLV sism.) 27	
28	SLU	Comb. SLU A1 (SLV sism.) 28	
29	SLU	Comb. SLU A1 (SLV sism.) 29	
30	SLU	Comb. SLU A1 (SLV sism.) 30	
31	SLU	Comb. SLU A1 (SLV sism.) 31	
32	SLU	Comb. SLU A1 (SLV sism.) 32	
33	SLU	Comb. SLU A1 (SLV sism.) 33	
34	SLU	Comb. SLU A1 (SLV sism.) 34	
35	SLU	Comb. SLU A1 (SLV sism.) 35	
36	SLU	Comb. SLU A1 (SLV sism.) 36	
37	SLU	Comb. SLU A1 (SLV sism.) 37	
38	SLU	Comb. SLU A1 (SLV sism.) 38	
39	SLU	Comb. SLU A1 (SLV sism.) 39	
40	SLU	Comb. SLU A1 (SLV sism.) 40	
41	SLU	Comb. SLU A1 (SLV sism.) 41	
42	SLU	Comb. SLU A1 (SLV sism.) 42	
43	SLU	Comb. SLU A1 (SLV sism.) 43	
44	SLU	Comb. SLU A1 (SLV sism.) 44	
45	SLU	Comb. SLU A1 (SLV sism.) 45	
46	SLU	Comb. SLU A1 (SLV sism.) 46	
47	SLD(sis)	Comb. SLE (SLD Danno sism.) 47	
48	SLD(sis)	Comb. SLE (SLD Danno sism.) 48	
49	SLD(sis)	Comb. SLE (SLD Danno sism.) 49	
50	SLD(sis)	Comb. SLE (SLD Danno sism.) 50	
51	SLD(sis)	Comb. SLE (SLD Danno sism.) 51	
52	SLD(sis)	Comb. SLE (SLD Danno sism.) 52	
53	SLD(sis)	Comb. SLE (SLD Danno sism.) 53	
54	SLD(sis)	Comb. SLE (SLD Danno sism.) 54	
55	SLD(sis)	Comb. SLE (SLD Danno sism.) 55	
56	SLD(sis)	Comb. SLE (SLD Danno sism.) 56	
57	SLD(sis)	Comb. SLE (SLD Danno sism.) 57	
58	SLD(sis)	Comb. SLE (SLD Danno sism.) 58	
59	SLD(sis)	Comb. SLE (SLD Danno sism.) 59	
60	SLD(sis)	Comb. SLE (SLD Danno sism.) 60	
61	SLD(sis)	Comb. SLE (SLD Danno sism.) 61	
62	SLD(sis)	Comb. SLE (SLD Danno sism.) 62	
63	SLD(sis)	Comb. SLE (SLD Danno sism.) 63	
64	SLD(sis)	Comb. SLE (SLD Danno sism.) 64	
65	SLD(sis)	Comb. SLE (SLD Danno sism.) 65	
66	SLD(sis)	Comb. SLE (SLD Danno sism.) 66	
67	SLD(sis)	Comb. SLE (SLD Danno sism.) 67	
68	SLD(sis)	Comb. SLE (SLD Danno sism.) 68	
69	SLD(sis)	Comb. SLE (SLD Danno sism.) 69	
70	SLD(sis)	Comb. SLE (SLD Danno sism.) 70	
71	SLD(sis)	Comb. SLE (SLD Danno sism.) 71	

Cmb	Tipo	Sigla Id	effetto P-delta
72	SLD(sis)	Comb. SLE (SLD Danno sism.) 72	
73	SLD(sis)	Comb. SLE (SLD Danno sism.) 73	
74	SLD(sis)	Comb. SLE (SLD Danno sism.) 74	
75	SLD(sis)	Comb. SLE (SLD Danno sism.) 75	
76	SLD(sis)	Comb. SLE (SLD Danno sism.) 76	
77	SLD(sis)	Comb. SLE (SLD Danno sism.) 77	
78	SLD(sis)	Comb. SLE (SLD Danno sism.) 78	
79	SLE(r)	Comb. SLE(rara) 79	
80	SLE(r)	Comb. SLE(rara) 80	
81	SLE(r)	Comb. SLE(rara) 81	
82	SLE(r)	Comb. SLE(rara) 82	
83	SLE(r)	Comb. SLE(rara) 83	
84	SLE(r)	Comb. SLE(rara) 84	
85	SLE(r)	Comb. SLE(rara) 85	
86	SLE(f)	Comb. SLE(freq.) 86	
87	SLE(f)	Comb. SLE(freq.) 87	
88	SLE(f)	Comb. SLE(freq.) 88	
89	SLE(f)	Comb. SLE(freq.) 89	
90	SLE(f)	Comb. SLE(freq.) 90	
91	SLE(p)	Comb. SLE(perm.) 91	
92	SLE(p)	Comb. SLE(perm.) 92	

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
1	1.30	1.30	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
2	1.30	1.30	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
3	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
4	1.30	1.30	1.50	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
5	1.00	1.00	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
6	1.00	1.00	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
7	1.00	1.00	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
8	1.00	1.00	0.80	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
9	1.30	1.30	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
10	1.30	1.30	1.50	1.05	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
11	1.30	1.30	1.50	1.05	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
12	1.00	1.00	0.80	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
13	1.00	1.00	0.80	1.05	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
14	1.00	1.00	0.80	1.05	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
15	1.00	1.00	1.00	0.30	0.0	-1.00	0.0	-0.30	0.0	0.0	0.0	0.0	0.0	
16	1.00	1.00	1.00	0.30	0.0	-1.00	0.0	0.30	0.0	0.0	0.0	0.0	0.0	
17	1.00	1.00	1.00	0.30	0.0	1.00	0.0	-0.30	0.0	0.0	0.0	0.0	0.0	
18	1.00	1.00	1.00	0.30	0.0	1.00	0.0	0.30	0.0	0.0	0.0	0.0	0.0	
19	1.00	1.00	1.00	0.30	0.0	-1.00	0.0	0.0	-0.30	0.0	0.0	0.0	0.0	
20	1.00	1.00	1.00	0.30	0.0	-1.00	0.0	0.0	0.30	0.0	0.0	0.0	0.0	
21	1.00	1.00	1.00	0.30	0.0	1.00	0.0	0.0	-0.30	0.0	0.0	0.0	0.0	
22	1.00	1.00	1.00	0.30	0.0	1.00	0.0	0.0	0.30	0.0	0.0	0.0	0.0	
23	1.00	1.00	1.00	0.30	0.0	0.0	-1.00	-0.30	0.0	0.0	0.0	0.0	0.0	
24	1.00	1.00	1.00	0.30	0.0	0.0	-1.00	0.30	0.0	0.0	0.0	0.0	0.0	
25	1.00	1.00	1.00	0.30	0.0	0.0	1.00	-0.30	0.0	0.0	0.0	0.0	0.0	
26	1.00	1.00	1.00	0.30	0.0	0.0	1.00	0.30	0.0	0.0	0.0	0.0	0.0	
27	1.00	1.00	1.00	0.30	0.0	0.0	-1.00	0.0	-0.30	0.0	0.0	0.0	0.0	
28	1.00	1.00	1.00	0.30	0.0	0.0	-1.00	0.0	0.30	0.0	0.0	0.0	0.0	
29	1.00	1.00	1.00	0.30	0.0	0.0	1.00	0.0	-0.30	0.0	0.0	0.0	0.0	
30	1.00	1.00	1.00	0.30	0.0	0.0	1.00	0.0	0.30	0.0	0.0	0.0	0.0	
31	1.00	1.00	1.00	0.30	0.0	-0.30	0.0	-1.00	0.0	0.0	0.0	0.0	0.0	
32	1.00	1.00	1.00	0.30	0.0	-0.30	0.0	1.00	0.0	0.0	0.0	0.0	0.0	
33	1.00	1.00	1.00	0.30	0.0	0.30	0.0	-1.00	0.0	0.0	0.0	0.0	0.0	
34	1.00	1.00	1.00	0.30	0.0	0.30	0.0	1.00	0.0	0.0	0.0	0.0	0.0	
35	1.00	1.00	1.00	0.30	0.0	0.0	-0.30	-1.00	0.0	0.0	0.0	0.0	0.0	
36	1.00	1.00	1.00	0.30	0.0	0.0	-0.30	1.00	0.0	0.0	0.0	0.0	0.0	
37	1.00	1.00	1.00	0.30	0.0	0.0	0.30	-1.00	0.0	0.0	0.0	0.0	0.0	
38	1.00	1.00	1.00	0.30	0.0	0.0	0.30	1.00	0.0	0.0	0.0	0.0	0.0	
39	1.00	1.00	1.00	0.30	0.0	-0.30	0.0	0.0	-1.00	0.0	0.0	0.0	0.0	
40	1.00	1.00	1.00	0.30	0.0	-0.30	0.0	0.0	1.00	0.0	0.0	0.0	0.0	
41	1.00	1.00	1.00	0.30	0.0	0.30	0.0	0.0	-1.00	0.0	0.0	0.0	0.0	
42	1.00	1.00	1.00	0.30	0.0	0.30	0.0	0.0	1.00	0.0	0.0	0.0	0.0	
43	1.00	1.00	1.00	0.30	0.0	0.0	-0.30	0.0	-1.00	0.0	0.0	0.0	0.0	
44	1.00	1.00	1.00	0.30	0.0	0.0	-0.30	0.0	1.00	0.0	0.0	0.0	0.0	
45	1.00	1.00	1.00	0.30	0.0	0.0	0.30	0.0	-1.00	0.0	0.0	0.0	0.0	
46	1.00	1.00	1.00	0.30	0.0	0.0	0.30	0.0	1.00	0.0	0.0	0.0	0.0	
47	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	-0.30	0.0	

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
48	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	0.30	0.0	
49	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	1.00	0.0	-0.30	0.0	
50	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	1.00	0.0	0.30	0.0	
51	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	0.0	-0.30	
52	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	0.0	0.30	
53	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	1.00	0.0	0.0	-0.30	
54	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	1.00	0.0	0.0	0.30	
55	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.0	-1.00	-0.30	0.0	
56	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.0	-1.00	0.30	0.0	
57	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.0	1.00	-0.30	0.0	
58	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.0	1.00	0.30	0.0	
59	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	-0.30	
60	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	0.30	
61	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.0	1.00	0.0	-0.30	
62	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.0	1.00	0.0	0.30	
63	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	-1.00	0.0	
64	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	1.00	0.0	
65	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.30	0.0	-1.00	0.0	
66	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.30	0.0	1.00	0.0	
67	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.0	-0.30	-1.00	0.0	
68	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.0	-0.30	1.00	0.0	
69	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.0	0.30	-1.00	0.0	
70	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.0	0.30	1.00	0.0	
71	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	0.0	-1.00	
72	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	0.0	1.00	
73	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.30	0.0	0.0	-1.00	
74	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.30	0.0	0.0	1.00	
75	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	-1.00	
76	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	1.00	
77	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.0	0.30	0.0	-1.00	
78	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.0	0.30	0.0	1.00	
79	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
80	1.00	1.00	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
81	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
82	1.00	1.00	1.00	1.00	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
83	1.00	1.00	1.00	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
84	1.00	1.00	1.00	0.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
85	1.00	1.00	1.00	0.70	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
86	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
87	1.00	1.00	1.00	0.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
88	1.00	1.00	1.00	0.0	0.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
89	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
90	1.00	1.00	1.00	0.30	0.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
91	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
92	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	

AZIONE SISMICA

L'azione sismica sulle costruzioni è valutata a partire dalla "pericolosità sismica di base", in condizioni ideali di sito di riferimento rigido con superficie topografica orizzontale.

Allo stato attuale, la pericolosità sismica su reticolo di riferimento nell'intervallo di riferimento è fornita dai dati pubblicati sul sito <http://esse1.mi.ingv.it/>. Per punti non coincidenti con il reticolo di riferimento e periodi di ritorno non contemplati direttamente si opera come indicato nell'allegato alle NTC (rispettivamente media pesata e interpolazione).

L'azione sismica viene definita in relazione ad un periodo di riferimento V_r che si ricava, per ciascun tipo di costruzione, moltiplicandone la vita nominale per il coefficiente d'uso (vedi tabella Parametri della struttura). Fissato il periodo di riferimento V_r e la probabilità di superamento P_{ver} associata a ciascuno degli stati limite considerati, si ottiene il periodo di ritorno T_r e i relativi parametri di pericolosità sismica (vedi tabella successiva):

ag: accelerazione orizzontale massima del terreno;

Fo: valore massimo del fattore di amplificazione dello spettro in accelerazione orizzontale;

T*c: periodo di inizio del tratto a velocità costante dello spettro in accelerazione orizzontale;

Parametri della struttura					
Classe d'uso	Vita V_n [anni]	Coeff. Uso	Periodo V_r [anni]	Tipo di suolo	Categoria topografica
III	100.0	1.5	150	B	T1

Individuati su reticolo di riferimento i parametri di pericolosità sismica si valutano i parametri spettrali riportati in tabella:

S è il coefficiente che tiene conto della categoria di sottosuolo e delle condizioni topografiche mediante la relazione seguente $S = S_s \cdot S_t$ (3.2.3)

Fo è il fattore che quantifica l'amplificazione spettrale massima, su sito di riferimento rigido orizzontale

Fv è il fattore che quantifica l'amplificazione spettrale massima verticale, in termini di accelerazione orizzontale massima del terreno ag su sito di riferimento rigido orizzontale

Tb è il periodo corrispondente all'inizio del tratto dello spettro ad accelerazione costante.

Tc è il periodo corrispondente all'inizio del tratto dello spettro a velocità costante.

Td è il periodo corrispondente all'inizio del tratto dello spettro a spostamento costante.

			Km				
Loc.	12.207	45.719					
11637	12.204	45.678	4.566				
11638	12.275	45.679	6.922				
11416	12.274	45.729	5.334				
11415	12.203	45.728	1.017				
SL	P _{ver}	T _r	ag	Fo	T*c		
		Anni	g		sec		
SLO	81.0	90.0	0.079	2.440	0.280		
SLD	63.0	151.0	0.101	2.430	0.290		
SLV	10.0	1424.0	0.259	2.490	0.350		
SLC	5.0	2475.0	0.322	2.490	0.360		
SL	ag	S	Fo	Fv	Tb	Tc	Td
	g				sec	sec	sec
SLO	0.079	1.200	2.440	0.926	0.132	0.397	1.916
SLD	0.101	1.200	2.430	1.043	0.136	0.409	2.004
SLV	0.259	1.142	2.490	1.712	0.158	0.475	2.637
SLC	0.322	1.079	2.490	1.909	0.162	0.486	2.890

RISULTATI ANALISI SISMICHE

Il programma consente l'analisi di diverse configurazioni sismiche.

Sono previsti, infatti, i seguenti casi di carico:

9. Esk caso di carico sismico con analisi statica equivalente

10. Edk caso di carico sismico con analisi dinamica

Ciascun caso di carico è caratterizzato da un angolo di ingresso e da una configurazione di masse determinante la forza sismica complessiva (si rimanda al capitolo relativo ai casi di carico per chiarimenti inerenti questo aspetto).

Nella colonna Note, in funzione della norma in uso sono riportati i parametri fondamentali che caratterizzano l'azione sismica: in particolare possono essere presenti i seguenti valori:

Angolo di ingresso	Angolo di ingresso dell'azione sismica orizzontale
Fattore di importanza	Fattore di importanza dell'edificio, in base alla categoria di appartenenza
Zona sismica	Zona sismica
Accelerazione ag	Accelerazione orizzontale massima sul suolo
Categoria suolo	Categoria di profilo stratigrafico del suolo di fondazione
Fattore q	Fattore di struttura/di comportamento. Dipendente dalla tipologia strutturale
Fattore di sito S	Fattore dipendente dalla stratigrafia e dal profilo topografico
Classe di duttilità CD	Classe di duttilità della struttura – “A” duttilità alta, “B” duttilità bassa
Fattore riduz. SLD	Fattore di riduzione dello spettro elastico per lo stato limite di danno
Periodo proprio T1	Periodo proprio di vibrazione della struttura
Coefficiente Lambda	Coefficiente dipendente dal periodo proprio T1 e dal numero di piani della struttura
Ordinata spettro Sd(T1)	Valore delle ordinate dello spettro di progetto per lo stato limite ultimo, componente orizzontale (verticale Svd)
Ordinata spettro Se(T1)	Valore delle ordinate dello spettro elastico ridotta del fattore SLD per lo stato limite di danno, componente orizzontale (verticale Sve)
Ordinata spettro S (Tb-Tc)	Valore dell' ordinata dello spettro in uso nel tratto costante
numero di modi considerati	Numero di modi di vibrare della struttura considerati nell'analisi dinamica

Per ciascun caso di carico sismico viene riportato l'insieme di dati sotto riportati (le masse sono espresse in unità di forza):

c) **analisi sismica statica equivalente:**

- quota, posizione del centro di applicazione e azione orizzontale risultante, posizione del baricentro delle rigidezze, rapporto r/L_s (per strutture a nucleo), indici di regolarità e/r secondo EC8 4.2.3.2
- azione sismica complessiva

d) **analisi sismica dinamica con spettro di risposta:**

- quota, posizione del centro di massa e massa risultante, posizione del baricentro delle rigidezze, rapporto r/L_s (per strutture a nucleo) , indici di regolarità e/r secondo EC8 4.2.3.2
- frequenza, periodo, accelerazione spettrale, massa eccitata nelle tre direzioni globali per tutti i modi
- massa complessiva ed aliquota di massa complessiva eccitata.

Per ciascuna combinazione sismica definita SLD o SLO viene riportato il livello di deformazione ϵ_T (dr) degli elementi strutturali verticali. Per semplicità di consultazione il livello è espresso anche in unità $1000 \cdot \epsilon_T/h$ da confrontare direttamente con i valori forniti nella norma (es. 5 per

edifici con tamponamenti collegati rigidamente alla struttura, 10.0 per edifici con tamponamenti collegati elasticamente, 3 per edifici in muratura ordinaria, 4 per edifici in muratura armata).

Qualora si applichi il D.M. 96 (vedi NOTA sul capitolo "normativa di riferimento") l'analisi sismica dinamica può essere comprensiva di sollecitazione verticale contemporanea a quella orizzontale, nel qual caso è effettuata una sovrapposizione degli effetti in ragione della radice dei quadrati degli effetti stessi. Per ciascuna combinazione sismica - analisi effettuate con il D.M. 96 (vedi NOTA sul capitolo "normativa di riferimento") - viene riportato il livello di deformazione η_T , η_P e η_D degli elementi strutturali verticali. Per semplicità di consultazione il livello è espresso in unità $1000 \cdot \eta_T/h$ da confrontare direttamente con il valore 2 o 4 per la verifica.

Per gli edifici sismicamente isolati si riportano di seguito le verifiche condotte sui dispositivi di isolamento. Le verifiche sono effettuate secondo la circolare 619/2009 del C.S.LL.PP nelle combinazioni in SLC come previsto dal DM 17-01-2018. Per ogni combinazione è riportato il codice di verifica ed i valori utilizzati per la verifica: spostamento d_E , area ridotta e dimensione A_2 , azione verticale, deformazioni di taglio dell'elastomero e tensioni nell'acciaio.

Qualora si applichi l'Ordinanza 3274 e s.m.i. le verifiche sono eseguite in accordo con l'allegato 10.A.

In particolare la tabella, per ogni combinazione di calcolo, riporta:

Nodo	Nodo di appoggio dell' isolatore
Cmb	Combinazione oggetto della verifica
Verif.	Codice di verifica ok – verifica positiva , NV – verifica negativa, ND – verifica non completata
d_E	Spostamento relativo tra le due facce (amplificato del 20% per Ordinanza 3274 e smi) combinato con la regola del 30%
Ang fi	Angolo utilizzato per il calcolo dell' area ridotta A_r (per dispositivi circolari)
V	Azione verticale agente
A_r	Area ridotta efficace
Dim A_2	Dimensione utile per il calcolo della deformazione per rotazione
Sig s	Tensione nell' inserto in acciaio
Gam c(a,s,t)	Deformazioni di taglio dell' elastomero
Vcr	Carico critico per instabilità

Affinché la verifica sia positiva deve essere:

- 7) $V > 0$
- 8) $\text{Sig s} < f_{yk}$
- 9) $\text{Gam t} < 5$
- 10) $\text{Gam s} < \text{Gam} * (\text{caratteristica dell' elastomero})$
- 11) $\text{Gam s} < 2$
- 12) $V < 0.5 V_{cr}$

La costruzione, nuova, è caratterizzata da regolarità sia in pianta sia in altezza ed è progettata in classe di duttilità media (CD"B").

Parametri fattore in direzione x e y

Sistema costruttivo: calcestruzzo
 Tipologia strutturale: strutture a pareti non accoppiate
 Valore base fattore $q_0 = 3.000$
 Fattore pareti $k_w = 1.000$
 Fattore di regolarità $K_R = 1.0$
 Fattore dissipativo $q_D = q_0 \cdot k_w \cdot K_R = 3.000$

Fattori di comportamento utilizzati

Dissipativi
 q SLU x 3.000
 q SLU y 3.000
 q SLU z 1.500

CDC	Tipo	Sigla Id	Note
6	Edk	CDC=Ed (dinamico SLU) alfa=0.0 (ecc. +)	
			categoria suolo: B
			fattore di sito S = 1.142
			ordinata spettro (tratto Tb-Tc) = 0.246 g
			angolo di ingresso: 0.0
			eccentricità aggiuntiva: positiva
			periodo proprio T1: 0.213 sec.
			fattore q: 3.000
			fattore per spost. μ_d : 5.455
			classe di duttilità CD: B
			numero di modi considerati: 9
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
cm	daN	cm	cm	cm	cm	cm	cm			
786.25	2.852e+05	2194.35	1435.93	0.0	-166.25	1893.33	1671.71	1.982	0.161	0.097
745.63	4.508e+04	1860.78	1731.99	0.0	-166.25	1893.33	1671.71	1.982	0.017	0.025
705.00	1.054e+05	2421.06	2356.95	0.0	-166.25	1893.33	1671.71	1.982	0.282	0.282
664.38	4.386e+04	1843.27	1764.03	0.0	-166.25	1759.11	1671.72	2.372	0.041	0.038
623.75	4.126e+04	1784.54	1821.02	0.0	-166.25	1598.12	1722.57	2.225	0.094	0.040
583.13	3.779e+04	1791.30	1862.46	0.0	-166.25	1679.12	1721.95	2.266	0.056	0.058
542.50	3.571e+04	1846.87	1881.13	0.0	-166.25	1679.12	1721.95	2.266	0.084	0.065
501.88	3.693e+04	1868.13	1838.16	0.0	-166.25	1848.83	1721.94	1.853	0.011	0.047
461.25	3.917e+04	1919.12	1759.38	0.0	-166.25	1964.11	1498.99	1.880	0.025	0.107
420.63	4.171e+04	1877.36	1709.59	0.0	-166.25	1890.11	1498.99	1.888	0.007	0.085
380.00	3.053e+05	2538.99	1664.97	0.0	-166.25	1902.93	1662.50	2.050	0.339	0.001
337.78	4.390e+04	1806.66	1662.50	0.0	-166.25	1902.93	1662.50	1.986	0.051	0.0
295.56	4.166e+04	1793.58	1688.98	0.0	-166.25	1875.33	1670.67	1.735	0.047	0.007
253.33	3.856e+04	1791.34	1723.46	0.0	-166.25	1950.72	1664.27	1.627	0.094	0.022
211.11	3.716e+04	1789.29	1730.42	0.0	-166.25	1943.51	1664.27	1.637	0.091	0.025
168.89	3.679e+04	1766.28	1725.52	0.0	-166.25	1867.78	1664.26	1.653	0.059	0.023
126.67	3.887e+04	1789.82	1697.70	0.0	-166.25	1982.84	1659.49	1.904	0.105	0.016
84.44	4.078e+04	1818.02	1678.49	0.0	-166.25	1982.84	1659.49	1.904	0.090	0.008
42.22	4.078e+04	1818.02	1678.49	0.0	-166.25	1982.84	1659.49	1.904	0.090	0.008
Risulta	1.336e+06									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	1.892	0.529	0.221	5.61	4.20e-04	2.129e+05	15.9	0.02	1.76e-06	0.0	0.0
2	3.933	0.254	0.246	2558.63	0.2	3.23	2.41e-04	5.589e+04	4.2	0.0	0.0
3	4.689	0.213	0.246	1.025e+06	76.7	1546.64	0.1	96.84	7.25e-03	0.0	0.0
4	4.894	0.204	0.246	1.383e+05	10.4	2.469e+04	1.8	0.16	1.23e-05	0.0	0.0
5	6.122	0.163	0.246	1.638e+04	1.2	4.042e+05	30.3	33.74	2.53e-03	0.0	0.0
6	7.167	0.140	0.252	1.071e+04	0.8	6.564e+05	49.1	107.67	8.06e-03	0.0	0.0
7	10.381	0.096	0.265	1.223e+05	9.2	5894.35	0.4	15.72	1.18e-03	0.0	0.0
8	12.124	0.082	0.270	446.16	3.34e-02	1054.75	7.90e-02	6.211e+05	46.5	0.0	0.0
9	15.780	0.063	0.276	151.22	1.13e-02	1048.19	7.85e-02	6.426e+05	48.1	0.0	0.0
Risulta				1.316e+06		1.308e+06		1.320e+06			
In percentuale				98.52		97.89		98.79			

CDC	Tipo	Sigla Id	Note
7	Edk	CDC=Ed (dinamico SLU) alfa=0.0 (ecc. -)	
			categoria suolo: B
			fattore di sito S = 1.142
			ordinata spettro (tratto Tb-Tc) = 0.246 g

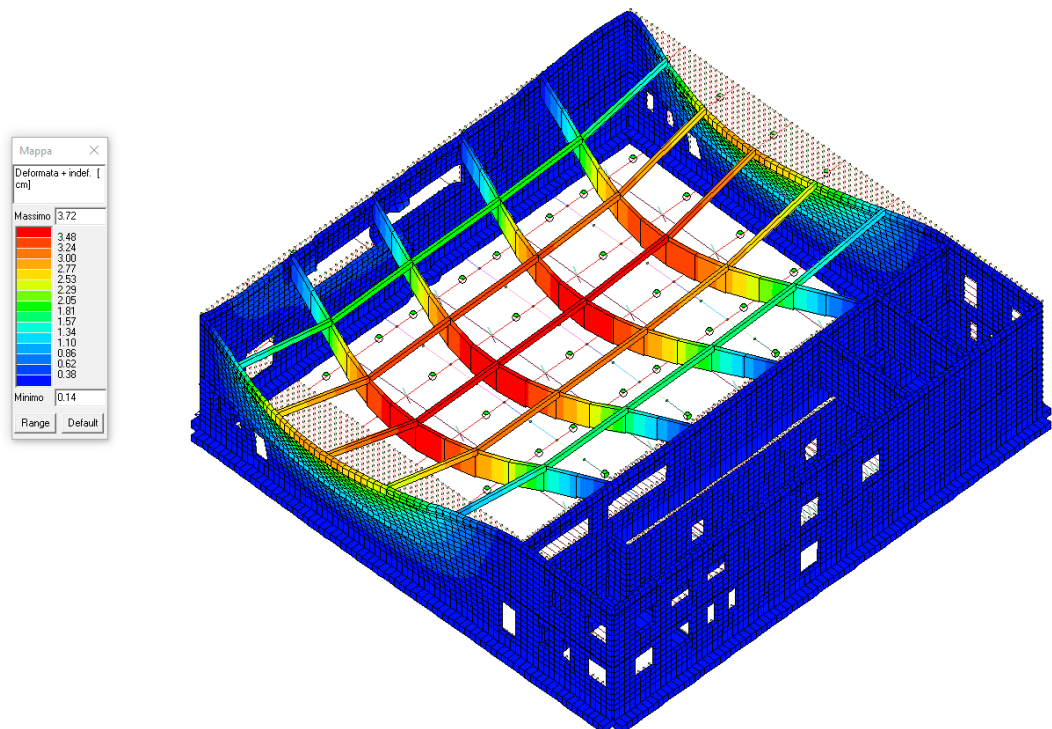
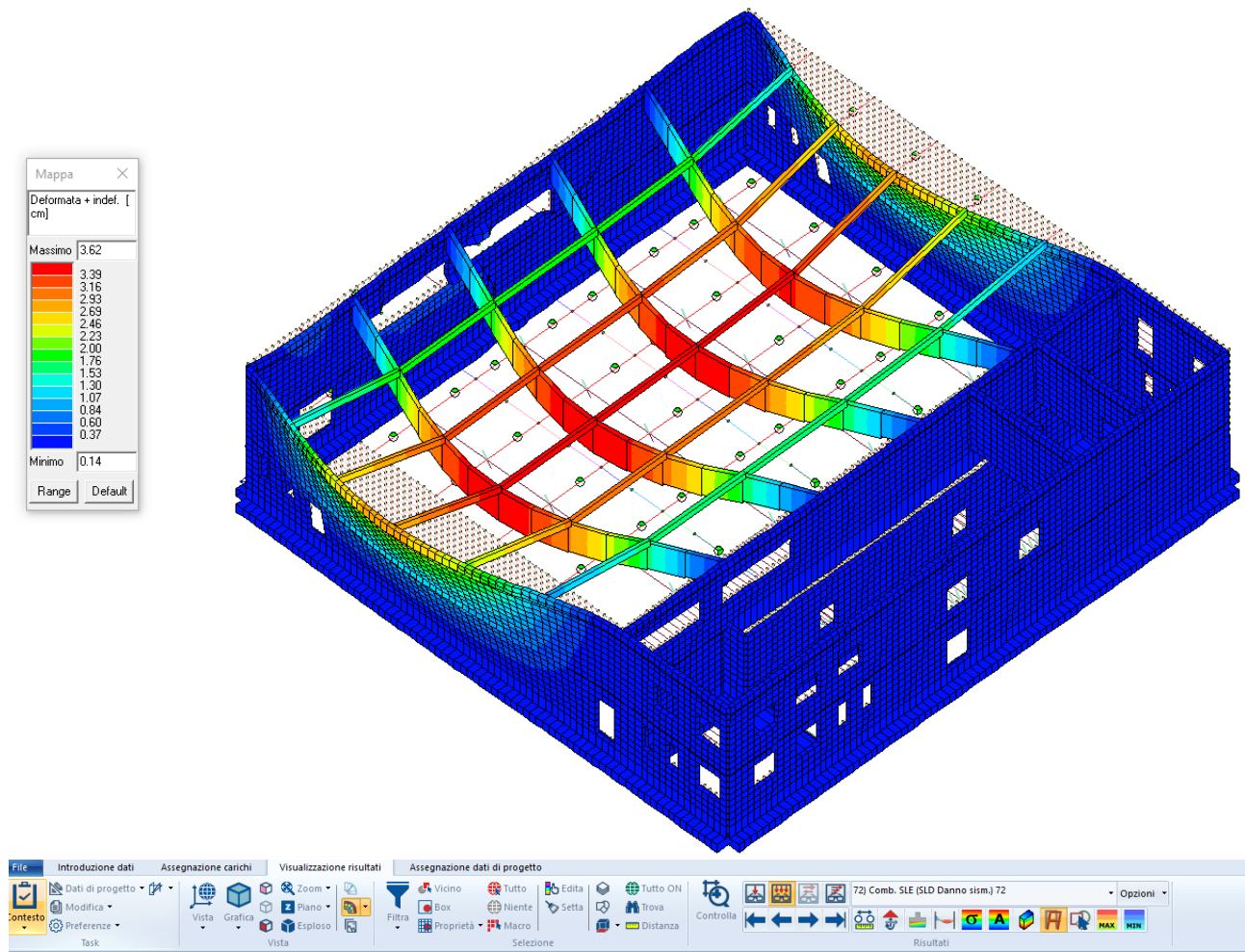
CDC	Tipo	Sigla Id	Note							
11	Edk	CDC=Ed (dinamico SLD) alfa=0.0 (ecc. -)								
			categoria suolo: B							
			fattore di sito S = 1.200							
			ordinata spettro (tratto Tb-Tc) = 0.295 g							
			angolo di ingresso:0.0							
			eccentricità aggiuntiva: negativa							
			periodo proprio T1: 0.213 sec.							
			numero di modi considerati: 9							
			combinaz. modale: CQC							
Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
cm	daN	cm	cm	cm	cm	cm	cm			
786.25	2.852e+05	2194.35	1435.93	0.0	166.25	1893.33	1671.71	1.982	0.161	0.097
745.63	4.508e+04	1860.78	1731.99	0.0	166.25	1893.33	1671.71	1.982	0.017	0.025
705.00	1.054e+05	2421.06	2356.95	0.0	166.25	1893.33	1671.71	1.982	0.282	0.282

CDC	Tipo	Sigla Id	Note											
664.38	4.386e+04	1843.27	1764.03	0.0	166.25	1759.11	1671.72	2.372	0.041	0.038				
623.75	4.126e+04	1784.54	1821.02	0.0	166.25	1598.12	1722.57	2.225	0.094	0.040				
583.13	3.779e+04	1791.30	1862.46	0.0	166.25	1679.12	1721.95	2.266	0.056	0.058				
542.50	3.571e+04	1846.87	1881.13	0.0	166.25	1679.12	1721.95	2.266	0.084	0.065				
501.88	3.693e+04	1868.13	1838.16	0.0	166.25	1848.83	1721.94	1.853	0.011	0.047				
461.25	3.917e+04	1919.12	1759.38	0.0	166.25	1964.11	1498.99	1.880	0.025	0.107				
420.63	4.171e+04	1877.36	1709.59	0.0	166.25	1890.11	1498.99	1.888	0.007	0.085				
380.00	3.053e+05	2538.99	1664.97	0.0	166.25	1902.93	1662.50	2.050	0.339	0.001				
337.78	4.390e+04	1806.66	1662.50	0.0	166.25	1902.93	1662.50	1.986	0.051	0.0				
295.56	4.166e+04	1793.58	1688.98	0.0	166.25	1875.33	1670.67	1.735	0.047	0.007				
253.33	3.856e+04	1791.34	1723.46	0.0	166.25	1950.72	1664.27	1.627	0.094	0.022				
211.11	3.716e+04	1789.29	1730.42	0.0	166.25	1943.51	1664.27	1.637	0.091	0.025				
168.89	3.679e+04	1766.28	1725.52	0.0	166.25	1867.78	1664.26	1.653	0.059	0.023				
126.67	3.887e+04	1789.82	1697.70	0.0	166.25	1982.84	1659.49	1.904	0.105	0.016				
84.44	4.078e+04	1818.02	1678.49	0.0	166.25	1982.84	1659.49	1.904	0.090	0.008				
42.22	4.078e+04	1818.02	1678.49	0.0	166.25	1982.84	1659.49	1.904	0.090	0.008				
Risulta	1.336e+06													
Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v			
	Hz	sec	g	daN		daN		daN						
1	1.892	0.529	0.228	3.88	2.90e-04	2.129e+05	15.9	0.02	1.46e-06	0.0	0.0			
2	3.932	0.254	0.295	2522.28	0.2	3.27	2.45e-04	5.585e+04	4.2	0.0	0.0			
3	4.691	0.213	0.295	1.114e+06	83.4	1904.03	0.1	80.26	6.01e-03	0.0	0.0			
4	4.960	0.202	0.295	7.179e+04	5.4	3.076e+04	2.3	1.25	9.37e-05	0.0	0.0			
5	6.171	0.162	0.295	2799.56	0.2	4.170e+05	31.2	53.95	4.04e-03	0.0	0.0			
6	7.172	0.139	0.295	4635.44	0.3	6.371e+05	47.7	165.14	1.24e-02	0.0	0.0			
7	10.755	0.093	0.240	1.202e+05	9.0	5469.43	0.4	575.30	4.31e-02	0.0	0.0			
8	12.199	0.082	0.226	1223.30	9.16e-02	1261.53	9.44e-02	6.594e+05	49.4	0.0	0.0			
9	15.985	0.063	0.201	392.26	2.94e-02	1624.89	0.1	6.055e+05	45.3	0.0	0.0			
Risulta				1.317e+06		1.308e+06		1.322e+06						
In percentuale				98.62		97.91		98.93						

CDC	Tipo	Sigla Id	Note								
12	Edk	CDC=Ed (dinamico SLD) alfa=90.00 (ecc. +)									
			categoria suolo: B								
			fattore di sito S = 1.200								
			ordinata spettro (tratto Tb-Tc) = 0.295 g								
			angolo di ingresso:90.00								
			eccentricità aggiuntiva: positiva								
			periodo proprio T1: 0.163 sec.								
			numero di modi considerati: 9								
			combinaz. modale: CQC								
Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry	
cm	daN	cm	cm	cm	cm	cm	cm				
786.25	2.852e+05	2194.35	1435.93	159.50	0.0	1893.33	1671.71	1.982	0.161	0.097	
745.63	4.508e+04	1860.78	1731.99	159.50	0.0	1893.33	1671.71	1.982	0.017	0.025	
705.00	1.054e+05	2421.06	2356.95	159.50	0.0	1893.33	1671.71	1.982	0.282	0.282	
664.38	4.386e+04	1843.27	1764.03	159.50	0.0	1759.11	1671.72	2.372	0.041	0.038	
623.75	4.126e+04	1784.54	1821.02	159.50	0.0	1598.12	1722.57	2.225	0.094	0.040	
583.13	3.779e+04	1791.30	1862.46	159.50	0.0	1679.12	1721.95	2.266	0.056	0.058	
542.50	3.571e+04	1846.87	1881.13	159.50	0.0	1679.12	1721.95	2.266	0.084	0.065	
501.88	3.693e+04	1868.13	1838.16	159.50	0.0	1848.83	1721.94	1.853	0.011	0.047	
461.25	3.917e+04	1919.12	1759.38	159.50	0.0	1964.11	1498.99	1.880	0.025	0.107	
420.63	4.171e+04	1877.36	1709.59	159.50	0.0	1890.11	1498.99	1.888	0.007	0.085	
380.00	3.053e+05	2538.99	1664.97	159.50	0.0	1902.93	1662.50	2.050	0.339	0.001	
337.78	4.390e+04	1806.66	1662.50	159.50	0.0	1902.93	1662.50	1.986	0.051	0.0	
295.56	4.166e+04	1793.58	1688.98	159.50	0.0	1875.33	1670.67	1.735	0.047	0.007	
253.33	3.856e+04	1791.34	1723.46	159.50	0.0	1950.72	1664.27	1.627	0.094	0.022	
211.11	3.716e+04	1789.29	1730.42	159.50	0.0	1943.51	1664.27	1.637	0.091	0.025	
168.89	3.679e+04	1766.28	1725.52	159.50	0.0	1867.78	1664.26	1.653	0.059	0.023	
126.67	3.887e+04	1789.82	1697.70	159.50	0.0	1982.84	1659.49	1.904	0.105	0.016	
84.44	4.078e+04	1818.02	1678.49	159.50	0.0	1982.84	1659.49	1.904	0.090	0.008	
42.22	4.078e+04	1818.02	1678.49	159.50	0.0	1982.84	1659.49	1.904	0.090	0.008	
Risulta	1.336e+06										
Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	2.031	0.492	0.245	0.02	1.16e-06	1.902e+05	14.2	0.03	2.11e-06	0.0	0.0
2	3.933	0.254	0.295	2398.91	0.2	3.89	2.91e-04	5.588e+04	4.2	0.0	0.0
3	4.730	0.211	0.295	1.149e+06	86.0	1178.49	8.82e-02	78.46	5.87e-03	0.0	0.0

CDC	Tipo	Sigla Id				Note						
4		5.128	0.195	0.295	2.974e+04	2.2	9.523e+04	7.1	3.69	2.77e-04	0.0	0.0
5		6.146	0.163	0.295	7914.66	0.6	5.236e+05	39.2	47.14	3.53e-03	0.0	0.0
6		7.099	0.141	0.295	8755.10	0.7	4.809e+05	36.0	177.67	1.33e-02	0.0	0.0
7		10.801	0.093	0.239	1.206e+05	9.0	3558.63	0.3	103.41	7.74e-03	0.0	0.0
8		12.259	0.082	0.225	110.20	8.25e-03	1100.59	8.24e-02	6.963e+05	52.1	0.0	0.0
9		16.228	0.062	0.200	65.03	4.87e-03	1362.36	0.1	5.716e+05	42.8	0.0	0.0
Risulta					1.319e+06		1.297e+06		1.324e+06			
In percentuale					98.72		97.10		99.12			

CDC	Tipo	Sigla Id	Note									
13	Edk	CDC=Ed (dinamico SLD) alfa=90.00 (ecc. -)										
			categoria suolo: B									
			fattore di sito S = 1.200									
			ordinata spettro (tratto Tb-Tc) = 0.295 g									
			angolo di ingresso:90.00									
			eccentricità aggiuntiva: negativa									
			periodo proprio T1: 0.134 sec.									
			numero di modi considerati: 9									
			combinaz. modale: CQC									
Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry		
cm	daN	cm	cm	cm	cm	cm	cm					
786.25	2.852e+05	2194.35	1435.93	-159.50	0.0	1893.33	1671.71	1.982	0.161	0.097		
745.63	4.508e+04	1860.78	1731.99	-159.50	0.0	1893.33	1671.71	1.982	0.017	0.025		
705.00	1.054e+05	2421.06	2356.95	-159.50	0.0	1893.33	1671.71	1.982	0.282	0.282		
664.38	4.386e+04	1843.27	1764.03	-159.50	0.0	1759.11	1671.72	2.372	0.041	0.038		
623.75	4.126e+04	1784.54	1821.02	-159.50	0.0	1598.12	1722.57	2.225	0.094	0.040		
583.13	3.779e+04	1791.30	1862.46	-159.50	0.0	1679.12	1721.95	2.266	0.056	0.058		
542.50	3.571e+04	1846.87	1881.13	-159.50	0.0	1679.12	1721.95	2.266	0.084	0.065		
501.88	3.693e+04	1868.13	1838.16	-159.50	0.0	1848.83	1721.94	1.853	0.011	0.047		
461.25	3.917e+04	1919.12	1759.38	-159.50	0.0	1964.11	1498.99	1.880	0.025	0.107		
420.63	4.171e+04	1877.36	1709.59	-159.50	0.0	1890.11	1498.99	1.888	0.007	0.085		
380.00	3.053e+05	2538.99	1664.97	-159.50	0.0	1902.93	1662.50	2.050	0.339	0.001		
337.78	4.390e+04	1806.66	1662.50	-159.50	0.0	1902.93	1662.50	1.986	0.051	0.0		
295.56	4.166e+04	1793.58	1688.98	-159.50	0.0	1875.33	1670.67	1.735	0.047	0.007		
253.33	3.856e+04	1791.34	1723.46	-159.50	0.0	1950.72	1664.27	1.627	0.094	0.022		
211.11	3.716e+04	1789.29	1730.42	-159.50	0.0	1943.51	1664.27	1.637	0.091	0.025		
168.89	3.679e+04	1766.28	1725.52	-159.50	0.0	1867.78	1664.26	1.653	0.059	0.023		
126.67	3.887e+04	1789.82	1697.70	-159.50	0.0	1982.84	1659.49	1.904	0.105	0.016		
84.44	4.078e+04	1818.02	1678.49	-159.50	0.0	1982.84	1659.49	1.904	0.090	0.008		
42.22	4.078e+04	1818.02	1678.49	-159.50	0.0	1982.84	1659.49	1.904	0.090	0.008		
Risulta	1.336e+06											
Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v	
	Hz	sec	g	daN		daN		daN				
1	1.776	0.563	0.214	0.05	4.11e-06	2.366e+05	17.7	0.02	1.28e-06	0.0	0.0	
2	3.933	0.254	0.295	2404.05	0.2	2.89	2.17e-04	5.588e+04	4.2	0.0	0.0	
3	4.657	0.215	0.295	3.605e+05	27.0	3362.23	0.3	56.53	4.23e-03	0.0	0.0	
4	4.781	0.209	0.295	8.231e+05	61.6	1475.17	0.1	25.13	1.88e-03	0.0	0.0	
5	6.183	0.162	0.295	2163.45	0.2	4.209e+05	31.5	14.71	1.10e-03	0.0	0.0	
6	7.437	0.134	0.293	4072.49	0.3	6.493e+05	48.6	95.16	7.12e-03	0.0	0.0	
7	10.348	0.097	0.245	1.178e+05	8.8	5954.88	0.4	3788.45	0.3	0.0	0.0	
8	12.097	0.083	0.227	5073.17	0.4	502.90	3.76e-02	5.918e+05	44.3	0.0	0.0	
9	15.630	0.064	0.203	1543.84	0.1	635.63	4.76e-02	6.663e+05	49.9	0.0	0.0	
Risulta				1.317e+06		1.319e+06		1.318e+06				
In percentuale				98.56		98.71		98.66				



VERIFICHE ELEMENTI TRAVE E/O PILASTRO IN C.A.

Legenda tabella verifiche elementi trave e/o pilastro in c.a.

In tabella vengono riportati per ogni elemento il numero identificativo ed il codice di verifica con le sigle **Ok** o **NV**.

Nel caso in cui si sia proceduto alla progettazione con le tensioni ammissibili (**T.A.**) vengono riportate le massime tensioni nell'elemento (massima compressione nel calcestruzzo, massima compressione media nel calcestruzzo, massima tensione nell'acciaio, massima tensione tangenziale) con l'indicazione delle combinazioni in cui si sono attinti i rispettivi valori.

Nel caso in cui si sia proceduto alla progettazione con il metodo degli stati limite (**S.L.**) vengono riportati: il rapporto x/d , le verifiche per sollecitazioni proporzionali e la verifica per compressione media con l'indicazione delle combinazioni in cui si sono attinti i rispettivi valori.

Nel caso in cui la struttura abbia comportamento dissipativo e sia prevista la progettazione con il criterio della gerarchia delle resistenze (**G.R.**) vengono riportate le verifiche di sovrarresistenza e del nodo.

Per gli elementi tipo pilastro sono riportati numero e diametro dei ferri di vertice, numero e diametro di ferri disposti lungo i lati L1 (paralleli alla base della sezione) e lungo i lati L2 (paralleli all'altezza della sezione).

Per gli elementi tipo trave sono riportati infine le quantità di armatura inferiore e superiore.

Schema della distribuzione delle armature longitudinali

	Orientamento elementi 2D non verticali Orientamento elementi 2D verticali
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342	ok,ok	0.0	0.34	30.0	32.3	0.0	0.05	0.10	0.13	0.10	2d8/25 L=40	17,18,22
	s=1,m=1	40.0	0.34	30.0	32.3	0.0	0.05	0.10	0.09	0.07	2d8/25 L=40	17,18,15
344	ok,ok	0.0	0.34	30.0	32.3	0.0	0.05	0.10	0.13	0.09	2d8/25 L=40	17,18,22
	s=1,m=1	40.0	0.34	30.0	32.3	0.0	0.05	0.09	0.09	0.07	2d8/25 L=40	17,15,15
346	ok,ok	0.0	0.34	30.0	32.3	0.0	0.05	0.09	0.12	0.08	2d8/25 L=40	17,18,22
	s=1,m=1	40.0	0.34	30.0	32.3	0.0	0.05	0.09	0.08	0.07	2d8/25 L=40	17,15,15
348	ok,ok	0.0	0.34	30.0	32.3	0.0	0.05	0.09	0.12	0.08	2d8/25 L=40	17,18,22
	s=1,m=1	40.0	0.34	30.0	32.3	0.0	0.05	0.08	0.08	0.06	2d8/25 L=40	17,15,15
350	ok,ok	0.0	0.34	30.0	32.3	0.0	0.05	0.08	0.12	0.08	2d8/25 L=40	17,22,22
	s=1,m=1	40.0	0.34	30.0	32.3	0.0	0.05	0.08	0.07	0.05	2d8/25 L=40	17,22,15
352	ok,ok	0.0	0.34	30.0	32.3	0.0	0.05	0.08	0.12	0.09	2d8/25 L=40	17,22,22
	s=1,m=1	40.0	0.34	30.0	32.3	0.0	0.05	0.07	0.08	0.06	2d8/25 L=40	17,22,15
354	ok,ok	0.0	0.34	30.0	32.3	0.0	0.05	0.07	0.12	0.08	2d8/25 L=40	17,22,22
	s=1,m=1	40.0	0.34	30.0	32.3	0.0	0.05	0.07	0.09	0.09	2d8/25 L=40	17,19,15
356	ok,ok	0.0	0.34	30.0	32.3	0.0	0.05	0.07	0.11	0.07	2d8/25 L=40	17,22,22
	s=1,m=1	40.0	0.34	30.0	32.3	0.0	0.05	0.07	0.12	0.13	2d8/25 L=40	17,19,15
358	ok,ok	0.0	0.34	30.0	32.3	0.0	0.05	0.07	0.09	0.09	2d8/25 L=40	17,19,15
	s=1,m=1	40.0	0.34	30.0	32.3	0.0	0.05	0.07	0.14	0.16	2d8/25 L=40	17,19,15
360	ok,ok	0.0	0.34	30.0	32.3	0.0	0.05	0.07	0.10	0.10	2d8/25 L=40	17,16,15
	s=1,m=1	40.0	0.34	30.0	32.3	0.0	0.08	0.07	0.15	0.17	2d8/25 L=40	17,19,3
362	ok,ok	0.0	0.34	30.0	32.3	0.0	0.05	0.07	0.10	0.08	2d8/25 L=40	17,16,15
	s=1,m=1	40.0	0.34	30.0	32.3	0.0	0.05	0.07	0.14	0.16	2d8/25 L=40	17,16,3
M_T= 3 Z=0.0 N=2 N=4												
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
3	ok,ok	0.0	0.34	30.0	32.3	0.0	0.05	0.06	0.13	0.05	2d8/25 L=40	17,18,19
	s=1,m=1	40.1	0.34	30.0	32.3	0.0	0.08	0.06	0.16	0.13	2d8/25 L=40	17,15,3
107	ok,ok	0.0	0.34	30.0	32.3	0.0	0.05	0.07	0.14	0.04	2d8/25 L=40	17,18,22
	s=1,m=1	40.1	0.34	30.0	32.3	0.0	0.08	0.07	0.14	0.09	2d8/25 L=40	17,21,3
101	ok,ok	0.0	0.34	30.0	32.3	0.0	0.08	0.07	0.15	0.07	2d8/25 L=40	17,18,22
	s=1,m=1	40.1	0.34	30.0	32.3	0.0	0.08	0.07	0.12	0.06	2d8/25 L=40	17,21,19
95	ok,ok	0.0	0.34	30.0	32.3	0.0	0.08	0.07	0.15	0.09	2d8/25 L=40	17,22,22
	s=1,m=1	40.1	0.34	30.0	32.3	0.0	0.05	0.07	0.10	0.06	2d8/25 L=40	17,18,19
89	ok,ok	0.0	0.34	30.0	32.3	0.0	0.08	0.07	0.15	0.09	2d8/25 L=40	17,22,22
	s=1,m=1	40.1	0.34	30.0	32.3	0.0	0.08	0.07	0.10	0.07	2d8/25 L=40	17,18,19
83	ok,ok	0.0	0.34	30.0	32.3	0.0	0.08	0.07	0.13	0.07	2d8/25 L=40	17,18,22
	s=1,m=1	40.1	0.34	30.0	32.3	0.0	0.08	0.07	0.11	0.10	2d8/25 L=40	17,29,39
77	ok,ok	0.0	0.34	30.0	32.3	0.0	0.08	0.07	0.11	0.05	2d8/25 L=40	17,18,22
	s=1,m=1	40.1	0.34	30.0	32.3	0.0	0.08	0.07	0.12	0.12	2d8/25 L=40	17,29,39
71	ok,ok	0.0	0.34	30.0	32.3	0.0	0.05	0.08	0.09	0.05	2d8/25 L=40	17,18,39
	s=1,m=1	40.1	0.34	30.0	32.3	0.0	0.08	0.08	0.13	0.13	2d8/25 L=40	17,3,3
65	ok,ok	0.0	0.34	30.0	32.3	0.0	0.05	0.08	0.10	0.04	2d8/25 L=40	17,18,42
	s=1,m=1	40.1	0.34	30.0	32.3	0.0	0.08	0.08	0.11	0.10	2d8/25 L=40	17,3,3
59	ok,ok	0.0	0.34	30.0	32.3	0.0	0.08	0.08	0.12	0.07	2d8/25 L=40	17,18,42
	s=1,m=1	40.1	0.34	30.0	32.3	0.0	0.08	0.08	0.09	0.06	2d8/25 L=40	17,21,39
53	ok,ok	0.0	0.34	30.0	32.3	0.0	0.08	0.08	0.14	0.12	2d8/25 L=40	17,18,4
	s=1,m=1	40.1	0.34	30.0	32.3	0.0	0.05	0.07	0.09	0.04	2d8/25 L=40	17,18,46
47	ok,ok	0.0	0.34	30.0	32.3	0.0	0.08	0.07	0.16	0.14	2d8/25 L=40	17,22,4
	s=1,m=1	40.1	0.34	30.0	32.3	0.0	0.05	0.06	0.11	0.07	2d8/25 L=40	17,18,46
41	ok,ok	0.0	0.34	30.0	32.3	0.0	0.08	0.06	0.17	0.14	2d8/25 L=40	17,30,46
	s=1,m=1	40.1	0.34	30.0	32.3	0.0	0.05	0.06	0.12	0.07	2d8/25 L=40	17,26,46
35	ok,ok	0.0	0.34	30.0	32.3	0.0	0.08	0.05	0.17	0.13	2d8/25 L=40	17,30,46
	s=1,m=1	40.1	0.34	30.0	32.3	0.0	0.05	0.05	0.13	0.06	2d8/25 L=40	17,30,43
29	ok,ok	0.0	0.34	30.0	32.3	0.0	0.05	0.04	0.18	0.13	2d8/25 L=40	17,30,46
	s=1,m=1	40.1	0.34	30.0	32.3	0.0	0.05	0.04	0.14	0.06	2d8/25 L=40	17,30,46
23	ok,ok	0.0	0.34	30.0	32.3	0.0	0.05	0.03	0.21	0.16	2d8/25 L=40	17,22,30
	s=1,m=1	40.1	0.34	30.0	32.3	0.0	0.05	0.03	0.17	0.08	2d8/25 L=40	17,22,30
18	ok,ok	0.0	0.34	30.0	32.3	0.0	0.05	0.03	0.27	0.20	2d8/25 L=40	17,22,30
	s=1,m=1	40.1	0.34	30.0	32.3	0.0	0.05	0.04	0.22	0.13	2d8/25 L=40	17,22,30
15	ok,ok	0.0	0.34	30.0	32.3	12.1	0.05	0.06	0.30	0.87	2d8/12 L=40	17,15,15
	s=1,m=1	40.1	0.34	30.0	32.3	12.1	0.05	0.06	0.35	0.96	2d8/12 L=40	17,31,15
238	ok,ok	0.0	0.34	30.0	32.3	12.1	0.05	0.06	0.36	0.76	2d8/12 L=40	17,27,15
	s=1,m=1	40.1	0.34	30.0	32.3	12.1	0.08	0.08	0.41	0.86	2d8/12 L=40	17,27,15
234	ok,ok	0.0	0.34	30.0	32.3	0.0	0.05	0.08	0.34	0.16	2d8/25 L=40	17,15,19
	s=1,m=1	40.1	0.34	30.0	32.3	0.0	0.08	0.09	0.39	0.25	2d8/25 L=40	17,15,4
230	ok,ok	0.0	0.34	30.0	32.3	0.0	0.05	0.09	0.30	0.13	2d8/25 L=40	17,15,39
	s=1,m=1	40.1	0.34	30.0	32.3	0.0	0.08	0.10	0.35	0.22	2d8/25 L=40	17,15,4
226	ok,ok	0.0	0.34	30.0	32.3	0.0	0.05	0.10	0.26	0.11	2d8/25 L=40	17,15,39
	s=1,m=1	40.1	0.34	30.0	32.3	0.0	0.08	0.11	0.32	0.20	2d8/25 L=40	17,15,4
222	ok,ok	0.0	0.34	30.0	32.3	0.0	0.08	0.11	0.23	0.10	2d8/25 L=40	17,15,39
	s=1,m=1	40.1	0.34	30.0	32.3	0.0	0.08	0.12	0.29	0.19	2d8/25 L=40	17,15,4
218	ok,ok	0.0	0.34	30.0	32.3	0.0	0.08	0.12	0.21	0.09	2d8/25 L=40	17,23,39
	s=1,m=1	40.1	0.34	30.0	32.3	0.0	0.08	0.13	0.27	0.18	2d8/25 L=40	17,23,4
214	ok,ok	0.0	0.34	30.0	32.3	0.0	0.08	0.13	0.19	0.07	2d8/25 L=40	17,23,43
	s=1,m=1	40.1	0.34	30.0	32.3	0.0	0.08	0.14	0.25	0.16	2d8/25 L=40	17,23,4
210	ok,ok	0.0	0.34	30.0	32.3	0.0	0.08	0.13	0.16	0.04	2d8/25 L=40	17,23,43
	s=1,m=1	40.1	0.34	30.0	32.3	0.0	0.08	0.14	0.22	0.14	2d8/25 L=40	17,23,4
206	ok,ok	0.0	0.34	30.0	32.3	0.0	0.08	0.14	0.14	0.03	2d8/25 L=40	17,23,46
	s=1,m=1	40.1	0.34	30.0	32.3	0.0	0.08	0.14	0.20	0.11	2d8/25 L=40	17,23,4
202	ok,ok	0.0	0.34	30.0	32.3	0.0	0.08	0.14	0.13	0.04	2d8/25 L=40	17,23,46
	s=1,m=1	40.1	0.34	30.0	32.3	0.0	0.08	0.14	0.17	0.09	2d8/25 L=40	17,23,4
198	ok,ok	0.0	0.34	30.0	32.3	0.0	0.08	0.14	0.12	0.05	2d8/25 L=40	17,23,46
	s=1,m=1	40.1	0.34	30.0	32.3	0.0	0.08	0.14	0.16	0.08	2d8/25 L=40	17,23,4
194	ok,ok	0.0	0.34	30.0	32.3	0.0	0.08	0.14	0.12	0.06	2d8/25 L=40	17,23,3
	s=1,m=1	40.1	0.34	30.0	32.3	0.0	0.08	0.14	0.14	0.07	2d8/25 L=40	17,23,4
190	ok,ok	0.0	0.34	30.0	32.3	0.0	0.08	0.14	0.11	0.06	2d8/25 L=40	17,23,3
	s=1,m=1	40.1	0.34	30.0	32.3	0.0	0.08	0.14	0.13	0.06	2d8/25 L=40	17,23,4
186	ok,ok	0.0	0.34	30.0	32.3	0.0	0.08	0.14	0.10	0.07	2d8/25 L=40	17,23,4
	s=1,m=1	40.1	0.34	30.0	32.3	0.0	0.08	0.13	0.11	0.05	2d8/25 L=40	17,23,4
182	ok,ok	0.0	0.34	30.0	32.3	0.0	0.08	0.13	0.10	0.09	2d8/25 L=40	17,23,4
	s=1,m=1	40.1	0.34	30.0	32.3	0.0	0.08	0.13	0.10	0.04	2d8/25 L=40	17,23,4
178	ok,ok	0.0	0.34	30.0	32.3	0.0	0.08	0.13	0.10	0.11	2d8/25 L=40	17,23,4
	s=1,m=1	40.1	0.34	30.0	32.3	0.0	0.08	0.12	0.08	0.02	2d8/25 L=40	17,23,43
174	ok,ok	0.0	0.34	30.0	32.3	0.0	0.08	0.12	0.11	0.14	2d8/25 L=40	33,26,3
	s=1,m=1	40.1	0.34	30.0	32.3	0.0	0.08	0.12	0.06	0.03	2d8/25 L=40	33,26,46
170	ok,ok	0.0	0.34	30.0	32.3	0.0	0.08	0.12	0.14	0.19	2d8/25 L=40	33,26,38
	s=1,m=1	40.1	0.34	30.0	32.3	0.0	0.05	0.10	0.09	0.11	2d8/25 L=40	

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259	ok,ok	0.0	0.34	30.0	32.3	16.1	0.05	0.11	0.28	0.91	2d8/12 L=41	28,46,42
	s=1,m=1	41.5	0.34	30.0	32.3	16.1	0.05	0.09	0.27	0.90	2d8/12 L=41	28,43,43
256	ok,ok	0.0	0.34	30.0	32.3	16.1	0.05	0.10	0.27	0.91	2d8/12 L=41	28,46,42
	s=1,m=1	41.5	0.34	30.0	32.3	16.1	0.05	0.09	0.27	0.91	2d8/12 L=41	28,43,43
253	ok,ok	0.0	0.34	30.0	32.3	16.1	0.08	0.09	0.27	0.90	2d8/12 L=41	28,46,42
	s=1,m=1	41.5	0.34	30.0	32.3	16.1	0.05	0.08	0.27	0.90	2d8/12 L=41	28,43,43
250	ok,ok	0.0	0.34	30.0	32.3	16.1	0.08	0.09	0.26	0.88	2d8/12 L=41	28,46,42
	s=1,m=1	41.5	0.34	30.0	32.3	16.1	0.05	0.08	0.27	0.90	2d8/12 L=41	28,43,43
247	ok,ok	0.0	0.34	30.0	32.3	16.1	0.08	0.09	0.26	0.89	2d8/12 L=41	28,46,46
	s=1,m=1	41.5	0.34	30.0	32.3	16.1	0.05	0.08	0.26	0.89	2d8/12 L=41	28,43,43
244	ok,ok	0.0	0.34	30.0	32.3	16.1	0.05	0.09	0.28	0.93	2d8/12 L=41	28,46,46
	s=1,m=1	41.5	0.34	30.0	32.3	16.1	0.05	0.07	0.26	0.90	2d8/12 L=41	28,46,46
241	ok,ok	0.0	0.34	30.0	32.3	20.9	0.05	0.08	0.36	0.82	2d8/8 L=41	28,46,46
	s=1,m=1	41.5	0.34	30.0	32.3	21.4	0.05	0.05	0.34	0.80	2d8/8 L=41	28,46,46
237	ok,ok	0.0	0.34	30.0	32.3	21.4	0.05	0.06	0.34	0.80	2d8/8 L=41	28,46,46
	s=1,m=1	41.5	0.34	30.0	32.3	21.9	0.05	0.08	0.36	0.84	2d8/8 L=41	28,43,43
233	ok,ok	0.0	0.34	30.0	32.3	21.9	0.05	0.09	0.36	0.84	2d8/8 L=41	28,43,43
	s=1,m=1	41.5	0.34	30.0	32.3	22.5	0.05	0.13	0.40	0.91	2d8/8 L=41	28,43,43
229	ok,ok	0.0	0.34	30.0	32.3	20.1	0.05	0.05	0.28	0.76	2d8/10 L=41	28,43,43
	s=1,m=1	41.5	0.34	30.0	32.3	20.1	0.08	0.06	0.32	0.86	2d8/10 L=41	28,43,43
225	ok,ok	0.0	0.34	30.0	32.3	16.1	0.05	0.05	0.24	0.83	2d8/12 L=41	28,43,43
	s=1,m=1	41.5	0.34	30.0	32.3	16.1	0.08	0.07	0.28	0.95	2d8/12 L=41	28,43,43
221	ok,ok	0.0	0.34	30.0	32.3	16.1	0.08	0.06	0.22	0.76	2d8/12 L=41	28,46,46
	s=1,m=1	41.5	0.34	30.0	32.3	16.1	0.08	0.07	0.25	0.86	2d8/12 L=41	28,43,43
217	ok,ok	0.0	0.34	30.0	32.3	16.1	0.08	0.05	0.21	0.87	2d8/15 L=41	28,46,46
	s=1,m=1	41.5	0.34	30.0	32.3	16.1	0.08	0.06	0.23	0.96	2d8/15 L=41	28,43,43
213	ok,ok	0.0	0.34	30.0	32.3	12.1	0.08	0.05	0.20	0.82	2d8/15 L=41	28,46,46
	s=1,m=1	41.5	0.34	30.0	32.3	16.1	0.08	0.06	0.21	0.88	2d8/15 L=41	28,43,43
209	ok,ok	0.0	0.34	30.0	32.3	12.1	0.08	0.05	0.19	0.76	2d8/15 L=41	28,46,46
	s=1,m=1	41.5	0.34	30.0	32.3	12.1	0.08	0.05	0.20	0.81	2d8/15 L=41	28,43,43
205	ok,ok	0.0	0.34	30.0	32.3	12.1	0.08	0.05	0.24	0.71	2d8/15 L=41	28,38,46
	s=1,m=1	41.5	0.34	30.0	32.3	12.1	0.08	0.05	0.26	0.75	2d8/15 L=41	28,35,43
201	ok,ok	0.0	0.34	30.0	32.3	0.0	0.08	0.04	0.23	0.13	2d8/25 L=41	28,46,30
	s=1,m=1	41.5	0.34	30.0	32.3	0.0	0.08	0.04	0.25	0.14	2d8/25 L=41	28,43,23
197	ok,ok	0.0	0.34	30.0	32.3	0.0	0.08	0.04	0.21	0.14	2d8/25 L=41	28,46,30
	s=1,m=1	41.5	0.34	30.0	32.3	0.0	0.08	0.03	0.22	0.14	2d8/25 L=41	28,43,23
193	ok,ok	0.0	0.34	30.0	32.3	0.0	0.08	0.03	0.19	0.14	2d8/25 L=41	44,38,26
	s=1,m=1	41.5	0.34	30.0	32.3	0.0	0.08	0.03	0.21	0.15	2d8/25 L=41	44,35,23
189	ok,ok	0.0	0.34	30.0	32.3	0.0	0.08	0.03	0.18	0.15	2d8/25 L=41	44,38,26
	s=1,m=1	41.5	0.34	30.0	32.3	0.0	0.08	0.03	0.19	0.15	2d8/25 L=41	44,35,23
185	ok,ok	0.0	0.34	30.0	32.3	0.0	0.08	0.03	0.16	0.15	2d8/25 L=41	44,38,26
	s=1,m=1	41.5	0.34	30.0	32.3	0.0	0.08	0.03	0.17	0.15	2d8/25 L=41	44,35,23
181	ok,ok	0.0	0.34	30.0	32.3	0.0	0.08	0.03	0.16	0.15	2d8/25 L=41	44,26,26
	s=1,m=1	41.5	0.34	30.0	32.3	0.0	0.08	0.03	0.16	0.15	2d8/25 L=41	44,23,23
177	ok,ok	0.0	0.34	30.0	32.3	0.0	0.08	0.03	0.16	0.15	2d8/25 L=41	44,26,26
	s=1,m=1	41.5	0.34	30.0	32.3	0.0	0.08	0.03	0.16	0.15	2d8/25 L=41	44,23,23
173	ok,ok	0.0	0.34	30.0	32.3	0.0	0.08	0.03	0.16	0.15	2d8/25 L=41	42,26,26
	s=1,m=1	41.5	0.34	30.0	32.3	0.0	0.08	0.03	0.16	0.16	2d8/25 L=41	42,23,23
169	ok,ok	0.0	0.34	30.0	32.3	0.0	0.05	0.03	0.16	0.15	2d8/25 L=41	42,26,26
	s=1,m=1	41.5	0.34	30.0	32.3	0.0	0.08	0.03	0.17	0.16	2d8/25 L=41	42,23,23
165	ok,ok	0.0	0.34	30.0	32.3	0.0	0.05	0.03	0.17	0.15	2d8/25 L=41	42,30,26
	s=1,m=1	41.5	0.34	30.0	32.3	0.0	0.08	0.03	0.17	0.16	2d8/25 L=41	42,27,23
161	ok,ok	0.0	0.34	30.0	32.3	0.0	0.05	0.03	0.18	0.15	2d8/25 L=41	42,30,26
	s=1,m=1	41.5	0.34	30.0	32.3	0.0	0.08	0.03	0.18	0.16	2d8/25 L=41	42,27,23
157	ok,ok	0.0	0.34	30.0	32.3	0.0	0.05	0.03	0.19	0.15	2d8/25 L=41	42,30,26
	s=1,m=1	41.5	0.34	30.0	32.3	0.0	0.08	0.03	0.19	0.16	2d8/25 L=41	42,27,23
153	ok,ok	0.0	0.34	30.0	32.3	0.0	0.05	0.04	0.21	0.15	2d8/25 L=41	18,46,26
	s=1,m=1	41.5	0.34	30.0	32.3	0.0	0.08	0.03	0.20	0.17	2d8/25 L=41	22,27,23
149	ok,ok	0.0	0.34	30.0	32.3	0.0	0.05	0.04	0.23	0.15	2d8/25 L=41	26,46,26
	s=1,m=1	41.5	0.34	30.0	32.3	0.0	0.08	0.04	0.22	0.17	2d8/25 L=41	22,43,23
145	ok,ok	0.0	0.34	30.0	32.3	12.1	0.05	0.05	0.25	0.94	2d8/20 L=41	26,46,42
	s=1,m=1	41.5	0.34	30.0	32.3	12.1	0.08	0.05	0.24	0.75	2d8/20 L=41	30,43,42
141	ok,ok	0.0	0.34	30.0	32.3	12.1	0.05	0.06	0.24	0.76	2d8/15 L=41	26,38,46
	s=1,m=1	41.5	0.34	30.0	32.3	12.1	0.08	0.05	0.24	0.73	2d8/15 L=41	26,35,43
137	ok,ok	0.0	0.34	30.0	32.3	12.1	0.05	0.07	0.26	0.81	2d8/15 L=41	26,38,46
	s=1,m=1	41.5	0.34	30.0	32.3	12.1	0.08	0.06	0.25	0.78	2d8/15 L=41	26,35,43
133	ok,ok	0.0	0.34	30.0	32.3	12.1	0.05	0.08	0.22	0.86	2d8/15 L=41	26,30,46
	s=1,m=1	41.5	0.34	30.0	32.3	12.1	0.08	0.07	0.23	0.83	2d8/15 L=41	26,27,43
129	ok,ok	0.0	0.34	30.0	32.3	16.1	0.05	0.09	0.22	0.89	2d8/15 L=41	26,37,46
	s=1,m=1	41.5	0.34	30.0	32.3	12.1	0.08	0.08	0.23	0.88	2d8/15 L=41	26,36,43
125	ok,ok	0.0	0.34	30.0	32.3	16.1	0.05	0.10	0.23	0.93	2d8/15 L=41	26,46,46
	s=1,m=1	41.5	0.34	30.0	32.3	16.1	0.08	0.09	0.23	0.92	2d8/15 L=41	26,27,43
121	ok,ok	0.0	0.34	30.0	32.3	16.1	0.05	0.11	0.24	0.96	2d8/15 L=41	26,46,46
	s=1,m=1	41.5	0.34	30.0	32.3	16.1	0.08	0.10	0.24	0.95	2d8/15 L=41	26,43,43
117	ok,ok	0.0	0.34	30.0	32.3	16.1	0.05	0.12	0.24	0.98	2d8/15 L=41	26,46,46
	s=1,m=1	41.5	0.34	30.0	32.3	16.1	0.08	0.11	0.24	0.98	2d8/15 L=41	26,43,43
113	ok,ok	0.0	0.34	30.0	32.3	16.1	0.05	0.13	0.25	0.84	2d8/12 L=41	26,46,46
	s=1,m=1	41.5	0.34	30.0	32.3	16.1	0.08	0.12	0.25	0.84	2d8/12 L=41	26,43,43
108	ok,ok	0.0	0.34	30.0	32.3	16.1	0.05	0.14	0.25	0.85	2d8/12 L=41	26,46,46
	s=1,m=1	41.5	0.34	30.0	32.3	16.1	0.08	0.13	0.26	0.85	2d8/12 L=41	26,43,43
102	ok,ok	0.0	0.34	30.0	32.3	16.1	0.05	0.16	0.26	0.86	2d8/12 L=41	26,46,46
	s=1,m=1	41.5	0.34	30.0	32.3	16.1	0.08	0.15	0.26	0.86	2d8/12 L=41	26,43,43
96	ok,ok	0.0	0.34	30.0	32.3	16.1	0.08	0.17	0.26	0.87	2d8/12 L=41	26,46,46
	s=1,m=1	41.5	0.34	30.0	32.3	16.1	0.08	0.16	0.26	0.88	2d8/12 L=41	26,43,43
90	ok,ok	0.0	0.34	30.0	32.3	16.1	0.08	0.18	0.26	0.89	2d8/12 L=41	26,46,46
	s=1,m=1	41.5	0.34	30.0	32.3	16.1	0.08	0.17	0.27	0.88	2d8/12 L=41	26,43,43
84	ok,ok	0.0	0.34	30.0	32.3	16.1	0.08	0.19	0.27	0.90	2d8/12 L=41	26,46,46
	s=1,m=1	41.5	0.34	30.0	32.3	16.1	0.08	0.18	0.27	0.89	2d8/12 L=41	26,43,43
78	ok,ok	0.0	0.34	30.0	32.3	16.1	0.08	0.20	0.27	0.90	2d8/12 L=41	26,46,46
	s=1,m=1	41.5	0.34	30.0	32.3	16.1	0.08	0.19	0.27	0.88	2d8/12 L=41	26,43,43
72	ok,ok	0.0	0.34	30.0	32.3	16.1	0.08	0.21	0.27	0.90	2d8/12 L=41	26,46,46
	s=1,m=1	41.5	0.34	30.0	32.3	16.1	0.08	0.21	0.26	0.86	2d8/12 L=41	26,43,43
66	ok,ok	0.0	0.34	30.0	32.3	16.1	0.08	0.21	0.27	0.91	2d8/12 L=41	26,46,42
	s=1,m=1	41.5	0.34	30.0	32.3	16.1	0.08	0.22	0.26	0.84	2d8/12 L=41	26,43,39
60	ok,ok	0.0	0.34	30.0	32.3	16.1	0.05	0.22	0.28	0.92	2d8/12 L=41	26,46,42
	s=1,m=1	41.5	0.34	30.0	32.3	16.1	0.05	0.22	0.25	0.82	2d8/12 L=41</	

	s=1,m=1	41.5	0.34	30.0	32.3	17.3	0.05	0.25	0.40	0.74	2d8/8 L=41	26,27,43
36	ok,ok	0.0	0.34	30.0	32.3	17.3	0.05	0.24	0.40	0.74	2d8/8 L=41	26,27,43
	s=1,m=1	41.5	0.34	30.0	32.3	17.1	0.05	0.27	0.44	0.79	2d8/8 L=41	26,27,43
30	ok,ok	0.0	0.34	30.0	32.3	17.1	0.05	0.27	0.45	0.79	2d8/8 L=41	26,27,43
	s=1,m=1	41.5	0.34	30.0	32.3	17.0	0.08	0.24	0.49	0.84	2d8/8 L=41	26,27,43
24	ok,ok	0.0	0.34	30.0	32.3	17.0	0.08	0.23	0.49	0.84	2d8/8 L=41	26,27,43
	s=1,m=1	41.5	0.34	30.0	32.3	16.9	0.08	0.22	0.53	0.90	2d8/8 L=41	18,27,43
19	ok,ok	0.0	0.34	30.0	32.3	12.1	0.08	0.34	0.46	0.73	2d8/10 L=41	25,35,43
	s=1,m=1	41.5	0.34	30.0	32.3	12.1	0.08	0.33	0.51	0.81	2d8/10 L=41	25,35,43
6	ok,ok	0.0	0.34	30.0	32.3	0.0	0.08	0.18	0.19	0.21	2d8/25 L=47	17,11,11
	s=1,m=1	46.7	0.34	30.0	32.3	0.0	0.08	0.17	0.12	0.10	2d8/25 L=47	17,25,46
337	ok,ok	0.0	0.34	30.0	32.3	0.0	0.08	0.16	0.20	0.23	2d8/25 L=47	17,11,11
	s=1,m=1	46.7	0.34	30.0	32.3	0.0	0.08	0.15	0.14	0.11	2d8/25 L=47	25,25,11
331	ok,ok	0.0	0.34	30.0	32.3	0.0	0.08	0.15	0.19	0.22	2d8/25 L=47	25,11,11
	s=1,m=1	46.7	0.34	30.0	32.3	0.0	0.05	0.13	0.12	0.10	2d8/25 L=47	25,25,11
297	ok,ok	0.0	0.34	30.0	32.3	0.0	0.08	0.13	0.17	0.19	2d8/25 L=40	25,25,11
	s=1,m=1	40.0	0.34	30.0	32.3	0.0	0.05	0.12	0.12	0.08	2d8/25 L=40	25,25,11
335	ok,ok	0.0	0.34	30.0	32.3	0.0	0.08	0.12	0.17	0.17	2d8/25 L=40	26,25,30
	s=1,m=1	40.0	0.34	30.0	32.3	0.0	0.05	0.11	0.12	0.08	2d8/25 L=40	26,25,26
341	ok,ok	0.0	0.34	30.0	32.3	0.0	0.08	0.11	0.17	0.17	2d8/25 L=40	26,25,30
	s=1,m=1	40.0	0.34	30.0	32.3	0.0	0.05	0.10	0.11	0.07	2d8/25 L=40	26,25,30
343	ok,ok	0.0	0.34	30.0	32.3	0.0	0.05	0.10	0.16	0.16	2d8/25 L=40	26,30,30
	s=1,m=1	40.0	0.34	30.0	32.3	0.0	0.05	0.09	0.11	0.07	2d8/25 L=40	26,25,30
345	ok,ok	0.0	0.34	30.0	32.3	0.0	0.05	0.10	0.16	0.15	2d8/25 L=40	26,30,30
	s=1,m=1	40.0	0.34	30.0	32.3	0.0	0.05	0.08	0.10	0.07	2d8/25 L=40	26,25,27
347	ok,ok	0.0	0.34	30.0	32.3	0.0	0.05	0.09	0.15	0.14	2d8/25 L=40	26,30,30
	s=1,m=1	40.0	0.34	30.0	32.3	0.0	0.05	0.08	0.09	0.06	2d8/25 L=40	26,25,27
349	ok,ok	0.0	0.34	30.0	32.3	0.0	0.05	0.08	0.14	0.12	2d8/25 L=40	26,30,30
	s=1,m=1	40.0	0.34	30.0	32.3	0.0	0.05	0.07	0.08	0.05	2d8/25 L=40	26,30,27
351	ok,ok	0.0	0.34	30.0	32.3	0.0	0.05	0.07	0.13	0.11	2d8/25 L=40	26,26,30
	s=1,m=1	40.0	0.34	30.0	32.3	0.0	0.05	0.07	0.07	0.05	2d8/25 L=40	26,23,23
353	ok,ok	0.0	0.34	30.0	32.3	0.0	0.05	0.07	0.12	0.09	2d8/25 L=40	26,26,30
	s=1,m=1	40.0	0.34	30.0	32.3	0.0	0.05	0.06	0.08	0.06	2d8/25 L=40	26,23,23
355	ok,ok	0.0	0.34	30.0	32.3	0.0	0.05	0.06	0.11	0.07	2d8/25 L=40	26,30,30
	s=1,m=1	40.0	0.34	30.0	32.3	0.0	0.05	0.06	0.10	0.10	2d8/25 L=40	26,23,15
357	ok,ok	0.0	0.34	30.0	32.3	0.0	0.05	0.06	0.09	0.08	2d8/25 L=40	26,27,27
	s=1,m=1	40.0	0.34	30.0	32.3	0.0	0.05	0.06	0.13	0.15	2d8/25 L=40	26,23,3
359	ok,ok	0.0	0.34	30.0	32.3	0.0	0.05	0.06	0.12	0.11	2d8/25 L=40	26,23,27
	s=1,m=1	40.0	0.34	30.0	32.3	0.0	0.05	0.07	0.16	0.21	2d8/25 L=40	26,15,3
361	ok,ok	0.0	0.34	30.0	32.3	0.0	0.05	0.06	0.13	0.12	2d8/25 L=40	26,23,15
	s=1,m=1	40.0	0.34	30.0	32.3	0.0	0.08	0.08	0.18	0.23	2d8/25 L=40	26,15,3
363	ok,ok	0.0	0.34	30.0	32.3	0.0	0.05	0.07	0.12	0.11	2d8/25 L=40	26,23,15
	s=1,m=1	40.0	0.34	30.0	32.3	0.0	0.08	0.08	0.18	0.23	2d8/25 L=40	26,15,3
M_T= 5 Z=0.0 N=5 N=7												
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
7	ok,ok	0.0	0.33	39.5	38.6	0.0	0.05	0.12	0.30	0.26	2d8/25 L=40	35,19,43
	s=2,m=1	40.1	0.33	39.5	38.6	0.0	0.09	0.11	0.37	0.36	2d8/25 L=40	35,19,43
328	ok,ok	0.0	0.33	39.5	38.6	0.0	0.05	0.11	0.26	0.23	2d8/25 L=40	35,19,43
	s=2,m=1	40.1	0.33	39.5	38.6	0.0	0.09	0.10	0.33	0.33	2d8/25 L=40	35,15,43
326	ok,ok	0.0	0.33	39.5	38.6	0.0	0.05	0.10	0.24	0.19	2d8/25 L=40	35,15,43
	s=2,m=1	40.1	0.33	39.5	38.6	0.0	0.09	0.09	0.31	0.29	2d8/25 L=40	35,15,43
324	ok,ok	0.0	0.33	39.5	38.6	0.0	0.05	0.09	0.22	0.17	2d8/25 L=40	35,15,27
	s=2,m=1	40.1	0.33	39.5	38.6	0.0	0.09	0.09	0.29	0.28	2d8/25 L=40	35,15,23
322	ok,ok	0.0	0.33	39.5	38.6	0.0	0.05	0.09	0.22	0.17	2d8/25 L=40	33,15,23
	s=2,m=1	40.1	0.33	39.5	38.6	0.0	0.09	0.10	0.29	0.28	2d8/25 L=40	33,15,23
320	ok,ok	0.0	0.33	39.5	38.6	0.0	0.05	0.10	0.21	0.18	2d8/25 L=40	33,15,23
	s=2,m=1	40.1	0.33	39.5	38.6	0.0	0.09	0.10	0.28	0.29	2d8/25 L=40	33,15,23
318	ok,ok	0.0	0.33	39.5	38.6	0.0	0.05	0.11	0.21	0.19	2d8/25 L=40	33,15,23
	s=2,m=1	40.1	0.33	39.5	38.6	0.0	0.09	0.11	0.28	0.30	2d8/25 L=40	33,15,23
316	ok,ok	0.0	0.33	39.5	38.6	0.0	0.05	0.11	0.21	0.20	2d8/25 L=40	33,15,23
	s=2,m=1	40.1	0.33	39.5	38.6	0.0	0.09	0.12	0.28	0.30	2d8/25 L=40	33,15,23
314	ok,ok	0.0	0.33	39.5	38.6	0.0	0.05	0.12	0.21	0.20	2d8/25 L=40	17,15,23
	s=2,m=1	40.1	0.33	39.5	38.6	0.0	0.09	0.13	0.28	0.31	2d8/25 L=40	33,15,23
312	ok,ok	0.0	0.33	39.5	38.6	0.0	0.09	0.14	0.20	0.20	2d8/25 L=40	17,15,23
	s=2,m=1	40.1	0.33	39.5	38.6	0.0	0.09	0.15	0.27	0.31	2d8/25 L=40	17,15,23
310	ok,ok	0.0	0.33	39.5	38.6	0.0	0.09	0.16	0.19	0.19	2d8/25 L=40	17,15,23
	s=2,m=1	40.1	0.33	39.5	38.6	0.0	0.09	0.17	0.26	0.30	2d8/25 L=40	17,15,23
308	ok,ok	0.0	0.33	39.5	38.6	0.0	0.09	0.18	0.18	0.17	2d8/25 L=40	17,15,23
	s=2,m=1	40.1	0.33	39.5	38.6	0.0	0.09	0.18	0.25	0.28	2d8/25 L=40	17,15,23
306	ok,ok	0.0	0.33	39.5	38.6	0.0	0.09	0.20	0.15	0.14	2d8/25 L=40	17,15,26
	s=2,m=1	40.1	0.33	39.5	38.6	0.0	0.09	0.19	0.23	0.25	2d8/25 L=40	17,15,23
304	ok,ok	0.0	0.33	39.5	38.6	0.0	0.09	0.21	0.16	0.16	2d8/25 L=40	17,18,26
	s=2,m=1	40.1	0.33	39.5	38.6	0.0	0.09	0.20	0.19	0.20	2d8/25 L=40	17,15,23
302	ok,ok	0.0	0.33	39.5	38.6	0.0	0.09	0.22	0.16	0.17	2d8/25 L=40	17,18,26
	s=2,m=1	40.1	0.33	39.5	38.6	0.0	0.09	0.21	0.15	0.15	2d8/25 L=40	17,23,23
300	ok,ok	0.0	0.33	39.5	38.6	0.0	0.09	0.22	0.17	0.16	2d8/25 L=40	17,11,46
	s=2,m=1	40.1	0.33	39.5	38.6	0.0	0.09	0.22	0.12	0.07	2d8/25 L=40	17,35,27
298	ok,ok	0.0	0.33	39.5	38.6	0.0	0.09	0.23	0.19	0.21	2d8/25 L=40	17,9,18
	s=2,m=1	40.1	0.33	39.5	38.6	0.0	0.05	0.22	0.12	0.10	2d8/25 L=40	17,31,18
M_T= 6 Z=0.0 N=7 N=12												
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
8	ok,ok	0.0	0.34	30.0	32.3	0.0	0.08	0.06	0.50	0.33	2d8/25 L=47	37,18,18
	s=1,m=1	46.7	0.34									

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Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
11	ok,ok	0.0	0.33	39.5	38.6	0.0	0.09	0.30	0.22	0.20	2d8/25 L=40	26,38,38
	s=2,m=1	40.1	0.33	39.5	38.6	0.0	0.05	0.29	0.14	0.10	2d8/25 L=40	26,38,35
299	ok,ok	0.0	0.33	39.5	38.6	0.0	0.09	0.28	0.21	0.17	2d8/25 L=40	26,26,30
	s=2,m=1	40.1	0.33	39.5	38.6	0.0	0.09	0.28	0.13	0.12	2d8/25 L=40	26,26,27
301	ok,ok	0.0	0.33	39.5	38.6	0.0	0.09	0.26	0.25	0.22	2d8/25 L=40	26,26,30
	s=2,m=1	40.1	0.33	39.5	38.6	0.0	0.09	0.27	0.17	0.18	2d8/25 L=40	26,26,27
303	ok,ok	0.0	0.33	39.5	38.6	0.0	0.09	0.24	0.28	0.25	2d8/25 L=40	26,26,30
	s=2,m=1	40.1	0.33	39.5	38.6	0.0	0.09	0.26	0.20	0.19	2d8/25 L=40	26,26,27
305	ok,ok	0.0	0.33	39.5	38.6	0.0	0.09	0.23	0.30	0.27	2d8/25 L=40	26,26,26
	s=2,m=1	40.1	0.33	39.5	38.6	0.0	0.09	0.24	0.22	0.17	2d8/25 L=40	26,26,27
307	ok,ok	0.0	0.33	39.5	38.6	0.0	0.09	0.21	0.31	0.29	2d8/25 L=40	26,26,30
	s=2,m=1	40.1	0.33	39.5	38.6	0.0	0.09	0.22	0.23	0.17	2d8/25 L=40	26,26,30
309	ok,ok	0.0	0.33	39.5	38.6	0.0	0.09	0.20	0.32	0.29	2d8/25 L=40	26,26,30
	s=2,m=1	40.1	0.33	39.5	38.6	0.0	0.09	0.20	0.25	0.18	2d8/25 L=40	26,26,30
311	ok,ok	0.0	0.33	39.5	38.6	0.0	0.09	0.18	0.33	0.29	2d8/25 L=40	26,26,30
	s=2,m=1	40.1	0.33	39.5	38.6	0.0	0.09	0.17	0.26	0.19	2d8/25 L=40	26,26,30
313	ok,ok	0.0	0.33	39.5	38.6	0.0	0.09	0.16	0.34	0.30	2d8/25 L=40	38,26,11
	s=2,m=1	40.1	0.33	39.5	38.6	0.0	0.09	0.15	0.27	0.18	2d8/25 L=40	26,26,30
315	ok,ok	0.0	0.33	39.5	38.6	0.0	0.09	0.15	0.34	0.31	2d8/25 L=40	38,26,11
	s=2,m=1	40.1	0.33	39.5	38.6	0.0	0.05	0.14	0.27	0.18	2d8/25 L=40	38,26,30
317	ok,ok	0.0	0.33	39.5	38.6	0.0	0.09	0.14	0.35	0.32	2d8/25 L=40	38,26,11
	s=2,m=1	40.1	0.33	39.5	38.6	0.0	0.05	0.12	0.28	0.18	2d8/25 L=40	38,26,30
319	ok,ok	0.0	0.33	39.5	38.6	0.0	0.09	0.13	0.35	0.32	2d8/25 L=40	38,26,11
	s=2,m=1	40.1	0.33	39.5	38.6	0.0	0.05	0.11	0.29	0.18	2d8/25 L=40	38,26,46
321	ok,ok	0.0	0.33	39.5	38.6	0.0	0.09	0.11	0.36	0.32	2d8/25 L=40	38,26,11
	s=2,m=1	40.1	0.33	39.5	38.6	0.0	0.05	0.10	0.29	0.19	2d8/25 L=40	38,26,46
323	ok,ok	0.0	0.33	39.5	38.6	0.0	0.09	0.10	0.37	0.33	2d8/25 L=40	32,26,11
	s=2,m=1	40.1	0.33	39.5	38.6	0.0	0.05	0.08	0.30	0.20	2d8/25 L=40	32,26,46
325	ok,ok	0.0	0.33	39.5	38.6	0.0	0.09	0.09	0.38	0.34	2d8/25 L=40	32,26,46
	s=2,m=1	40.1	0.33	39.5	38.6	0.0	0.05	0.07	0.32	0.23	2d8/25 L=40	32,26,46
327	ok,ok	0.0	0.33	39.5	38.6	0.0	0.09	0.08	0.41	0.38	2d8/25 L=40	32,30,46
	s=2,m=1	40.1	0.33	39.5	38.6	0.0	0.05	0.06	0.35	0.28	2d8/25 L=40	40,26,46
329	ok,ok	0.0	0.33	39.5	38.6	0.0	0.09	0.06	0.46	0.43	2d8/25 L=40	32,30,46
	s=2,m=1	40.1	0.33	39.5	38.6	0.0	0.05	0.08	0.39	0.33	2d8/25 L=40	40,30,46
M. T= 26 Z=380.0 N=17 N=18												
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
922	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	0.06	0.33	0.69	2d8/25 L=41	43,40,46
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	0.01	0.34	0.70	2d8/25 L=41	46,45,43
1299	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	0.02	0.29	0.72	2d8/25 L=41	43,46,46
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	6.74e-03	0.29	0.71	2d8/25 L=41	28,43,43
1296	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	8.12e-03	0.30	0.73	2d8/25 L=41	27,42,42
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	9.50e-03	0.30	0.72	2d8/25 L=41	23,39,39
1293	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	7.79e-03	0.31	0.73	2d8/25 L=41	27,42,42
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	4.16e-03	0.31	0.74	2d8/25 L=41	23,39,39
1290	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	3.35e-03	0.32	0.75	2d8/25 L=41	11,39,42
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	3.31e-03	0.32	0.77	2d8/25 L=41	27,39,39
1287	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	2.95e-03	0.33	0.78	2d8/25 L=41	27,39,39
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	3.27e-03	0.33	0.79	2d8/25 L=41	11,39,39
1284	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	4.84e-03	0.33	0.80	2d8/25 L=41	30,39,39
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	4.51e-03	0.33	0.79	2d8/25 L=41	27,39,39
1281	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	6.65e-03	0.33	0.78	2d8/25 L=41	27,42,42
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	2.95e-03	0.33	0.78	2d8/25 L=41	9,39,39
1278	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	4.57e-03	0.32	0.76	2d8/25 L=41	27,46,46
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	3.58e-03	0.32	0.77	2d8/25 L=41	27,43,43
1274	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	1.08e-03	0.32	0.75	2d8/25 L=41	27,40,40
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	3.78e-03	0.32	0.76	2d8/25 L=41	27,41,41
1270	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	2.83e-03	0.31	0.73	2d8/25 L=41	29,44,44
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	2.83e-03	0.31	0.73	2d8/25 L=41	25,45,45
1266	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	3.98e-03	0.29	0.70	2d8/25 L=41	27,44,44
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	4.56e-03	0.29	0.70	2d8/25 L=41	27,44,44
1262	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	3.31e-03	0.28	0.67	2d8/25 L=41	28,44,44
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	2.59e-03	0.28	0.67	2d8/25 L=41	9,44,44
1258	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	4.55e-03	0.28	0.66	2d8/25 L=41	26,44,44
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	3.77e-03	0.28	0.66	2d8/25 L=41	30,44,44
1254	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	5.17e-03	0.28	0.65	2d8/25 L=41	30,44,44
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	4.83e-03	0.28	0.65	2d8/25 L=41	27,44,44
1250	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	5.77e-03	0.27	0.64	2d8/25 L=41	27,44,44
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	3.59e-03	0.27	0.64	2d8/25 L=41	27,44,44
1246	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	4.34e-03	0.26	0.62	2d8/25 L=41	27,40,40
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	1.68e-03	0.26	0.62	2d8/25 L=41	43,40,40
1242	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	2.88e-03	0.25	0.59	2d8/25 L=41	27,40,40
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	1.54e-03	0.25	0.59	2d8/25 L=41	29,40,40
1238	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	2.16e-03	0.30	0.55	2d8/25 L=41	27,32,40
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	1.97e-03	0.30	0.55	2d8/25 L=41	25,32,40
1234	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	1.98e-03	0.30	0.50	2d8/25 L=41	27,39,40
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	2.11e-03	0.30	0.50	2d8/25 L=41	25,42,40
1230	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	1.98e-03	0.28	7.34e-03	2d8/25 L=41	27,40,23
	s=12,m=1	41.5	0.45	4.0	4.0	0.0	0.13	2.11e-03	0.28	7.72e-03	2d8/25 L=41	25,40,26
1226	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	2.03e-03	0.25	7.46e-03	2d8/25 L=41	27,40,23
	s=12,m=1	41.5	0.45	4.0	4.0	0.0	0.13	2.02e-03	0.25	7.82e-03	2d8/25 L=41	25,40,26
1222	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	2.07e-03	0.22	7.51e-03	2d8/25 L=41	27,40,23
	s=12,m=1	41.5	0.45	4.0	4.0	0.0	0.13	1.90e-03	0.22	7.80e-03	2d8/25 L=41	25,40,26
1218	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	2.09e-03	0.19	7.50e-03	2d8/25 L=41	23,40,23
	s=12,m=1	41.5	0.45	4.0	4.0	0.0	0.13	1.77e-03	0.19	7.70e-03	2d8/25 L=41	29,40,26
1214	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	2.10e-03	0.17	7.47e-03	2d8/25 L=41	23,32,23
	s=12,m=1	41.5	0.45	4.0	4.0	0.0	0.13	1.64e-03	0.17	7.56e-03	2d8/25 L=41	29,32,26
1210	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	2.11e-03	0.14	7.42e-03	2d8/25 L=41	23,32,23
	s=12,m=1	41.5	0.45	4.0	4.0	0.0	0.13	1.52e-03	0.14	7.43e-03	2d8/25 L=41	29,32,26
1206	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	2.12e-03	0.12	7.37e-03	2d8/25 L=41	23,32,23
	s=12,m=1	41.5	0.45	4.0	4.0	0.0	0.13	1.42e-03	0.12	7.31e-03	2d8/25 L=41	29,32,26
1202	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	2.13e-03	0.11	7.30e-03	2d8/25 L=41	23,32,23
	s=12,m=1	41.5	0.45	4.0	4.0	0.0	0.13	1.33e-03	0.11	7.22e-03	2d8/25 L=41	28,32,26
1198	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	2.16e-03	0.10	7.22e-03	2d8/25 L=41	23,32,23
	s=12,m=1	41.5	0.45	4.0	4.0	0.0	0.13	1.25e-03	0.10	7.17e-03	2d8/2	

1182	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	2.34e-03	0.17	6.89e-03	2d8/25 L=41	23,39,23
	s=12,m=1	41.5	0.45	4.0	4.0	0.0	0.13	1.01e-03	0.17	7.23e-03	2d8/25 L=41	29,42,26
1178	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	2.43e-03	0.21	6.86e-03	2d8/25 L=41	23,39,23
	s=12,m=1	41.5	0.45	4.0	4.0	0.0	0.13	9.60e-04	0.21	7.28e-03	2d8/25 L=41	29,42,26
1174	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	2.53e-03	0.24	6.86e-03	2d8/25 L=41	23,39,23
	s=12,m=1	41.5	0.45	4.0	4.0	0.0	0.13	9.20e-04	0.24	7.34e-03	2d8/25 L=41	29,42,26
1170	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	2.64e-03	0.27	6.89e-03	2d8/25 L=41	23,39,24
	s=12,m=1	41.5	0.45	4.0	4.0	0.0	0.13	8.88e-04	0.27	7.43e-03	2d8/25 L=41	29,39,25
1166	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	2.76e-03	0.29	6.94e-03	2d8/25 L=41	23,39,24
	s=12,m=1	41.5	0.45	4.0	4.0	0.0	0.13	8.66e-04	0.29	7.53e-03	2d8/25 L=41	29,39,25
1161	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	2.89e-03	0.29	0.52	2d8/25 L=41	23,44,39
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	8.53e-04	0.29	0.52	2d8/25 L=41	29,45,39
1153	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	3.02e-03	0.28	0.55	2d8/25 L=41	23,31,39
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	8.49e-04	0.28	0.55	2d8/25 L=41	29,31,39
1146	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	3.15e-03	0.30	0.58	2d8/25 L=41	23,31,39
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	8.67e-04	0.30	0.58	2d8/25 L=41	45,31,39
1140	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	3.30e-03	0.30	0.61	2d8/25 L=41	23,37,39
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	8.96e-04	0.30	0.61	2d8/25 L=41	45,37,39
1135	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	3.45e-03	0.27	0.63	2d8/25 L=41	23,39,39
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	9.27e-04	0.27	0.63	2d8/25 L=41	45,39,39
1128	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	3.63e-03	0.28	0.66	2d8/25 L=41	23,39,39
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	9.58e-04	0.28	0.66	2d8/25 L=41	45,39,39
1121	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	3.84e-03	0.29	0.67	2d8/25 L=41	23,39,39
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	9.87e-04	0.29	0.67	2d8/25 L=41	45,39,39
1114	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	4.07e-03	0.29	0.69	2d8/25 L=41	23,39,39
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	1.01e-03	0.29	0.69	2d8/25 L=41	45,39,39
1107	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	4.33e-03	0.30	0.71	2d8/25 L=41	23,39,39
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	1.02e-03	0.30	0.71	2d8/25 L=41	45,39,39
1098	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	4.61e-03	0.31	0.72	2d8/25 L=41	23,39,39
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	1.02e-03	0.31	0.72	2d8/25 L=41	45,39,39
1089	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	4.89e-03	0.31	0.73	2d8/25 L=41	23,39,39
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	1.01e-03	0.31	0.73	2d8/25 L=41	45,39,39
1078	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	5.15e-03	0.31	0.74	2d8/25 L=41	23,39,39
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	1.02e-03	0.31	0.74	2d8/25 L=41	37,39,39
1068	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	5.32e-03	0.32	0.75	2d8/25 L=41	23,39,39
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	1.21e-03	0.31	0.74	2d8/25 L=41	31,39,39
1057	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	5.34e-03	0.31	0.74	2d8/25 L=41	23,39,39
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	1.53e-03	0.31	0.74	2d8/25 L=41	31,39,39
1045	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	5.04e-03	0.31	0.73	2d8/25 L=41	23,39,39
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	2.22e-03	0.31	0.73	2d8/25 L=41	3,39,39
1032	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	4.16e-03	0.29	0.70	2d8/25 L=41	23,39,39
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	4.25e-03	0.29	0.70	2d8/25 L=41	25,39,39
1019	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	3.90e-03	0.27	0.65	2d8/25 L=41	4,41,41
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	7.32e-03	0.27	0.66	2d8/25 L=41	25,41,41
1004	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	5.55e-03	0.25	0.60	2d8/25 L=41	29,41,41
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	8.19e-03	0.25	0.59	2d8/25 L=41	25,41,41
987	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	4.44e-03	0.29	0.54	2d8/25 L=41	29,43,41
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	9.43e-03	0.29	0.52	2d8/25 L=41	24,43,41
970	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	2.75e-03	0.28	0.01	2d8/25 L=41	34,41,23
	s=12,m=1	41.5	0.45	4.0	4.0	0.0	0.13	9.35e-03	0.27	6.52e-03	2d8/25 L=41	24,41,26
955	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	9.50e-03	0.24	0.02	2d8/25 L=41	26,41,23
	s=12,m=1	41.5	0.45	4.0	4.0	0.0	0.13	8.33e-03	0.23	9.48e-03	2d8/25 L=41	23,41,26
941	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.20	0.02	2d8/25 L=41	26,41,23
	s=12,m=1	41.5	0.45	4.0	4.0	0.0	0.13	0.01	0.19	0.01	2d8/25 L=41	4,41,23
932	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.02	0.17	0.04	2d8/25 L=41	26,45,4
	s=12,m=1	41.5	0.45	4.0	4.0	0.0	0.13	0.04	0.17	0.03	2d8/25 L=41	25,45,25
927	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.04	0.13	0.04	2d8/25 L=47	30,40,30
	s=12,m=1	46.7	0.45	4.0	4.0	0.0	0.13	5.73e-03	0.14	0.04	2d8/25 L=47	43,40,30
959	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	8.50e-03	0.04	0.03	2d8/25 L=47	42,32,16
	s=12,m=1	46.7	0.45	4.0	4.0	0.0	0.13	0.05	0.05	0.04	2d8/25 L=47	16,32,16
945	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.07	0.06	0.05	2d8/25 L=47	24,45,26
	s=12,m=1	46.7	0.45	4.0	4.0	0.0	0.13	0.03	0.07	0.06	2d8/25 L=47	16,45,26
936	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.02	0.02	0.03	2d8/25 L=40	29,37,25
	s=12,m=1	40.0	0.45	4.0	4.0	0.0	0.13	0.02	0.03	0.03	2d8/25 L=40	24,27,24
1102	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.03	0.04	2d8/25 L=40	29,3,18
	s=12,m=1	40.0	0.45	4.0	4.0	0.0	0.13	0.03	0.02	0.03	2d8/25 L=40	16,3,18
1093	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.04	0.02	0.03	2d8/25 L=40	16,25,17
	s=12,m=1	40.0	0.45	4.0	4.0	0.0	0.13	6.76e-03	0.03	0.03	2d8/25 L=40	19,24,16
1082	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.04	0.03	0.03	2d8/25 L=40	24,24,25
	s=12,m=1	40.0	0.45	4.0	4.0	0.0	0.13	3.83e-03	0.03	0.04	2d8/25 L=40	25,24,24
1072	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.02	0.02	0.03	2d8/25 L=40	24,25,25
	s=12,m=1	40.0	0.45	4.0	4.0	0.0	0.13	5.18e-03	0.02	0.02	2d8/25 L=40	26,24,25
1061	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.02	0.02	2d8/25 L=40	23,26,26
	s=12,m=1	40.0	0.45	4.0	4.0	0.0	0.13	7.37e-03	0.02	0.02	2d8/25 L=40	23,23,23
1049	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	9.76e-03	0.02	0.02	2d8/25 L=40	15,27,19
	s=12,m=1	40.0	0.45	4.0	4.0	0.0	0.13	0.02	0.02	0.03	2d8/25 L=40	27,27,19
1036	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.04	0.05	2d8/25 L=40	28,16,15
	s=12,m=1	40.0	0.45	4.0	4.0	0.0	0.13	0.07	0.05	0.06	2d8/25 L=40	24,16,15
1023	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.08	0.04	0.05	2d8/25 L=40	23,24,25
	s=12,m=1	40.0	0.45	4.0	4.0	0.0	0.13	0.03	0.04	0.06	2d8/25 L=40	3,24,25
1009	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.06	0.02	0.02	2d8/25 L=40	3,11,25
	s=12,m=1	40.0	0.45	4.0	4.0	0.0	0.13	0.03	0.01	0.01	2d8/25 L=40	15,27,25
992	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.03	0.02	0.03	2d8/25 L=40	3,25,25
	s=12,m=1	40.0	0.45	4.0	4.0	0.0	0.13	0.02	0.02	0.02	2d8/25 L=40	26,23,25
975	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.02	0.05	0.07	2d8/25 L=40	23,3,19
	s=12,m=1	40.0	0.45	4.0	4.0	0.0	0.13	0.09	0.04	0.06	2d8/25 L=40	15,15,19
961	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.08	0.05	0.06	2d8/25 L=40	15,23,23
	s=12,m=1	40.0	0.45	4.0	4.0	0.0	0.13	0.02	0.06	0.07	2d8/25 L=40	3,23,23
950	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.04	0.05	0.04	2d8/25 L=40	15,26,23
	s=12,m=1	40.0	0.45	4.0	4.0	0.0	0.13	0.02	0.05	0.05	2d8/25 L=40	25,23,23
M_T= 27 Z=380.0 N=16 N=18												
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
923	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.11	0.11	2d8/25 L=40	17,18,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.01	0.09	0.08	2d8/25 L=40	3,18,3
1129	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	7.16e-03	0.12	0.10	2d8/25 L=40	3,18,3
	s=12,m											

	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	3.84e-03	0.12	0.09	2d8/25 L=40	34,18,4
1099	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	6.86e-03	0.13	0.11	2d8/25 L=40	37,18,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	6.12e-03	0.12	0.08	2d8/25 L=40	24,18,4
1090	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	9.41e-03	0.13	0.11	2d8/25 L=40	25,18,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	8.99e-03	0.12	0.08	2d8/25 L=40	24,18,4
1079	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	9.93e-03	0.13	0.11	2d8/25 L=40	18,18,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	8.99e-03	0.13	0.09	2d8/25 L=40	25,18,4
1069	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.13	0.09	2d8/25 L=40	15,18,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.02	0.15	0.10	2d8/25 L=40	42,18,3
1058	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	8.56e-03	0.12	0.09	2d8/25 L=40	19,18,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.02	0.15	0.11	2d8/25 L=40	18,18,3
1046	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.04	0.12	0.09	2d8/25 L=40	16,18,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.05	0.13	0.11	2d8/25 L=40	16,18,4
1033	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.02	0.12	0.09	2d8/25 L=40	15,22,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	5.10e-03	0.11	0.11	2d8/25 L=40	37,17,4
1020	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.11	0.10	2d8/25 L=40	37,18,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	8.21e-03	0.10	0.09	2d8/25 L=40	36,18,4
1005	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.10	0.10	2d8/25 L=40	37,18,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.01	0.10	0.09	2d8/25 L=40	36,21,4
988	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.09	0.10	2d8/25 L=40	4,18,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.01	0.10	0.10	2d8/25 L=40	37,18,4
971	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.08	0.09	2d8/25 L=40	34,17,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.01	0.10	0.11	2d8/25 L=40	4,18,3
956	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	9.20e-03	0.07	0.08	2d8/25 L=40	31,25,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.02	0.09	0.11	2d8/25 L=40	34,22,3
942	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.06	0.05	2d8/25 L=40	16,15,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.01	0.07	0.08	2d8/25 L=40	18,18,3
1276	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.03	0.05	0.05	2d8/25 L=40	16,24,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.01	0.06	0.08	2d8/25 L=40	16,25,3
1272	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	8.61e-03	0.04	0.05	2d8/25 L=40	36,3,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.02	0.06	0.08	2d8/25 L=40	15,4,4
1268	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	7.03e-03	0.06	0.07	2d8/25 L=40	16,4,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.02	0.06	0.06	2d8/25 L=40	15,4,4
1264	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.02	0.09	0.09	2d8/25 L=40	16,4,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	4.82e-03	0.05	0.04	2d8/25 L=40	18,4,4
1260	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.08	0.09	2d8/25 L=40	15,4,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.01	0.05	0.04	2d8/25 L=40	24,4,4
1256	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.07	0.07	2d8/25 L=40	34,4,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	8.04e-03	0.07	0.06	2d8/25 L=40	24,4,3
1252	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.06	0.06	2d8/25 L=40	32,4,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	6.94e-03	0.07	0.07	2d8/25 L=40	18,4,3
1248	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	8.59e-03	0.06	0.06	2d8/25 L=40	17,4,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	9.46e-03	0.07	0.07	2d8/25 L=40	11,4,3
1244	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	5.68e-03	0.06	0.06	2d8/25 L=40	34,4,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	7.26e-03	0.06	0.07	2d8/25 L=40	16,4,4
1240	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	3.51e-03	0.06	0.06	2d8/25 L=40	23,4,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	5.98e-03	0.06	0.07	2d8/25 L=40	16,4,3
1236	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	5.08e-03	0.06	0.07	2d8/25 L=40	24,4,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	4.63e-03	0.05	0.06	2d8/25 L=40	16,4,3
1232	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	6.19e-03	0.05	0.07	2d8/25 L=40	24,4,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	3.59e-03	0.05	0.06	2d8/25 L=40	15,4,3
1228	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	7.08e-03	0.05	0.07	2d8/25 L=40	24,4,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	3.30e-03	0.05	0.06	2d8/25 L=40	37,4,3
1224	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	8.18e-03	0.05	0.07	2d8/25 L=40	16,3,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	5.53e-03	0.05	0.06	2d8/25 L=40	25,4,4
1220	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	9.80e-03	0.05	0.06	2d8/25 L=40	16,23,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	9.43e-03	0.05	0.06	2d8/25 L=40	25,3,4
1216	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.06	0.06	2d8/25 L=40	16,23,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.01	0.06	0.07	2d8/25 L=40	26,26,4
1212	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.06	0.06	2d8/25 L=40	24,24,23
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.02	0.07	0.07	2d8/25 L=40	38,25,4
1208	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	5.84e-03	0.07	0.04	2d8/25 L=40	24,25,33
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.03	0.07	0.09	2d8/25 L=40	32,30,4
1204	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.05	0.07	0.07	2d8/25 L=40	16,24,16
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	7.83e-03	0.10	0.09	2d8/25 L=40	38,25,17
1200	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.02	0.04	0.06	2d8/25 L=40	23,23,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	7.48e-03	0.05	0.07	2d8/25 L=40	32,4,4
1196	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.05	0.06	2d8/25 L=40	35,17,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	7.97e-03	0.05	0.07	2d8/25 L=40	17,4,3
1192	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.11	0.10	2d8/25 L=40	17,22,18
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.05	0.06	0.05	2d8/25 L=40	34,22,15
1188	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.03	0.08	0.06	2d8/25 L=40	36,17,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	3.68e-03	0.08	0.06	2d8/25 L=40	36,22,4
1184	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.03	0.07	0.06	2d8/25 L=40	16,17,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	6.38e-03	0.07	0.07	2d8/25 L=40	15,16,3
1180	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.06	0.07	2d8/25 L=40	16,17,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	5.98e-03	0.06	0.06	2d8/25 L=40	15,16,3
1176	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	6.03e-03	0.05	0.07	2d8/25 L=40	18,4,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	3.00e-03	0.05	0.06	2d8/25 L=40	31,15,3
1172	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	4.03e-03	0.05	0.07	2d8/25 L=40	36,4,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	7.61e-03	0.04	0.06	2d8/25 L=40	24,4,3
1168	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	7.30e-03	0.05	0.07	2d8/25 L=40	24,20,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.02	0.05	0.06	2d8/25 L=40	23,4,4
1163	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	6.91e-03	0.05	0.07	2d8/25 L=40	23,4,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.02	0.05	0.06	2d8/25 L=40	23,26,4
1156	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	1.84e-03	0.06	0.05	2d8/25 L=40	31,25,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.02	0.06	0.07	2d8/25 L=40	33,3,4
1149	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.04	0.05	0.04	2d8/25 L=40	25,25,24
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.02	0.09	0.11	2d8/25 L=40	3,25,4
1143	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.03	0.05	0.06	2d8/25 L=40	23,19,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.02	0.05	0.07	2d8/25 L=40	24,16,4
1138	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.02	0.08	0.07	2d8/25 L=40	23,17,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.02	0.08	0.06	2d8/25 L=40	24,16,3
1133	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.03	0.15	0.12	2d8/25 L=40	4,17,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.05	0.10	0.02	2d8/25 L=40	38,17,26
1126	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.13	0.07	2d8/25 L=40	32,24,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	8.70e-03				

1104	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	6.41e-03	0.10	0.07	2d8/25 L=40	26,25,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	7.89e-03	0.10	0.06	2d8/25 L=40	26,24,3
1095	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	6.16e-03	0.09	0.08	2d8/25 L=40	24,24,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.01	0.07	0.05	2d8/25 L=40	9,25,3
1084	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.03	0.12	0.11	2d8/25 L=40	24,24,24
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.04	0.07	0.06	2d8/25 L=40	24,25,25
1074	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.07	0.10	0.08	2d8/25 L=40	23,23,26
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.03	0.15	0.13	2d8/25 L=40	26,23,23
1063	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.06	0.05	2d8/25 L=40	26,26,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.02	0.07	0.07	2d8/25 L=40	23,4,4
1051	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.05	0.05	2d8/25 L=40	9,25,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.02	0.06	0.08	2d8/25 L=40	23,4,4
1038	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.05	0.06	2d8/25 L=40	9,3,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.01	0.06	0.07	2d8/25 L=40	23,4,4
1025	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	8.67e-03	0.05	0.06	2d8/25 L=40	9,3,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	9.12e-03	0.05	0.07	2d8/25 L=40	23,3,4
1011	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	4.78e-03	0.05	0.07	2d8/25 L=40	9,4,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	7.04e-03	0.04	0.06	2d8/25 L=40	11,3,3
994	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	1.92e-03	0.05	0.07	2d8/25 L=40	9,26,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.01	0.05	0.06	2d8/25 L=40	23,23,3
977	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	3.53e-03	0.08	0.06	2d8/25 L=40	24,26,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.04	0.08	0.07	2d8/25 L=40	24,23,4
963	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.03	0.10	0.09	2d8/25 L=40	24,26,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.01	0.10	0.11	2d8/25 L=40	23,23,4
981	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	9.01e-03	0.10	0.10	2d8/25 L=40	9,25,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	6.03e-03	0.10	0.10	2d8/25 L=40	11,25,4
999	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	9.00e-03	0.10	0.12	2d8/25 L=40	25,24,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.02	0.10	0.08	2d8/25 L=40	24,25,3
933	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.02	0.07	0.09	2d8/25 L=40	23,4,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	8.58e-03	0.08	0.11	2d8/25 L=40	9,3,3
947	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.02	0.08	0.10	2d8/25 L=40	24,4,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.01	0.07	0.09	2d8/25 L=40	23,4,3
966	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	3.64e-03	0.08	0.10	2d8/25 L=40	3,4,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	8.94e-03	0.08	0.10	2d8/25 L=40	23,4,3
983	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	1.66e-03	0.08	0.10	2d8/25 L=40	3,4,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	8.71e-03	0.08	0.10	2d8/25 L=40	23,4,4
1001	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	1.79e-03	0.08	0.10	2d8/25 L=40	12,4,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	9.87e-03	0.08	0.10	2d8/25 L=40	23,4,4
1016	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	2.10e-03	0.08	0.10	2d8/25 L=40	12,26,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.01	0.08	0.10	2d8/25 L=40	23,4,4
1029	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	8.98e-03	0.08	0.10	2d8/25 L=40	24,26,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	3.03e-03	0.08	0.10	2d8/25 L=40	4,4,4
1042	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	5.39e-03	0.08	0.10	2d8/25 L=40	23,29,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.01	0.08	0.10	2d8/25 L=40	23,25,4
928	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	5.92e-03	0.09	0.10	2d8/25 L=40	36,26,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	4.34e-03	0.08	0.10	2d8/25 L=40	27,30,4
937	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	3.56e-03	0.09	0.10	2d8/25 L=40	3,25,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	6.09e-03	0.08	0.10	2d8/25 L=40	23,25,3
951	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	3.60e-03	0.09	0.10	2d8/25 L=40	3,25,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	6.70e-03	0.08	0.10	2d8/25 L=40	23,25,3
979	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	5.00e-03	0.08	0.10	2d8/25 L=40	3,25,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.01	0.08	0.10	2d8/25 L=40	23,3,3
968	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	6.40e-03	0.08	0.09	2d8/25 L=40	3,3,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.01	0.09	0.10	2d8/25 L=40	15,3,3
985	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	7.20e-03	0.08	0.09	2d8/25 L=40	3,3,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.01	0.10	0.11	2d8/25 L=40	25,3,3
M_T= 28 Z=380.0 N=19 N=20												
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T	cls	Staffe	Rif. cmb
924	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.02	0.15	0.10	2d8/25 L=40	42,42,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	6.35e-03	0.15	0.09	2d8/25 L=40	20,39,4
1130	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.12	0.09	2d8/25 L=40	18,22,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.01	0.13	0.11	2d8/25 L=40	46,42,4
1123	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.02	0.13	0.10	2d8/25 L=40	18,18,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.02	0.12	0.10	2d8/25 L=40	40,22,4
1116	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.02	0.14	0.10	2d8/25 L=40	41,21,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	9.50e-03	0.12	0.10	2d8/25 L=40	39,21,4
1109	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.02	0.14	0.10	2d8/25 L=40	22,21,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	7.55e-03	0.13	0.10	2d8/25 L=40	40,21,4
1100	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.14	0.09	2d8/25 L=40	11,21,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	8.29e-03	0.14	0.11	2d8/25 L=40	4,21,4
1091	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.13	0.09	2d8/25 L=40	11,21,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	9.34e-03	0.15	0.11	2d8/25 L=40	4,21,4
1080	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.14	0.08	2d8/25 L=40	11,21,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.01	0.15	0.12	2d8/25 L=40	4,21,4
1070	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.02	0.14	0.08	2d8/25 L=40	11,21,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.01	0.15	0.12	2d8/25 L=40	40,21,4
1059	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.02	0.14	0.09	2d8/25 L=40	11,21,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	5.34e-03	0.15	0.10	2d8/25 L=40	18,21,4
1047	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.02	0.15	0.11	2d8/25 L=40	11,21,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	8.67e-03	0.14	0.09	2d8/25 L=40	16,21,3
1034	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.02	0.16	0.12	2d8/25 L=40	11,17,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	9.12e-03	0.14	0.08	2d8/25 L=40	17,17,3
1021	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.02	0.15	0.09	2d8/25 L=40	35,17,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.01	0.15	0.11	2d8/25 L=40	16,17,4
1006	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.02	0.11	0.06	2d8/25 L=40	35,17,9
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.05	0.18	0.23	2d8/25 L=40	11,17,11
989	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.02	0.18	0.25	2d8/25 L=40	35,9,9
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.11	0.28	0.42	2d8/25 L=40	11,11,11
972	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.04	0.32	0.52	2d8/25 L=40	33,9,9
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.22	0.43	0.70	2d8/25 L=40	11,11,11
957	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.07	0.65	0.74	2d8/20 L=40	33,20,11
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.41	0.72	0.88	2d8/20 L=40	11,20,11
943	ok,ok	0.0	0.34	10.3	10.3	0.0	0.05	0.12	0.22	0.21	2d8/25 L=40	11,15,9
	s=13,m=1	40.1	0.34	10.3	10.3	0.0	0.05	0.07	0.23	0.22	2d8/25 L=40	11,15,9
964	ok,ok	0.0	0.34	10.3	10.3	0.0	0.05	0.06	0.15	0.20	2d8/25 L=40	11,9,9
	s=13,m=1	40.1	0.34	10.3	10.3	0.0	0.05	0.04	0.16	0.21	2d8/25 L=40	11,9,9
934	ok,ok	0.0	0.34	10.3	10.3	0.0	0.05	0.03	0.21	0.30	2d8/25 L=40	11,9,9
	s=13,m=1	40.1	0.34	10.3	10.3	0.0	0.05	0.04	0.22	0.32	2d8/25 L=4	

	s=13,m=1	40.1	0.34	10.3	10.3	0.0	0.05	0.11	0.32	0.46	2d8/25 L=40	11,11,11
1008	ok,ok	0.0	0.34	10.3	10.3	0.0	0.05	0.08	0.33	0.48	2d8/25 L=40	11,11,11
	s=13,m=1	40.1	0.34	10.3	10.3	0.0	0.05	0.18	0.34	0.49	2d8/25 L=40	11,11,11
991	ok,ok	0.0	0.34	10.3	10.3	0.0	0.05	0.16	0.34	0.50	2d8/25 L=40	11,11,11
	s=13,m=1	40.1	0.34	10.3	10.3	0.0	0.05	0.29	0.35	0.51	2d8/25 L=40	11,11,11
974	ok,ok	0.0	0.34	10.3	10.3	0.0	0.05	0.29	0.34	0.50	2d8/25 L=40	11,11,11
	s=13,m=1	40.1	0.45	13.4	10.3	0.0	0.06	0.28	0.35	0.51	2d8/25 L=40	11,11,11
1052	ok,ok	0.0	0.45	13.4	10.3	0.0	0.06	0.28	0.32	0.46	2d8/25 L=40	11,11,11
	s=13,m=1	40.1	0.45	13.4	10.3	0.0	0.06	0.38	0.33	0.48	2d8/25 L=40	11,11,11
1039	ok,ok	0.0	0.55	16.6	10.3	0.0	0.07	0.26	0.26	0.38	2d8/25 L=40	11,11,11
	s=13,m=1	40.1	0.55	16.6	10.3	0.0	0.07	0.32	0.27	0.39	2d8/25 L=40	11,11,11
1026	ok,ok	0.0	0.55	16.6	10.3	0.0	0.07	0.33	0.15	0.21	2d8/25 L=40	11,11,11
	s=13,m=1	40.1	0.55	16.6	10.3	0.0	0.07	0.36	0.16	0.22	2d8/25 L=40	11,11,11
1054	ok,ok	0.0	0.66	19.7	10.3	0.0	0.11	0.26	0.04	0.02	2d8/25 L=40	11,33,32
	s=13,m=1	40.1	0.55	16.6	10.3	0.0	0.07	0.37	0.04	0.02	2d8/25 L=40	11,33,33
1041	ok,ok	0.0	0.66	19.7	10.3	0.0	0.11	0.27	0.12	0.17	2d8/25 L=40	11,11,11
	s=13,m=1	40.1	0.55	16.6	10.3	0.0	0.07	0.33	0.11	0.16	2d8/25 L=40	11,11,11
1013	ok,ok	0.0	0.55	16.6	10.3	0.0	0.07	0.35	0.17	0.25	2d8/25 L=40	11,11,11
	s=13,m=1	40.1	0.55	16.6	10.3	0.0	0.07	0.27	0.17	0.24	2d8/25 L=40	11,11,11
1085	ok,ok	0.0	0.55	16.6	10.3	0.0	0.07	0.29	0.18	0.27	2d8/25 L=40	11,11,11
	s=13,m=1	40.1	0.45	13.4	10.3	0.0	0.06	0.35	0.17	0.25	2d8/25 L=40	11,11,11
1075	ok,ok	0.0	0.45	13.4	10.3	0.0	0.06	0.36	0.16	0.24	2d8/25 L=40	11,11,11
	s=13,m=1	40.1	0.45	13.4	10.3	0.0	0.06	0.26	0.15	0.23	2d8/25 L=40	11,11,11
1086	ok,ok	0.0	0.45	13.4	10.3	0.0	0.06	0.28	0.14	0.21	2d8/25 L=40	11,16,11
	s=13,m=1	40.1	0.45	13.4	10.3	0.0	0.06	0.20	0.13	0.19	2d8/25 L=40	11,16,11
1064	ok,ok	0.0	0.45	13.4	10.3	0.0	0.06	0.22	0.13	0.17	2d8/25 L=40	11,16,11
	s=13,m=1	40.1	0.34	10.3	10.3	0.0	0.05	0.31	0.12	0.16	2d8/25 L=40	11,16,11
1053	ok,ok	0.0	0.34	10.3	10.3	0.0	0.05	0.33	0.12	0.14	2d8/25 L=40	11,16,11
	s=13,m=1	40.1	0.34	10.3	10.3	0.0	0.05	0.24	0.12	0.13	2d8/25 L=40	11,16,11
1065	ok,ok	0.0	0.34	10.3	10.3	0.0	0.05	0.26	0.12	0.11	2d8/25 L=40	11,16,11
	s=13,m=1	40.1	0.34	10.3	10.3	0.0	0.05	0.20	0.11	0.10	2d8/25 L=40	11,16,11
1040	ok,ok	0.0	0.34	10.3	10.3	0.0	0.05	0.22	0.11	0.10	2d8/25 L=40	11,16,11
	s=13,m=1	40.1	0.34	10.3	10.3	0.0	0.05	0.17	0.11	0.09	2d8/25 L=40	11,16,11
1028	ok,ok	0.0	0.34	10.3	10.3	0.0	0.05	0.19	0.11	0.08	2d8/25 L=40	11,16,11
	s=13,m=1	40.1	0.34	10.3	10.3	0.0	0.05	0.15	0.10	0.07	2d8/25 L=40	11,16,11
998	ok,ok	0.0	0.34	10.3	10.3	0.0	0.05	0.17	0.10	0.08	2d8/25 L=40	11,16,11
	s=13,m=1	40.1	0.34	10.3	10.3	0.0	0.05	0.14	0.10	0.06	2d8/25 L=40	11,16,9
1027	ok,ok	0.0	0.34	10.3	10.3	0.0	0.05	0.15	0.10	0.07	2d8/25 L=40	11,16,11
	s=13,m=1	40.1	0.34	10.3	10.3	0.0	0.05	0.12	0.09	0.06	2d8/25 L=40	11,16,9
1015	ok,ok	0.0	0.34	10.3	10.3	0.0	0.05	0.14	0.09	0.07	2d8/25 L=40	11,20,11
	s=13,m=1	40.1	0.34	10.3	10.3	0.0	0.05	0.11	0.09	0.06	2d8/25 L=40	11,20,9
960	ok,ok	0.0	0.34	10.3	10.3	0.0	0.05	0.12	0.10	0.07	2d8/25 L=40	11,15,11
	s=13,m=1	40.1	0.34	10.3	10.3	0.0	0.05	0.10	0.09	0.06	2d8/25 L=40	11,15,9
996	ok,ok	0.0	0.34	10.3	10.3	0.0	0.05	0.11	0.10	0.07	2d8/25 L=40	11,15,11
	s=13,m=1	40.1	0.34	10.3	10.3	0.0	0.05	0.10	0.09	0.06	2d8/25 L=40	11,15,9
980	ok,ok	0.0	0.34	10.3	10.3	0.0	0.05	0.11	0.10	0.08	2d8/25 L=40	11,15,11
	s=13,m=1	40.1	0.34	10.3	10.3	0.0	0.05	0.09	0.09	0.07	2d8/25 L=40	11,15,9
946	ok,ok	0.0	0.34	10.3	10.3	0.0	0.05	0.10	0.10	0.08	2d8/25 L=40	11,15,11
	s=13,m=1	40.1	0.34	10.3	10.3	0.0	0.05	0.08	0.10	0.07	2d8/25 L=40	11,15,9
995	ok,ok	0.0	0.34	10.3	10.3	0.0	0.05	0.09	0.11	0.09	2d8/25 L=40	11,15,11
	s=13,m=1	40.1	0.34	10.3	10.3	0.0	0.05	0.07	0.11	0.08	2d8/25 L=40	11,15,9
978	ok,ok	0.0	0.34	10.3	10.3	0.0	0.05	0.08	0.12	0.10	2d8/25 L=40	11,15,11
	s=13,m=1	40.1	0.34	10.3	10.3	0.0	0.05	0.06	0.11	0.09	2d8/25 L=40	11,15,9
965	ok,ok	0.0	0.34	10.3	10.3	0.0	0.05	0.08	0.13	0.12	2d8/25 L=40	11,15,11
	s=13,m=1	40.1	0.34	10.3	10.3	0.0	0.05	0.06	0.13	0.11	2d8/25 L=40	11,15,9
1012	ok,ok	0.0	0.34	10.3	10.3	0.0	0.05	0.07	0.14	0.13	2d8/25 L=40	11,15,11
	s=13,m=1	40.1	0.34	10.3	10.3	0.0	0.05	0.05	0.14	0.12	2d8/25 L=40	11,15,9
997	ok,ok	0.0	0.34	10.3	10.3	0.0	0.05	0.06	0.16	0.15	2d8/25 L=40	11,15,11
	s=13,m=1	40.1	0.34	10.3	10.3	0.0	0.05	0.04	0.15	0.14	2d8/25 L=40	11,15,9
982	ok,ok	0.0	0.34	10.3	10.3	0.0	0.05	0.05	0.16	0.16	2d8/25 L=40	11,20,11
	s=13,m=1	40.1	0.34	10.3	10.3	0.0	0.05	0.03	0.16	0.15	2d8/25 L=40	11,20,9
1014	ok,ok	0.0	0.34	10.3	10.3	0.0	0.05	0.04	0.17	0.17	2d8/25 L=40	11,28,11
	s=13,m=1	40.1	0.34	10.3	10.3	0.0	0.05	0.02	0.17	0.16	2d8/25 L=40	11,28,9
1000	ok,ok	0.0	0.34	10.3	10.3	0.0	0.05	0.04	0.18	0.19	2d8/25 L=40	11,28,11
	s=13,m=1	40.1	0.34	10.3	10.3	0.0	0.05	0.01	0.18	0.18	2d8/25 L=40	11,28,9
938	ok,ok	0.0	0.34	10.3	10.3	0.0	0.05	0.03	0.19	0.20	2d8/25 L=40	11,24,11
	s=13,m=1	40.1	0.34	10.3	10.3	0.0	0.05	6.24e-03	0.18	0.19	2d8/25 L=40	32,24,9
1155	ok,ok	0.0	0.34	10.3	10.3	0.0	0.05	0.02	0.18	0.20	2d8/25 L=40	11,28,11
	s=13,m=1	40.1	0.34	10.3	10.3	0.0	0.05	5.03e-03	0.17	0.19	2d8/25 L=40	33,28,9
1148	ok,ok	0.0	0.34	10.3	10.3	0.0	0.05	0.02	0.15	0.19	2d8/25 L=40	11,23,11
	s=13,m=1	40.1	0.34	10.3	10.3	0.0	0.05	6.62e-03	0.15	0.18	2d8/25 L=40	33,23,9
1142	ok,ok	0.0	0.34	10.3	10.3	0.0	0.05	0.01	0.15	0.16	2d8/25 L=40	24,11,11
	s=13,m=1	40.1	0.34	10.3	10.3	0.0	0.05	7.69e-03	0.14	0.15	2d8/25 L=40	25,9,9
1158	ok,ok	0.0	0.34	10.3	10.3	0.0	0.05	6.11e-03	0.09	0.04	2d8/25 L=40	17,16,17
	s=13,m=1	40.1	0.34	10.3	10.3	0.0	0.05	0.02	0.09	0.04	2d8/25 L=40	24,16,16
1151	ok,ok	0.0	0.34	10.3	10.3	0.0	0.05	6.82e-03	0.06	0.06	2d8/25 L=40	17,16,16
	s=13,m=1	40.1	0.34	10.3	10.3	0.0	0.05	0.02	0.06	0.06	2d8/25 L=40	24,16,16
1137	ok,ok	0.0	0.34	10.3	10.3	0.0	0.05	7.25e-03	0.06	0.07	2d8/25 L=40	31,23,16
	s=13,m=1	40.1	0.34	10.3	10.3	0.0	0.05	0.03	0.06	0.07	2d8/25 L=40	11,23,16
1164	ok,ok	0.0	0.34	10.3	10.3	0.0	0.05	0.01	0.07	0.07	2d8/25 L=40	35,23,24
	s=13,m=1	40.1	0.34	10.3	10.3	0.0	0.05	0.04	0.08	0.08	2d8/25 L=40	11,23,24
1157	ok,ok	0.0	0.34	10.3	10.3	0.0	0.05	0.02	0.08	0.08	2d8/25 L=40	11,23,24
	s=13,m=1	40.1	0.34	10.3	10.3	0.0	0.05	0.06	0.09	0.08	2d8/25 L=40	11,23,24
1150	ok,ok	0.0	0.34	10.3	10.3	0.0	0.05	0.04	0.09	0.07	2d8/25 L=40	11,23,23
	s=13,m=1	40.1	0.34	10.3	10.3	0.0	0.05	0.08	0.09	0.08	2d8/25 L=40	11,23,23
1159	ok,ok	0.0	0.34	10.3	10.3	0.0	0.05	0.06	0.06	0.04	2d8/25 L=40	11,30,26
	s=13,m=1	40.1	0.34	10.3	10.3	0.0	0.05	0.10	0.07	0.04	2d8/25 L=40	11,27,23
1144	ok,ok	0.0	0.34	10.3	10.3	0.0	0.05	0.09	0.15	0.17	2d8/25 L=40	11,11,11
	s=13,m=1	40.1	0.34	10.3	10.3	0.0	0.05	0.12	0.14	0.15	2d8/25 L=40	11,11,11
1132	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.23	0.41	0.61	2d8/25 L=40	23,11,11
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.03	0.34	0.43	2d8/25 L=40	26,27,9
1125	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.11	0.24	0.39	2d8/25 L=40	11,11,11
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.02	0.15	0.22	2d8/25 L=40	26,23,9
1118	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.05	0.21	0.28	2d8/25 L=40	11,11,11
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.01	0.11	0.11	2d8/25 L=40	11,9,9
1111	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.04	0.14	0.		

1083	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	8.29e-03	0.09	0.12	2d8/25 L=40	23,4,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.01	0.07	0.08	2d8/25 L=40	25,26,3
1073	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	9.19e-03	0.09	0.12	2d8/25 L=40	23,4,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	9.28e-03	0.07	0.08	2d8/25 L=40	25,26,3
1062	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	8.78e-03	0.08	0.12	2d8/25 L=40	23,4,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	8.14e-03	0.07	0.08	2d8/25 L=40	25,30,3
1050	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	8.20e-03	0.08	0.12	2d8/25 L=40	23,4,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	6.35e-03	0.08	0.08	2d8/25 L=40	4,30,3
1037	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	5.51e-03	0.09	0.11	2d8/25 L=40	27,30,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	7.03e-03	0.08	0.09	2d8/25 L=40	46,30,3
1024	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	6.37e-03	0.09	0.11	2d8/25 L=40	41,30,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	5.60e-03	0.09	0.09	2d8/25 L=40	30,30,3
1010	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	7.24e-03	0.09	0.11	2d8/25 L=40	35,26,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	5.94e-03	0.09	0.09	2d8/25 L=40	30,30,3
993	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	8.57e-03	0.09	0.11	2d8/25 L=40	43,26,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	7.96e-03	0.09	0.09	2d8/25 L=40	46,26,3
976	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.09	0.11	2d8/25 L=40	43,25,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.01	0.09	0.09	2d8/25 L=40	30,25,3
962	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.10	0.10	2d8/25 L=40	27,41,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.02	0.11	0.10	2d8/25 L=40	25,45,3
952	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.02	0.12	0.09	2d8/25 L=40	27,27,24
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.05	0.15	0.13	2d8/25 L=40	25,45,4
M_T= 29 Z=380.0 N=15 N=17												
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
925	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.09	0.30	0.11	2d8/25 L=40	41,40,40
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.01	0.29	0.10	2d8/25 L=40	39,40,41
930	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.03	0.26	0.04	2d8/25 L=40	40,40,40
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	8.16e-03	0.26	0.04	2d8/25 L=40	39,40,41
939	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	9.65e-03	0.20	0.02	2d8/25 L=40	40,40,40
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	4.51e-03	0.19	0.02	2d8/25 L=40	42,40,41
953	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	4.10e-03	0.15	0.01	2d8/25 L=40	41,20,44
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	4.22e-03	0.15	8.48e-03	2d8/25 L=40	42,20,45
969	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	4.03e-03	0.14	7.35e-03	2d8/25 L=40	45,20,44
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	2.63e-03	0.14	7.26e-03	2d8/25 L=40	44,20,45
986	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	3.69e-03	0.12	5.20e-03	2d8/25 L=40	39,16,44
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	2.93e-03	0.12	7.88e-03	2d8/25 L=40	9,16,45
1003	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	5.96e-03	0.11	5.87e-03	2d8/25 L=40	42,15,44
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	9.44e-03	0.11	7.51e-03	2d8/25 L=40	9,15,45
1018	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.10	0.01	2d8/25 L=40	11,15,11
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	7.87e-03	0.10	4.43e-03	2d8/25 L=40	11,15,45
1031	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	9.71e-03	0.09	0.02	2d8/25 L=40	40,15,11
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	3.26e-03	0.09	0.01	2d8/25 L=40	36,15,11
1044	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	5.90e-03	0.08	0.02	2d8/25 L=40	41,19,11
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.01	0.08	0.01	2d8/25 L=40	11,19,11
1056	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	7.99e-03	0.08	0.02	2d8/25 L=40	41,19,11
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.01	0.08	0.01	2d8/25 L=40	11,19,11
1067	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.10	0.02	2d8/25 L=40	9,19,11
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.02	0.09	9.60e-03	2d8/25 L=40	11,19,11
1077	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.11	0.02	2d8/25 L=40	11,19,11
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.02	0.11	7.92e-03	2d8/25 L=40	11,19,11
1088	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.13	0.01	2d8/25 L=40	11,19,11
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.01	0.13	6.65e-03	2d8/25 L=40	11,19,45
1097	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	8.95e-03	0.16	0.02	2d8/25 L=40	11,15,9
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	9.90e-03	0.15	6.01e-03	2d8/25 L=40	11,15,9
1106	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	4.72e-03	0.19	0.02	2d8/25 L=40	11,15,9
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.01	0.18	0.01	2d8/25 L=40	11,15,9
1113	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	6.85e-03	0.22	0.02	2d8/25 L=40	11,15,9
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.02	0.22	0.01	2d8/25 L=40	9,15,9
1120	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.26	0.02	2d8/25 L=40	11,15,11
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	8.08e-03	0.26	0.03	2d8/25 L=40	36,15,11
1127	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.02	0.28	0.05	2d8/25 L=40	9,18,9
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.01	0.29	0.06	2d8/25 L=40	9,18,9
1134	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	8.44e-03	0.27	0.01	2d8/25 L=40	36,18,11
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.01	0.27	0.02	2d8/25 L=40	9,18,11
1139	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.23	0.01	2d8/25 L=40	9,18,17
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	9.35e-03	0.22	4.55e-03	2d8/25 L=40	9,34,16
1145	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.18	0.01	2d8/25 L=40	9,31,37
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	7.55e-03	0.18	6.72e-03	2d8/25 L=40	36,34,37
1152	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	8.57e-03	0.15	0.01	2d8/25 L=40	9,31,37
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	6.79e-03	0.15	8.65e-03	2d8/25 L=40	34,34,36
1160	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	6.44e-03	0.12	0.01	2d8/25 L=40	25,35,37
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	6.23e-03	0.12	0.01	2d8/25 L=40	34,38,36
1165	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	5.15e-03	0.09	8.84e-03	2d8/25 L=40	25,35,37
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	6.00e-03	0.09	0.01	2d8/25 L=40	34,38,36
1169	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	4.35e-03	0.06	7.11e-03	2d8/25 L=40	25,26,37
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	6.15e-03	0.06	0.01	2d8/25 L=40	34,38,36
1173	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	3.96e-03	0.04	6.09e-03	2d8/25 L=40	25,23,36
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	6.73e-03	0.04	0.01	2d8/25 L=40	34,23,11
1177	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	3.94e-03	0.04	7.88e-03	2d8/25 L=40	37,16,36
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	8.32e-03	0.04	0.02	2d8/25 L=40	9,16,11
1181	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	4.20e-03	0.07	0.01	2d8/25 L=40	37,16,11
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.01	0.07	0.02	2d8/25 L=40	9,16,11
1185	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	5.07e-03	0.11	0.02	2d8/25 L=40	9,17,11
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.01	0.11	0.03	2d8/25 L=40	9,17,11
1189	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	6.40e-03	0.15	8.84e-03	2d8/25 L=40	9,17,11
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	9.77e-03	0.16	0.02	2d8/25 L=40	9,17,11
1193	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	6.36e-03	0.21	0.03	2d8/25 L=40	9,32,11
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.02	0.20	0.02	2d8/25 L=40	36,32,11
1197	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	6.00e-03	0.19	0.11	2d8/25 L=40	9,17,9
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.05	0.19	0.10	2d8/25 L=40	11,17,9
1201	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.02	0.08	0.05	2d8/25 L=40	36,17,9
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.04	0.07	0.04	2d8/25 L=40	9,17,9
1205	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.04	0.12	0.05	2d8/25 L=40	11,36,11
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.02	0.12	0.06	2d8/25 L=40	37,36,11
1209	ok,ok	0.0	0.45	4.0	4.0	0.0						

	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	5.61e-03	0.12	0.01	2d8/25 L=40	9,37,9
1225	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	9.69e-03	0.08	0.02	2d8/25 L=40	9,37,9
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	4.76e-03	0.08	7.58e-03	2d8/25 L=40	34,37,37
1229	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	7.13e-03	0.05	0.01	2d8/25 L=40	9,25,37
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	4.49e-03	0.04	6.29e-03	2d8/25 L=40	34,25,36
1233	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	6.02e-03	0.03	0.01	2d8/25 L=40	37,15,37
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	4.44e-03	0.03	8.22e-03	2d8/25 L=40	34,15,36
1237	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	5.30e-03	0.06	9.40e-03	2d8/25 L=40	37,15,37
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	4.67e-03	0.06	9.93e-03	2d8/25 L=40	34,18,36
1241	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	4.93e-03	0.09	8.05e-03	2d8/25 L=40	37,31,31
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	5.23e-03	0.10	0.01	2d8/25 L=40	34,34,34
1245	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	4.85e-03	0.13	6.80e-03	2d8/25 L=40	37,34,31
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	6.09e-03	0.13	0.01	2d8/25 L=40	34,34,34
1249	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	4.96e-03	0.17	7.85e-03	2d8/25 L=40	37,34,34
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	7.07e-03	0.17	0.02	2d8/25 L=40	34,34,34
1253	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	5.10e-03	0.21	8.66e-03	2d8/25 L=40	37,34,34
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	8.27e-03	0.21	0.02	2d8/25 L=40	9,34,9
1257	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	4.86e-03	0.25	4.48e-03	2d8/25 L=40	37,34,9
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	6.85e-03	0.26	0.01	2d8/25 L=40	9,34,9
1261	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	4.31e-03	0.31	0.02	2d8/25 L=40	9,34,36
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.01	0.30	0.01	2d8/25 L=40	36,34,36
1265	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	4.43e-03	0.30	0.05	2d8/25 L=40	9,34,11
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.02	0.29	0.04	2d8/25 L=40	11,34,11
1269	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.23	0.02	2d8/25 L=40	36,34,9
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.01	0.22	9.01e-03	2d8/25 L=40	11,34,9
1273	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.02	0.16	0.01	2d8/25 L=40	9,34,9
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	8.44e-03	0.16	0.02	2d8/25 L=40	11,34,9
1277	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.10	0.01	2d8/25 L=40	9,34,9
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	4.94e-03	0.11	0.02	2d8/25 L=40	11,34,9
1280	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	8.92e-03	0.07	8.60e-03	2d8/25 L=40	9,18,9
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	3.64e-03	0.07	0.02	2d8/25 L=40	36,18,9
1283	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	6.01e-03	0.05	5.39e-03	2d8/25 L=40	11,18,37
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	3.13e-03	0.06	0.02	2d8/25 L=40	36,18,9
1286	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	4.33e-03	0.05	5.37e-03	2d8/25 L=40	31,18,36
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	2.70e-03	0.05	0.01	2d8/25 L=40	36,18,9
1289	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	3.27e-03	0.04	5.96e-03	2d8/25 L=40	31,18,36
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	2.39e-03	0.04	8.96e-03	2d8/25 L=40	36,18,37
1292	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	2.43e-03	0.05	6.39e-03	2d8/25 L=40	31,16,36
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	2.18e-03	0.05	7.19e-03	2d8/25 L=40	36,17,37
1295	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	1.81e-03	0.05	6.72e-03	2d8/25 L=40	31,17,34
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	2.06e-03	0.05	5.76e-03	2d8/25 L=40	36,17,31
1298	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	1.42e-03	0.06	7.96e-03	2d8/25 L=40	15,16,11
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	2.01e-03	0.06	4.69e-03	2d8/25 L=40	36,16,31
1301	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	1.26e-03	0.07	9.22e-03	2d8/25 L=40	15,24,11
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	2.00e-03	0.06	3.89e-03	2d8/25 L=40	36,24,31
1303	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	1.20e-03	0.07	0.01	2d8/25 L=40	23,24,11
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	2.00e-03	0.07	3.34e-03	2d8/25 L=40	36,24,31
1304	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	1.19e-03	0.08	0.01	2d8/25 L=40	23,28,11
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	2.18e-03	0.08	3.02e-03	2d8/25 L=40	11,28,31
1305	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	1.23e-03	0.08	0.01	2d8/25 L=40	23,28,11
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	2.28e-03	0.08	2.90e-03	2d8/25 L=40	11,28,31
1306	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	1.28e-03	0.09	9.37e-03	2d8/25 L=40	24,28,11
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	2.27e-03	0.08	2.96e-03	2d8/25 L=40	11,28,31
1307	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	1.37e-03	0.09	8.32e-03	2d8/25 L=40	24,44,11
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	2.15e-03	0.09	3.30e-03	2d8/25 L=40	11,44,1
1308	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	1.44e-03	0.10	7.11e-03	2d8/25 L=40	24,44,11
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	1.95e-03	0.09	3.81e-03	2d8/25 L=40	11,44,1
1309	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	1.50e-03	0.10	5.97e-03	2d8/25 L=40	24,40,11
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	1.74e-03	0.10	4.30e-03	2d8/25 L=40	24,40,1
1310	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	1.55e-03	0.10	5.56e-03	2d8/25 L=40	11,40,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	1.65e-03	0.10	5.17e-03	2d8/25 L=40	24,40,9
1311	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	1.52e-03	0.10	5.31e-03	2d8/25 L=40	11,40,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	1.58e-03	0.10	5.72e-03	2d8/25 L=40	28,40,9
1312	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	1.46e-03	0.10	5.19e-03	2d8/25 L=40	24,44,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	1.53e-03	0.10	5.93e-03	2d8/25 L=40	44,44,9
1313	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	1.39e-03	0.10	5.19e-03	2d8/25 L=40	24,44,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	1.55e-03	0.10	5.86e-03	2d8/25 L=40	44,44,9
1314	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	1.31e-03	0.09	5.25e-03	2d8/25 L=40	24,44,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	1.60e-03	0.09	5.62e-03	2d8/25 L=40	44,44,9
1315	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	1.21e-03	0.09	5.35e-03	2d8/25 L=40	24,28,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	1.67e-03	0.09	5.30e-03	2d8/25 L=40	44,28,9
1316	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	1.11e-03	0.09	5.44e-03	2d8/25 L=40	24,24,3
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	1.76e-03	0.09	4.99e-03	2d8/25 L=40	44,24,9
1317	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	1.00e-03	0.10	5.51e-03	2d8/25 L=40	24,24,4
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	1.86e-03	0.10	4.81e-03	2d8/25 L=40	44,24,41
1318	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	8.98e-04	0.10	5.69e-03	2d8/25 L=40	24,23,40
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	1.96e-03	0.10	5.06e-03	2d8/25 L=40	44,23,41
1319	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	8.67e-04	0.11	6.09e-03	2d8/25 L=40	35,23,40
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	2.11e-03	0.11	5.48e-03	2d8/25 L=40	44,23,41
1320	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	1.11e-03	0.12	6.86e-03	2d8/25 L=40	43,43,40
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	2.50e-03	0.12	6.37e-03	2d8/25 L=40	44,43,41
1321	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	1.76e-03	0.15	8.87e-03	2d8/25 L=40	43,43,40
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	3.78e-03	0.16	8.75e-03	2d8/25 L=40	40,43,41
1322	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	3.21e-03	0.19	0.01	2d8/25 L=40	41,43,46
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	8.53e-03	0.20	0.02	2d8/25 L=40	46,43,43
1323	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	6.53e-03	0.25	0.04	2d8/25 L=40	41,43,46
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.03	0.26	0.04	2d8/25 L=40	43,43,43
1324	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.29	0.10	2d8/25 L=40	40,43,43
	s=12,m=1	40.1	0.45	4.0	4.0	0.0	0.13	0.08	0.29	0.10	2d8/25 L=40	46,43,43
M_T= 30 Z=380.0 N=15 N=16												
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
926	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	0.07	0.34	0.72	2d8/25 L=41	40,43,41
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	0.01	0.33	0.72	2d8/25 L=41	39,43,40
1302	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	0.02	0.30	0.72	2d8/25 L=41</	

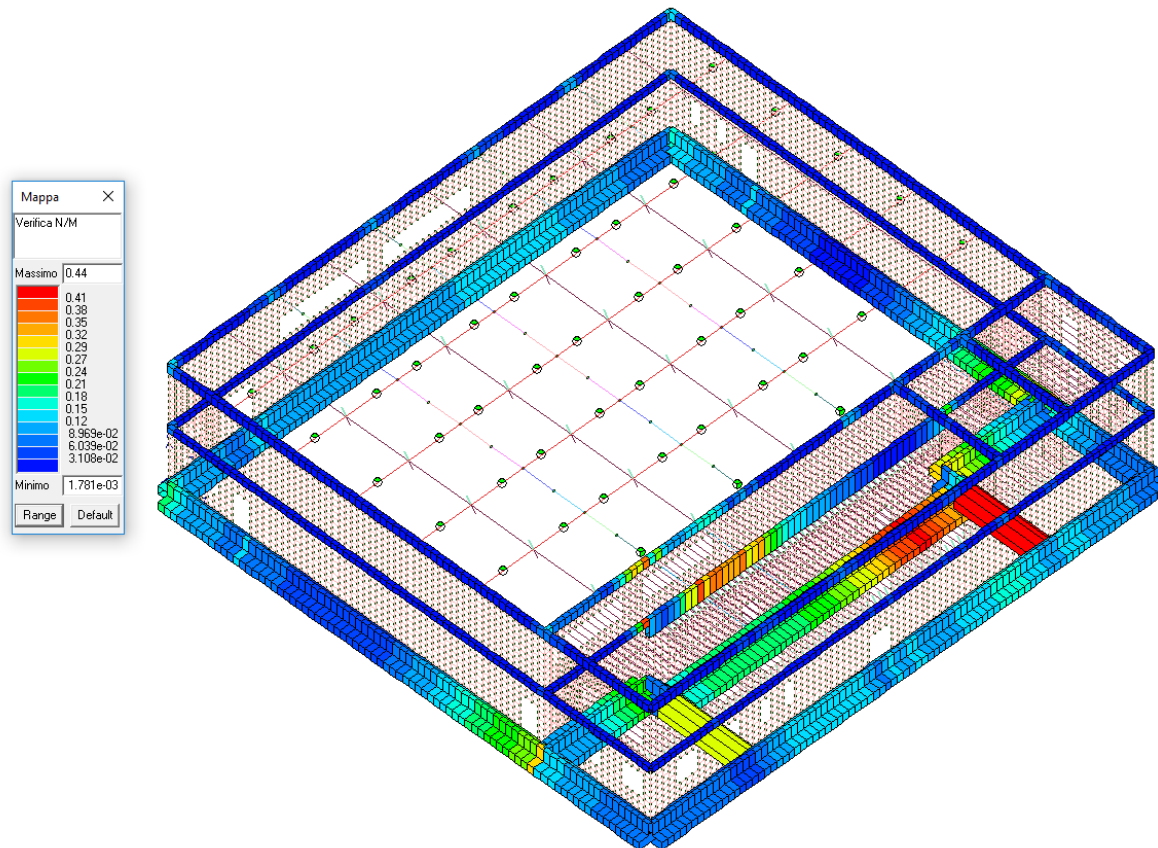
1291	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	4.42e-03	0.33	0.79	2d8/25 L=41	21,40,40
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	4.26e-03	0.33	0.78	2d8/25 L=41	20,40,40
1288	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	6.00e-03	0.33	0.78	2d8/25 L=41	20,40,41
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	3.07e-03	0.33	0.78	2d8/25 L=41	9,40,40
1285	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	4.24e-03	0.32	0.76	2d8/25 L=41	20,40,41
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	2.98e-03	0.32	0.78	2d8/25 L=41	17,40,40
1282	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	1.19e-03	0.32	0.76	2d8/25 L=41	21,40,41
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	3.15e-03	0.32	0.77	2d8/25 L=41	32,40,40
1279	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	2.46e-03	0.31	0.75	2d8/25 L=41	22,46,42
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	2.76e-03	0.32	0.75	2d8/25 L=41	18,46,42
1275	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	3.61e-03	0.30	0.72	2d8/25 L=41	20,42,42
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	4.51e-03	0.30	0.72	2d8/25 L=41	20,42,42
1271	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	3.15e-03	0.29	0.69	2d8/25 L=41	20,42,42
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	2.86e-03	0.29	0.69	2d8/25 L=41	9,42,42
1267	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	4.74e-03	0.29	0.68	2d8/25 L=41	21,42,42
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	3.88e-03	0.29	0.68	2d8/25 L=41	21,42,42
1263	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	5.40e-03	0.29	0.68	2d8/25 L=41	21,42,42
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	3.98e-03	0.29	0.68	2d8/25 L=41	20,42,42
1259	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	4.96e-03	0.29	0.67	2d8/25 L=41	20,42,42
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	2.94e-03	0.29	0.67	2d8/25 L=41	20,42,42
1255	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	3.71e-03	0.28	0.65	2d8/25 L=41	20,42,42
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	1.34e-03	0.28	0.66	2d8/25 L=41	40,42,42
1251	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	2.41e-03	0.27	0.62	2d8/25 L=41	20,42,42
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	1.40e-03	0.27	0.63	2d8/25 L=41	22,42,42
1247	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	1.77e-03	0.25	0.59	2d8/25 L=41	20,42,39
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	1.78e-03	0.25	0.59	2d8/25 L=41	22,42,42
1243	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	1.59e-03	0.30	0.55	2d8/25 L=41	20,31,39
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	1.91e-03	0.30	0.55	2d8/25 L=41	22,31,42
1239	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	1.60e-03	0.30	0.51	2d8/25 L=41	20,45,39
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	1.88e-03	0.30	0.51	2d8/25 L=41	18,45,42
1235	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	1.74e-03	0.28	7.05e-03	2d8/25 L=41	21,42,16
	s=12,m=1	41.5	0.45	4.0	4.0	0.0	0.13	1.81e-03	0.28	7.70e-03	2d8/25 L=41	15,42,17
1231	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	1.85e-03	0.25	7.08e-03	2d8/25 L=41	21,42,16
	s=12,m=1	41.5	0.45	4.0	4.0	0.0	0.13	1.79e-03	0.25	7.65e-03	2d8/25 L=41	15,42,17
1227	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	1.90e-03	0.22	7.07e-03	2d8/25 L=41	21,42,16
	s=12,m=1	41.5	0.45	4.0	4.0	0.0	0.13	1.73e-03	0.22	7.53e-03	2d8/25 L=41	15,42,17
1223	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	1.91e-03	0.19	7.04e-03	2d8/25 L=41	21,42,16
	s=12,m=1	41.5	0.45	4.0	4.0	0.0	0.13	1.66e-03	0.19	7.37e-03	2d8/25 L=41	15,42,17
1219	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	1.90e-03	0.17	7.00e-03	2d8/25 L=41	21,34,16
	s=12,m=1	41.5	0.45	4.0	4.0	0.0	0.13	1.58e-03	0.17	7.20e-03	2d8/25 L=41	19,34,17
1215	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	1.89e-03	0.14	6.96e-03	2d8/25 L=41	21,34,16
	s=12,m=1	41.5	0.45	4.0	4.0	0.0	0.13	1.50e-03	0.15	7.04e-03	2d8/25 L=41	19,34,17
1211	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	1.88e-03	0.12	6.91e-03	2d8/25 L=41	21,34,16
	s=12,m=1	41.5	0.45	4.0	4.0	0.0	0.13	1.42e-03	0.13	6.91e-03	2d8/25 L=41	19,34,17
1207	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	1.88e-03	0.11	6.86e-03	2d8/25 L=41	21,34,16
	s=12,m=1	41.5	0.45	4.0	4.0	0.0	0.13	1.34e-03	0.11	6.81e-03	2d8/25 L=41	19,34,17
1203	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	1.89e-03	0.10	6.78e-03	2d8/25 L=41	21,34,16
	s=12,m=1	41.5	0.45	4.0	4.0	0.0	0.13	1.26e-03	0.10	6.76e-03	2d8/25 L=41	19,34,17
1199	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	1.91e-03	0.10	6.70e-03	2d8/25 L=41	21,34,16
	s=12,m=1	41.5	0.45	4.0	4.0	0.0	0.13	1.17e-03	0.10	6.73e-03	2d8/25 L=41	19,34,17
1195	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	1.94e-03	0.10	6.61e-03	2d8/25 L=41	21,33,16
	s=12,m=1	41.5	0.45	4.0	4.0	0.0	0.13	1.07e-03	0.11	6.72e-03	2d8/25 L=41	19,33,17
1191	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	1.98e-03	0.14	6.52e-03	2d8/25 L=41	21,41,16
	s=12,m=1	41.5	0.45	4.0	4.0	0.0	0.13	9.76e-04	0.14	6.73e-03	2d8/25 L=41	19,41,17
1187	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	2.02e-03	0.17	6.46e-03	2d8/25 L=41	21,41,16
	s=12,m=1	41.5	0.45	4.0	4.0	0.0	0.13	8.84e-04	0.17	6.74e-03	2d8/25 L=41	19,41,17
1183	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	2.07e-03	0.21	6.42e-03	2d8/25 L=41	21,41,16
	s=12,m=1	41.5	0.45	4.0	4.0	0.0	0.13	7.99e-04	0.21	6.77e-03	2d8/25 L=41	19,41,17
1179	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	2.13e-03	0.24	6.40e-03	2d8/25 L=41	21,41,16
	s=12,m=1	41.5	0.45	4.0	4.0	0.0	0.13	7.24e-04	0.24	6.80e-03	2d8/25 L=41	19,41,17
1175	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	2.20e-03	0.27	6.40e-03	2d8/25 L=41	21,41,16
	s=12,m=1	41.5	0.45	4.0	4.0	0.0	0.13	6.58e-04	0.27	6.85e-03	2d8/25 L=41	19,41,17
1171	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	2.28e-03	0.29	6.41e-03	2d8/25 L=41	17,40,15
	s=12,m=1	41.5	0.45	4.0	4.0	0.0	0.13	5.98e-04	0.29	6.92e-03	2d8/25 L=41	19,41,18
1167	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	2.37e-03	0.29	0.52	2d8/25 L=41	17,43,40
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	5.74e-04	0.29	0.52	2d8/25 L=41	39,43,41
1162	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	2.46e-03	0.27	0.55	2d8/25 L=41	17,33,40
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	5.54e-04	0.28	0.55	2d8/25 L=41	39,33,41
1154	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	2.55e-03	0.29	0.58	2d8/25 L=41	17,32,40
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	5.45e-04	0.30	0.58	2d8/25 L=41	42,33,41
1147	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	2.65e-03	0.30	0.61	2d8/25 L=41	17,35,40
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	5.67e-04	0.30	0.61	2d8/25 L=41	42,38,41
1141	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	2.75e-03	0.27	0.63	2d8/25 L=41	16,40,40
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	5.93e-04	0.27	0.63	2d8/25 L=41	42,41,41
1136	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	2.87e-03	0.27	0.65	2d8/25 L=41	16,40,40
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	6.22e-04	0.28	0.65	2d8/25 L=41	42,41,41
1131	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	3.01e-03	0.28	0.67	2d8/25 L=41	16,40,40
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	6.54e-04	0.28	0.67	2d8/25 L=41	42,40,41
1124	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	3.17e-03	0.29	0.68	2d8/25 L=41	16,40,40
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	6.94e-04	0.29	0.68	2d8/25 L=41	46,40,41
1117	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	3.34e-03	0.29	0.70	2d8/25 L=41	16,40,40
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	7.36e-04	0.30	0.70	2d8/25 L=41	46,40,41
1110	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	3.51e-03	0.30	0.71	2d8/25 L=41	16,40,40
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	7.81e-04	0.30	0.71	2d8/25 L=41	46,40,41
1101	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	3.68e-03	0.31	0.72	2d8/25 L=41	16,40,40
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	8.74e-04	0.31	0.72	2d8/25 L=41	28,40,40
1092	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	3.84e-03	0.31	0.73	2d8/25 L=41	16,40,40
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	1.08e-03	0.31	0.73	2d8/25 L=41	28,40,40
1081	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	3.94e-03	0.31	0.73	2d8/25 L=41	16,40,40
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	1.36e-03	0.31	0.73	2d8/25 L=41	28,40,40
1071	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	3.96e-03	0.31	0.73	2d8/25 L=41	16,40,40
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	1.77e-03	0.31	0.73	2d8/25 L=41	20,40,40
1060	ok,ok	0.0	0.45	4.0	4.0	4.0	0.13	3.81e-03	0.30	0.71	2d8/25 L=41	16,40,40

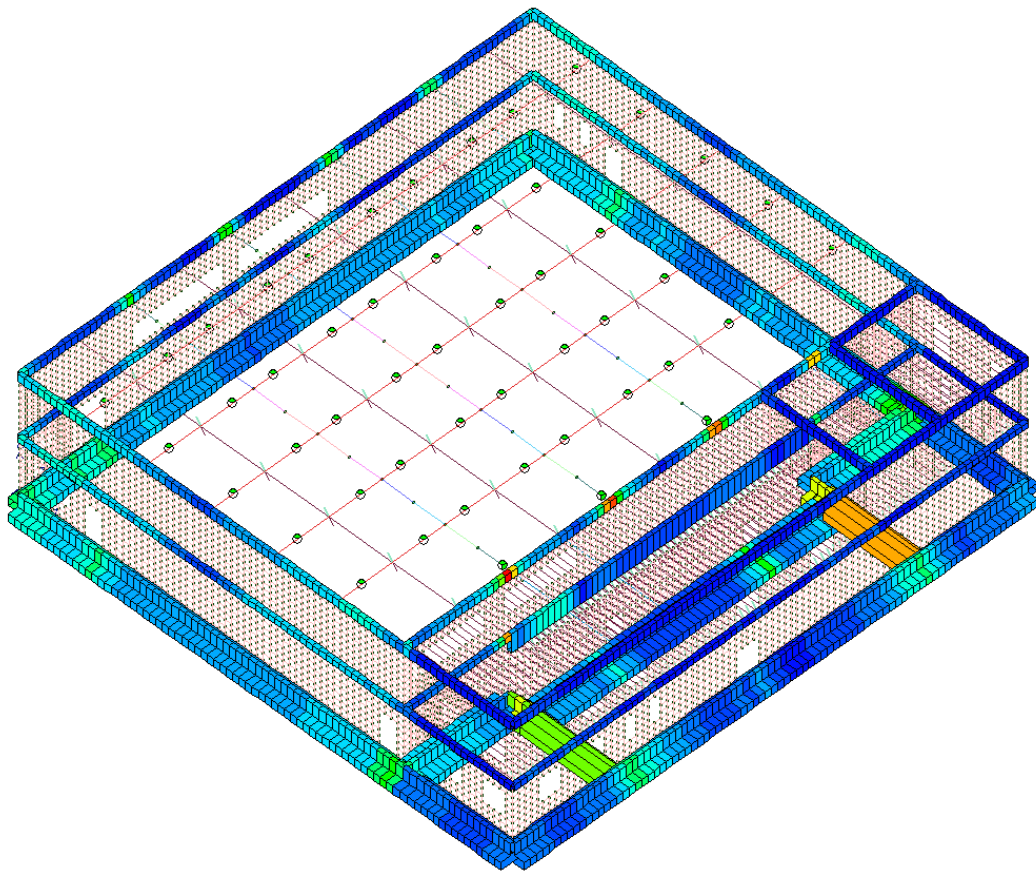
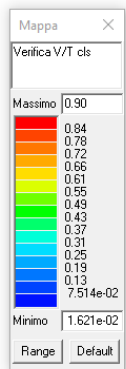
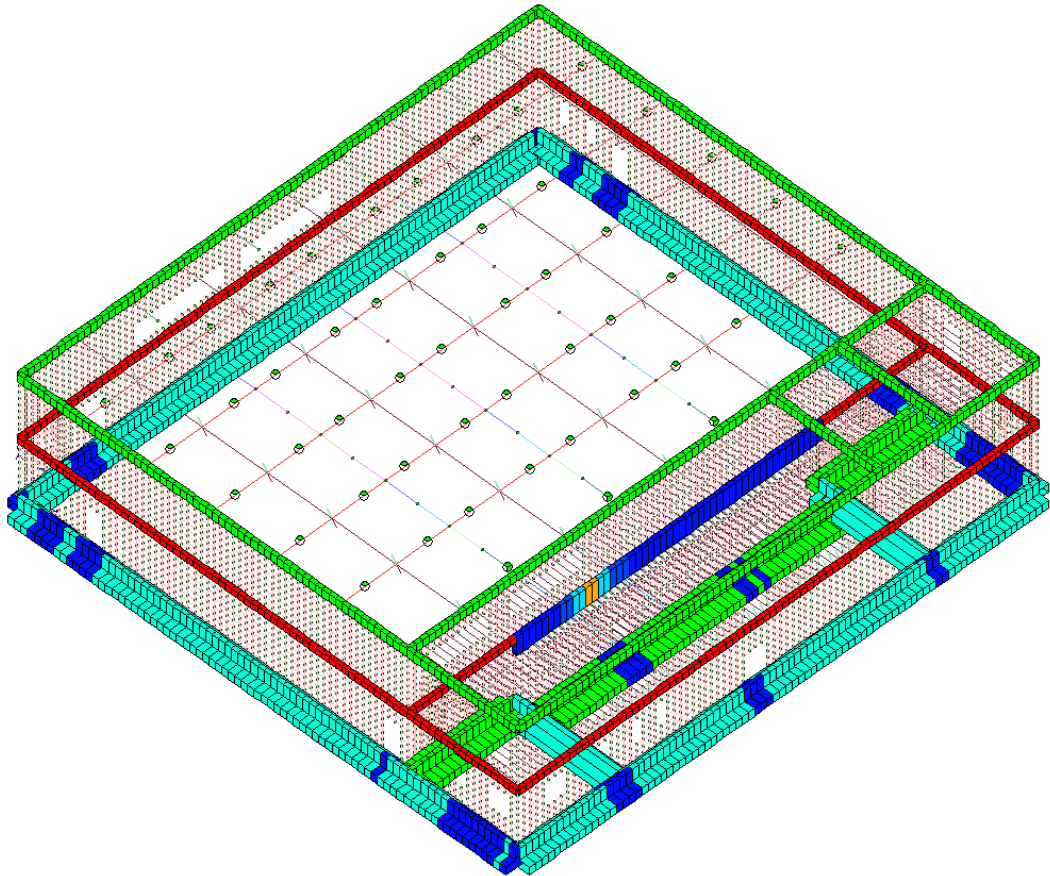
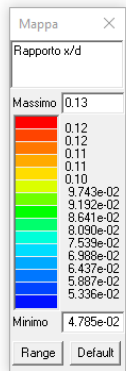
	s=12,m=1	41.5	0.45	4.0	4.0	4.0	0.13	3.41e-03	0.28	0.54	2d8/25 L=41	15,36,42
990	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	2.08e-03	0.29	9.03e-03	2d8/25 L=41	19,42,4
	s=12,m=1	41.5	0.45	4.0	4.0	0.0	0.13	4.28e-03	0.28	4.58e-03	2d8/25 L=41	16,42,43
973	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	4.87e-03	0.25	9.55e-03	2d8/25 L=41	21,42,4
	s=12,m=1	41.5	0.45	4.0	4.0	0.0	0.13	7.84e-03	0.25	5.56e-03	2d8/25 L=41	22,42,43
958	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.21	0.01	2d8/25 L=41	17,42,46
	s=12,m=1	41.5	0.45	4.0	4.0	0.0	0.13	0.01	0.21	8.39e-03	2d8/25 L=41	18,42,43
944	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.17	0.03	2d8/25 L=41	17,42,22
	s=12,m=1	41.5	0.45	4.0	4.0	0.0	0.13	0.04	0.17	0.02	2d8/25 L=41	18,42,19
935	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.14	0.01	2d8/25 L=47	33,42,42
	s=12,m=1	46.7	0.45	4.0	4.0	0.0	0.13	0.01	0.14	0.02	2d8/25 L=47	18,39,39
949	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	6.28e-03	0.08	0.01	2d8/25 L=47	44,39,46
	s=12,m=1	46.7	0.45	4.0	4.0	0.0	0.13	7.32e-03	0.09	0.01	2d8/25 L=47	46,39,43
967	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	6.70e-03	0.04	0.01	2d8/25 L=47	42,43,46
	s=12,m=1	46.7	0.45	4.0	4.0	0.0	0.13	0.01	0.04	0.01	2d8/25 L=47	40,43,43
984	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	6.10e-03	0.01	0.01	2d8/25 L=40	42,31,22
	s=12,m=1	40.0	0.45	4.0	4.0	0.0	0.13	0.01	0.02	0.01	2d8/25 L=40	26,31,19
1002	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	3.26e-03	0.01	0.02	2d8/25 L=40	31,31,15
	s=12,m=1	40.0	0.45	4.0	4.0	0.0	0.13	0.01	0.02	0.02	2d8/25 L=40	18,31,15
1017	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	5.77e-03	0.02	0.01	2d8/25 L=40	24,39,15
	s=12,m=1	40.0	0.45	4.0	4.0	0.0	0.13	0.01	0.03	0.02	2d8/25 L=40	16,39,11
1030	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.02	5.29e-03	2d8/25 L=40	23,42,23
	s=12,m=1	40.0	0.45	4.0	4.0	0.0	0.13	6.65e-03	0.03	0.01	2d8/25 L=40	16,42,11
1043	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.03	0.02	2d8/25 L=40	23,42,23
	s=12,m=1	40.0	0.45	4.0	4.0	0.0	0.13	6.65e-03	0.03	9.46e-03	2d8/25 L=40	17,42,23
1055	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	4.82e-03	0.03	0.02	2d8/25 L=40	4,42,3
	s=12,m=1	40.0	0.45	4.0	4.0	0.0	0.13	5.65e-03	0.03	8.47e-03	2d8/25 L=40	17,42,17
1066	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	5.14e-03	0.02	0.01	2d8/25 L=40	16,46,25
	s=12,m=1	40.0	0.45	4.0	4.0	0.0	0.13	5.98e-03	0.02	9.60e-03	2d8/25 L=40	16,44,24
1076	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	8.63e-03	0.03	0.02	2d8/25 L=40	26,36,24
	s=12,m=1	40.0	0.45	4.0	4.0	0.0	0.13	0.02	0.03	0.03	2d8/25 L=40	24,36,24
1087	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.01	0.02	0.02	2d8/25 L=40	18,36,24
	s=12,m=1	40.0	0.45	4.0	4.0	0.0	0.13	0.01	0.03	0.02	2d8/25 L=40	24,36,24
1096	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	0.02	0.02	0.01	2d8/25 L=40	3,42,18
	s=12,m=1	40.0	0.45	4.0	4.0	0.0	0.13	6.20e-03	0.02	0.01	2d8/25 L=40	24,40,15
1105	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	9.54e-03	0.02	0.02	2d8/25 L=40	3,44,18
	s=12,m=1	40.0	0.45	4.0	4.0	0.0	0.13	8.73e-03	0.02	0.01	2d8/25 L=40	18,44,18
931	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	3.01e-03	0.03	0.02	2d8/25 L=40	22,17,18
	s=12,m=1	40.0	0.45	4.0	4.0	0.0	0.13	0.01	0.03	0.01	2d8/25 L=40	18,17,18
940	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	5.55e-03	0.05	0.02	2d8/25 L=40	24,17,17
	s=12,m=1	40.0	0.45	4.0	4.0	0.0	0.13	0.02	0.05	0.02	2d8/25 L=40	18,17,17
954	ok,ok	0.0	0.45	4.0	4.0	0.0	0.13	7.92e-03	0.07	0.03	2d8/25 L=40	24,17,17
	s=12,m=1	40.0	0.45	4.0	4.0	0.0	0.13	0.02	0.06	0.02	2d8/25 L=40	18,17,17
M_T=19 Z=786.3 N=4939 N=5775												
Trave	Note	Pos.	%Af	Af inf.	Af sup.	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
485	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	0.12	0.27	0.90	2d8/25 L=41	39,38,42
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	0.02	0.26	0.92	2d8/25 L=41	43,38,39
896	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	0.05	0.27	0.95	2d8/25 L=41	39,42,42
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	4.03e-03	0.27	0.95	2d8/25 L=41	35,39,39
893	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	0.01	0.30	0.81	2d8/20 L=41	41,40,40
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	3.36e-03	0.30	0.80	2d8/20 L=41	44,41,41
890	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	1.85e-03	0.32	0.85	2d8/20 L=41	41,40,40
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	3.25e-03	0.32	0.85	2d8/20 L=41	44,41,41
887	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	1.89e-03	0.34	0.89	2d8/20 L=41	42,41,40
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	3.39e-03	0.34	0.89	2d8/20 L=41	27,40,40
884	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	2.13e-03	0.35	0.92	2d8/20 L=41	39,40,40
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	3.35e-03	0.35	0.92	2d8/20 L=41	23,40,40
881	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	2.46e-03	0.36	0.94	2d8/20 L=41	11,40,40
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	3.30e-03	0.36	0.94	2d8/20 L=41	26,40,40
878	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	3.57e-03	0.36	0.94	2d8/20 L=41	11,40,40
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	2.64e-03	0.36	0.93	2d8/20 L=41	26,40,40
875	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	2.29e-03	0.35	0.92	2d8/20 L=41	11,40,40
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	8.62e-03	0.34	0.91	2d8/20 L=41	9,40,40
871	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	8.89e-03	0.33	0.89	2d8/20 L=41	9,41,40
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	0.02	0.32	0.88	2d8/20 L=41	9,41,40
867	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	0.02	0.29	0.93	2d8/25 L=41	11,39,39
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	0.01	0.29	0.93	2d8/25 L=41	11,39,39
863	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	0.01	0.29	0.93	2d8/25 L=41	9,39,39
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	3.05e-03	0.29	0.93	2d8/25 L=41	23,39,42
859	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	4.00e-03	0.29	0.94	2d8/25 L=41	11,39,39
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	4.05e-03	0.29	0.92	2d8/25 L=41	11,39,42
855	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	6.05e-03	0.29	0.93	2d8/25 L=41	11,39,39
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	3.89e-03	0.29	0.92	2d8/25 L=41	11,42,42
851	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	6.60e-03	0.29	0.92	2d8/25 L=41	27,39,39
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	3.93e-03	0.29	0.91	2d8/25 L=41	11,42,42
847	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	6.80e-03	0.28	0.90	2d8/25 L=41	27,39,39
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	4.58e-03	0.28	0.89	2d8/25 L=41	11,42,42
843	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	6.83e-03	0.27	0.88	2d8/25 L=41	27,39,39
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	5.46e-03	0.27	0.87	2d8/25 L=41	11,42,42
839	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	6.55e-03	0.26	0.84	2d8/25 L=41	27,39,39
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	4.46e-03	0.26	0.84	2d8/25 L=41	11,42,42
835	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	3.88e-03	0.24	0.79	2d8/25 L=41	23,39,39
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	5.69e-03	0.24	0.78	2d8/25 L=41	12,39,39
831	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	6.39e-03	0.22	0.74	2d8/25 L=41	9,39,42
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	0.01	0.22	0.73	2d8/25 L=41	9,39,39
827	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	0.02	0.24	0.55	2d8/25 L=41	9,45,39
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	7.83e-03	0.24	0.56	2d8/25 L=41	9,45,42
823	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	6.71e-03	0.23	7.32e-03	2d8/25 L=41	9,39,23
	s=11,m=1	41.5	0.32	4.0	4.0	0.0	0.09	3.51e-03	0.23	0.01	2d8/25 L=41	29,42,9
819	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	4.47e-03	0.21	8.20e-03	2d8/25 L=41	11,39,23
	s=11,m=1	41.5	0.32	4.0	4.0	0.0	0.09	5.17e-03	0.21	7.55e-03	2d8/25 L=41	11,42,26
815	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	5.82e-03	0.19	9.42e-03	2d8/25 L=41	11,39,23
	s=11,m=1	41.5	0.32	4.0	4.0	0.0	0.09	4.83e-03	0.19	8.33e-03	2d8/25 L=41	11,42,26
811	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	5.82e-03	0.17	9.57e-03	2d8/25 L=41	23,31,23
	s=11,m=1	41.5	0.32	4.0	4.0	0.0	0.09	4.69e-03	0.17	9.17e-03	2d8/25 L=41	11,34,26
807	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	5.85e-03	0.16	9.38e-03	2d	

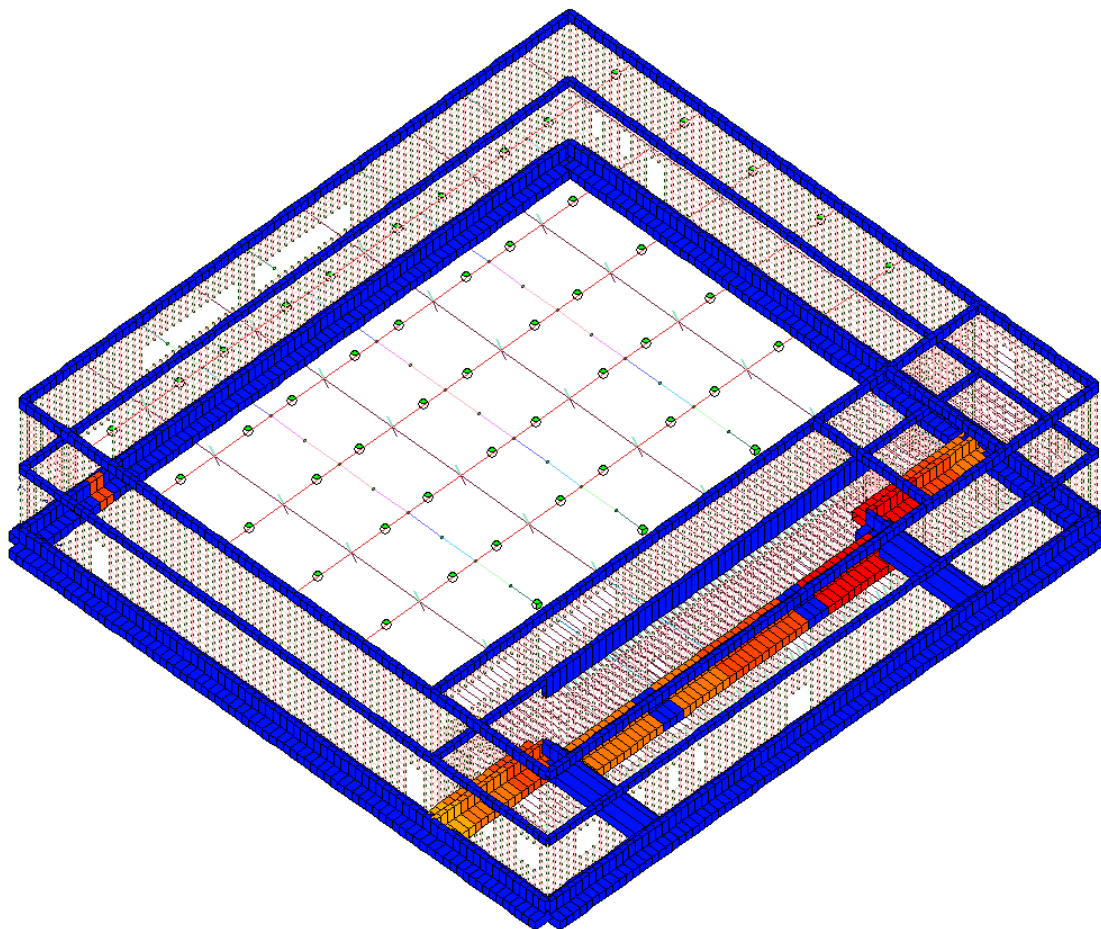
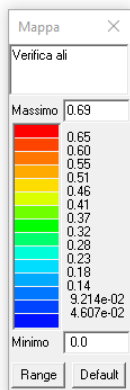
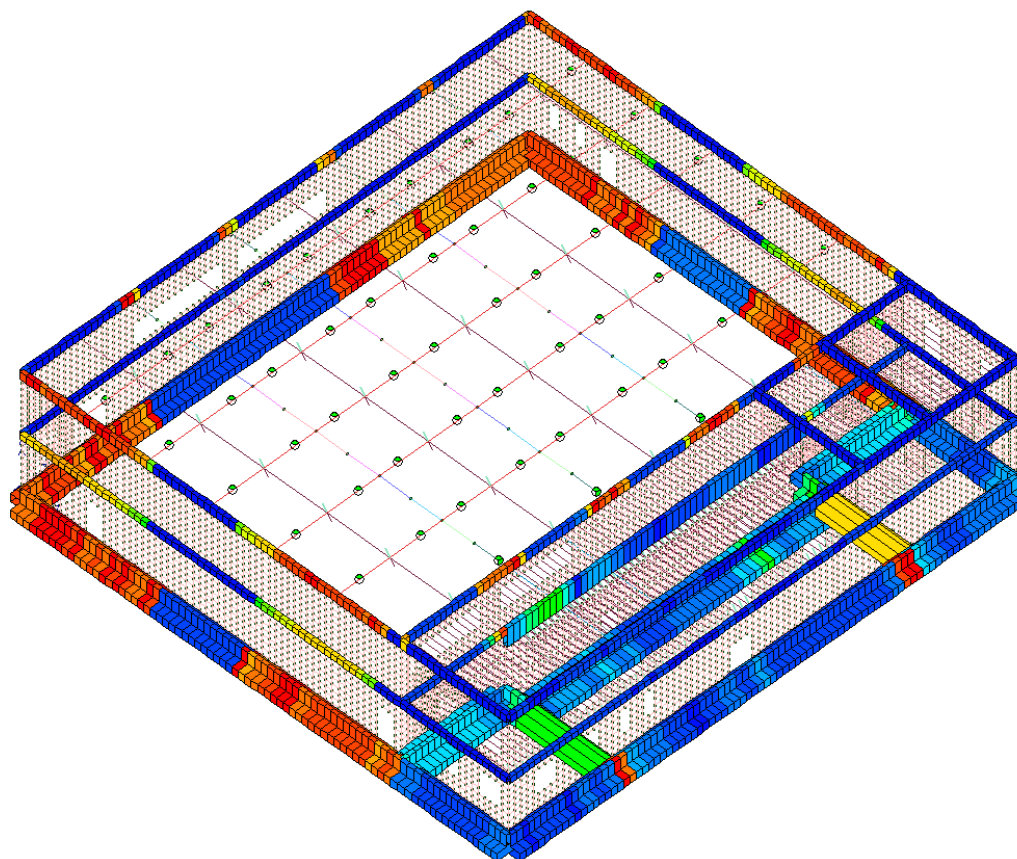
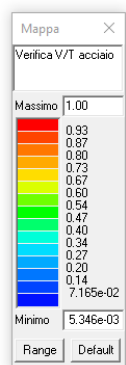
795	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	2.57e-03	0.11	0.01	2d8/25 L=41	11,34,9
	s=11,m=1	41.5	0.32	4.0	4.0	0.0	0.09	7.59e-03	0.11	4.60e-03	2d8/25 L=41	9,31,12
791	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	8.86e-03	0.09	0.01	2d8/25 L=41	9,34,9
	s=11,m=1	41.5	0.32	4.0	4.0	0.0	0.09	0.02	0.09	5.45e-03	2d8/25 L=41	9,31,27
787	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.02	0.13	7.83e-03	2d8/25 L=41	9,40,23
	s=11,m=1	41.5	0.32	4.0	4.0	0.0	0.09	8.11e-03	0.13	0.01	2d8/25 L=41	9,40,9
783	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	7.33e-03	0.17	9.37e-03	2d8/25 L=41	9,40,23
	s=11,m=1	41.5	0.32	4.0	4.0	0.0	0.09	5.13e-03	0.17	0.02	2d8/25 L=41	26,40,9
779	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	4.97e-03	0.21	9.49e-03	2d8/25 L=41	23,40,24
	s=11,m=1	41.5	0.32	4.0	4.0	0.0	0.09	4.95e-03	0.21	9.93e-03	2d8/25 L=41	11,41,25
775	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	7.46e-03	0.23	0.01	2d8/25 L=41	23,40,23
	s=11,m=1	41.5	0.32	4.0	4.0	0.0	0.09	4.56e-03	0.24	0.01	2d8/25 L=41	11,41,26
771	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	8.18e-03	0.22	0.58	2d8/25 L=41	23,43,40
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	4.40e-03	0.22	0.58	2d8/25 L=41	11,46,41
767	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	8.46e-03	0.24	0.61	2d8/25 L=41	23,39,40
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	4.84e-03	0.24	0.62	2d8/25 L=41	11,46,41
763	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	8.58e-03	0.22	0.65	2d8/25 L=41	23,39,40
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	5.48e-03	0.22	0.65	2d8/25 L=41	11,33,41
758	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	8.19e-03	0.23	0.67	2d8/25 L=41	23,33,41
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	4.07e-03	0.23	0.67	2d8/25 L=41	11,33,41
750	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	2.32e-03	0.24	0.69	2d8/25 L=41	11,33,41
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	7.73e-03	0.24	0.69	2d8/25 L=41	9,33,41
743	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	8.96e-03	0.23	0.71	2d8/25 L=41	9,35,41
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	0.02	0.23	0.71	2d8/25 L=41	9,35,41
737	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	0.01	0.25	0.83	2d8/25 L=41	9,41,41
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	6.70e-03	0.25	0.84	2d8/25 L=41	9,41,41
732	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	6.34e-03	0.27	0.86	2d8/25 L=41	12,41,41
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	6.09e-03	0.27	0.87	2d8/25 L=41	25,41,41
725	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	6.67e-03	0.28	0.90	2d8/25 L=41	23,40,40
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	5.50e-03	0.28	0.90	2d8/25 L=41	11,41,41
718	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	9.65e-03	0.29	0.91	2d8/25 L=41	23,40,40
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	5.32e-03	0.29	0.92	2d8/25 L=41	11,41,41
711	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	0.01	0.29	0.92	2d8/25 L=41	23,40,40
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	5.45e-03	0.29	0.93	2d8/25 L=41	11,41,41
704	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	0.01	0.29	0.92	2d8/25 L=41	23,41,40
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	6.19e-03	0.29	0.93	2d8/25 L=41	11,41,41
695	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	0.01	0.29	0.91	2d8/25 L=41	23,41,40
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	7.08e-03	0.29	0.93	2d8/25 L=41	11,41,41
686	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	9.53e-03	0.29	0.90	2d8/25 L=41	23,41,41
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	5.43e-03	0.29	0.92	2d8/25 L=41	11,41,41
675	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	2.83e-03	0.28	0.89	2d8/25 L=41	11,41,41
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	0.01	0.28	0.90	2d8/25 L=41	9,41,41
665	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	0.01	0.28	0.89	2d8/25 L=41	9,41,41
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	0.02	0.28	0.88	2d8/25 L=41	9,41,41
653	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	0.02	0.32	0.86	2d8/20 L=41	9,39,39
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	8.86e-03	0.32	0.86	2d8/20 L=41	28,39,39
639	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	7.34e-03	0.33	0.87	2d8/20 L=41	12,39,39
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	0.01	0.33	0.88	2d8/20 L=41	24,39,39
624	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	8.98e-03	0.33	0.86	2d8/20 L=41	23,39,39
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	8.67e-03	0.33	0.88	2d8/20 L=41	25,39,39
609	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	0.01	0.32	0.84	2d8/20 L=41	27,39,39
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	8.55e-03	0.32	0.85	2d8/20 L=41	28,39,39
592	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	0.02	0.30	0.80	2d8/20 L=41	24,39,39
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	8.95e-03	0.30	0.81	2d8/20 L=41	28,39,39
571	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	0.02	0.27	0.92	2d8/25 L=41	24,39,39
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	7.61e-03	0.28	0.94	2d8/25 L=41	28,39,39
550	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	0.02	0.24	0.82	2d8/25 L=41	24,39,39
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	3.21e-03	0.24	0.83	2d8/25 L=41	28,39,39
530	ok,ok	0.0	0.32	4.0	4.0	4.0	0.09	0.03	0.19	0.68	2d8/25 L=41	24,41,33
	s=11,m=1	41.5	0.32	4.0	4.0	4.0	0.09	7.62e-03	0.20	0.70	2d8/25 L=41	24,41,33
512	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.03	0.21	0.01	2d8/25 L=41	24,41,43
	s=11,m=1	41.5	0.32	4.0	4.0	0.0	0.09	0.03	0.21	0.02	2d8/25 L=41	28,41,46
499	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.03	0.15	0.03	2d8/25 L=41	28,41,25
	s=11,m=1	41.5	0.32	4.0	4.0	0.0	0.09	0.06	0.15	0.03	2d8/25 L=41	28,41,24
492	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.06	0.17	0.02	2d8/25 L=47	27,41,43
	s=11,m=1	46.7	0.32	4.0	4.0	0.0	0.09	0.05	0.16	0.02	2d8/25 L=47	27,40,46
535	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.02	0.08	0.02	2d8/25 L=47	19,41,37
	s=11,m=1	46.7	0.32	4.0	4.0	0.0	0.09	0.03	0.08	0.02	2d8/25 L=47	24,40,36
517	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.01	0.05	0.03	2d8/25 L=47	24,45,25
	s=11,m=1	46.7	0.32	4.0	4.0	0.0	0.09	0.02	0.05	0.02	2d8/25 L=47	24,45,24
505	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.03	0.05	0.03	2d8/25 L=40	24,45,25
	s=11,m=1	40.0	0.32	4.0	4.0	0.0	0.09	6.49e-03	0.04	0.03	2d8/25 L=40	21,37,25
699	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.03	0.05	0.04	2d8/25 L=40	24,45,25
	s=11,m=1	40.0	0.32	4.0	4.0	0.0	0.09	5.69e-03	0.05	0.03	2d8/25 L=40	9,45,25
690	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.03	0.04	0.04	2d8/25 L=40	24,37,25
	s=11,m=1	40.0	0.32	4.0	4.0	0.0	0.09	6.29e-03	0.04	0.03	2d8/25 L=40	25,37,25
679	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.02	0.04	0.04	2d8/25 L=40	24,37,25
	s=11,m=1	40.0	0.32	4.0	4.0	0.0	0.09	0.02	0.03	0.03	2d8/25 L=40	24,37,25
669	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	7.59e-03	0.03	0.03	2d8/25 L=40	17,37,25
	s=11,m=1	40.0	0.32	4.0	4.0	0.0	0.09	0.03	0.02	0.03	2d8/25 L=40	24,27,25
657	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.01	0.02	0.03	2d8/25 L=40	19,25,25
	s=11,m=1	40.0	0.32	4.0	4.0	0.0	0.09	0.04	0.03	0.03	2d8/25 L=40	23,27,24
643	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.02	0.02	0.03	2d8/25 L=40	19,25,25
	s=11,m=1	40.0	0.32	4.0	4.0	0.0	0.09	0.05	0.03	0.03	2d8/25 L=40	27,27,24
628	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.03	0.02	0.03	2d8/25 L=40	15,25,25
	s=11,m=1	40.0	0.32	4.0	4.0	0.0	0.09	0.05	0.03	0.03	2d8/25 L=40	23,27,24
613	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.02	0.03	0.03	2d8/25 L=40	3,25,25
	s=11,m=1	40.0	0.32	4.0	4.0	0.0	0.09	0.04	0.02	0.03	2d8/25 L=40	23,24,24
597	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.01	0.03	0.03	2d8/25 L=40	25,30,25
	s=11,m=1	40.0	0.32	4.0	4.0	0.0	0.09	0.02	0.02	0.03	2d8/25 L=40	23,24,24
576	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.02	0.03	0.03	2d8/25 L=40	24,30,25
	s=11,m=1	40.0	0.32	4.0	4.0	0.0	0.09	0.01	0.02	0.03	2d8/25 L=40	25,24,24
555	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.03	0.03	0.03	2d8/25 L=40	23,30,25
	s=11,m=1	40.0	0.32	4.0	4.0	0.0	0.09	7.97e-03	0.02	0.03	2d8/25 L=40	4,24,24
537	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.03	0.03	0.03	2d8/25 L=40	23,26,26
	s=11,m=1	40.0	0.32	4.0	4.0	0.0	0.09	7.18e-03	0.03	0.03	2d8/25 L=40	19,24,23
523	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.02	0.04			

	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	4.08e-03	0.06	0.06	2d8/25 L=40	15,17,4
726	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.03	0.06	0.06	2d8/25 L=40	17,16,16
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	8.13e-03	0.08	0.08	2d8/25 L=40	23,17,4
719	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.02	0.07	0.06	2d8/25 L=40	16,16,16
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	7.64e-03	0.09	0.08	2d8/25 L=40	3,17,4
712	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.02	0.07	0.06	2d8/25 L=40	16,16,16
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	0.01	0.09	0.07	2d8/25 L=40	18,17,4
705	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.02	0.07	0.06	2d8/25 L=40	16,16,16
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	0.01	0.09	0.07	2d8/25 L=40	15,17,4
696	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.01	0.06	0.06	2d8/25 L=40	17,16,3
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	0.02	0.08	0.07	2d8/25 L=40	15,17,4
687	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.02	0.06	0.06	2d8/25 L=40	17,16,3
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	0.02	0.08	0.07	2d8/25 L=40	15,17,4
676	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.02	0.05	0.06	2d8/25 L=40	17,4,3
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	8.80e-03	0.07	0.07	2d8/25 L=40	19,17,4
666	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.02	0.05	0.06	2d8/25 L=40	17,4,3
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	9.01e-03	0.07	0.07	2d8/25 L=40	18,17,4
654	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.02	0.05	0.05	2d8/25 L=40	15,16,15
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	0.02	0.07	0.08	2d8/25 L=40	11,17,4
640	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.02	0.04	0.05	2d8/25 L=40	16,3,15
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	0.02	0.07	0.08	2d8/25 L=40	11,17,4
625	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.01	0.04	0.05	2d8/25 L=40	17,16,16
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	0.01	0.07	0.08	2d8/25 L=40	18,17,4
610	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.02	0.04	0.05	2d8/25 L=40	17,16,20
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	0.01	0.07	0.09	2d8/25 L=40	26,17,4
593	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.03	0.03	0.04	2d8/25 L=40	11,3,20
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	8.19e-03	0.07	0.09	2d8/25 L=40	26,4,4
572	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.03	0.04	0.05	2d8/25 L=40	11,4,15
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	7.05e-03	0.06	0.08	2d8/25 L=40	11,4,4
551	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.03	0.05	0.06	2d8/25 L=40	18,4,4
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	0.02	0.05	0.07	2d8/25 L=40	11,4,3
531	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.03	0.06	0.08	2d8/25 L=40	15,4,4
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	0.03	0.04	0.05	2d8/25 L=40	11,3,3
513	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.05	0.06	0.09	2d8/25 L=40	11,4,4
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	0.04	0.03	0.04	2d8/25 L=40	18,3,3
873	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.03	0.06	0.09	2d8/25 L=40	19,4,4
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	0.03	0.04	0.05	2d8/25 L=40	16,21,18
869	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.02	0.07	0.09	2d8/25 L=40	19,4,4
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	0.04	0.03	0.04	2d8/25 L=40	16,3,25
865	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.02	0.07	0.09	2d8/25 L=40	15,4,4
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	0.04	0.03	0.04	2d8/25 L=40	16,3,3
861	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.03	0.06	0.09	2d8/25 L=40	15,4,4
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	0.02	0.03	0.04	2d8/25 L=40	24,3,3
857	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.02	0.06	0.08	2d8/25 L=40	15,4,4
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	0.01	0.03	0.05	2d8/25 L=40	36,3,3
853	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.02	0.05	0.08	2d8/25 L=40	15,4,4
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	6.92e-03	0.04	0.05	2d8/25 L=40	34,3,3
849	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.03	0.05	0.07	2d8/25 L=40	15,4,4
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	9.02e-03	0.04	0.06	2d8/25 L=40	15,3,3
845	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.03	0.05	0.07	2d8/25 L=40	15,4,4
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	0.01	0.04	0.06	2d8/25 L=40	15,3,3
841	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.03	0.04	0.06	2d8/25 L=40	16,4,3
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	0.02	0.05	0.07	2d8/25 L=40	16,4,4
837	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.02	0.04	0.05	2d8/25 L=40	16,3,3
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	0.02	0.06	0.08	2d8/25 L=40	16,4,4
833	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.02	0.04	0.05	2d8/25 L=40	24,3,3
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	0.03	0.06	0.08	2d8/25 L=40	16,4,4
829	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.01	0.04	0.04	2d8/25 L=40	24,3,3
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	0.04	0.07	0.09	2d8/25 L=40	16,4,4
825	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.02	0.04	0.04	2d8/25 L=40	27,3,3
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	0.05	0.07	0.09	2d8/25 L=40	16,4,4
821	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.07	0.04	0.05	2d8/25 L=40	19,4,3
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	0.07	0.06	0.08	2d8/25 L=40	19,4,4
817	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.05	0.06	0.06	2d8/25 L=40	16,23,4
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	0.03	0.05	0.07	2d8/25 L=40	16,26,3
813	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.04	0.05	0.06	2d8/25 L=40	16,4,4
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	0.02	0.05	0.07	2d8/25 L=40	16,4,3
809	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.03	0.05	0.06	2d8/25 L=40	24,4,3
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	0.02	0.06	0.07	2d8/25 L=40	16,4,4
805	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.02	0.05	0.06	2d8/25 L=40	24,4,3
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	9.46e-03	0.06	0.07	2d8/25 L=40	35,4,4
801	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	6.49e-03	0.05	0.06	2d8/25 L=40	24,4,3
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	0.01	0.05	0.07	2d8/25 L=40	23,4,4
797	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	6.46e-03	0.05	0.06	2d8/25 L=40	15,4,3
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	0.01	0.05	0.07	2d8/25 L=40	23,4,4
793	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.01	0.05	0.06	2d8/25 L=40	16,4,3
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	0.01	0.06	0.07	2d8/25 L=40	24,4,4
789	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.01	0.05	0.06	2d8/25 L=40	16,4,3
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	6.53e-03	0.06	0.07	2d8/25 L=40	36,4,4
785	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.01	0.05	0.06	2d8/25 L=40	32,4,3
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	9.08e-03	0.06	0.07	2d8/25 L=40	15,4,4
781	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.01	0.06	0.06	2d8/25 L=40	32,4,3
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	0.02	0.06	0.07	2d8/25 L=40	15,4,4
777	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.01	0.06	0.06	2d8/25 L=40	38,4,3
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	0.02	0.06	0.07	2d8/25 L=40	15,11,4
773	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.01	0.06	0.06	2d8/25 L=40	23,4,3
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	0.03	0.06	0.07	2d8/25 L=40	15,11,4
769	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.01	0.06	0.06	2d8/25 L=40	23,4,3
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	0.03	0.06	0.07	2d8/25 L=40	16,11,4
765	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.01	0.06	0.06	2d8/25 L=40	24,4,3
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	0.03	0.07	0.07	2d8/25 L=40	16,11,4
760	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	8.35e-03	0.06	0.06	2d8/25 L=40	24,4,3
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	0.03	0.07	0.07	2d8/25 L=40	20,11,4
753	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	4.21e-03	0.06	0.05	2d8/25 L=40	37,4,3
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	0.03	0.07	0.08	2d8/25 L=40	24,11,4
746	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	7.02e-03	0.06	0.05	2d8/25 L=40	15,17,3
	s=11,m=1	40.1	0.32	4.0	4.0	0.0	0.09	0.04	0.08	0.08	2d8/25 L=40	24,11,4
740	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.05	0.06	0.05	2d8/25 L=40	23,17,3
	s=11,m											

498	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.02	0.04	9.68e-03	2d8/25 L=40	38,25,25
	s=11,m=1	40.0	0.32	4.0	4.0	0.0	0.09	0.02	0.03	0.01	2d8/25 L=40	24,25,24
511	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.02	0.04	0.02	2d8/25 L=40	25,26,26
	s=11,m=1	40.0	0.32	4.0	4.0	0.0	0.09	3.28e-03	0.04	0.02	2d8/25 L=40	38,11,23
659	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.04	0.05	0.01	2d8/25 L=40	26,26,26
	s=11,m=1	40.0	0.32	4.0	4.0	0.0	0.09	0.02	0.04	0.02	2d8/25 L=40	25,26,23
645	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.02	0.04	2.40e-03	2d8/25 L=40	26,26,26
	s=11,m=1	40.0	0.32	4.0	4.0	0.0	0.09	0.01	0.04	0.01	2d8/25 L=40	25,26,9
630	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	5.41e-03	0.03	6.43e-03	2d8/25 L=40	11,26,29
	s=11,m=1	40.0	0.32	4.0	4.0	0.0	0.09	8.93e-03	0.04	0.01	2d8/25 L=40	25,26,29
615	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	3.94e-03	0.03	0.01	2d8/25 L=40	24,25,25
	s=11,m=1	40.0	0.32	4.0	4.0	0.0	0.09	7.64e-03	0.03	0.02	2d8/25 L=40	25,25,25
599	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	6.60e-03	0.01	0.01	2d8/25 L=40	29,15,26
	s=11,m=1	40.0	0.32	4.0	4.0	0.0	0.09	6.29e-03	0.02	0.02	2d8/25 L=40	26,9,26
578	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	9.15e-03	0.02	0.01	2d8/25 L=40	26,26,26
	s=11,m=1	40.0	0.32	4.0	4.0	0.0	0.09	6.72e-03	0.03	0.02	2d8/25 L=40	11,26,26
557	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.01	0.05	0.01	2d8/25 L=40	26,26,26
	s=11,m=1	40.0	0.32	4.0	4.0	0.0	0.09	9.37e-03	0.05	0.02	2d8/25 L=40	11,26,26
540	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.01	0.07	0.01	2d8/25 L=40	23,26,26
	s=11,m=1	40.0	0.32	4.0	4.0	0.0	0.09	0.01	0.08	0.02	2d8/25 L=40	16,26,26
529	ok,ok	0.0	0.32	4.0	4.0	0.0	0.09	0.02	0.10	0.02	2d8/25 L=40	26,26,26
	s=11,m=1	40.0	0.32	4.0	4.0	0.0	0.09	0.02	0.11	0.03	2d8/25 L=40	16,26,26
Trave		%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc			
		0.66	39.45	38.58	23.32	0.13	0.44	0.90	1.00			







STATI LIMITE D' ESERCIZIO

Legenda tabella stati limite d' esercizio

In tabella vengono riportati i valori di interesse per il controllo degli stati limite d'esercizio.

In particolare vengono riportati, in relazione al tipo di elemento strutturale, i risultati relativi alle tre categorie di combinazione considerate:

- Combinazioni rare
- Combinazioni frequenti
- Combinazioni quasi permanenti.

I valori di interesse sono i seguenti:

rRfck	rapporto tra la massima compressione nel calcestruzzo e la tensione fck in combinazioni rare [normalizzato a 1]
rRfyk	rapporto tra la massima tensione nell'acciaio e la tensione fyk in combinazioni rare [normalizzato a 1]
rPfck	rapporto tra la massima compressione nel calcestruzzo e la tensione fck in combinazioni quasi permanenti [normalizzato a 1]
wR	apertura caratteristica delle fessure in combinazioni rare [mm]
wF	apertura caratteristica delle fessure in combinazioni frequenti [mm]
wP	apertura caratteristica delle fessure in combinazioni quasi permanenti [mm]
dR	massima deformazione in combinazioni rare
dF	massima deformazione in combinazioni frequenti
dP	massima deformazione in combinazioni quasi permanenti

Per ognuno dei nove valori soprariportati viene indicata (Rif.cmb) la combinazione in cui si è verificato.

In relazione al tipo di elemento strutturale i valori sono selezionati nel modo seguente:

pilastri	rRfck	rRfyk	rPfck	per sezioni significative
travi	rRfck	rRfyk	rPfck	per sezioni significative
	wR	wF	wP	per sezioni significative
	dR	dF	dP	massimi in campata
setti e gusci	rRfck	rRfyk	rPfck	massimi nei nodi dell'elemento
	wR	wF	wP	massimi nei nodi dell'elemento

Si precisa che i valori di massima deformazione per travi sono riferiti al piano verticale (piano locale 1-2 con momenti flettenti 3-3).

Trave	Pos. cm	rRfck	rRfyk	rPfck	Rif. cmb	wR mm	wF mm	wP mm	Rif. cmb	dR cm	dF cm	dP cm	Rif. cmb
1	0.0	1.30e-03	5.43e-03	9.64e-04	85,85,92	0.0	0.0	0.0	0,0,0	-3.07e-04	-3.07e-04	-3.07e-04	79,86,91
	40.1	1.27e-04	1.68e-03	0.0	85,83,0	0.0	0.0	0.0	0,0,0				
2	0.0	1.71e-03	2.14e-03	4.28e-04	85,85,92	0.0	0.0	0.0	0,0,0	-5.54e-04	-3.94e-04	-3.30e-04	81,87,92
	41.5	7.69e-04	1.84e-03	1.03e-03	79,79,91	0.0	0.0	0.0	0,0,0				
3	0.0	0.0	0.01	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-9.73e-04	-8.74e-04	-8.34e-04	81,87,92
	40.1	0.0	0.02	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
4	0.0	2.05e-03	3.71e-03	6.72e-04	85,85,92	0.0	0.0	0.0	0,0,0	-4.33e-04	-2.69e-04	-2.03e-04	81,87,92
	41.5	5.24e-04	1.53e-03	6.98e-04	79,79,91	0.0	0.0	0.0	0,0,0				
5	0.0	8.50e-03	0.04	8.04e-03	85,83,92	0.0	0.0	0.0	0,0,0	2.08e-03	1.69e-03	1.53e-03	81,87,92
	46.7	4.20e-03	0.03	4.54e-03	82,83,92	0.0	0.0	0.0	0,0,0				
6	0.0	0.02	0.07	0.02	85,85,92	0.0	0.0	0.0	0,0,0	2.60e-03	2.20e-03	2.04e-03	81,87,92
	46.7	6.39e-03	0.05	7.31e-03	81,85,92	0.0	0.0	0.0	0,0,0				
7	0.0	5.37e-03	0.01	5.06e-03	85,85,92	0.0	0.0	0.0	0,0,0	-3.12e-03	-2.18e-03	-2.02e-03	85,90,92
	40.1	9.65e-04	9.87e-04	9.44e-04	85,85,92	0.0	0.0	0.0	0,0,0				
8	0.0	4.90e-03	0.06	5.96e-03	83,85,91	0.0	0.0	0.0	0,0,0	-0.01	-8.66e-03	-8.28e-03	83,88,91
	46.7	0.0	0.05	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
9	0.0	0.0	0.14	0.0	0,85,0	0.0	0.0	0.0	0,0,0	2.71e-03	1.84e-03	1.54e-03	81,87,92
	40.1	0.0	0.14	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
10	0.0	0.0	0.06	0.0	0,85,0	0.0	0.0	0.0	0,0,0	6.10e-03	5.36e-03	5.17e-03	83,88,91
	46.7	0.01	0.08	0.01	82,85,92	0.0	0.0	0.0	0,0,0				
11	0.0	0.0	0.18	0.0	0,85,0	0.0	0.0	0.0	0,0,0	1.55e-03	1.19e-03	1.13e-03	85,90,92
	40.1	0.0	0.17	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
12	0.0	0.11	0.16	0.12	85,85,92	0.0	0.0	0.0	0,0,0	0.05	0.05	0.05	81,87,92
	280.0	0.05	0.15	0.06	82,82,92	0.0	0.0	0.0	0,0,0				
	560.0	0.03	0.03	0.04	81,81,92	0.0	0.0	0.0	0,0,0				
13	0.0	0.05	0.06	0.06	82,82,92	0.0	0.0	0.0	0,0,0	0.05	0.05	0.05	81,87,92

316	0.0	0.0	0.07	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-4.54e-03	-3.14e-03	-2.93e-03	85,90,92
	40.1	0.0	0.08	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
317	0.0	0.0	0.10	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-6.62e-03	-5.12e-03	-4.84e-03	85,90,92
	40.1	0.0	0.08	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
318	0.0	0.0	0.05	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-4.66e-03	-3.37e-03	-3.16e-03	85,90,92
	40.1	0.0	0.07	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
319	0.0	0.0	0.08	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-6.66e-03	-5.15e-03	-4.86e-03	85,90,92
	40.1	0.0	0.06	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
320	0.0	0.0	0.04	0.0	0,85,0	0.0	0.0	0.0	0,0,0	4.92e-03	3.41e-03	3.21e-03	85,90,92
	40.1	0.0	0.05	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
321	0.0	0.0	0.06	0.0	0,85,0	0.0	0.0	0.0	0,0,0	6.61e-03	5.15e-03	4.86e-03	85,90,92
	40.1	0.0	0.04	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
322	0.0	0.0	0.03	0.0	0,85,0	0.0	0.0	0.0	0,0,0	4.89e-03	-3.73e-03	-3.54e-03	85,90,92
	40.1	4.32e-04	0.04	3.62e-04	85,85,92	0.0	0.0	0.0	0,0,0				
323	0.0	3.21e-03	0.05	3.16e-03	85,85,92	0.0	0.0	0.0	0,0,0	6.59e-03	5.16e-03	4.88e-03	85,90,92
	40.1	0.0	0.03	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
324	0.0	0.0	0.01	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-4.66e-03	-1.04e-03	-9.62e-04	85,90,92
	40.1	2.17e-03	0.03	1.88e-03	85,85,92	0.0	0.0	0.0	0,0,0				
325	0.0	5.46e-03	0.03	5.63e-03	85,85,92	0.0	0.0	0.0	0,0,0	-6.15e-03	-4.89e-03	-4.65e-03	85,90,92
	40.1	0.0	0.01	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
326	0.0	0.0	9.96e-03	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-2.59e-03	-1.89e-03	-1.76e-03	85,90,92
	40.1	3.23e-03	0.01	2.81e-03	85,85,92	0.0	0.0	0.0	0,0,0				
327	0.0	5.71e-03	0.01	6.03e-03	85,82,92	0.0	0.0	0.0	0,0,0	-4.46e-03	-3.43e-03	-3.24e-03	85,90,92
	40.1	3.45e-03	0.01	3.34e-03	85,85,92	0.0	0.0	0.0	0,0,0				
328	0.0	2.85e-03	9.08e-03	2.66e-03	85,85,92	0.0	0.0	0.0	0,0,0	-3.12e-03	-2.20e-03	-2.04e-03	85,90,92
	40.1	2.97e-03	2.91e-03	2.55e-03	85,85,92	0.0	0.0	0.0	0,0,0				
329	0.0	2.27e-03	2.26e-03	2.31e-03	85,85,92	0.0	0.0	0.0	0,0,0	4.61e-03	3.57e-03	3.37e-03	85,90,92
	40.1	7.68e-03	0.02	8.02e-03	85,85,92	0.0	0.0	0.0	0,0,0				
330	0.0	4.77e-03	0.02	4.77e-03	82,83,92	0.0	0.0	0.0	0,0,0	-1.57e-03	-1.34e-03	-1.23e-03	81,87,92
	46.7	8.82e-04	0.01	5.45e-04	81,83,92	0.0	0.0	0.0	0,0,0				
331	0.0	8.59e-03	0.03	9.73e-03	82,83,92	0.0	0.0	0.0	0,0,0	1.94e-03	1.61e-03	1.48e-03	81,87,92
	46.7	6.96e-04	0.02	0.0	81,83,0	0.0	0.0	0.0	0,0,0				
332	0.0	0.01	0.04	0.02	85,82,92	0.0	0.0	0.0	0,0,0	1.00e-02	8.50e-03	8.12e-03	85,90,92
	46.7	3.82e-03	0.02	4.25e-03	83,83,91	0.0	0.0	0.0	0,0,0				
333	0.0	0.02	0.10	0.02	85,85,92	0.0	0.0	0.0	0,0,0	7.08e-03	6.24e-03	6.03e-03	83,88,91
	46.7	0.02	0.10	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
334	0.0	1.29e-03	6.66e-03	1.04e-03	85,83,92	0.0	0.0	0.0	0,0,0	-1.88e-03	-1.45e-03	-1.28e-03	81,87,92
	40.0	2.19e-03	3.49e-03	2.04e-03	81,83,92	0.0	0.0	0.0	0,0,0				
335	0.0	2.25e-03	6.27e-03	2.03e-03	85,83,92	0.0	0.0	0.0	0,0,0	1.93e-03	1.55e-03	1.38e-03	81,87,92
	40.0	3.64e-03	6.52e-03	3.94e-03	81,83,92	0.0	0.0	0.0	0,0,0				
336	0.0	6.84e-03	0.03	6.78e-03	82,83,92	0.0	0.0	0.0	0,0,0	1.88e-03	1.52e-03	1.38e-03	81,87,92
	46.7	1.32e-03	0.02	1.32e-03	81,83,92	0.0	0.0	0.0	0,0,0				
337	0.0	0.01	0.05	0.01	82,85,92	0.0	0.0	0.0	0,0,0	-2.20e-03	-1.83e-03	-1.68e-03	81,87,92
	46.7	1.09e-03	0.03	6.65e-04	81,83,92	0.0	0.0	0.0	0,0,0				
338	0.0	0.01	0.05	0.01	85,85,92	0.0	0.0	0.0	0,0,0	9.83e-03	8.36e-03	8.00e-03	83,88,91
	46.7	2.89e-03	0.04	0.0	81,82,0	0.0	0.0	0.0	0,0,0				
339	0.0	5.01e-03	0.08	6.69e-03	79,85,91	0.0	0.0	0.0	0,0,0	6.25e-03	5.51e-03	5.32e-03	83,88,91
	46.7	0.02	0.10	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
340	0.0	1.92e-03	1.96e-03	1.71e-03	81,83,92	0.0	0.0	0.0	0,0,0	-1.87e-03	-1.45e-03	-1.28e-03	81,87,92
	40.0	2.67e-03	3.67e-03	2.61e-03	81,83,92	0.0	0.0	0.0	0,0,0				
341	0.0	2.63e-03	2.59e-03	2.71e-03	81,81,92	0.0	0.0	0.0	0,0,0	1.98e-03	1.60e-03	1.45e-03	81,87,92
	40.0	4.77e-03	6.97e-03	5.31e-03	81,85,92	0.0	0.0	0.0	0,0,0				
342	0.0	2.41e-03	2.33e-03	2.29e-03	81,81,92	0.0	0.0	0.0	0,0,0	1.94e-03	1.52e-03	1.35e-03	81,87,92
	40.0	2.94e-03	3.56e-03	2.94e-03	81,83,92	0.0	0.0	0.0	0,0,0				
343	0.0	3.76e-03	3.65e-03	4.08e-03	81,81,92	0.0	0.0	0.0	0,0,0	-2.14e-03	1.75e-03	1.59e-03	81,87,92
	40.0	5.61e-03	7.21e-03	6.33e-03	81,85,92	0.0	0.0	0.0	0,0,0				
344	0.0	2.78e-03	2.67e-03	2.72e-03	81,81,92	0.0	0.0	0.0	0,0,0	2.04e-03	1.60e-03	1.43e-03	81,87,92
	40.0	3.10e-03	3.26e-03	3.13e-03	81,83,92	0.0	0.0	0.0	0,0,0				
345	0.0	4.74e-03	4.57e-03	5.26e-03	81,81,92	0.0	0.0	0.0	0,0,0	2.33e-03	1.92e-03	1.76e-03	81,87,92
	40.0	6.20e-03	7.02e-03	7.06e-03	81,85,92	0.0	0.0	0.0	0,0,0				
346	0.0	3.17e-03	3.00e-03	3.19e-03	81,81,92	0.0	0.0	0.0	0,0,0	2.12e-03	1.68e-03	1.50e-03	81,87,92
	40.0	3.41e-03	3.79e-03	3.52e-03	81,85,92	0.0	0.0	0.0	0,0,0				
347	0.0	5.68e-03	5.42e-03	6.40e-03	81,81,92	0.0	0.0	0.0	0,0,0	-2.53e-03	-2.11e-03	-1.94e-03	81,87,92
	40.0	6.80e-03	7.27e-03	7.78e-03	81,85,92	0.0	0.0	0.0	0,0,0				
348	0.0	3.52e-03	3.48e-03	3.63e-03	81,85,92	0.0	0.0	0.0	0,0,0	2.23e-03	1.78e-03	1.60e-03	81,87,92
	40.0	3.99e-03	5.26e-03	4.24e-03	81,85,92	0.0	0.0	0.0	0,0,0				
349	0.0	6.50e-03	6.15e-03	7.40e-03	81,81,92	0.0	0.0	0.0	0,0,0	-2.76e-03	-2.32e-03	-2.14e-03	81,87,92
	40.0	7.45e-03	8.11e-03	8.59e-03	81,85,92	0.0	0.0	0.0	0,0,0				
350	0.0	3.81e-03	3.85e-03	3.99e-03	81,85,92	0.0	0.0	0.0	0,0,0	2.38e-03	1.92e-03	1.73e-03	81,87,92
	40.0	4.55e-03	6.32e-03	4.97e-03	81,85,92	0.0	0.0	0.0	0,0,0				
351	0.0	7.12e-03	6.70e-03	8.16e-03	81,81,92	0.0	0.0	0.0	0,0,0	3.04e-03	2.57e-03	2.39e-03	81,87,92
	40.0	7.87e-03	8.46e-03	9.14e-03	81,85,92	0.0	0.0	0.0	0,0,0				
352	0.0	4.14e-03	3.89e-03	4.41e-03	81,81,92	0.0	0.0	0.0	0,0,0	2.58e-03	2.09e-03	1.90e-03	81,87,92
	40.0	4.71e-03	5.95e-03	5.27e-03	81,85,92	0.0	0.0	0.0	0,0,0				
353	0.0	7.59e-03	7.14e-03	8.75e-03	81,81,92	0.0	0.0	0.0	0,0,0	3.34e-03	2.85e-03	2.66e-03	81,87,92
	40.0	7.68e-03	7.43e-03	8.99e-03	81,85,92	0.0	0.0	0.0	0,0,0				
354	0.0	4.52e-03	4.36e-03	4.92e-03	81,82,92	0.0	0.0	0.0	0,0,0	-2.79e-03	-2.28e-03	-2.08e-03	81,87,92
	40.0	4.21e-03	4.26e-03	4.79e-03	81,83,92	0.0	0.0	0.0	0,0,0				
355	0.0	7.92e-03	7.85e-03	9.18e-03	81,82,92	0.0	0.0	0.0	0,0,0	3.65e-03	3.14e-03	2.93e-03	81,87,92
	40.0	6.68e-03	6.34e-03	7.85e-03	81,81,92	0.0	0.0	0.0	0,0,0				
356	0.0	4.74e-03	5.69e-03	5.27e-03	81,82,92	0.0	0.0	0.0	0,0,0	-2.96e-03	-2.44e-03	-2.23e-03	81,87,92
	40.0	3.06e-03	2.95e-03	3.53e-03	81,81,92	0.0	0.0	0.0	0,0,0				
357	0.0	7.86e-03	9.52e-03	9.16e-03	81,82,92	0.0	0.0	0.0	0,0,0	3.91e-03	3.38e-03	3.17e-03	81,87,92
	40.0	4.90e-03	4.74e-03	5.79e-03	81,81,92	0.0	0.0	0.0	0,0,0				
358	0.0	4.52e-03	7.61e-03	5.11e-03	81,82,92	0.0	0.0	0.0	0,0,0	-3.05e-03	-2.52e-03	-2.31e-03	81,87,92
	40.0	1.60e-03	1.58e-03	1.84e-03	81,81,92	0.0	0.0	0.0	0,0,0				
359	0.0	7.14e-03	0.01	8.38e-03	81,82,92	0.0	0.0	0.0	0,0,0	4.07e-03	3.53e-03	3.31e-03	81,87,92
	40.0	2.72e-03	2.68e-03	3.19e-03	81,81,92	0.0	0.0	0.0	0,0,0				
360	0.0	3.60e-03	0.01	4.12e-03	81,82,92	0.0	0.0	0.0	0,0,0	-3.01e-03	-2.51e-03	-2.31e-03	81,87,92
	40.0	5.05e-04	8.97e-04	3.14e-04	81,83,92	0.0	0.0	0.0	0,0,0				
361	0.0	5.56e-03	0.01	6.55e-03	81,82,92	0.0	0.0	0.0	0,0,0	4.08e-03	3.55e-03	3.33e-03	81,87,92

	40.1	0.0	0.24	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
367	0.0	0.0	0.26	0.0	0,85,0	0.0	0.0	0.0	0,0,0	1.51e-03	1.05e-03	8.95e-04	82,87,92
	40.1	0.0	0.25	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
368	0.0	0.0	0.27	0.0	0,85,0	0.0	0.0	0.0	0,0,0	8.30e-04	4.56e-04	3.10e-04	82,87,92
	40.1	0.0	0.26	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
369	0.0	0.0	0.27	0.0	0,85,0	0.0	0.0	0.0	0,0,0	5.80e-04	5.05e-04	4.87e-04	83,88,91
	40.1	0.0	0.27	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
370	0.0	0.0	0.28	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-1.26e-03	-1.11e-03	-1.07e-03	83,88,91
	40.1	0.0	0.27	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
371	0.0	0.0	0.28	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-1.95e-03	-1.72e-03	-1.66e-03	83,88,91
	40.1	0.0	0.28	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
372	0.0	0.0	0.27	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-2.66e-03	-2.34e-03	-2.26e-03	83,88,91
	40.1	0.0	0.28	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
373	0.0	0.0	0.27	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-3.41e-03	-3.01e-03	-2.90e-03	83,88,91
	40.1	0.0	0.27	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
374	0.0	0.0	0.25	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-4.25e-03	-3.75e-03	-3.62e-03	83,88,91
	40.1	0.0	0.27	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
375	0.0	0.0	0.21	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-6.08e-03	-5.25e-03	-5.07e-03	83,88,91
	40.1	0.0	0.25	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
376	0.0	0.0	0.18	0.0	0,85,0	0.0	0.0	0.0	0,0,0	0.01	9.77e-03	9.45e-03	83,88,91
	40.1	2.52e-03	0.22	3.36e-03	79,85,91	0.0	0.0	0.0	0,0,0				
377	0.0	0.0	0.14	0.0	0,85,0	0.0	0.0	0.0	0,0,0	0.01	9.77e-03	9.45e-03	83,88,91
	40.1	0.0	0.18	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
378	0.0	0.0	0.12	0.0	0,85,0	0.0	0.0	0.0	0,0,0	0.01	9.77e-03	9.45e-03	83,88,91
	40.1	0.0	0.14	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
379	0.0	0.0	0.13	0.0	0,82,0	0.0	0.0	0.0	0,0,0	1.34e-03	1.17e-03	1.13e-03	83,88,91
	40.1	0.0	0.14	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
380	0.0	0.0	0.12	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-1.58e-03	-1.36e-03	-1.30e-03	83,88,91
	40.1	0.0	0.13	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
381	0.0	0.0	0.12	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-1.50e-03	-1.28e-03	-1.23e-03	83,88,91
	40.1	0.0	0.12	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
382	0.0	0.0	0.11	0.0	0,82,0	0.0	0.0	0.0	0,0,0	1.23e-03	1.03e-03	9.84e-04	83,88,91
	40.1	0.0	0.12	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
383	0.0	0.0	0.11	0.0	0,82,0	0.0	0.0	0.0	0,0,0	9.94e-04	8.83e-04	8.55e-04	83,88,91
	40.1	0.0	0.11	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
384	0.0	0.0	0.10	0.0	0,82,0	0.0	0.0	0.0	0,0,0	9.43e-04	8.42e-04	8.16e-04	83,88,91
	40.1	0.0	0.11	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
385	0.0	0.0	0.09	0.0	0,82,0	0.0	0.0	0.0	0,0,0	9.01e-04	8.09e-04	7.86e-04	83,88,91
	40.1	0.0	0.10	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
386	0.0	0.0	0.09	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-8.62e-04	-7.78e-04	-7.57e-04	83,88,91
	40.1	0.0	0.09	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
387	0.0	0.0	0.08	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-8.60e-04	-7.48e-04	-7.29e-04	83,88,91
	40.1	0.0	0.09	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
388	0.0	0.0	0.08	0.0	0,82,0	0.0	0.0	0.0	0,0,0	8.81e-04	7.62e-04	7.33e-04	83,88,91
	40.1	0.0	0.08	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
389	0.0	0.0	0.07	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-7.51e-04	-6.88e-04	-6.73e-04	85,90,92
	40.1	0.0	0.08	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
390	0.0	0.0	0.07	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-7.23e-04	-6.63e-04	-6.50e-04	85,90,92
	40.1	0.0	0.07	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
391	0.0	0.0	0.07	0.0	0,82,0	0.0	0.0	0.0	0,0,0	6.97e-04	-6.39e-04	-6.28e-04	85,90,92
	40.1	0.0	0.07	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
392	0.0	0.0	0.07	0.0	0,82,0	0.0	0.0	0.0	0,0,0	6.76e-04	6.21e-04	6.10e-04	85,87,92
	40.1	0.0	0.07	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
393	0.0	0.0	0.07	0.0	0,82,0	0.0	0.0	0.0	0,0,0	6.64e-04	1.11e-03	5.97e-04	82,87,92
	40.1	0.0	0.07	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
394	0.0	0.0	0.07	0.0	0,82,0	0.0	0.0	0.0	0,0,0	6.62e-04	-1.28e-03	-5.86e-04	82,87,92
	40.1	0.0	0.07	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
395	0.0	0.0	0.06	0.0	0,82,0	0.0	0.0	0.0	0,0,0	6.61e-04	-5.97e-04	-5.74e-04	82,87,92
	40.1	0.0	0.07	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
396	0.0	0.0	0.06	0.0	0,82,0	0.0	0.0	0.0	0,0,0	8.29e-04	5.84e-04	5.56e-04	81,87,92
	40.1	0.0	0.06	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
397	0.0	0.0	0.05	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-7.66e-04	-8.38e-04	-8.45e-04	81,87,92
	40.1	0.0	0.06	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
398	0.0	0.0	0.06	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-9.32e-04	-8.40e-04	-7.71e-04	81,87,92
	40.1	0.0	0.05	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
399	0.0	0.0	0.05	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-9.32e-04	-8.40e-04	-7.71e-04	81,87,92
	40.1	0.0	0.06	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
400	0.0	0.0	0.06	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-9.32e-04	-8.40e-04	-7.71e-04	83,88,91
	40.1	0.0	0.05	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
401	0.0	0.0	0.07	0.0	0,82,0	0.0	0.0	0.0	0,0,0	5.03e-04	3.75e-04	3.39e-04	83,88,91
	40.1	0.0	0.06	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
402	0.0	0.0	0.08	0.0	0,82,0	0.0	0.0	0.0	0,0,0	1.46e-03	1.03e-03	9.49e-04	83,88,91
	40.1	0.0	0.07	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
403	0.0	0.0	0.09	0.0	0,82,0	0.0	0.0	0.0	0,0,0	1.21e-03	8.43e-04	7.51e-04	83,88,91
	40.1	0.0	0.08	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
404	0.0	0.0	0.09	0.0	0,85,0	0.0	0.0	0.0	0,0,0	1.06e-03	7.09e-04	6.22e-04	83,88,91
	40.1	0.0	0.09	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
405	0.0	0.0	0.10	0.0	0,85,0	0.0	0.0	0.0	0,0,0	9.44e-04	5.92e-04	5.07e-04	83,88,91
	40.1	0.0	0.09	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
406	0.0	0.0	0.11	0.0	0,85,0	0.0	0.0	0.0	0,0,0	7.91e-04	4.55e-04	3.76e-04	83,88,91
	40.1	0.0	0.10	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
407	0.0	0.0	0.11	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-5.94e-04	-2.92e-04	-2.21e-04	83,88,91
	40.1	0.0	0.11	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
408	0.0	0.0	0.12	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-6.92e-04	-3.25e-04	-1.77e-04	81,87,92
	40.1	0.0	0.11	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
409	0.0	0.0	0.13	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-9.37e-04	-5.48e-04	-3.93e-04	81,87,92
	40.1	0.0	0.12	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
410	0.0	0.0	0.14	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-1.23e-03	-8.09e-04	-6.43e-04	81,87,92
	40.1	0.0	0.13	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
411	0.0	0.0	0.14	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-1.57e-03	-1.12e-03	-9.35e-04	81,87,92
	40.1	0.0	0.14	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
485	0.0	2.84e-03	3.93e-03	1.40e-03	85,85,92	0.0	0.0	0.0	0,0,0	-9.23e-04	-7.85e-04	-7.29e-04	81,87,92
	41.5	1.09e-03	1.15e-03	7.94e-04	85,81,92	0.0	0.0	0.0	0,0,0				
486	0.0	1.41e-03	3.82e-03	1.30e-03	81,81,92	0.0	0.0	0.0	0,0,0	-2.31e-03	-2.11e-03	-2.03e-03	81,87,92
	40.1	0.0	1.34e-03	0.0	81,0	0.0	0.0	0.0	0,0,0				
487	0.0	0.02	0.05	0.02	82,85,92	0.0	0.0	0.0	0,0,0	-9.48e-03	-8.27e-03	-7.95e-03	82,87,92
	40.1	5.00e-03	0.02	3.80e-03	82,85,92	0.0	0.0	0.0	0,0,0				
488	0.0	3.66e-03	4.63e-03	2.10e-03	85,85,92	0.0	0.0	0.0	0,0,0	-1.62e-03	-9.94e-04	-8.49e-04	85,90,92
	40.1	7.58e-04	4.29e-04	3.82e-04	85,85,92	0.0	0.0	0.0					

490	0.0	0.0	0.02	0.0	0,85,0	0.0	0.0	0.0	0,0,0	1.89e-03	3.41e-04	-1.82e-04	83,88,92
	46.7	0.0	0.02	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
491	0.0	0.02	0.03	0.02	83,85,91	0.0	0.0	0.0	0,0,0	0.01	7.70e-03	7.03e-03	83,88,91
	46.7	3.91e-04	8.93e-03	0.0	83,82,0	0.0	0.0	0.0	0,0,0				
492	0.0	0.01	7.00e-03	8.52e-03	85,85,92	0.0	0.0	0.0	0,0,0	-2.18e-03	-1.84e-03	-1.71e-03	81,87,92
	46.7	9.67e-03	5.91e-03	6.61e-03	85,85,92	0.0	0.0	0.0	0,0,0				
493	0.0	5.54e-03	3.41e-03	6.07e-03	85,85,92	0.0	0.0	0.0	0,0,0	1.60e-03	1.40e-03	1.35e-03	82,87,92
	40.1	6.35e-03	3.84e-03	6.97e-03	85,85,92	0.0	0.0	0.0	0,0,0				
494	0.0	0.03	0.02	0.02	85,85,92	0.0	0.0	0.0	0,0,0	-0.03	-0.02	-0.02	85,90,92
	40.1	0.06	0.03	0.06	85,85,92	0.0	0.0	0.0	0,0,0				
495	0.0	1.07e-03	1.35e-03	5.47e-04	85,83,92	0.0	0.0	0.0	0,0,0	-1.63e-03	-1.01e-03	-8.60e-04	85,90,92
	40.1	1.44e-04	5.81e-04	0.0	85,79,0	0.0	0.0	0.0	0,0,0				
496	0.0	0.0	0.02	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.49e-03	-1.24e-03	-1.14e-03	81,87,92
	40.0	0.0	0.02	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
497	0.0	5.06e-03	3.02e-03	6.75e-03	79,79,91	0.0	0.0	0.0	0,0,0	-9.75e-04	-7.57e-04	-6.69e-04	81,87,92
	40.0	4.64e-03	2.80e-03	6.18e-03	79,79,91	0.0	0.0	0.0	0,0,0				
498	0.0	0.0	0.10	0.0	0,85,0	0.0	0.0	0.0	0,0,0	6.15e-03	4.22e-03	3.73e-03	83,88,91
	40.0	0.0	0.10	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
499	0.0	0.01	6.47e-03	7.67e-03	85,85,92	0.0	0.0	0.0	0,0,0	-2.17e-03	-1.82e-03	-1.68e-03	81,87,92
	41.5	0.01	7.44e-03	9.15e-03	85,85,92	0.0	0.0	0.0	0,0,0				
500	0.0	0.01	8.20e-03	0.02	85,85,92	0.0	0.0	0.0	0,0,0	1.24e-03	1.09e-03	1.05e-03	82,87,92
	40.1	0.01	7.70e-03	0.01	85,85,92	0.0	0.0	0.0	0,0,0				
501	0.0	0.06	0.05	0.07	85,79,92	0.0	0.0	0.0	0,0,0	-0.03	-0.02	-0.02	85,90,92
	40.1	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
502	0.0	0.01	0.02	0.01	82,81,92	0.0	0.0	0.0	0,0,0	-1.66e-03	-1.31e-03	-1.18e-03	81,87,92
	46.7	7.25e-03	7.52e-03	6.76e-03	85,81,92	0.0	0.0	0.0	0,0,0				
503	0.0	0.0	0.03	0.0	0,85,0	0.0	0.0	0.0	0,0,0	1.50e-03	-5.55e-04	-4.62e-04	83,87,92
	46.7	1.23e-03	0.03	1.64e-03	79,85,91	0.0	0.0	0.0	0,0,0				
504	0.0	0.0	0.11	0.0	0,85,0	0.0	0.0	0.0	0,0,0	6.47e-03	4.49e-03	3.99e-03	83,88,91
	40.0	0.0	0.11	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
505	0.0	7.20e-03	4.47e-03	5.09e-03	83,83,91	0.0	0.0	0.0	0,0,0	-1.86e-03	-1.60e-03	-1.49e-03	81,87,92
	40.0	8.44e-03	5.13e-03	6.44e-03	83,83,91	0.0	0.0	0.0	0,0,0				
506	0.0	4.79e-03	2.94e-03	5.21e-03	85,85,92	0.0	0.0	0.0	0,0,0	1.66e-03	1.45e-03	1.39e-03	82,87,92
	40.1	5.53e-03	3.34e-03	6.03e-03	85,85,92	0.0	0.0	0.0	0,0,0				
507	0.0	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0	0.01	9.66e-03	9.15e-03	85,90,92
	40.1	0.02	0.02	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
508	0.0	5.62e-05	1.23e-03	0.0	85,79,0	0.0	0.0	0.0	0,0,0	-1.63e-03	-1.00e-03	-8.55e-04	85,90,92
	40.1	0.0	1.51e-03	0.0	0,79,0	0.0	0.0	0.0	0,0,0				
509	0.0	0.0	9.12e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.49e-03	-1.23e-03	-1.13e-03	81,87,92
	40.0	0.0	0.01	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
510	0.0	7.57e-03	4.49e-03	0.01	79,79,91	0.0	0.0	0.0	0,0,0	9.36e-04	-6.49e-04	-5.61e-04	83,87,92
	40.0	7.23e-03	4.32e-03	9.65e-03	79,79,91	0.0	0.0	0.0	0,0,0				
511	0.0	0.0	0.08	0.0	0,85,0	0.0	0.0	0.0	0,0,0	5.97e-03	4.06e-03	3.57e-03	83,88,91
	40.0	0.0	0.08	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
512	0.0	9.45e-03	5.77e-03	6.59e-03	85,85,92	0.0	0.0	0.0	0,0,0	-2.22e-03	-1.86e-03	-1.71e-03	81,87,92
	41.5	9.57e-03	5.83e-03	6.60e-03	85,85,92	0.0	0.0	0.0	0,0,0				
513	0.0	0.02	0.01	0.03	85,85,92	0.0	0.0	0.0	0,0,0	-1.11e-03	-1.04e-03	-1.01e-03	81,87,92
	40.1	0.01	7.28e-03	0.01	82,82,92	0.0	0.0	0.0	0,0,0				
514	0.0	0.07	0.10	0.09	81,81,92	0.0	0.0	0.0	0,0,0	-0.02	-0.02	-0.02	85,90,92
	40.1	0.06	0.09	0.08	82,79,92	0.0	0.0	0.0	0,0,0				
515	0.0	6.42e-03	3.75e-03	4.58e-03	85,85,92	0.0	0.0	0.0	0,0,0	-2.17e-03	-1.82e-03	-1.67e-03	81,87,92
	41.5	0.02	0.02	0.02	82,81,92	0.0	0.0	0.0	0,0,0				
516	0.0	0.0	0.11	0.0	0,85,0	0.0	0.0	0.0	0,0,0	6.87e-03	4.83e-03	4.32e-03	83,88,91
	40.0	0.0	0.11	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
517	0.0	7.88e-03	4.88e-03	5.73e-03	83,83,91	0.0	0.0	0.0	0,0,0	-2.18e-03	-1.88e-03	-1.75e-03	81,87,92
	46.7	8.46e-03	5.18e-03	6.16e-03	85,85,92	0.0	0.0	0.0	0,0,0				
518	0.0	0.06	0.04	0.07	85,85,92	0.0	0.0	0.0	0,0,0	7.05e-03	5.87e-03	5.61e-03	85,90,92
	40.1	0.06	0.04	0.06	85,85,92	0.0	0.0	0.0	0,0,0				
519	0.0	0.01	6.88e-03	0.01	85,85,92	0.0	0.0	0.0	0,0,0	1.32e-03	1.16e-03	1.12e-03	82,87,92
	40.1	0.01	6.91e-03	0.01	85,85,92	0.0	0.0	0.0	0,0,0				
520	0.0	0.03	0.02	0.03	85,85,92	0.0	0.0	0.0	0,0,0	-0.03	-0.02	-0.02	85,90,92
	40.1	0.03	0.02	0.04	85,85,92	0.0	0.0	0.0	0,0,0				
521	0.0	2.59e-03	7.62e-03	0.0	83,81,0	0.0	0.0	0.0	0,0,0	-1.63e-03	-1.30e-03	-1.16e-03	81,87,92
	46.7	3.45e-03	8.38e-03	0.0	83,81,0	0.0	0.0	0.0	0,0,0				
522	0.0	2.21e-03	0.02	2.95e-03	79,85,91	0.0	0.0	0.0	0,0,0	1.17e-03	-7.90e-04	-6.94e-04	83,87,92
	46.7	2.27e-03	0.02	3.02e-03	79,85,91	0.0	0.0	0.0	0,0,0				
523	0.0	2.06e-03	1.11e-03	2.30e-03	81,81,92	0.0	0.0	0.0	0,0,0	-3.06e-03	-2.60e-03	-2.42e-03	81,87,92
	40.0	1.64e-03	9.53e-04	1.63e-03	85,85,92	0.0	0.0	0.0	0,0,0				
524	0.0	3.89e-03	2.40e-03	4.20e-03	85,85,92	0.0	0.0	0.0	0,0,0	1.71e-03	1.49e-03	1.43e-03	82,87,92
	40.1	4.47e-03	2.70e-03	4.83e-03	85,85,92	0.0	0.0	0.0	0,0,0				
525	0.0	8.58e-05	0.02	0.0	81,83,0	0.0	0.0	0.0	0,0,0	5.37e-03	4.23e-03	4.01e-03	85,90,92
	40.1	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
526	0.0	0.0	1.98e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.62e-03	-9.96e-04	-8.51e-04	85,90,92
	40.1	0.0	2.15e-03	0.0	0,79,0	0.0	0.0	0.0	0,0,0				
527	0.0	8.11e-04	5.75e-03	0.0	83,81,0	0.0	0.0	0.0	0,0,0	-3.01e-03	-1.28e-03	-1.18e-03	81,87,92
	40.0	0.0	5.29e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
528	0.0	0.01	7.04e-03	0.02	79,79,91	0.0	0.0	0.0	0,0,0	1.33e-03	-2.48e-04	-1.58e-04	83,87,92
	40.0	0.01	7.06e-03	0.02	79,79,91	0.0	0.0	0.0	0,0,0				
529	0.0	0.0	0.02	0.0	0,85,0	0.0	0.0	0.0	0,0,0	5.35e-03	3.59e-03	3.15e-03	83,88,91
	40.0	0.0	0.03	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
530	0.0	8.48e-03	5.20e-03	5.65e-03	83,83,91	0.0	0.0	0.0	0,0,0	-2.24e-03	-1.87e-03	-1.73e-03	81,87,92
	41.5	8.04e-03	4.96e-03	5.13e-03	83,83,91	0.0	0.0	0.0	0,0,0				
531	0.0	0.02	9.96e-03	0.02	85,85,92	0.0	0.0	0.0	0,0,0	-9.10e-04	-8.46e-04	-8.20e-04	81,87,92
	40.1	0.02	0.01	0.03	85,85,92	0.0	0.0	0.0	0,0,0				
532	0.0	0.11	0.37	0.12	85,85,92	0.0	0.0	0.0	0,0,0	-0.02	-0.02	-0.02	85,90,92
	40.1	0.0	0.14	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
533	0.0	3.88e-03	2.36e-03	1.31e-03	83,83,91	0.0	0.0	0.0	0,0,0	-2.23e-03	-1.86e-03	-1.72e-03	81,87,92
	41.5	5.13e-03	4.70e-03	3.64e-03	83,81,92	0.0	0.0	0.0	0,0,0				
534	0.0	0.0	0.05	0.0	0,85,0	0.0	0.0	0.0	0,0,0	9.83e-03	7.20e-03	6.54e-03	83,88,91
	46.7	0.0	0.05	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
535	0.0	8.81e-03	5.43e-03	5.93e-03	85,85,92	0.0	0.0	0.0	0,0,0	-2.16e-03	-1.84e-03	-1.72e-03	81,87,92
	46.7	8.72e-03	5.38e-03	5.93e-03	85,85,92	0.0	0.0	0.0	0,0,0				
536	0.0	0.07	0.04	0.07	85,85,92	0.0	0.0	0.0	0,0,0	5.59e-03	4.55e-03	4.32e-03	85,90,92
	40.1	0.07	0.04	0.07	85,85,92	0.0	0.0	0.0	0,0,0				

	40.0	0.0	0.05	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
541	0.0	0.01	7.77e-03	0.01	85,85,92	0.0	0.0	0.0	0,0,0	9.14e-04	7.68e-04	7.28e-04	82,87,92
	40.1	0.01	8.13e-03	0.01	85,85,92	0.0	0.0	0.0	0,0,0				
542	0.0	0.10	0.13	0.12	82,81,92	0.0	0.0	0.0	0,0,0	-0.03	-0.02	-0.02	85,90,92
	40.1	0.01	7.40e-03	0.01	85,85,92	0.0	0.0	0.0	0,0,0				
543	0.0	0.05	0.03	0.06	85,85,92	0.0	0.0	0.0	0,0,0	6.94e-03	6.14e-03	5.98e-03	85,90,92
	40.1	0.05	0.03	0.06	85,85,92	0.0	0.0	0.0	0,0,0				
544	0.0	9.77e-03	6.05e-03	0.01	85,85,92	0.0	0.0	0.0	0,0,0	1.35e-03	1.20e-03	1.15e-03	82,87,92
	40.1	0.01	6.38e-03	0.01	85,85,92	0.0	0.0	0.0	0,0,0				
545	0.0	3.82e-03	0.02	0.0	85,81,0	0.0	0.0	0.0	0,0,0	-1.75e-03	-1.41e-03	-1.28e-03	81,87,92
	46.7	1.34e-03	0.02	0.0	83,81,0	0.0	0.0	0.0	0,0,0				
546	0.0	2.21e-03	7.53e-03	2.07e-03	83,85,92	0.0	0.0	0.0	0,0,0	-9.96e-04	-7.83e-04	-6.97e-04	81,87,92
	40.0	2.26e-03	7.40e-03	2.39e-03	82,85,92	0.0	0.0	0.0	0,0,0				
547	0.0	2.51e-03	1.51e-03	2.71e-03	85,85,92	0.0	0.0	0.0	0,0,0	8.89e-04	7.73e-04	7.40e-04	82,87,92
	40.1	2.27e-03	1.38e-03	2.47e-03	85,85,92	0.0	0.0	0.0	0,0,0				
548	0.0	0.0	3.03e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.63e-03	-9.96e-04	-8.49e-04	85,90,92
	40.1	0.0	2.97e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
549	0.0	0.01	7.89e-03	0.02	79,79,91	0.0	0.0	0.0	0,0,0	1.62e-03	5.37e-04	2.66e-04	83,88,91
	40.0	0.01	7.95e-03	0.02	79,79,91	0.0	0.0	0.0	0,0,0				
550	0.0	7.32e-03	4.50e-03	4.53e-03	83,83,91	0.0	0.0	0.0	0,0,0	-2.24e-03	-1.88e-03	-1.73e-03	81,87,92
	41.5	6.80e-03	4.22e-03	4.01e-03	83,83,91	0.0	0.0	0.0	0,0,0				
551	0.0	0.02	0.01	0.03	85,85,92	0.0	0.0	0.0	0,0,0	-1.06e-03	-9.87e-04	-9.57e-04	81,87,92
	40.1	0.02	0.01	0.03	85,85,92	0.0	0.0	0.0	0,0,0				
552	0.0	0.11	0.27	0.11	85,85,92	0.0	0.0	0.0	0,0,0	-0.02	-0.01	-0.01	85,90,92
	40.1	0.08	0.21	0.10	82,85,92	0.0	0.0	0.0	0,0,0				
553	0.0	2.55e-03	5.82e-03	6.84e-04	83,81,91	0.0	0.0	0.0	0,0,0	-1.13e-03	-9.36e-04	-8.60e-04	81,87,92
	41.5	2.61e-03	6.01e-03	8.19e-04	83,81,91	0.0	0.0	0.0	0,0,0				
554	0.0	0.07	0.04	0.07	85,85,92	0.0	0.0	0.0	0,0,0	-0.02	-0.02	-0.02	85,90,92
	40.1	0.09	0.05	0.10	85,85,92	0.0	0.0	0.0	0,0,0				
555	0.0	3.61e-03	6.58e-03	4.63e-03	82,81,92	0.0	0.0	0.0	0,0,0	-3.28e-03	-2.81e-03	-2.62e-03	81,87,92
	40.0	3.80e-03	6.63e-03	4.69e-03	82,81,92	0.0	0.0	0.0	0,0,0				
556	0.0	0.0	0.04	0.0	0,83,0	0.0	0.0	0.0	0,0,0	4.92e-03	3.88e-03	3.69e-03	85,90,92
	40.1	0.0	0.04	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
557	0.0	0.0	0.04	0.0	0,85,0	0.0	0.0	0.0	0,0,0	5.51e-03	3.74e-03	3.30e-03	83,88,91
	40.0	0.0	0.05	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
558	0.0	0.01	8.07e-03	0.01	85,85,92	0.0	0.0	0.0	0,0,0	8.97e-04	7.53e-04	7.15e-04	82,87,92
	40.1	0.01	8.34e-03	0.01	85,85,92	0.0	0.0	0.0	0,0,0				
559	0.0	0.06	0.03	0.06	85,85,92	0.0	0.0	0.0	0,0,0	7.43e-03	6.36e-03	6.12e-03	85,90,92
	40.1	0.06	0.04	0.06	85,85,92	0.0	0.0	0.0	0,0,0				
560	0.0	2.78e-03	1.73e-03	3.02e-03	85,85,92	0.0	0.0	0.0	0,0,0	1.74e-03	1.51e-03	1.45e-03	82,87,92
	40.1	3.10e-03	1.90e-03	3.30e-03	85,85,92	0.0	0.0	0.0	0,0,0				
561	0.0	0.0	0.11	0.0	0,85,0	0.0	0.0	0.0	0,0,0	7.33e-03	5.23e-03	4.70e-03	83,88,91
	40.0	0.0	0.10	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
562	0.0	0.06	0.04	0.07	85,85,92	0.0	0.0	0.0	0,0,0	6.62e-03	5.47e-03	5.21e-03	85,90,92
	40.1	0.06	0.04	0.07	85,85,92	0.0	0.0	0.0	0,0,0				
563	0.0	0.01	7.62e-03	0.01	85,85,92	0.0	0.0	0.0	0,0,0	9.35e-04	7.86e-04	7.44e-04	82,87,92
	40.1	0.01	8.32e-03	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
564	0.0	0.07	0.04	0.06	85,85,92	0.0	0.0	0.0	0,0,0	0.01	9.60e-03	8.99e-03	85,90,92
	40.1	0.04	0.02	0.04	85,85,92	0.0	0.0	0.0	0,0,0				
565	0.0	8.83e-03	5.49e-03	9.98e-03	85,85,92	0.0	0.0	0.0	0,0,0	1.38e-03	1.22e-03	1.18e-03	82,87,92
	40.1	9.65e-03	5.92e-03	0.01	85,85,92	0.0	0.0	0.0	0,0,0				
566	0.0	2.91e-03	0.03	0.0	83,81,0	0.0	0.0	0.0	0,0,0	-1.62e-03	-1.32e-03	-1.20e-03	81,87,92
	40.0	2.07e-04	0.02	0.0	83,81,0	0.0	0.0	0.0	0,0,0				
567	0.0	2.44e-03	1.49e-03	3.26e-03	79,79,91	0.0	0.0	0.0	0,0,0	-1.02e-03	-8.02e-04	-7.16e-04	81,87,92
	40.0	2.12e-03	1.32e-03	2.82e-03	79,79,91	0.0	0.0	0.0	0,0,0				
568	0.0	2.31e-03	1.33e-03	2.51e-03	85,85,92	0.0	0.0	0.0	0,0,0	1.68e-03	1.46e-03	1.40e-03	82,87,92
	40.1	1.56e-03	9.35e-04	1.69e-03	85,85,92	0.0	0.0	0.0	0,0,0				
569	0.0	0.0	4.03e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.64e-03	-9.98e-04	-8.49e-04	85,90,92
	40.1	0.0	3.90e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
570	0.0	4.20e-03	2.60e-03	5.04e-03	83,83,92	0.0	0.0	0.0	0,0,0	3.03e-03	1.89e-03	1.60e-03	83,88,91
	40.0	4.33e-03	2.67e-03	5.22e-03	83,83,91	0.0	0.0	0.0	0,0,0				
571	0.0	6.01e-03	3.72e-03	3.29e-03	83,83,91	0.0	0.0	0.0	0,0,0	-1.14e-03	-1.87e-03	-1.73e-03	81,87,92
	41.5	5.96e-03	3.69e-03	3.29e-03	83,83,91	0.0	0.0	0.0	0,0,0				
572	0.0	0.03	0.02	0.03	85,85,92	0.0	0.0	0.0	0,0,0	-1.29e-03	-1.20e-03	-1.16e-03	81,87,92
	40.1	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
573	0.0	0.06	0.16	0.06	85,85,92	0.0	0.0	0.0	0,0,0	-9.03e-03	-6.82e-03	-6.30e-03	85,90,92
	40.1	0.13	0.27	0.13	85,85,92	0.0	0.0	0.0	0,0,0				
574	0.0	2.11e-03	0.01	0.0	83,81,0	0.0	0.0	0.0	0,0,0	-2.13e-03	-1.76e-03	-1.62e-03	81,87,92
	41.5	2.51e-03	0.01	0.0	83,81,0	0.0	0.0	0.0	0,0,0				
575	0.0	0.06	0.03	0.06	85,85,92	0.0	0.0	0.0	0,0,0	-0.02	-0.02	-0.02	85,90,92
	40.1	0.08	0.05	0.09	85,85,92	0.0	0.0	0.0	0,0,0				
576	0.0	1.16e-03	7.43e-03	0.0	83,81,0	0.0	0.0	0.0	0,0,0	-3.41e-03	-2.93e-03	-2.75e-03	81,87,92
	40.0	2.79e-03	0.01	2.69e-03	83,81,91	0.0	0.0	0.0	0,0,0				
577	0.0	0.0	0.05	0.0	0,83,0	0.0	0.0	0.0	0,0,0	4.79e-03	3.77e-03	3.58e-03	85,90,92
	40.1	0.0	0.05	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
578	0.0	0.0	0.05	0.0	0,85,0	0.0	0.0	0.0	0,0,0	5.55e-03	3.78e-03	3.33e-03	83,88,91
	40.0	0.0	0.06	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
579	0.0	0.01	8.53e-03	0.02	85,85,92	0.0	0.0	0.0	0,0,0	8.73e-04	7.37e-04	7.00e-04	82,87,92
	40.1	0.01	8.75e-03	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
580	0.0	0.06	0.04	0.06	85,85,92	0.0	0.0	0.0	0,0,0	7.36e-03	6.19e-03	5.94e-03	85,90,92
	40.1	0.06	0.03	0.06	85,85,92	0.0	0.0	0.0	0,0,0				
581	0.0	0.0	0.09	0.0	0,85,0	0.0	0.0	0.0	0,0,0	9.17e-03	6.63e-03	5.99e-03	83,88,91
	46.7	0.0	0.08	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
582	0.0	0.07	0.04	0.07	85,85,92	0.0	0.0	0.0	0,0,0	6.12e-03	5.02e-03	4.78e-03	85,90,92
	40.1	0.06	0.04	0.07	85,85,92	0.0	0.0	0.0	0,0,0				
583	0.0	0.08	0.04	0.07	85,85,92	0.0	0.0	0.0	0,0,0	0.01	8.60e-03	8.10e-03	85,90,92
	40.1	0.06	0.03	0.05	85,85,92	0.0	0.0	0.0	0,0,0				
584	0.0	0.01	8.29e-03	0.02	83,83,91	0.0	0.0	0.0	0,0,0	1.95e-03	8.61e-04	5.89e-04	83,88,91
	40.0	0.01	8.32e-03	0.02	83,83,91	0.0	0.0	0.0	0,0,0				
585	0.0	0.07	0.04	0.07	85,85,92	0.0	0.0	0.0	0,0,0	3.91e-03	3.08e-03	2.89e-03	85,90,92
	40.1	0.07	0.04	0.07	85,85,92	0.0	0.0	0.0	0,0,0				
586	0.0	0.01	7.83e-03	0.01	85,85,92	0.0	0.0	0.0	0,0,0	1.00e-03	8.55e-04	8.13e-04	82,87,92
	40.1	0.02	9.10e-03	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
587	0.0	0.03	0.02	0.04	85,85,92	0.0	0.0	0.0	0,0,0	0.01	9.57e-03	9.05e-03	85,90,92
	40.1	0.03	0.02	0.03	85								

591	0.0	3.54e-03	2.11e-03	4.53e-03	83,83,91	0.0	0.0	0.0	0,0,0	3.04e-03	1.89e-03	1.61e-03	83,88,91
	40.0	4.39e-03	2.56e-03	5.59e-03	83,83,91	0.0	0.0	0.0	0,0,0				
592	0.0	5.10e-03	3.15e-03	2.04e-03	83,83,91	0.0	0.0	0.0	0,0,0	-1.13e-03	-9.52e-04	-8.81e-04	81,87,92
	41.5	5.44e-03	3.33e-03	2.60e-03	83,83,91	0.0	0.0	0.0	0,0,0				
593	0.0	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0	-1.56e-03	-1.44e-03	-1.40e-03	81,87,92
	40.1	0.02	9.59e-03	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
594	0.0	0.02	0.09	0.02	85,83,92	0.0	0.0	0.0	0,0,0	-5.10e-03	-3.56e-03	-3.18e-03	85,90,92
	40.1	0.10	0.24	0.11	85,85,92	0.0	0.0	0.0	0,0,0				
595	0.0	1.69e-03	0.02	0.0	83,81,0	0.0	0.0	0.0	0,0,0	-2.06e-03	-1.70e-03	-1.56e-03	81,87,92
	41.5	2.20e-03	0.02	0.0	85,81,0	0.0	0.0	0.0	0,0,0				
596	0.0	0.04	0.03	0.04	85,85,92	0.0	0.0	0.0	0,0,0	-0.02	-0.02	-0.02	85,90,92
	40.1	0.07	0.04	0.07	85,85,92	0.0	0.0	0.0	0,0,0				
597	0.0	3.69e-03	0.02	0.0	83,81,0	0.0	0.0	0.0	0,0,0	-3.38e-03	-2.92e-03	-2.73e-03	81,87,92
	40.0	4.86e-04	0.02	0.0	83,81,0	0.0	0.0	0.0	0,0,0				
598	0.0	0.0	0.06	0.0	0,83,0	0.0	0.0	0.0	0,0,0	4.73e-03	3.72e-03	3.53e-03	85,90,92
	40.1	0.0	0.06	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
599	0.0	0.0	0.06	0.0	0,85,0	0.0	0.0	0.0	0,0,0	5.59e-03	1.95e-03	1.72e-03	83,88,91
	40.0	0.0	0.06	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
600	0.0	0.01	9.04e-03	0.02	85,85,92	0.0	0.0	0.0	0,0,0	8.48e-04	7.17e-04	6.81e-04	82,87,92
	40.1	0.01	9.27e-03	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
601	0.0	0.11	0.06	0.10	85,85,92	0.0	0.0	0.0	0,0,0	8.43e-03	7.15e-03	6.87e-03	85,90,92
	40.1	0.10	0.06	0.09	85,85,92	0.0	0.0	0.0	0,0,0				
602	0.0	0.08	0.05	0.08	85,85,92	0.0	0.0	0.0	0,0,0	-1.58e-03	-1.13e-03	-1.02e-03	83,88,91
	40.1	0.06	0.04	0.06	85,85,92	0.0	0.0	0.0	0,0,0				
603	0.0	0.04	0.03	0.04	85,85,92	0.0	0.0	0.0	0,0,0	0.01	9.49e-03	8.94e-03	85,90,92
	40.1	0.04	0.02	0.04	85,85,92	0.0	0.0	0.0	0,0,0				
604	0.0	0.01	8.13e-03	0.02	83,83,91	0.0	0.0	0.0	0,0,0	2.28e-03	1.18e-03	9.11e-04	83,88,91
	40.0	0.01	8.14e-03	0.02	83,83,91	0.0	0.0	0.0	0,0,0				
605	0.0	0.07	0.04	0.07	85,85,92	0.0	0.0	0.0	0,0,0	5.03e-03	4.07e-03	3.84e-03	85,90,92
	40.1	0.07	0.04	0.07	85,85,92	0.0	0.0	0.0	0,0,0				
606	0.0	7.46e-03	4.63e-03	8.31e-03	85,85,92	0.0	0.0	0.0	0,0,0	1.46e-03	1.28e-03	1.23e-03	82,87,92
	40.1	8.34e-03	5.10e-03	9.31e-03	85,85,92	0.0	0.0	0.0	0,0,0				
607	0.0	0.0	0.03	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.77e-03	-1.45e-03	-1.32e-03	81,87,92
	40.0	0.0	0.03	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
608	0.0	0.0	6.13e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.68e-03	-1.01e-03	-8.50e-04	85,90,92
	40.1	0.0	6.00e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
609	0.0	4.85e-03	4.52e-03	1.52e-03	83,81,91	0.0	0.0	0.0	0,0,0	-2.16e-03	-1.82e-03	-1.69e-03	81,87,92
	41.5	5.07e-03	6.06e-03	1.99e-03	83,81,91	0.0	0.0	0.0	0,0,0				
610	0.0	0.02	9.52e-03	0.02	85,85,92	0.0	0.0	0.0	0,0,0	-1.78e-03	-1.65e-03	-1.60e-03	81,87,92
	40.1	0.01	8.28e-03	0.01	85,85,92	0.0	0.0	0.0	0,0,0				
611	0.0	0.0	0.06	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-3.14e-03	-1.82e-03	-1.50e-03	83,88,91
	40.1	0.07	0.17	0.07	85,85,92	0.0	0.0	0.0	0,0,0				
612	0.0	1.67e-03	0.02	0.0	83,81,0	0.0	0.0	0.0	0,0,0	-1.99e-03	-1.64e-03	-1.50e-03	81,87,92
	41.5	2.12e-03	0.02	0.0	83,81,0	0.0	0.0	0.0	0,0,0				
613	0.0	6.56e-03	0.04	2.64e-03	83,81,91	0.0	0.0	0.0	0,0,0	-3.14e-03	-2.71e-03	-2.54e-03	81,87,92
	40.0	3.96e-03	0.03	0.0	83,81,0	0.0	0.0	0.0	0,0,0				
614	0.0	0.0	0.07	0.0	0,83,0	0.0	0.0	0.0	0,0,0	4.74e-03	3.72e-03	3.51e-03	85,90,92
	40.1	0.0	0.07	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
615	0.0	0.0	0.07	0.0	0,85,0	0.0	0.0	0.0	0,0,0	5.62e-03	1.96e-03	1.73e-03	83,88,91
	40.0	0.0	0.07	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
616	0.0	0.02	9.62e-03	0.02	85,85,92	0.0	0.0	0.0	0,0,0	8.23e-04	6.98e-04	6.63e-04	82,87,92
	40.1	0.02	9.91e-03	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
617	0.0	0.10	0.06	0.11	85,85,92	0.0	0.0	0.0	0,0,0	-8.02e-03	-6.75e-03	-6.43e-03	83,88,91
	40.1	0.09	0.05	0.09	85,85,92	0.0	0.0	0.0	0,0,0				
618	0.0	0.07	0.04	0.07	85,85,92	0.0	0.0	0.0	0,0,0	4.47e-03	3.57e-03	3.37e-03	85,90,92
	40.1	0.07	0.04	0.07	85,85,92	0.0	0.0	0.0	0,0,0				
619	0.0	0.07	0.04	0.07	85,85,92	0.0	0.0	0.0	0,0,0	3.38e-03	2.61e-03	2.43e-03	85,90,92
	40.1	0.07	0.04	0.07	85,85,92	0.0	0.0	0.0	0,0,0				
620	0.0	0.01	7.37e-03	0.02	83,83,91	0.0	0.0	0.0	0,0,0	2.58e-03	1.47e-03	1.20e-03	83,88,91
	40.0	0.01	7.36e-03	0.02	83,83,91	0.0	0.0	0.0	0,0,0				
621	0.0	6.85e-03	4.24e-03	7.59e-03	85,85,92	0.0	0.0	0.0	0,0,0	1.50e-03	1.32e-03	1.27e-03	82,87,92
	40.1	7.70e-03	4.69e-03	8.54e-03	85,85,92	0.0	0.0	0.0	0,0,0				
622	0.0	0.0	0.03	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.80e-03	-1.47e-03	-6.85e-04	81,87,92
	40.0	0.0	0.03	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
623	0.0	0.0	7.70e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-8.76e-04	-1.02e-03	-8.54e-04	85,90,92
	40.1	0.0	7.82e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
624	0.0	4.25e-03	0.01	9.63e-04	83,81,91	0.0	0.0	0.0	0,0,0	-2.10e-03	-1.77e-03	-1.64e-03	81,87,92
	41.5	4.81e-03	0.01	1.89e-03	83,81,91	0.0	0.0	0.0	0,0,0				
625	0.0	0.01	6.22e-03	0.01	85,85,92	0.0	0.0	0.0	0,0,0	-1.89e-03	-1.74e-03	-1.69e-03	81,87,92
	40.1	0.01	7.01e-03	0.01	85,85,92	0.0	0.0	0.0	0,0,0				
626	0.0	0.0	0.04	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-2.26e-03	-1.04e-03	-7.28e-04	83,88,91
	40.1	0.03	0.10	0.04	85,83,92	0.0	0.0	0.0	0,0,0				
627	0.0	2.09e-03	0.03	0.0	83,81,0	0.0	0.0	0.0	0,0,0	-1.91e-03	-1.57e-03	-1.43e-03	81,87,92
	41.5	2.25e-03	0.03	0.0	83,81,0	0.0	0.0	0.0	0,0,0				
628	0.0	7.62e-03	0.04	3.80e-03	83,81,91	0.0	0.0	0.0	0,0,0	-2.76e-03	-2.36e-03	-2.20e-03	81,87,92
	40.0	6.64e-03	0.04	2.25e-03	83,81,91	0.0	0.0	0.0	0,0,0				
629	0.0	0.0	0.09	0.0	0,83,0	0.0	0.0	0.0	0,0,0	4.73e-03	3.71e-03	3.55e-03	85,90,92
	40.1	0.0	0.09	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
630	0.0	0.0	0.07	0.0	0,85,0	0.0	0.0	0.0	0,0,0	5.67e-03	3.85e-03	3.39e-03	83,88,91
	40.0	0.0	0.07	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
631	0.0	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0	7.96e-04	6.76e-04	6.43e-04	82,87,92
	40.1	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
632	0.0	0.09	0.05	0.10	85,85,92	0.0	0.0	0.0	0,0,0	-0.01	-9.99e-03	-9.54e-03	85,90,92
	40.1	0.09	0.05	0.10	85,85,92	0.0	0.0	0.0	0,0,0				
633	0.0	0.06	0.04	0.07	85,85,92	0.0	0.0	0.0	0,0,0	2.90e-03	2.17e-03	2.00e-03	85,90,92
	40.1	0.07	0.04	0.07	85,85,92	0.0	0.0	0.0	0,0,0				
634	0.0	0.09	0.05	0.10	85,85,92	0.0	0.0	0.0	0,0,0	-2.50e-03	-1.98e-03	-1.85e-03	83,88,91
	40.1	0.06	0.04	0.07	85,85,92	0.0	0.0	0.0	0,0,0				
635	0.0	7.35e-03	4.42e-03	9.01e-03	83,83,91	0.0	0.0	0.0	0,0,0	2.97e-03	1.83e-03	1.55e-03	83,88,91
	40.0	7.37e-03	4.44e-03	9.12e-03	83,83,91	0.0	0.0	0.0	0,0,0				
636	0.0	6.21e-03	3.83e-03	6.84e-03	85,85,92	0.0	0.0	0.0	0,0,0	1.55e-03	1.36e-03	1.31e-03	82,87,92
	40.1	7.04e-03	4.28e-03	7.78e-03	85,85,92	0.0	0.0	0.0	0,0,0				
637	0.0	0.0	0.03	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.84e-03	-1.50e-03	-1.36e-03	81,87,92
	40.0	0.0	0.03	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
638	0.0	0.0	0.01	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.75e-03	-5.31e-04	-4.45e-04	85,90,92
	40.1	0.0	0.01	0.0	0,83,0	0.0	0.0	0					

	40.1	0.01	0.05	0.02	85,83,92	0.0	0.0	0.0	0,0,0				
642	0.0	1.57e-03	0.03	0.0	83,81,0	0.0	0.0	0.0	0,0,0	-1.83e-03	-1.50e-03	-1.36e-03	81,87,92
	41.5	2.21e-03	0.03	0.0	83,81,0	0.0	0.0	0.0	0,0,0				
643	0.0	7.06e-03	0.04	3.84e-03	85,81,91	0.0	0.0	0.0	0,0,0	-2.35e-03	-1.99e-03	-1.85e-03	81,87,92
	40.0	7.62e-03	0.04	5.24e-03	85,81,91	0.0	0.0	0.0	0,0,0				
644	0.0	0.0	0.11	0.0	0,83,0	0.0	0.0	0.0	0,0,0	4.87e-03	3.83e-03	3.62e-03	85,90,92
	40.1	0.0	0.11	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
645	0.0	0.0	0.08	0.0	0,85,0	0.0	0.0	0.0	0,0,0	5.74e-03	3.89e-03	3.43e-03	83,88,91
	40.0	0.0	0.08	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
646	0.0	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0	7.64e-04	6.50e-04	6.18e-04	82,87,92
	40.1	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
647	0.0	0.08	0.05	0.09	85,85,92	0.0	0.0	0.0	0,0,0	-0.02	-0.01	-0.01	85,90,92
	40.1	0.10	0.05	0.10	85,85,92	0.0	0.0	0.0	0,0,0				
648	0.0	0.07	0.04	0.07	85,85,92	0.0	0.0	0.0	0,0,0	2.31e-03	1.52e-03	1.33e-03	85,90,92
	40.1	0.06	0.04	0.07	85,85,92	0.0	0.0	0.0	0,0,0				
649	0.0	0.10	0.06	0.11	85,85,92	0.0	0.0	0.0	0,0,0	-4.69e-03	-3.88e-03	-3.68e-03	83,88,91
	40.1	0.07	0.04	0.08	85,85,92	0.0	0.0	0.0	0,0,0				
650	0.0	0.01	6.08e-03	0.01	83,83,91	0.0	0.0	0.0	0,0,0	2.81e-03	1.69e-03	1.41e-03	83,88,91
	40.0	0.01	6.07e-03	0.01	83,83,91	0.0	0.0	0.0	0,0,0				
651	0.0	0.0	0.02	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.89e-03	-1.54e-03	-7.19e-04	81,87,92
	40.0	0.0	0.03	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
652	0.0	0.0	0.01	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.82e-03	-1.07e-03	-8.95e-04	85,90,92
	40.1	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
653	0.0	6.84e-03	0.02	0.0	83,81,0	0.0	0.0	0.0	0,0,0	-1.02e-03	-1.68e-03	-1.56e-03	81,87,92
	41.5	3.93e-03	0.02	0.0	83,81,0	0.0	0.0	0.0	0,0,0				
654	0.0	5.35e-03	3.23e-03	5.91e-03	82,82,92	0.0	0.0	0.0	0,0,0	-1.71e-03	-1.57e-03	-1.52e-03	81,87,92
	40.1	9.68e-03	5.54e-03	0.01	85,85,92	0.0	0.0	0.0	0,0,0				
655	0.0	0.02	0.03	0.02	81,83,92	0.0	0.0	0.0	0,0,0	-2.39e-03	-1.16e-03	-8.75e-04	85,90,92
	40.1	3.22e-03	7.42e-03	1.99e-03	81,83,91	0.0	0.0	0.0	0,0,0				
656	0.0	1.83e-03	0.03	0.0	83,81,0	0.0	0.0	0.0	0,0,0	-1.76e-03	-7.34e-04	-6.67e-04	81,87,92
	41.5	1.28e-03	0.03	0.0	83,81,0	0.0	0.0	0.0	0,0,0				
657	0.0	5.11e-03	0.02	3.91e-03	85,81,91	0.0	0.0	0.0	0,0,0	-2.03e-03	-1.70e-03	-1.57e-03	81,87,92
	40.0	6.04e-03	0.03	5.53e-03	85,81,91	0.0	0.0	0.0	0,0,0				
658	0.0	0.0	0.12	0.0	0,83,0	0.0	0.0	0.0	0,0,0	5.00e-03	3.94e-03	3.73e-03	85,90,92
	40.1	0.0	0.13	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
659	0.0	0.0	0.09	0.0	0,85,0	0.0	0.0	0.0	0,0,0	5.85e-03	3.98e-03	3.51e-03	83,88,91
	40.0	0.0	0.08	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
660	0.0	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0	7.52e-04	6.41e-04	6.09e-04	82,87,92
	40.1	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
661	0.0	0.08	0.05	0.08	85,85,92	0.0	0.0	0.0	0,0,0	2.37e-03	1.43e-03	1.20e-03	85,90,92
	40.1	0.06	0.04	0.06	85,85,92	0.0	0.0	0.0	0,0,0				
662	0.0	0.06	0.04	0.07	85,85,92	0.0	0.0	0.0	0,0,0	2.52e-03	1.79e-03	1.62e-03	85,90,92
	40.1	0.07	0.04	0.07	85,85,92	0.0	0.0	0.0	0,0,0				
663	0.0	0.0	0.03	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-2.00e-03	-1.64e-03	-1.49e-03	81,87,92
	40.0	0.0	0.03	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
664	0.0	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.94e-03	-1.14e-03	-9.56e-04	85,90,92
	40.1	2.86e-03	0.02	0.0	85,83,0	0.0	0.0	0.0	0,0,0				
665	0.0	5.20e-03	0.03	0.0	83,81,0	0.0	0.0	0.0	0,0,0	-2.07e-03	-1.77e-03	-1.65e-03	81,87,92
	41.5	0.01	0.03	0.0	83,81,0	0.0	0.0	0.0	0,0,0				
666	0.0	6.64e-03	3.95e-03	7.20e-03	82,82,92	0.0	0.0	0.0	0,0,0	-1.67e-03	-1.53e-03	-1.47e-03	81,87,92
	40.1	6.20e-03	3.70e-03	6.81e-03	85,85,92	0.0	0.0	0.0	0,0,0				
667	0.0	0.04	0.03	0.04	81,83,92	0.0	0.0	0.0	0,0,0	-3.18e-03	-1.90e-03	-1.63e-03	85,90,92
	40.1	0.03	0.01	0.03	81,81,92	0.0	0.0	0.0	0,0,0				
668	0.0	5.08e-03	0.03	0.0	83,81,0	0.0	0.0	0.0	0,0,0	-1.72e-03	-1.40e-03	-1.28e-03	81,87,92
	41.5	1.35e-03	0.03	0.0	83,81,0	0.0	0.0	0.0	0,0,0				
669	0.0	4.02e-03	0.01	2.97e-03	83,81,92	0.0	0.0	0.0	0,0,0	-1.84e-03	-1.54e-03	-1.42e-03	81,87,92
	40.0	4.19e-03	0.01	3.87e-03	83,81,92	0.0	0.0	0.0	0,0,0				
670	0.0	0.0	0.14	0.0	0,83,0	0.0	0.0	0.0	0,0,0	5.20e-03	4.09e-03	3.87e-03	85,90,92
	40.1	0.0	0.14	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
671	0.0	0.03	0.02	0.03	85,85,92	0.0	0.0	0.0	0,0,0	7.90e-04	6.75e-04	6.38e-04	82,87,92
	40.1	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
672	0.0	0.07	0.04	0.07	85,85,92	0.0	0.0	0.0	0,0,0	-4.82e-04	-2.64e-04	-2.42e-04	83,88,91
	40.1	0.08	0.05	0.08	85,85,92	0.0	0.0	0.0	0,0,0				
673	0.0	0.0	0.04	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-2.21e-03	-1.83e-03	-1.67e-03	81,87,92
	40.0	0.0	0.04	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
674	0.0	2.56e-03	0.02	0.0	85,83,0	0.0	0.0	0.0	0,0,0	-2.15e-03	-1.28e-03	-1.07e-03	85,90,92
	40.1	7.24e-03	0.03	0.0	85,83,0	0.0	0.0	0.0	0,0,0				
675	0.0	1.08e-03	0.03	0.0	83,81,0	0.0	0.0	0.0	0,0,0	-2.08e-03	-1.78e-03	-1.66e-03	81,87,92
	41.5	4.42e-03	0.03	0.0	83,81,0	0.0	0.0	0.0	0,0,0				
676	0.0	7.28e-03	4.26e-03	8.10e-03	82,82,92	0.0	0.0	0.0	0,0,0	-1.82e-03	-1.65e-03	-1.59e-03	81,87,92
	40.1	5.38e-03	3.24e-03	5.51e-03	81,81,92	0.0	0.0	0.0	0,0,0				
677	0.0	0.03	0.02	0.03	81,83,92	0.0	0.0	0.0	0,0,0	-4.27e-03	-2.92e-03	-2.66e-03	85,90,92
	40.1	0.02	0.01	0.02	81,81,92	0.0	0.0	0.0	0,0,0				
678	0.0	1.83e-03	0.03	0.0	83,81,0	0.0	0.0	0.0	0,0,0	-1.77e-03	-1.46e-03	-1.34e-03	81,87,92
	41.5	6.02e-03	0.03	0.0	83,81,0	0.0	0.0	0.0	0,0,0				
679	0.0	4.48e-03	2.78e-03	2.02e-03	83,83,91	0.0	0.0	0.0	0,0,0	-9.08e-04	-7.60e-04	-7.00e-04	81,87,92
	40.0	4.75e-03	2.92e-03	2.02e-03	83,83,91	0.0	0.0	0.0	0,0,0				
680	0.0	0.0	0.16	0.0	0,83,0	0.0	0.0	0.0	0,0,0	5.46e-03	4.30e-03	4.06e-03	85,90,92
	40.1	0.0	0.16	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
681	0.0	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0	7.27e-04	6.13e-04	5.73e-04	82,87,92
	40.1	0.02	0.01	0.03	85,85,92	0.0	0.0	0.0	0,0,0				
682	0.0	0.06	0.04	0.07	85,85,92	0.0	0.0	0.0	0,0,0	-1.65e-03	-1.05e-03	-8.95e-04	83,88,91
	40.1	0.08	0.05	0.07	85,85,92	0.0	0.0	0.0	0,0,0				
683	0.0	0.07	0.04	0.06	85,85,92	0.0	0.0	0.0	0,0,0	1.67e-03	1.00e-03	8.43e-04	85,90,92
	40.1	0.05	0.03	0.05	85,85,92	0.0	0.0	0.0	0,0,0				
684	0.0	0.0	0.04	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-2.48e-03	-2.06e-03	-1.89e-03	81,87,92
	40.0	0.0	0.04	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
685	0.0	7.19e-03	0.03	0.0	85,79,0	0.0	0.0	0.0	0,0,0	-2.54e-03	-1.53e-03	-1.28e-03	85,90,92
	40.1	0.01	0.04	0.0	85,83,0	0.0	0.0	0.0	0,0,0				
686	0.0	1.46e-03	0.03	0.0	83,81,0	0.0	0.0	0.0	0,0,0	-2.00e-03	-1.71e-03	-1.59e-03	81,87,92
	41.5	1.70e-03	0.03	0.0	83,81,0	0.0	0.0	0.0	0,0,0				
687	0.0	6.38e-03	3.74e-03	7.18e-03	82,82,92	0.0	0.0	0.0	0,0,0	-2.06e-03	-1.87e-03	-1.79e-03	81,87,92
	40.1	6.60e-03	3.85e-03	7.22e-03	81,81,92	0.0	0.0	0.0	0,0,0				
688	0.0	0.03	0.02	0.04	81,83,92	0.0	0.0	0.0	0,0,0	-5.42e-03	-4.00e-03	-3.75e-03	85,90,92
	40.1	0.03	0.02	0.04	81,81,92	0.0	0.0	0.0	0,0,0				
689	0.0	0.0	0.03	0.0	0,81,0	0.0	0.0						

692	0.0	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0	5.89e-04	4.86e-04	4.51e-04	82,87,92
	40.1	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
693	0.0	0.0	0.04	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-2.72e-03	-2.27e-03	-2.09e-03	81,87,92
	40.0	0.0	0.03	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
694	0.0	0.01	0.03	0.0	85,79,0	0.0	0.0	0.0	0,0,0	-3.19e-03	-1.94e-03	-1.63e-03	85,90,92
	40.1	0.01	0.03	0.0	85,79,0	0.0	0.0	0.0	0,0,0				
695	0.0	0.0	0.03	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.92e-03	-1.64e-03	-1.52e-03	81,87,92
	41.5	5.03e-04	0.04	0.0	83,81,0	0.0	0.0	0.0	0,0,0				
696	0.0	4.16e-03	2.49e-03	4.66e-03	82,82,92	0.0	0.0	0.0	0,0,0	-2.29e-03	-2.08e-03	-1.99e-03	81,87,92
	40.1	6.17e-03	3.56e-03	6.97e-03	81,81,92	0.0	0.0	0.0	0,0,0				
697	0.0	0.03	0.02	0.03	81,81,92	0.0	0.0	0.0	0,0,0	-6.70e-03	-5.21e-03	-4.96e-03	85,87,92
	40.1	0.04	0.02	0.04	81,85,92	0.0	0.0	0.0	0,0,0				
698	0.0	0.0	0.03	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.70e-03	-1.41e-03	-1.29e-03	81,87,92
	41.5	0.0	0.03	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
699	0.0	6.98e-03	4.29e-03	4.99e-03	83,83,91	0.0	0.0	0.0	0,0,0	-1.82e-03	-1.55e-03	-1.44e-03	81,87,92
	40.0	8.07e-03	4.87e-03	6.06e-03	83,83,91	0.0	0.0	0.0	0,0,0				
700	0.0	0.0	0.19	0.0	0,83,0	0.0	0.0	0.0	0,0,0	6.19e-03	4.87e-03	4.59e-03	85,90,92
	40.1	0.0	0.19	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
701	0.0	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0	5.06e-04	4.13e-04	3.81e-04	82,87,92
	40.1	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
702	0.0	0.0	0.03	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-2.87e-03	-2.39e-03	-2.20e-03	81,87,92
	40.0	0.0	0.02	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
703	0.0	0.01	0.03	0.0	85,79,0	0.0	0.0	0.0	0,0,0	-4.12e-03	-2.52e-03	-2.13e-03	85,90,92
	40.1	0.01	0.03	0.0	85,83,0	0.0	0.0	0.0	0,0,0				
704	0.0	0.0	0.04	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.86e-03	-1.58e-03	-1.47e-03	81,87,92
	41.5	0.0	0.04	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
705	0.0	2.96e-03	1.78e-03	3.12e-03	81,81,92	0.0	0.0	0.0	0,0,0	-2.39e-03	-2.18e-03	-2.09e-03	81,87,92
	40.1	3.86e-03	2.26e-03	4.44e-03	81,82,92	0.0	0.0	0.0	0,0,0				
706	0.0	0.02	0.01	0.03	81,81,92	0.0	0.0	0.0	0,0,0	-7.94e-03	-6.44e-03	-6.14e-03	85,87,92
	40.1	0.04	0.03	0.04	81,85,92	0.0	0.0	0.0	0,0,0				
707	0.0	0.0	0.04	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.64e-03	-1.35e-03	-1.24e-03	81,87,92
	41.5	0.0	0.04	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
708	0.0	0.0	0.21	0.0	0,83,0	0.0	0.0	0.0	0,0,0	6.78e-03	5.29e-03	4.97e-03	85,90,92
	40.1	0.0	0.20	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
709	0.0	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0	4.52e-04	3.67e-04	3.37e-04	82,87,92
	40.1	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
710	0.0	0.02	0.03	0.0	85,83,0	0.0	0.0	0.0	0,0,0	-3.78e-03	-2.44e-03	-2.12e-03	85,90,92
	40.1	0.04	0.08	0.02	85,83,92	0.0	0.0	0.0	0,0,0				
711	0.0	0.0	0.04	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.80e-03	-1.53e-03	-1.42e-03	81,87,92
	41.5	0.0	0.04	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
712	0.0	2.92e-03	1.67e-03	3.17e-03	81,81,92	0.0	0.0	0.0	0,0,0	-2.35e-03	-2.14e-03	-2.06e-03	81,87,92
	40.1	2.28e-03	1.34e-03	2.34e-03	82,82,92	0.0	0.0	0.0	0,0,0				
713	0.0	0.01	7.58e-03	0.02	81,81,92	0.0	0.0	0.0	0,0,0	-8.96e-03	-7.49e-03	-7.16e-03	85,87,92
	40.1	0.03	0.03	0.04	81,85,92	0.0	0.0	0.0	0,0,0				
714	0.0	0.0	0.04	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.59e-03	-1.31e-03	-1.19e-03	81,87,92
	41.5	0.0	0.04	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
715	0.0	0.0	0.20	0.0	0,83,0	0.0	0.0	0.0	0,0,0	7.99e-03	6.12e-03	5.71e-03	85,90,92
	40.1	0.0	0.21	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
716	0.0	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0	3.98e-04	3.21e-04	2.91e-04	82,87,92
	40.1	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
717	0.0	0.04	0.04	0.02	85,83,92	0.0	0.0	0.0	0,0,0	-2.01e-03	-1.52e-03	-1.40e-03	85,90,92
	40.1	0.01	8.11e-03	3.75e-03	85,85,92	0.0	0.0	0.0	0,0,0				
718	0.0	0.0	0.04	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.74e-03	-1.48e-03	-1.37e-03	81,87,92
	41.5	0.0	0.04	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
719	0.0	1.28e-03	7.39e-04	1.36e-03	81,81,92	0.0	0.0	0.0	0,0,0	-2.23e-03	-2.04e-03	-1.96e-03	81,87,92
	40.1	3.48e-03	2.40e-03	3.93e-03	81,81,92	0.0	0.0	0.0	0,0,0				
720	0.0	3.69e-03	2.16e-03	4.92e-03	79,79,91	0.0	0.0	0.0	0,0,0	-9.56e-03	-8.16e-03	-7.82e-03	85,87,92
	40.1	0.02	0.02	0.03	81,85,92	0.0	0.0	0.0	0,0,0				
721	0.0	0.0	0.04	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.54e-03	-1.26e-03	-1.15e-03	81,87,92
	41.5	0.0	0.04	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
722	0.0	0.0	0.18	0.0	0,83,0	0.0	0.0	0.0	0,0,0	8.98e-03	6.77e-03	6.27e-03	85,90,92
	40.1	0.0	0.19	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
723	0.0	0.02	0.01	0.03	85,85,92	0.0	0.0	0.0	0,0,0	3.18e-04	2.48e-04	2.20e-04	81,87,92
	40.1	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
724	0.0	0.02	9.37e-03	5.48e-03	85,85,92	0.0	0.0	0.0	0,0,0	-1.66e-03	-1.44e-03	-1.39e-03	85,90,92
	40.1	0.01	7.13e-03	7.38e-03	85,85,92	0.0	0.0	0.0	0,0,0				
725	0.0	0.0	0.04	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.68e-03	-1.42e-03	-1.32e-03	81,87,92
	41.5	0.0	0.04	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
726	0.0	1.61e-03	1.98e-03	1.37e-03	85,83,92	0.0	0.0	0.0	0,0,0	-2.18e-03	-1.99e-03	-1.92e-03	81,87,92
	40.1	2.76e-03	4.31e-03	3.15e-03	81,81,92	0.0	0.0	0.0	0,0,0				
727	0.0	0.01	0.02	9.51e-03	85,85,92	0.0	0.0	0.0	0,0,0	-9.64e-03	-8.34e-03	-8.01e-03	82,87,92
	40.1	5.99e-03	9.67e-03	7.98e-03	79,83,91	0.0	0.0	0.0	0,0,0				
728	0.0	0.0	0.04	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.49e-03	-1.22e-03	-1.12e-03	81,87,92
	41.5	0.0	0.04	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
729	0.0	0.0	0.22	0.0	0,83,0	0.0	0.0	0.0	0,0,0	8.72e-03	6.78e-03	6.36e-03	85,90,92
	40.1	0.0	0.18	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
730	0.0	0.02	0.01	0.03	85,85,92	0.0	0.0	0.0	0,0,0	1.90e-04	-1.45e-04	-1.32e-04	81,87,91
	40.1	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
731	0.0	0.01	7.77e-03	7.13e-03	85,85,92	0.0	0.0	0.0	0,0,0	-2.34e-03	-1.84e-03	-1.72e-03	85,90,92
	40.1	0.01	7.85e-03	6.92e-03	85,85,92	0.0	0.0	0.0	0,0,0				
732	0.0	0.0	0.04	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-8.36e-04	-7.04e-04	-6.51e-04	81,87,92
	41.5	0.0	0.04	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
733	0.0	0.0	0.03	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.44e-03	-6.03e-04	-5.50e-04	81,87,92
	41.5	0.0	0.03	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
734	0.0	0.0	0.11	0.0	0,83,0	0.0	0.0	0.0	0,0,0	9.18e-03	7.57e-03	7.23e-03	85,90,92
	40.1	0.0	0.10	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
735	0.0	0.03	0.02	0.03	85,85,92	0.0	0.0	0.0	0,0,0	-1.47e-04	-1.44e-04	-1.43e-04	83,88,91
	40.1	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
736	0.0	0.01	8.16e-03	7.12e-03	85,85,92	0.0	0.0	0.0	0,0,0	-2.64e-03	-1.02e-03	-1.84e-03	85,90,92
	40.1	0.01	7.11e-03	6.87e-03	85,85,92	0.0	0.0	0.0	0,0,0				
737	0.0	0.0	0.04	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.62e-03	-1.37e-03	-1.27e-03	81,87,92
	41.5	0.0	0.04	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
738	0.0	0.0	0.03	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.39e-03	-1.13e-03	-1.03e-03	81,87,92
	41.5	0.0	0.03	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
739	0.0	0.02	0.02	0.01	83,83,91	0.0	0.0	0.0	0,0,0	0.01	9.63e-03	9.17e-03	85,90,92
	40.1	0.04	0.05	0.04	85,83,92	0.0	0.0	0.0	0,0,0				

	40.1	0.02	9.33e-03	0.01	85,85,92	0.0	0.0	0.0	0,0,0				
743	0.0	0.0	0.04	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.66e-03	-1.42e-03	-1.33e-03	81,87,92
	41.5	0.0	0.04	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
744	0.0	2.62e-03	0.04	0.0	83,82,0	0.0	0.0	0.0	0,0,0	-1.40e-03	-1.15e-03	-1.04e-03	81,87,92
	41.5	0.0	0.03	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
745	0.0	0.01	7.41e-03	0.01	85,85,92	0.0	0.0	0.0	0,0,0	0.01	9.82e-03	9.33e-03	85,90,92
	40.1	0.02	9.94e-03	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
746	0.0	0.01	8.28e-03	0.02	82,82,92	0.0	0.0	0.0	0,0,0	-5.53e-04	-5.14e-04	-5.04e-04	83,88,91
	40.1	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
747	0.0	0.0	0.15	0.0	0,83,0	0.0	0.0	0.0	0,0,0	7.77e-03	6.61e-03	6.38e-03	85,90,92
	40.1	0.0	0.15	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
748	0.0	2.49e-03	0.10	0.0	81,83,0	0.0	0.0	0.0	0,0,0	9.52e-03	7.84e-03	7.47e-03	85,90,92
	40.1	0.0	0.08	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
749	0.0	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0	-2.38e-03	-1.72e-03	-1.56e-03	85,90,92
	40.1	0.02	0.01	0.01	85,85,92	0.0	0.0	0.0	0,0,0				
750	0.0	0.0	0.04	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.67e-03	-1.43e-03	-1.34e-03	81,87,92
	41.5	0.0	0.04	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
751	0.0	0.0	0.03	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-1.46e-03	-1.22e-03	-1.12e-03	81,87,92
	41.5	3.26e-03	0.04	0.0	83,82,0	0.0	0.0	0.0	0,0,0				
752	0.0	0.02	0.01	0.02	82,82,92	0.0	0.0	0.0	0,0,0	0.01	9.75e-03	9.25e-03	85,90,92
	40.1	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
753	0.0	0.01	7.29e-03	0.01	85,82,92	0.0	0.0	0.0	0,0,0	-4.76e-04	-4.61e-04	-4.58e-04	83,88,91
	40.1	0.02	9.12e-03	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
754	0.0	0.0	0.14	0.0	0,83,0	0.0	0.0	0.0	0,0,0	8.44e-03	7.06e-03	6.77e-03	85,90,92
	40.1	0.0	0.14	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
755	0.0	0.02	0.10	0.02	85,83,92	0.0	0.0	0.0	0,0,0	0.01	8.40e-03	8.00e-03	85,90,92
	40.1	8.34e-03	0.07	6.78e-04	81,83,92	0.0	0.0	0.0	0,0,0				
756	0.0	0.0	0.15	0.0	0,83,0	0.0	0.0	0.0	0,0,0	6.91e-03	6.06e-03	5.90e-03	85,90,92
	40.1	0.0	0.15	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
757	0.0	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0	-2.05e-03	-1.45e-03	-1.31e-03	85,90,92
	40.1	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
758	0.0	0.0	0.04	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.62e-03	-7.13e-04	-6.65e-04	81,87,92
	41.5	0.0	0.04	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
759	0.0	0.0	0.03	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.47e-03	-1.24e-03	-1.14e-03	81,87,92
	41.5	0.0	0.03	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
760	0.0	0.01	6.65e-03	0.01	85,82,92	0.0	0.0	0.0	0,0,0	-4.48e-04	-4.38e-04	-4.36e-04	83,88,91
	40.1	0.01	7.86e-03	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
761	0.0	0.0	0.12	0.0	0,83,0	0.0	0.0	0.0	0,0,0	8.87e-03	7.35e-03	7.03e-03	85,90,92
	40.1	0.0	0.12	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
762	0.0	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0	-1.68e-03	-1.14e-03	-1.02e-03	85,90,92
	40.1	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
763	0.0	0.0	0.04	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.57e-03	-1.34e-03	-1.25e-03	81,87,92
	41.5	0.0	0.04	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
764	0.0	0.0	0.03	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-7.36e-04	-6.15e-04	-5.66e-04	81,87,92
	41.5	0.0	0.03	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
765	0.0	0.01	6.33e-03	0.01	82,82,92	0.0	0.0	0.0	0,0,0	-4.23e-04	-4.14e-04	-4.12e-04	83,88,91
	40.1	0.01	7.27e-03	0.01	82,82,92	0.0	0.0	0.0	0,0,0				
766	0.0	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0	-1.29e-03	-8.24e-04	-7.13e-04	85,90,92
	40.1	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
767	0.0	0.0	0.04	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.52e-03	-1.30e-03	-6.20e-04	81,87,92
	41.5	0.0	0.04	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
768	0.0	0.0	0.03	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-1.39e-03	-5.94e-04	-5.46e-04	81,87,92
	41.5	0.0	0.03	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
769	0.0	0.01	6.25e-03	0.01	82,82,92	0.0	0.0	0.0	0,0,0	-4.06e-04	-3.97e-04	-3.94e-04	83,88,91
	40.1	0.01	6.90e-03	0.01	82,82,92	0.0	0.0	0.0	0,0,0				
770	0.0	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0	-8.93e-04	-5.03e-04	-4.11e-04	85,90,92
	40.1	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
771	0.0	0.0	0.04	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.48e-03	-1.26e-03	-6.00e-04	81,87,92
	41.5	0.0	0.04	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
772	0.0	0.0	0.03	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-6.93e-04	-5.76e-04	-5.29e-04	81,87,92
	41.5	0.0	0.03	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
773	0.0	0.01	6.30e-03	0.01	82,82,92	0.0	0.0	0.0	0,0,0	-4.07e-04	-3.96e-04	-3.93e-04	83,88,91
	40.1	0.01	6.56e-03	0.01	82,82,92	0.0	0.0	0.0	0,0,0				
774	0.0	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0	-5.14e-04	-1.97e-04	-1.24e-04	85,90,92
	40.1	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
775	0.0	0.0	0.04	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.43e-03	-1.22e-03	-1.13e-03	81,87,92
	41.5	0.0	0.04	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
776	0.0	0.0	0.03	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-6.75e-04	-5.61e-04	-5.15e-04	81,87,92
	41.5	0.0	0.03	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
777	0.0	0.01	6.42e-03	0.01	82,82,92	0.0	0.0	0.0	0,0,0	-4.34e-04	-4.20e-04	-4.17e-04	83,88,91
	40.1	0.01	6.19e-03	0.01	82,82,92	0.0	0.0	0.0	0,0,0				
778	0.0	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0	-1.92e-04	1.37e-04	1.37e-04	85,86,91
	40.1	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
779	0.0	0.0	0.04	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.38e-03	-6.00e-04	-5.56e-04	81,87,92
	41.5	0.0	0.04	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
780	0.0	0.0	0.03	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-6.56e-04	-5.44e-04	-4.99e-04	81,87,92
	41.5	0.0	0.03	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
781	0.0	0.01	6.53e-03	0.01	82,82,92	0.0	0.0	0.0	0,0,0	-4.91e-04	-4.75e-04	-4.71e-04	83,88,91
	40.1	9.25e-03	5.73e-03	0.01	82,82,92	0.0	0.0	0.0	0,0,0				
782	0.0	0.02	0.01	0.01	85,85,92	0.0	0.0	0.0	0,0,0	2.92e-04	2.92e-04	2.92e-04	79,86,91
	40.1	0.02	9.43e-03	0.01	85,85,92	0.0	0.0	0.0	0,0,0				
783	0.0	0.0	0.04	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-1.34e-03	-1.13e-03	-1.04e-03	81,87,92
	41.5	0.0	0.04	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
784	0.0	0.0	0.03	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-6.34e-04	-5.23e-04	-4.79e-04	81,87,92
	41.5	0.0	0.03	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
785	0.0	0.01	6.49e-03	0.01	82,82,92	0.0	0.0	0.0	0,0,0	-5.83e-04	-5.65e-04	-5.61e-04	83,88,91
	40.1	9.23e-03	5.70e-03	0.01	82,82,92	0.0	0.0	0.0	0,0,0				
786	0.0	0.02	9.22e-03	8.35e-03	85,85,92	0.0	0.0	0.0	0,0,0	2.79e-04	2.79e-04	2.79e-04	79,86,91
	40.1	0.02	9.37e-03	8.91e-03	85,85,92	0.0	0.0	0.0	0,0,0				
787	0.0	0.0	0.05	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-1.35e-03	-1.14e-03	-1.05e-03	81,87,92
	41.5	0.0	0.04	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
788	0.0	0.0	0.03	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-1.20e-03	-9.82e-04	-8.97e-04	81,87,92
	41.5	0.0	0.03	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
789	0.0	0.01	6.16e-03	0.01	82,82,92	0.0	0.0	0.0	0,0,0	-7.11e-04	-6.90e-04	-6.86e-04	85,90,92
	40.1	9.73e-03	5.93e-03	0.01	82,82,92	0.0	0.0	0.0	0,0,0				
790	0.0	0.01	8.94e-03	8.46e-03	85,85,92	0.0	0.0	0.0	0,0,0	-6.46e-04	-1.05e-04	3.76e-05	85,90,91
	40.1	0.02	0.01	8.37e-03	85,85,92	0.0	0.0	0.0	0,0,0	</			

793	0.0	8.98e-03	5.49e-03	0.01	82,82,92	0.0	0.0	0.0	0,0,0	-8.63e-04	-8.36e-04	-8.30e-04	85,87,92
	40.1	9.96e-03	6.01e-03	0.01	82,82,92	0.0	0.0	0.0	0,0,0				
794	0.0	0.02	0.01	4.94e-03	85,85,92	0.0	0.0	0.0	0,0,0	-2.90e-04	-7.20e-05	-5.15e-05	85,90,92
	40.1	0.04	0.02	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
795	0.0	0.0	0.04	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.40e-03	-1.21e-03	-1.13e-03	81,87,92
	41.5	0.0	0.04	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
796	0.0	0.0	0.03	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-1.28e-03	-1.08e-03	-9.96e-04	81,87,92
	41.5	0.0	0.04	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
797	0.0	7.44e-03	4.62e-03	8.58e-03	81,81,92	0.0	0.0	0.0	0,0,0	-1.00e-03	-9.66e-04	-9.56e-04	82,87,92
	40.1	9.69e-03	5.82e-03	0.01	81,81,92	0.0	0.0	0.0	0,0,0				
798	0.0	0.04	0.06	0.02	85,83,92	0.0	0.0	0.0	0,0,0	1.46e-03	8.47e-04	6.93e-04	83,88,91
	40.1	9.54e-03	0.02	0.0	85,79,0	0.0	0.0	0.0	0,0,0				
799	0.0	0.0	0.05	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-1.36e-03	-5.97e-04	-5.57e-04	81,87,92
	41.5	0.0	0.05	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
800	0.0	0.0	0.03	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-1.30e-03	-1.10e-03	-1.02e-03	81,87,92
	41.5	0.0	0.03	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
801	0.0	7.94e-03	4.85e-03	9.18e-03	81,81,92	0.0	0.0	0.0	0,0,0	-1.09e-03	-1.04e-03	-1.03e-03	82,87,92
	40.1	8.81e-03	5.31e-03	0.01	81,81,92	0.0	0.0	0.0	0,0,0				
802	0.0	8.71e-03	0.02	0.0	85,79,0	0.0	0.0	0.0	0,0,0	1.51e-03	6.82e-04	4.76e-04	83,88,91
	40.1	0.02	0.04	0.01	85,79,92	0.0	0.0	0.0	0,0,0				
803	0.0	0.0	0.05	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-1.30e-03	-1.11e-03	-1.04e-03	81,87,92
	41.5	0.0	0.05	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
804	0.0	0.0	0.03	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-6.45e-04	-5.45e-04	-5.04e-04	81,87,92
	41.5	0.0	0.03	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
805	0.0	8.12e-03	4.91e-03	9.36e-03	81,81,92	0.0	0.0	0.0	0,0,0	-1.10e-03	-1.06e-03	-1.04e-03	82,87,92
	40.1	7.45e-03	4.55e-03	8.52e-03	81,81,92	0.0	0.0	0.0	0,0,0				
806	0.0	0.02	0.03	0.01	83,79,92	0.0	0.0	0.0	0,0,0	3.03e-04	-2.25e-04	-2.22e-04	83,87,92
	40.1	0.02	0.03	0.01	83,79,92	0.0	0.0	0.0	0,0,0				
807	0.0	0.0	0.05	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-1.26e-03	-1.07e-03	-9.92e-04	81,87,92
	41.5	0.0	0.05	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
808	0.0	0.0	0.03	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-6.23e-04	-5.24e-04	-4.84e-04	81,87,92
	41.5	0.0	0.04	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
809	0.0	8.35e-03	4.98e-03	9.66e-03	81,81,92	0.0	0.0	0.0	0,0,0	-1.06e-03	-1.01e-03	-1.00e-03	82,87,92
	40.1	6.38e-03	3.91e-03	7.15e-03	82,82,92	0.0	0.0	0.0	0,0,0				
810	0.0	0.02	0.02	0.01	83,79,92	0.0	0.0	0.0	0,0,0	-6.85e-04	-6.80e-04	-6.78e-04	81,87,92
	40.1	0.01	0.01	8.36e-03	85,79,92	0.0	0.0	0.0	0,0,0				
811	0.0	0.0	0.05	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-1.21e-03	-1.02e-03	-9.51e-04	81,87,92
	41.5	0.0	0.05	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
812	0.0	0.0	0.03	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-6.04e-04	-5.06e-04	-4.67e-04	81,87,92
	41.5	0.0	0.04	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
813	0.0	8.67e-03	5.09e-03	9.90e-03	82,82,92	0.0	0.0	0.0	0,0,0	-9.66e-04	-9.32e-04	-9.19e-04	81,87,92
	40.1	6.55e-03	3.96e-03	7.36e-03	82,82,92	0.0	0.0	0.0	0,0,0				
814	0.0	0.01	6.40e-03	5.29e-03	85,85,92	0.0	0.0	0.0	0,0,0	-8.75e-04	-8.71e-04	-8.70e-04	81,87,92
	40.1	8.60e-03	5.15e-03	3.73e-03	85,85,92	0.0	0.0	0.0	0,0,0				
815	0.0	0.0	0.05	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-1.16e-03	-9.78e-04	-9.05e-04	81,87,92
	41.5	0.0	0.05	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
816	0.0	0.0	0.03	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-5.85e-04	-4.90e-04	-4.52e-04	81,87,92
	41.5	0.0	0.03	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
817	0.0	8.90e-03	5.18e-03	0.01	82,82,92	0.0	0.0	0.0	0,0,0	-8.40e-04	-8.08e-04	-7.95e-04	81,87,92
	40.1	6.28e-03	3.80e-03	7.14e-03	81,81,92	0.0	0.0	0.0	0,0,0				
818	0.0	8.74e-03	5.44e-03	6.11e-03	85,85,92	0.0	0.0	0.0	0,0,0	-8.92e-04	-8.69e-04	-8.64e-04	85,90,92
	40.1	9.54e-03	5.87e-03	6.47e-03	85,85,92	0.0	0.0	0.0	0,0,0				
819	0.0	0.0	0.05	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-1.10e-03	-9.24e-04	-8.53e-04	81,87,92
	41.5	0.0	0.05	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
820	0.0	0.0	0.03	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-1.10e-03	-4.72e-04	-4.34e-04	81,87,92
	41.5	0.0	0.03	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
821	0.0	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0	-9.30e-04	-8.97e-04	-8.85e-04	81,87,92
	40.1	0.02	9.84e-03	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
822	0.0	0.01	8.38e-03	0.01	85,85,92	0.0	0.0	0.0	0,0,0	-7.55e-04	-7.36e-04	-7.32e-04	85,90,92
	40.1	0.01	8.28e-03	0.01	85,85,92	0.0	0.0	0.0	0,0,0				
823	0.0	0.0	0.04	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-1.06e-03	-8.75e-04	-8.04e-04	81,87,92
	41.5	0.0	0.04	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
824	0.0	0.0	0.03	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-5.42e-04	-4.50e-04	-4.13e-04	81,87,92
	41.5	0.0	0.03	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
825	0.0	5.30e-03	3.16e-03	5.87e-03	82,82,92	0.0	0.0	0.0	0,0,0	-1.06e-03	-1.01e-03	-9.95e-04	82,87,92
	40.1	9.13e-03	5.10e-03	0.01	85,85,92	0.0	0.0	0.0	0,0,0				
826	0.0	0.02	0.01	0.01	85,85,92	0.0	0.0	0.0	0,0,0	-5.27e-04	-5.27e-04	-5.27e-04	79,86,91
	40.1	0.02	0.01	0.01	85,85,92	0.0	0.0	0.0	0,0,0				
827	0.0	0.0	0.05	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-1.06e-03	-8.82e-04	-8.13e-04	81,87,92
	41.5	0.0	0.04	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
828	0.0	0.0	0.03	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-1.01e-03	-8.35e-04	-7.63e-04	81,87,92
	41.5	0.0	0.03	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
829	0.0	3.02e-03	3.96e-03	2.97e-03	81,83,92	0.0	0.0	0.0	0,0,0	-9.67e-04	-9.28e-04	-9.14e-04	82,87,92
	40.1	8.42e-03	0.01	9.32e-03	85,83,92	0.0	0.0	0.0	0,0,0				
830	0.0	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0	-2.79e-04	-2.79e-04	-2.79e-04	79,86,91
	40.1	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
831	0.0	0.0	0.04	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-1.10e-03	-9.30e-04	-8.64e-04	81,87,92
	41.5	0.0	0.05	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
832	0.0	0.0	0.04	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-1.03e-03	-8.56e-04	-7.86e-04	81,87,92
	41.5	0.0	0.03	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
833	0.0	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-8.99e-04	-8.65e-04	-8.51e-04	82,87,92
	40.1	6.47e-03	0.03	6.50e-03	81,83,92	0.0	0.0	0.0	0,0,0				
834	0.0	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0	1.12e-04	-5.37e-05	-5.37e-05	85,86,91
	40.1	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
835	0.0	0.0	0.04	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-5.56e-04	-4.73e-04	-4.40e-04	81,87,92
	41.5	0.0	0.04	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
836	0.0	0.0	0.03	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-1.09e-03	-9.23e-04	-8.56e-04	81,87,92
	41.5	0.0	0.04	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
837	0.0	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-8.08e-04	-7.77e-04	-3.92e-04	81,87,92
	40.1	0.0	0.04	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
838	0.0	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0	4.62e-04	3.17e-04	2.82e-04	85,90,92
	40.1	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
839	0.0	0.0	0.04	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-1.03e-03	-8.75e-04	-8.11e-04	81,87,92
	41.5	0.0	0.04	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
840	0.0	0.0	0.03	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-1.09e-03	-9.31e-04	-8.64e-04	81,87,92
	41.5	0.0	0.03	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
841	0.0	0.0	0.04	0.0	0,83,0	0.0	0.0	0.0					

	41.5	0.0	0.04	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
844	0.0	0.0	0.03	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-1.05e-03	-4.57e-04	-4.23e-04	81,87,92
	41.5	0.0	0.03	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
845	0.0	0.0	0.04	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-5.92e-04	-5.70e-04	-5.61e-04	81,87,92
	40.1	0.0	0.04	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
846	0.0	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0	1.12e-03	8.78e-04	8.19e-04	85,90,92
	40.1	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
847	0.0	0.0	0.04	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-9.31e-04	-7.78e-04	-7.17e-04	81,87,92
	41.5	0.0	0.04	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
848	0.0	0.0	0.03	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-1.01e-03	-4.35e-04	-4.03e-04	81,87,92
	41.5	0.0	0.03	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
849	0.0	0.0	0.04	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-4.93e-04	-4.76e-04	-4.70e-04	81,87,92
	40.1	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
850	0.0	0.02	0.01	0.01	85,85,92	0.0	0.0	0.0	0,0,0	1.31e-03	1.06e-03	1.00e-03	85,90,92
	40.1	0.02	0.01	0.01	85,85,92	0.0	0.0	0.0	0,0,0				
851	0.0	0.0	0.04	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-8.88e-04	-7.39e-04	-6.79e-04	81,87,92
	41.5	0.0	0.03	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
852	0.0	0.0	0.03	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-4.98e-04	-4.18e-04	-3.86e-04	81,87,92
	41.5	0.0	0.03	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
853	0.0	4.34e-03	0.03	3.91e-03	81,83,92	0.0	0.0	0.0	0,0,0	-4.18e-04	-4.06e-04	-4.02e-04	81,87,92
	40.1	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
854	0.0	0.01	9.25e-03	0.01	85,85,92	0.0	0.0	0.0	0,0,0	1.24e-03	1.08e-03	1.04e-03	85,90,92
	40.1	0.01	9.08e-03	0.01	85,85,92	0.0	0.0	0.0	0,0,0				
855	0.0	0.0	0.03	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-8.46e-04	-3.59e-04	-3.29e-04	81,87,92
	41.5	0.0	0.03	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
856	0.0	0.0	0.03	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-4.81e-04	-4.04e-04	-3.73e-04	81,87,92
	41.5	0.0	0.02	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
857	0.0	7.37e-03	0.02	8.59e-03	82,83,92	0.0	0.0	0.0	0,0,0	-3.95e-04	-3.85e-04	-3.81e-04	81,87,92
	40.1	3.43e-03	0.01	4.36e-03	82,83,92	0.0	0.0	0.0	0,0,0				
858	0.0	0.01	8.73e-03	8.65e-03	85,85,92	0.0	0.0	0.0	0,0,0	9.14e-04	9.06e-04	9.03e-04	81,87,92
	40.1	0.03	0.02	0.01	85,85,92	0.0	0.0	0.0	0,0,0				
859	0.0	0.0	0.03	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-4.10e-04	-3.36e-04	-3.07e-04	81,87,92
	41.5	0.0	0.03	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
860	0.0	0.0	0.02	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-4.64e-04	-3.89e-04	-3.58e-04	81,87,92
	41.5	0.0	0.02	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
861	0.0	0.01	0.01	0.01	85,83,92	0.0	0.0	0.0	0,0,0	-4.30e-04	-4.16e-04	-4.11e-04	81,87,92
	40.1	6.91e-03	6.80e-03	8.29e-03	85,83,92	0.0	0.0	0.0	0,0,0				
862	0.0	0.02	0.01	0.01	85,85,92	0.0	0.0	0.0	0,0,0	1.48e-03	1.19e-03	1.12e-03	85,90,92
	40.1	0.04	0.02	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
863	0.0	0.0	0.03	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-7.55e-04	-6.13e-04	-5.56e-04	81,87,92
	41.5	0.0	0.02	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
864	0.0	0.0	0.02	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-4.45e-04	-3.71e-04	-3.41e-04	81,87,92
	41.5	0.0	0.02	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
865	0.0	8.49e-03	5.05e-03	9.93e-03	82,82,92	0.0	0.0	0.0	0,0,0	-6.20e-04	-5.93e-04	-5.82e-04	81,87,92
	40.1	0.02	9.79e-03	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
866	0.0	0.05	0.07	0.03	85,83,92	0.0	0.0	0.0	0,0,0	3.34e-03	2.18e-03	1.89e-03	85,90,92
	40.1	0.02	0.02	7.84e-03	85,83,92	0.0	0.0	0.0	0,0,0				
867	0.0	4.04e-03	0.04	0.0	83,85,0	0.0	0.0	0.0	0,0,0	-8.09e-04	-6.68e-04	-6.12e-04	81,87,92
	41.5	0.0	0.03	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
868	0.0	2.10e-03	0.02	0.0	83,85,0	0.0	0.0	0.0	0,0,0	-8.28e-04	-6.85e-04	-6.28e-04	81,87,92
	41.5	0.0	0.01	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
869	0.0	0.01	6.45e-03	0.01	85,82,92	0.0	0.0	0.0	0,0,0	-9.35e-04	-8.88e-04	-8.69e-04	81,87,92
	40.1	0.02	0.01	0.02	82,82,92	0.0	0.0	0.0	0,0,0				
870	0.0	0.02	0.03	1.84e-03	85,83,92	0.0	0.0	0.0	0,0,0	3.83e-03	2.37e-03	2.00e-03	85,90,92
	40.1	0.01	0.03	5.19e-03	85,79,92	0.0	0.0	0.0	0,0,0				
871	0.0	0.0	0.02	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-9.02e-04	-7.64e-04	-7.09e-04	81,87,92
	41.5	4.08e-03	0.03	0.0	83,85,0	0.0	0.0	0.0	0,0,0				
872	0.0	7.82e-03	0.03	1.50e-03	83,85,91	0.0	0.0	0.0	0,0,0	-8.89e-04	-7.48e-04	-6.91e-04	81,87,92
	41.5	3.66e-03	0.02	0.0	83,85,0	0.0	0.0	0.0	0,0,0				
873	0.0	0.01	7.54e-03	0.01	85,85,92	0.0	0.0	0.0	0,0,0	-1.23e-03	-1.16e-03	-1.13e-03	81,87,92
	40.1	0.02	0.01	0.02	82,82,92	0.0	0.0	0.0	0,0,0				
874	0.0	0.01	0.03	3.71e-03	85,79,92	0.0	0.0	0.0	0,0,0	2.82e-03	1.74e-03	1.47e-03	85,90,92
	40.1	0.02	0.03	3.31e-03	85,79,92	0.0	0.0	0.0	0,0,0				
875	0.0	0.0	0.01	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-9.28e-04	-7.93e-04	-7.39e-04	81,87,92
	41.5	0.0	0.02	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
876	0.0	3.56e-03	0.01	2.63e-04	83,85,91	0.0	0.0	0.0	0,0,0	-9.93e-04	-8.56e-04	-8.01e-04	81,87,92
	41.5	6.93e-03	0.02	1.83e-03	83,85,91	0.0	0.0	0.0	0,0,0				
877	0.0	0.02	0.05	0.0	85,83,0	0.0	0.0	0.0	0,0,0	2.06e-03	1.25e-03	1.05e-03	85,90,92
	40.1	9.80e-03	0.04	0.0	85,83,0	0.0	0.0	0.0	0,0,0				
878	0.0	0.0	0.01	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-4.64e-04	-3.95e-04	-3.67e-04	81,87,92
	41.5	0.0	0.01	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
879	0.0	0.0	6.59e-03	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-1.03e-03	-8.97e-04	-8.43e-04	81,87,92
	41.5	3.55e-03	0.01	7.62e-04	83,85,91	0.0	0.0	0.0	0,0,0				
880	0.0	8.55e-03	0.05	0.0	85,83,0	0.0	0.0	0.0	0,0,0	1.54e-03	9.11e-04	7.58e-04	85,90,92
	40.1	2.55e-03	0.04	0.0	85,83,0	0.0	0.0	0.0	0,0,0				
881	0.0	0.0	0.01	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-8.87e-04	-7.52e-04	-6.98e-04	81,87,92
	41.5	0.0	0.01	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
882	0.0	5.75e-04	6.62e-03	0.0	83,82,0	0.0	0.0	0.0	0,0,0	-1.01e-03	-8.75e-04	-8.21e-04	81,87,92
	41.5	3.64e-05	6.03e-03	0.0	83,82,0	0.0	0.0	0.0	0,0,0				
883	0.0	5.77e-04	0.04	0.0	85,83,0	0.0	0.0	0.0	0,0,0	1.19e-03	6.79e-04	5.56e-04	85,90,92
	40.1	0.0	0.04	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
884	0.0	0.0	8.97e-03	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-8.82e-04	-7.47e-04	-6.92e-04	81,87,92
	41.5	0.0	9.14e-03	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
885	0.0	0.0	5.09e-03	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-9.95e-04	-8.61e-04	-8.08e-04	81,87,92
	41.5	6.72e-04	5.59e-03	0.0	83,85,0	0.0	0.0	0.0	0,0,0				
886	0.0	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	9.45e-04	5.17e-04	4.15e-04	85,90,92
	40.1	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
887	0.0	0.0	6.51e-03	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-8.85e-04	-7.49e-04	-6.95e-04	81,87,92
	41.5	0.0	6.48e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
888	0.0	0.0	3.46e-03	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-9.94e-04	-8.60e-04	-8.07e-04	81,87,92
	41.5	2.40e-04	3.63e-03	0.0	83,85,0	0.0	0.0	0.0	0,0,0				
889	0.0	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	7.66e-04	4.00e-04	3.13e-04	85,90,92
	40.1	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
890	0.0	0.0	4.38e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-8.92e-04	-7.57e-04	-7.02e-04	81,87,92
	41.5	0.0	4.93e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
891	0.0	0.0	2.65e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.00e-03	-8.66e-04	-8.13e-04	81,87,92
	41.5	2.54e-05	2.85e-03</										

894	0.0	2.66e-04	1.87e-03	3.55e-04	79,81,91	0.0	0.0	0.0	0,0,0	-1.01e-03	-8.76e-04	-8.23e-04	81,87,92
	41.5	3.13e-04	2.11e-03	4.17e-04	79,81,91	0.0	0.0	0.0	0,0,0				
895	0.0	8.04e-04	0.01	0.0	85,79,0	0.0	0.0	0.0	0,0,0	5.03e-04	2.33e-04	1.71e-04	85,90,92
	40.1	2.77e-03	0.02	0.0	85,80,0	0.0	0.0	0.0	0,0,0				
896	0.0	7.10e-04	1.83e-03	8.87e-05	83,81,91	0.0	0.0	0.0	0,0,0	-9.12e-04	-7.75e-04	-7.20e-04	81,87,92
	41.5	5.17e-04	2.08e-03	2.96e-04	85,81,91	0.0	0.0	0.0	0,0,0				
897	0.0	4.37e-04	1.21e-03	4.62e-04	83,81,91	0.0	0.0	0.0	0,0,0	-1.02e-03	-8.87e-04	-8.33e-04	81,87,92
	41.5	4.37e-04	1.41e-03	5.13e-04	82,81,92	0.0	0.0	0.0	0,0,0				
898	0.0	2.70e-03	9.43e-03	0.0	85,79,0	0.0	0.0	0.0	0,0,0	3.77e-04	1.59e-04	1.10e-04	85,90,92
	40.1	5.16e-03	0.01	0.0	85,79,0	0.0	0.0	0.0	0,0,0				
899	0.0	9.92e-04	9.74e-04	6.68e-04	85,81,92	0.0	0.0	0.0	0,0,0	-1.03e-03	-8.98e-04	-8.44e-04	81,87,92
	41.5	6.11e-04	8.99e-04	5.78e-04	85,81,92	0.0	0.0	0.0	0,0,0				
900	0.0	3.54e-03	5.24e-03	1.27e-03	85,79,92	0.0	0.0	0.0	0,0,0	2.16e-04	6.74e-05	3.62e-05	85,90,92
	40.1	7.36e-03	8.49e-03	3.71e-03	83,79,92	0.0	0.0	0.0	0,0,0				
901	0.0	5.66e-03	3.25e-03	2.79e-03	85,85,91	0.0	0.0	0.0	0,0,0	-9.29e-05	-9.29e-05	-9.29e-05	79,86,91
	40.1	9.35e-03	5.17e-03	5.46e-03	83,79,92	0.0	0.0	0.0	0,0,0				
902	0.0	8.15e-03	4.70e-03	3.99e-03	85,85,92	0.0	0.0	0.0	0,0,0	-4.99e-04	-3.21e-04	-2.77e-04	83,88,91
	40.1	7.54e-03	4.37e-03	3.69e-03	85,85,92	0.0	0.0	0.0	0,0,0				
903	0.0	7.38e-03	4.43e-03	3.61e-03	85,85,92	0.0	0.0	0.0	0,0,0	-1.11e-03	-6.54e-04	-5.41e-04	83,88,91
	40.1	0.03	0.02	0.02	83,83,92	0.0	0.0	0.0	0,0,0				
904	0.0	0.03	0.02	0.02	83,83,91	0.0	0.0	0.0	0,0,0	-2.81e-04	-1.94e-04	-1.72e-04	83,88,91
	40.1	0.05	0.05	0.03	85,83,92	0.0	0.0	0.0	0,0,0				
905	0.0	0.05	0.05	0.03	85,83,92	0.0	0.0	0.0	0,0,0	1.72e-03	8.98e-04	7.00e-04	85,90,92
	40.1	0.03	0.02	0.02	85,83,92	0.0	0.0	0.0	0,0,0				
906	0.0	0.03	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0	2.54e-03	1.35e-03	1.06e-03	85,90,92
	40.1	8.14e-03	4.89e-03	4.58e-03	85,85,92	0.0	0.0	0.0	0,0,0				
907	0.0	8.95e-03	5.28e-03	5.07e-03	85,85,92	0.0	0.0	0.0	0,0,0	1.95e-03	1.03e-03	8.07e-04	85,90,92
	40.1	9.71e-03	5.68e-03	5.54e-03	85,85,92	0.0	0.0	0.0	0,0,0				
908	0.0	9.75e-03	5.60e-03	5.56e-03	85,85,92	0.0	0.0	0.0	0,0,0	1.55e-03	8.13e-04	6.37e-04	85,90,92
	40.1	7.47e-03	4.40e-03	4.27e-03	85,85,92	0.0	0.0	0.0	0,0,0				
909	0.0	7.33e-03	4.23e-03	4.19e-03	85,85,92	0.0	0.0	0.0	0,0,0	1.33e-03	6.95e-04	5.45e-04	85,90,92
	40.1	5.32e-03	3.16e-03	3.05e-03	85,85,92	0.0	0.0	0.0	0,0,0				
910	0.0	5.17e-03	3.01e-03	2.96e-03	85,85,92	0.0	0.0	0.0	0,0,0	1.21e-03	6.33e-04	4.98e-04	85,90,92
	40.1	3.82e-03	2.29e-03	2.20e-03	85,85,92	0.0	0.0	0.0	0,0,0				
911	0.0	3.71e-03	2.18e-03	2.13e-03	85,85,92	0.0	0.0	0.0	0,0,0	1.14e-03	3.08e-04	2.43e-04	85,90,92
	40.1	2.85e-03	1.72e-03	1.64e-03	85,85,92	0.0	0.0	0.0	0,0,0				
912	0.0	2.77e-03	1.64e-03	1.60e-03	85,85,92	0.0	0.0	0.0	0,0,0	5.64e-04	2.98e-04	2.36e-04	85,90,92
	40.1	2.21e-03	1.35e-03	1.27e-03	85,85,92	0.0	0.0	0.0	0,0,0				
913	0.0	2.16e-03	1.29e-03	1.24e-03	85,85,92	0.0	0.0	0.0	0,0,0	5.50e-04	5.68e-04	4.51e-04	85,90,92
	40.1	1.76e-03	1.08e-03	1.05e-03	85,85,92	0.0	0.0	0.0	0,0,0				
914	0.0	1.72e-03	1.04e-03	9.88e-04	85,85,92	0.0	0.0	0.0	0,0,0	1.05e-03	5.61e-04	4.47e-04	85,90,92
	40.1	1.42e-03	8.75e-04	9.40e-04	85,85,92	0.0	0.0	0.0	0,0,0				
915	0.0	1.39e-03	8.40e-04	7.84e-04	85,85,92	0.0	0.0	0.0	0,0,0	1.04e-03	5.57e-04	4.45e-04	85,90,92
	40.1	1.14e-03	7.06e-04	8.39e-04	85,85,92	0.0	0.0	0.0	0,0,0				
916	0.0	1.11e-03	6.77e-04	6.10e-04	85,85,92	0.0	0.0	0.0	0,0,0	1.03e-03	5.56e-04	4.46e-04	85,90,92
	40.1	9.80e-04	6.06e-04	7.45e-04	85,85,92	0.0	0.0	0.0	0,0,0				
917	0.0	8.70e-04	5.33e-04	5.23e-04	85,85,92	0.0	0.0	0.0	0,0,0	1.03e-03	5.58e-04	4.48e-04	85,90,92
	40.1	8.91e-04	5.44e-04	6.55e-04	85,85,92	0.0	0.0	0.0	0,0,0				
918	0.0	6.48e-04	4.03e-04	4.52e-04	85,85,92	0.0	0.0	0.0	0,0,0	1.04e-03	5.62e-04	4.53e-04	85,90,92
	40.1	7.89e-04	4.78e-04	5.51e-04	85,85,92	0.0	0.0	0.0	0,0,0				
919	0.0	5.70e-04	3.51e-04	3.78e-04	85,85,92	0.0	0.0	0.0	0,0,0	1.05e-03	5.70e-04	4.60e-04	85,90,92
	40.1	5.69e-04	3.50e-04	3.69e-04	85,85,92	0.0	0.0	0.0	0,0,0				
920	0.0	4.52e-04	2.80e-04	2.51e-04	85,85,92	0.0	0.0	0.0	0,0,0	1.06e-03	5.77e-04	4.66e-04	85,90,92
	40.1	9.34e-04	5.36e-04	4.94e-04	85,85,92	0.0	0.0	0.0	0,0,0				
921	0.0	9.12e-04	5.22e-04	4.84e-04	85,85,92	0.0	0.0	0.0	0,0,0	1.05e-03	5.68e-04	2.35e-04	85,90,92
	40.1	3.48e-03	3.64e-03	1.92e-03	85,83,92	0.0	0.0	0.0	0,0,0				
922	0.0	0.0	0.01	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-1.02e-03	-8.77e-04	-8.18e-04	81,87,92
	41.5	0.0	9.83e-03	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
923	0.0	5.80e-03	0.01	6.37e-03	81,81,92	0.0	0.0	0.0	0,0,0	-1.43e-03	-1.31e-03	-1.27e-03	81,87,92
	40.1	5.09e-03	0.01	5.67e-03	81,82,92	0.0	0.0	0.0	0,0,0				
924	0.0	6.61e-03	0.01	4.64e-03	82,81,92	0.0	0.0	0.0	0,0,0	-2.31e-03	-1.55e-03	-1.42e-03	85,87,92
	40.1	1.71e-03	5.86e-03	0.0	82,79,0	0.0	0.0	0.0	0,0,0				
925	0.0	2.91e-03	4.51e-03	1.09e-03	85,83,92	0.0	0.0	0.0	0,0,0	-1.27e-03	-8.25e-04	-7.24e-04	85,90,92
	40.1	1.25e-03	3.14e-03	0.0	85,79,0	0.0	0.0	0.0	0,0,0				
926	0.0	0.0	0.01	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-1.18e-03	-1.04e-03	-9.84e-04	81,87,92
	41.5	0.0	0.01	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
927	0.0	2.04e-03	0.04	0.0	85,82,0	0.0	0.0	0.0	0,0,0	-1.41e-03	-1.13e-03	-1.02e-03	81,87,92
	46.7	0.0	0.02	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
928	0.0	2.40e-03	5.53e-03	0.0	83,81,0	0.0	0.0	0.0	0,0,0	1.46e-03	1.28e-03	1.23e-03	82,87,92
	40.1	1.70e-03	7.33e-03	1.17e-04	85,81,91	0.0	0.0	0.0	0,0,0				
929	0.0	0.0	0.14	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-0.03	-0.02	-0.02	85,90,92
	40.1	0.0	0.19	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
930	0.0	1.09e-03	5.51e-03	0.0	85,79,0	0.0	0.0	0.0	0,0,0	-1.35e-03	-8.91e-04	-7.84e-04	85,90,92
	40.1	8.23e-04	4.73e-03	0.0	85,79,0	0.0	0.0	0.0	0,0,0				
931	0.0	2.51e-03	1.49e-03	2.62e-03	81,82,92	0.0	0.0	0.0	0,0,0	-2.95e-03	-2.45e-03	-2.25e-03	81,87,92
	40.0	7.46e-03	3.79e-03	9.04e-03	81,81,92	0.0	0.0	0.0	0,0,0				
932	0.0	0.0	0.02	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-2.05e-03	-1.70e-03	-1.56e-03	81,87,92
	41.5	8.26e-03	0.03	8.22e-03	82,82,92	0.0	0.0	0.0	0,0,0				
933	0.0	5.09e-03	8.86e-03	5.55e-03	83,81,91	0.0	0.0	0.0	0,0,0	1.26e-03	1.11e-03	1.07e-03	82,87,92
	40.1	5.00e-03	7.39e-03	4.79e-03	83,81,91	0.0	0.0	0.0	0,0,0				
934	0.0	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0	-0.02	-0.02	-0.02	85,90,92
	40.1	0.03	0.02	0.03	85,85,92	0.0	0.0	0.0	0,0,0				
935	0.0	2.74e-03	4.56e-03	1.79e-03	82,81,92	0.0	0.0	0.0	0,0,0	-1.64e-03	-1.32e-03	-1.19e-03	81,87,92
	46.7	3.59e-03	4.55e-03	3.13e-03	85,81,92	0.0	0.0	0.0	0,0,0				
936	0.0	3.31e-03	0.02	4.41e-03	79,81,91	0.0	0.0	0.0	0,0,0	-1.95e-03	-1.69e-03	-1.58e-03	81,87,92
	40.0	0.0	0.02	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
937	0.0	0.0	0.01	0.0	0,81,0	0.0	0.0	0.0	0,0,0	1.51e-03	1.32e-03	1.27e-03	82,87,92
	40.1	3.48e-04	0.01	0.0	83,81,0	0.0	0.0	0.0	0,0,0				
938	0.0	0.0	0.07	0.0	0,85,0	0.0	0.0	0.0	0,0,0	0.01	8.84e-03	8.40e-03	85,90,92
	40.1	0.0	0.05	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
939	0.0	5.83e-04	5.53e-03	0.0	85,79,0	0.0	0.0	0.0	0,0,0	-1.45e-03	-9.47e-04	-8.32e-04	85,90,92
	40.1	0.0	4.99e-03	0.0	0,79,0	0.0	0.0	0.0	0				

	41.5	6.52e-03	4.08e-03	5.17e-03	85,81,92	0.0	0.0	0.0	0.0,0				
945	0.0	0.0	0.02	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-1.48e-03	-1.22e-03	-1.11e-03	81,87,92
	46.7	5.50e-03	0.03	7.02e-03	81,81,92	0.0	0.0	0.0	0,0,0				
946	0.0	0.0	0.39	0.0	0,85,0	0.0	0.0	0.0	0,0,0	7.09e-03	5.82e-03	5.52e-03	85,90,92
	40.1	0.0	0.38	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
947	0.0	3.76e-03	0.02	2.94e-03	83,82,91	0.0	0.0	0.0	0,0,0	1.25e-03	1.10e-03	1.06e-03	82,87,92
	40.1	0.0	0.02	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
948	0.0	8.27e-03	0.03	5.65e-03	85,83,92	0.0	0.0	0.0	0,0,0	-0.03	-0.02	-0.02	85,90,92
	40.1	0.03	0.06	0.03	85,83,92	0.0	0.0	0.0	0,0,0				
949	0.0	2.15e-03	5.98e-03	2.29e-03	83,81,91	0.0	0.0	0.0	0,0,0	-1.66e-03	-1.34e-03	-1.21e-03	81,87,92
	46.7	2.97e-03	5.93e-03	2.11e-03	83,81,91	0.0	0.0	0.0	0,0,0				
950	0.0	0.01	0.03	0.02	81,81,92	0.0	0.0	0.0	0,0,0	-1.85e-03	-1.51e-03	-1.37e-03	81,87,92
	40.0	3.45e-03	9.40e-03	3.53e-03	81,81,92	0.0	0.0	0.0	0,0,0				
951	0.0	0.0	0.01	0.0	0,81,0	0.0	0.0	0.0	0,0,0	1.54e-03	1.34e-03	1.29e-03	82,87,92
	40.1	0.0	0.01	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
952	0.0	4.49e-03	3.25e-03	4.54e-03	85,81,92	0.0	0.0	0.0	0,0,0	4.48e-03	3.53e-03	3.36e-03	85,90,92
	40.1	0.02	0.02	0.02	82,81,92	0.0	0.0	0.0	0,0,0				
953	0.0	0.0	4.95e-03	0.0	0,79,0	0.0	0.0	0.0	0,0,0	-1.49e-03	-9.52e-04	-8.27e-04	85,90,92
	40.1	6.12e-04	6.41e-03	0.0	85,79,0	0.0	0.0	0.0	0,0,0				
954	0.0	0.0	7.02e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-2.52e-03	-2.06e-03	-1.87e-03	81,87,92
	40.0	2.61e-03	0.01	2.73e-03	82,81,92	0.0	0.0	0.0	0,0,0				
955	0.0	1.85e-03	6.29e-03	2.34e-03	83,82,91	0.0	0.0	0.0	0,0,0	-2.38e-03	-2.01e-03	-1.86e-03	81,87,92
	41.5	3.56e-03	9.02e-03	4.21e-03	85,82,92	0.0	0.0	0.0	0,0,0				
956	0.0	0.0	0.01	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-5.62e-04	-5.45e-04	-5.38e-04	81,87,92
	40.1	4.63e-03	0.02	4.72e-03	85,81,92	0.0	0.0	0.0	0,0,0				
957	0.0	0.17	0.10	0.18	85,85,92	0.0	0.0	0.0	0,0,0	-0.01	-8.87e-03	-8.46e-03	85,90,92
	40.1	0.41	0.22	0.44	85,85,92	0.0	0.0	0.0	0,0,0				
958	0.0	3.78e-03	2.14e-03	3.83e-03	83,83,91	0.0	0.0	0.0	0,0,0	-1.82e-03	-1.47e-03	-1.32e-03	81,87,92
	41.5	4.10e-03	2.28e-03	3.84e-03	85,85,92	0.0	0.0	0.0	0,0,0				
959	0.0	0.0	0.02	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-1.29e-03	-1.02e-03	-9.13e-04	81,87,92
	46.7	0.0	0.02	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
960	0.0	0.0	0.44	0.0	0,85,0	0.0	0.0	0.0	0,0,0	5.53e-03	4.50e-03	4.26e-03	85,90,92
	40.1	0.0	0.43	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
961	0.0	0.03	0.05	0.04	81,81,92	0.0	0.0	0.0	0,0,0	-2.56e-03	-2.17e-03	-2.01e-03	81,87,92
	40.0	7.28e-03	0.02	8.49e-03	81,81,92	0.0	0.0	0.0	0,0,0				
962	0.0	4.33e-03	2.36e-03	4.24e-03	85,85,92	0.0	0.0	0.0	0,0,0	4.33e-03	3.39e-03	3.22e-03	85,90,92
	40.1	3.21e-03	1.81e-03	3.09e-03	85,85,92	0.0	0.0	0.0	0,0,0				
963	0.0	0.01	6.95e-03	0.01	83,83,91	0.0	0.0	0.0	0,0,0	7.57e-04	6.38e-04	6.07e-04	82,87,92
	40.1	7.33e-03	4.07e-03	7.69e-03	85,85,92	0.0	0.0	0.0	0,0,0				
964	0.0	0.05	0.03	0.05	85,85,92	0.0	0.0	0.0	0,0,0	-0.02	-0.02	-0.02	85,90,92
	40.1	0.04	0.03	0.04	85,85,92	0.0	0.0	0.0	0,0,0				
965	0.0	0.0	0.31	0.0	0,85,0	0.0	0.0	0.0	0,0,0	8.59e-03	7.05e-03	6.70e-03	85,90,92
	40.1	0.0	0.30	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
966	0.0	0.0	0.01	0.0	0,81,0	0.0	0.0	0.0	0,0,0	1.25e-03	1.10e-03	1.05e-03	82,87,92
	40.1	8.76e-04	0.01	0.0	85,82,0	0.0	0.0	0.0	0,0,0				
967	0.0	2.18e-03	8.14e-03	2.21e-03	83,81,91	0.0	0.0	0.0	0,0,0	-1.71e-03	-1.39e-03	-1.26e-03	81,87,92
	46.7	4.23e-03	9.54e-03	3.54e-03	83,82,91	0.0	0.0	0.0	0,0,0				
968	0.0	0.0	0.02	0.0	0,81,0	0.0	0.0	0.0	0,0,0	1.51e-03	1.31e-03	1.26e-03	82,87,92
	40.1	1.64e-03	0.02	1.03e-03	85,81,92	0.0	0.0	0.0	0,0,0				
969	0.0	1.19e-03	6.19e-03	0.0	85,79,0	0.0	0.0	0.0	0,0,0	-1.44e-03	-8.85e-04	-7.56e-04	85,90,92
	40.1	1.07e-03	5.81e-03	0.0	85,79,0	0.0	0.0	0.0	0,0,0				
970	0.0	8.19e-04	2.23e-03	9.88e-04	83,79,91	0.0	0.0	0.0	0,0,0	-2.53e-03	-2.16e-03	-2.01e-03	81,87,92
	41.5	2.83e-03	5.45e-03	3.44e-03	85,82,92	0.0	0.0	0.0	0,0,0				
971	0.0	3.25e-03	0.01	2.97e-03	83,81,91	0.0	0.0	0.0	0,0,0	-5.59e-04	-5.38e-04	-5.29e-04	81,87,92
	40.1	6.04e-03	0.02	6.35e-03	85,81,92	0.0	0.0	0.0	0,0,0				
972	0.0	0.08	0.05	0.08	85,85,92	0.0	0.0	0.0	0,0,0	-4.94e-03	-4.03e-03	-3.83e-03	85,90,92
	40.1	0.18	0.10	0.19	85,85,92	0.0	0.0	0.0	0,0,0				
973	0.0	3.31e-03	1.92e-03	3.41e-03	83,83,91	0.0	0.0	0.0	0,0,0	-2.00e-03	-1.63e-03	-1.49e-03	81,87,92
	41.5	4.17e-03	2.34e-03	4.31e-03	85,85,92	0.0	0.0	0.0	0,0,0				
974	0.0	0.0	0.53	0.0	0,85,0	0.15	0.0	0.0	85,0,0	-0.12	-0.09	-0.06	85,90,92
	40.1	0.0	0.45	0.0	0,85,0	0.12	0.10	0.10	83,90,92				
975	0.0	3.41e-03	8.80e-03	3.79e-03	85,83,92	0.0	0.0	0.0	0,0,0	-4.90e-03	-4.31e-03	-4.08e-03	81,87,92
	40.0	0.04	0.07	0.05	81,81,92	0.0	0.0	0.0	0,0,0				
976	0.0	5.78e-03	3.27e-03	5.57e-03	85,85,92	0.0	0.0	0.0	0,0,0	4.28e-03	3.35e-03	3.18e-03	85,90,92
	40.1	3.79e-03	2.31e-03	3.81e-03	83,83,91	0.0	0.0	0.0	0,0,0				
977	0.0	0.0	4.54e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	7.60e-04	6.44e-04	6.13e-04	82,87,92
	40.1	0.02	0.03	0.02	85,83,92	0.0	0.0	0.0	0,0,0				
978	0.0	0.0	0.34	0.0	0,85,0	0.0	0.0	0.0	0,0,0	8.10e-03	6.65e-03	6.32e-03	85,90,92
	40.1	0.0	0.33	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
979	0.0	0.0	0.02	0.0	0,81,0	0.0	0.0	0.0	0,0,0	1.55e-03	1.35e-03	1.30e-03	82,87,92
	40.1	0.0	0.02	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
980	0.0	0.0	0.41	0.0	0,85,0	0.0	0.0	0.0	0,0,0	6.58e-03	5.38e-03	5.11e-03	85,90,92
	40.1	0.0	0.40	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
981	0.0	6.66e-03	3.74e-03	6.48e-03	83,83,91	0.0	0.0	0.0	0,0,0	8.24e-04	6.94e-04	6.59e-04	82,87,92
	40.1	5.33e-03	3.06e-03	5.24e-03	85,85,92	0.0	0.0	0.0	0,0,0				
982	0.0	0.0	0.21	0.0	0,85,0	0.0	0.0	0.0	0,0,0	9.90e-03	8.12e-03	7.72e-03	85,90,92
	40.1	0.0	0.19	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
983	0.0	0.0	8.30e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0	1.28e-03	1.12e-03	1.07e-03	82,87,92
	40.1	1.80e-03	0.01	0.0	85,82,0	0.0	0.0	0.0	0,0,0				
984	0.0	0.0	5.60e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.39e-03	-1.11e-03	-1.00e-03	81,87,92
	40.0	4.45e-03	0.01	4.15e-03	83,85,91	0.0	0.0	0.0	0,0,0				
985	0.0	4.87e-05	0.01	0.0	81,81,0	0.0	0.0	0.0	0,0,0	1.43e-03	1.22e-03	1.16e-03	82,87,92
	40.1	3.57e-03	0.02	3.71e-03	81,81,92	0.0	0.0	0.0	0,0,0				
986	0.0	8.44e-04	6.05e-03	0.0	85,79,0	0.0	0.0	0.0	0,0,0	-1.40e-03	-8.38e-04	-7.08e-04	85,90,92
	40.1	1.53e-03	6.42e-03	0.0	85,79,0	0.0	0.0	0.0	0,0,0				
987	0.0	1.29e-03	2.71e-03	1.15e-03	82,81,92	0.0	0.0	0.0	0,0,0	-2.56e-03	-2.19e-03	-2.05e-03	81,87,92
	41.5	9.85e-04	2.21e-03	1.11e-03	83,79,91	0.0	0.0	0.0	0,0,0				
988	0.0	7.32e-03	0.01	8.52e-03	85,81,92	0.0	0.0	0.0	0,0,0	-7.72e-04	-7.25e-04	-7.07e-04	81,87,92
	40.1	4.35e-03	8.53e-03	4.56e-03	85,81,92	0.0	0.0	0.0	0,0,0				
989	0.0	0.03	0.02	0.03	83,85,91	0.0	0.0	0.0	0,0,0	-3.81e-03	-3.05e-03	-2.90e-03	85,90,92
	40.1	0.08	0.04	0.08	85,85,92	0.0	0.0	0.0	0,0,0				
990	0.0	2.25e-03	1.38e-03	2.06e-03	85,85,91	0.0	0.0	0.0	0,0,0	-2.08e-03	-1.72e-03	-1.58e-03	81,87,92
	41.5	3.20e-03	1.86e-03	3.32e-03	83,83,91	0.0	0.0	0.0	0,0,0				
991	0.0	0.0	0.39	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-0.05	-		

995	0.0	0.0	0.36	0.0	0,85,0	0.0	0.0	0.0	0,0,0	7.60e-03	6.24e-03	5.93e-03	85,90,92
	40.1	0.0	0.35	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
996	0.0	0.0	0.42	0.0	0,85,0	0.0	0.0	0.0	0,0,0	6.06e-03	4.94e-03	4.69e-03	85,90,92
	40.1	0.0	0.42	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
997	0.0	0.0	0.25	0.0	0,85,0	0.0	0.0	0.0	0,0,0	9.50e-03	7.80e-03	7.41e-03	85,90,92
	40.1	0.0	0.23	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
998	0.0	0.0	0.50	0.0	0,85,0	0.0	0.0	0.0	0,0,0	3.91e-03	3.12e-03	2.94e-03	85,90,92
	40.1	0.0	0.49	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
999	0.0	3.73e-03	2.18e-03	3.10e-03	83,83,91	0.0	0.0	0.0	0,0,0	8.26e-04	6.92e-04	6.56e-04	82,87,92
	40.1	4.95e-03	2.78e-03	5.73e-03	83,83,91	0.0	0.0	0.0	0,0,0				
1000	0.0	0.0	0.12	0.0	0,85,0	0.0	0.0	0.0	0,0,0	0.01	8.66e-03	8.23e-03	85,90,92
	40.1	0.0	0.10	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
1001	0.0	0.0	7.38e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0	1.31e-03	1.15e-03	1.10e-03	82,87,92
	40.1	2.75e-03	0.01	1.54e-03	85,82,92	0.0	0.0	0.0	0,0,0				
1002	0.0	6.43e-04	3.40e-03	4.54e-04	83,82,91	0.0	0.0	0.0	0,0,0	-1.21e-03	-9.29e-04	-8.18e-04	81,87,92
	40.0	1.16e-03	3.77e-03	3.68e-04	83,85,91	0.0	0.0	0.0	0,0,0				
1003	0.0	1.69e-03	9.24e-03	0.0	85,79,0	0.0	0.0	0.0	0,0,0	-1.55e-03	-9.53e-04	-8.15e-04	85,90,92
	40.1	4.53e-03	0.01	5.75e-04	85,79,92	0.0	0.0	0.0	0,0,0				
1004	0.0	2.34e-03	4.08e-03	2.46e-03	82,81,92	0.0	0.0	0.0	0,0,0	-2.44e-03	-2.09e-03	-1.95e-03	81,87,92
	41.5	1.33e-03	2.54e-03	1.21e-03	82,81,92	0.0	0.0	0.0	0,0,0				
1005	0.0	6.55e-03	9.83e-03	7.47e-03	85,81,92	0.0	0.0	0.0	0,0,0	-1.19e-03	-1.10e-03	-1.06e-03	81,87,92
	40.1	1.18e-03	2.21e-03	1.08e-03	83,81,91	0.0	0.0	0.0	0,0,0				
1006	0.0	0.01	7.63e-03	0.01	83,83,91	0.0	0.0	0.0	0,0,0	-4.11e-03	-3.24e-03	-3.07e-03	85,90,92
	40.1	0.03	0.02	0.03	85,85,92	0.0	0.0	0.0	0,0,0				
1007	0.0	2.81e-03	1.65e-03	2.56e-03	85,85,92	0.0	0.0	0.0	0,0,0	-2.05e-03	-9.00e-04	-8.26e-04	81,87,92
	41.5	2.25e-03	1.37e-03	1.84e-03	85,85,92	0.0	0.0	0.0	0,0,0				
1008	0.0	0.0	0.26	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-0.02	-0.02	-0.02	85,90,92
	40.1	0.0	0.32	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1009	0.0	0.02	0.08	0.02	81,81,92	0.0	0.0	0.0	0,0,0	-4.16e-03	-3.66e-03	-3.46e-03	81,87,92
	40.0	0.0	0.05	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
1010	0.0	9.58e-03	5.65e-03	9.55e-03	85,85,92	0.0	0.0	0.0	0,0,0	4.28e-03	3.35e-03	3.17e-03	85,90,92
	40.1	7.89e-03	4.81e-03	8.19e-03	85,83,92	0.0	0.0	0.0	0,0,0				
1011	0.0	2.74e-03	2.28e-03	2.54e-03	83,83,91	0.0	0.0	0.0	0,0,0	8.34e-04	7.12e-04	6.78e-04	82,87,92
	40.1	3.88e-03	3.68e-03	4.08e-03	85,85,92	0.0	0.0	0.0	0,0,0				
1012	0.0	0.0	0.28	0.0	0,85,0	0.0	0.0	0.0	0,0,0	9.06e-03	7.44e-03	7.07e-03	85,90,92
	40.1	0.0	0.27	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
1013	0.0	0.0	0.57	0.0	0,85,0	0.16	0.14	0.13	85,90,92	-0.03	-0.02	-0.02	85,90,92
	40.1	0.0	0.56	0.0	0,85,0	0.19	0.17	0.16	85,90,92				
1014	0.0	0.0	0.17	0.0	0,85,0	0.0	0.0	0.0	0,0,0	0.01	8.41e-03	7.99e-03	85,90,92
	40.1	0.0	0.15	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
1015	0.0	0.0	0.46	0.0	0,85,0	0.0	0.0	0.0	0,0,0	5.00e-03	4.05e-03	3.83e-03	85,90,92
	40.1	0.0	0.45	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
1016	0.0	0.0	6.44e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0	1.34e-03	1.18e-03	1.13e-03	82,87,92
	40.1	4.97e-03	0.01	4.36e-03	85,82,92	0.0	0.0	0.0	0,0,0				
1017	0.0	1.19e-03	6.97e-04	1.49e-03	81,81,92	0.0	0.0	0.0	0,0,0	-1.20e-03	-9.16e-04	-8.03e-04	81,87,92
	40.0	2.81e-03	1.47e-03	3.14e-03	81,81,92	0.0	0.0	0.0	0,0,0				
1018	0.0	4.47e-03	0.02	0.0	85,79,0	0.0	0.0	0.0	0,0,0	-1.95e-03	-1.26e-03	-1.10e-03	85,90,92
	40.1	2.18e-03	0.01	0.0	85,79,0	0.0	0.0	0.0	0,0,0				
1019	0.0	2.08e-03	2.99e-03	2.24e-03	82,81,92	0.0	0.0	0.0	0,0,0	-2.25e-03	-1.93e-03	-1.80e-03	81,87,92
	41.5	2.30e-03	3.32e-03	2.46e-03	82,81,92	0.0	0.0	0.0	0,0,0				
1020	0.0	4.04e-03	4.86e-03	3.66e-03	83,81,91	0.0	0.0	0.0	0,0,0	-1.62e-03	-1.48e-03	-1.42e-03	81,87,92
	40.1	3.13e-03	6.70e-03	3.85e-03	82,81,92	0.0	0.0	0.0	0,0,0				
1021	0.0	0.01	6.50e-03	0.01	85,85,92	0.0	0.0	0.0	0,0,0	-4.67e-03	-3.64e-03	-3.44e-03	85,90,92
	40.1	7.99e-03	4.72e-03	8.78e-03	83,83,91	0.0	0.0	0.0	0,0,0				
1022	0.0	2.64e-03	1.55e-03	2.46e-03	85,85,92	0.0	0.0	0.0	0,0,0	-1.92e-03	-1.59e-03	-1.46e-03	81,87,92
	41.5	2.81e-03	1.63e-03	2.56e-03	85,85,92	0.0	0.0	0.0	0,0,0				
1023	0.0	0.01	0.05	0.01	81,82,92	0.0	0.0	0.0	0,0,0	-2.69e-03	-2.31e-03	-2.15e-03	81,87,92
	40.0	9.83e-03	0.05	0.01	81,81,92	0.0	0.0	0.0	0,0,0				
1024	0.0	0.01	6.58e-03	0.01	85,85,92	0.0	0.0	0.0	0,0,0	4.30e-03	3.36e-03	3.18e-03	85,90,92
	40.1	0.01	6.36e-03	0.01	85,85,92	0.0	0.0	0.0	0,0,0				
1025	0.0	4.99e-03	4.24e-03	5.19e-03	83,83,91	0.0	0.0	0.0	0,0,0	8.25e-04	7.04e-04	6.70e-04	82,87,92
	40.1	4.59e-03	3.49e-03	4.89e-03	85,85,92	0.0	0.0	0.0	0,0,0				
1026	0.0	0.0	0.56	0.0	0,85,0	0.16	0.13	0.13	85,90,92	-0.08	-0.07	-0.07	85,90,92
	40.1	0.0	0.57	0.0	0,85,0	0.16	0.14	0.13	85,90,92				
1027	0.0	0.0	0.48	0.0	0,85,0	0.0	0.0	0.0	0,0,0	4.46e-03	3.59e-03	3.39e-03	85,90,92
	40.1	0.0	0.47	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
1028	0.0	0.0	0.52	0.0	0,85,0	0.0	0.0	0.0	0,0,0	3.34e-03	2.64e-03	2.48e-03	85,90,92
	40.1	0.0	0.51	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
1029	0.0	3.82e-03	4.77e-03	3.00e-03	83,82,91	0.0	0.0	0.0	0,0,0	1.39e-03	1.22e-03	1.17e-03	82,87,92
	40.1	1.37e-03	4.04e-03	8.23e-04	85,81,92	0.0	0.0	0.0	0,0,0				
1030	0.0	4.95e-03	2.72e-03	6.05e-03	81,81,92	0.0	0.0	0.0	0,0,0	-1.50e-03	-1.19e-03	-1.07e-03	81,87,92
	40.0	3.00e-03	1.76e-03	3.54e-03	81,81,92	0.0	0.0	0.0	0,0,0				
1031	0.0	9.99e-04	0.02	0.0	85,83,0	0.0	0.0	0.0	0,0,0	-2.30e-03	-1.50e-03	-1.31e-03	85,90,92
	40.1	0.0	0.01	0.0	0,79,0	0.0	0.0	0.0	0,0,0				
1032	0.0	1.40e-03	1.27e-03	1.55e-03	81,79,92	0.0	0.0	0.0	0,0,0	-2.10e-03	-1.79e-03	-1.67e-03	81,87,92
	41.5	1.92e-03	2.00e-03	2.13e-03	82,81,92	0.0	0.0	0.0	0,0,0				
1033	0.0	6.28e-03	0.01	4.06e-03	83,83,91	0.0	0.0	0.0	0,0,0	-1.82e-03	-1.66e-03	-1.60e-03	81,87,92
	40.1	1.88e-04	7.17e-03	0.0	83,81,0	0.0	0.0	0.0	0,0,0				
1034	0.0	0.01	8.38e-03	0.02	85,85,92	0.0	0.0	0.0	0,0,0	-4.81e-03	-3.70e-03	-3.49e-03	85,90,92
	40.1	8.65e-03	5.26e-03	7.11e-03	85,85,92	0.0	0.0	0.0	0,0,0				
1035	0.0	2.24e-03	1.34e-03	2.07e-03	85,85,92	0.0	0.0	0.0	0,0,0	-1.82e-03	-1.50e-03	-1.37e-03	81,87,92
	41.5	2.63e-03	1.53e-03	2.45e-03	85,85,92	0.0	0.0	0.0	0,0,0				
1036	0.0	0.0	0.03	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-1.31e-03	-1.03e-03	-9.19e-04	81,87,92
	40.0	0.02	0.07	0.02	81,82,92	0.0	0.0	0.0	0,0,0				
1037	0.0	0.01	7.88e-03	0.01	85,85,92	0.0	0.0	0.0	0,0,0	4.32e-03	3.38e-03	3.20e-03	85,90,92
	40.1	0.01	8.11e-03	0.01	85,85,92	0.0	0.0	0.0	0,0,0				
1038	0.0	6.25e-03	9.46e-03	6.71e-03	83,83,91	0.0	0.0	0.0	0,0,0	8.12e-04	6.93e-04	6.60e-04	82,87,92
	40.1	6.16e-03	9.22e-03	6.76e-03	85,85,92	0.0	0.0	0.0	0,0,0				
1039	0.0	0.0	0.50	0.0	0,85,0	0.14	0.12	0.11	85,90,92	-0.09	-0.08	-0.07	85,90,92
	40.1	0.0	0.52	0.0	0,85,0	0.14	0.12	0.11	85,90,92				
1040	0.0	0.0	0.54	0.0	0,85,0	0.17	0.0	0.0	85,0,0	0.04	2.15e-03	2.01e-03	85,90,92
	40.1	0.0	0.53	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
1041	0.0	0.0	0.55	0.0	0,85,0	0.19	0.16	0.15	85,90,92	-0.04	-0.03	-0.03	85,90,92
	40.1	0.0	0.58	0.0	0,85,0	0.42	0.18	0.17	85,88,91				</

	41.5	1.23e-03	6.17e-04	1.36e-03	81,82,92	0.0	0.0	0.0	0,0,0				
1046	0.0	0.0	0.06	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-1.60e-03	-1.47e-03	-1.42e-03	81,87,92
	40.1	0.0	0.06	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
1047	0.0	0.02	9.68e-03	0.02	85,85,92	0.0	0.0	0.0	0,0,0	-4.52e-03	-3.42e-03	-3.22e-03	85,90,92
	40.1	8.98e-03	5.52e-03	8.96e-03	85,85,92	0.0	0.0	0.0	0,0,0				
1048	0.0	1.88e-03	1.14e-03	1.72e-03	85,85,92	0.0	0.0	0.0	0,0,0	-9.27e-04	-7.62e-04	-6.97e-04	81,87,92
	41.5	2.22e-03	1.31e-03	2.06e-03	85,85,92	0.0	0.0	0.0	0,0,0				
1049	0.0	0.0	0.03	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-1.24e-03	-9.65e-04	-8.55e-04	81,87,92
	40.0	0.0	0.04	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
1050	0.0	0.02	9.48e-03	0.02	85,85,92	0.0	0.0	0.0	0,0,0	4.36e-03	3.41e-03	3.23e-03	85,90,92
	40.1	0.02	9.45e-03	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
1051	0.0	5.97e-03	0.02	6.61e-03	83,83,91	0.0	0.0	0.0	0,0,0	8.00e-04	6.82e-04	6.49e-04	82,87,92
	40.1	5.57e-03	0.02	6.19e-03	85,85,92	0.0	0.0	0.0	0,0,0				
1052	0.0	0.0	0.51	0.0	0,85,0	0.14	0.13	0.12	85,90,92	-0.12	-0.10	-0.10	85,90,92
	40.1	0.0	0.55	0.0	0,85,0	0.15	0.13	0.12	85,90,92				
1053	0.0	0.0	0.61	0.0	0,85,0	0.19	0.17	0.0	85,90,0	0.02	2.93e-03	9.76e-04	85,90,92
	40.1	0.0	0.59	0.0	0,85,0	0.19	0.0	0.0	85,0,0				
1054	0.0	0.0	0.55	0.0	0,85,0	0.19	0.16	0.15	85,90,92	-0.05	-0.05	-0.05	85,90,92
	40.1	0.0	0.59	0.0	0,85,0	0.17	0.14	0.14	85,90,92				
1055	0.0	4.01e-03	2.30e-03	4.15e-03	85,85,92	0.0	0.0	0.0	0,0,0	-1.92e-03	-1.58e-03	-1.44e-03	81,87,92
	40.0	3.40e-03	1.99e-03	3.88e-03	85,85,92	0.0	0.0	0.0	0,0,0				
1056	0.0	0.0	0.03	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-1.93e-03	-1.16e-03	-9.77e-04	85,90,92
	40.1	0.0	0.03	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
1057	0.0	6.91e-04	3.95e-04	6.58e-04	82,82,92	0.0	0.0	0.0	0,0,0	-1.03e-03	-8.71e-04	-8.09e-04	81,87,92
	41.5	8.20e-04	4.59e-04	8.25e-04	82,82,92	0.0	0.0	0.0	0,0,0				
1058	0.0	0.0	0.02	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-1.28e-03	-1.18e-03	-1.14e-03	81,87,92
	40.1	0.0	0.03	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
1059	0.0	0.01	8.27e-03	0.01	85,85,92	0.0	0.0	0.0	0,0,0	-4.09e-03	-3.06e-03	-2.87e-03	85,90,92
	40.1	9.25e-03	5.70e-03	8.94e-03	85,85,92	0.0	0.0	0.0	0,0,0				
1060	0.0	1.60e-03	9.86e-04	1.45e-03	85,85,92	0.0	0.0	0.0	0,0,0	-8.98e-04	-1.39e-03	-1.27e-03	81,87,92
	41.5	1.86e-03	1.12e-03	1.70e-03	85,85,92	0.0	0.0	0.0	0,0,0				
1061	0.0	0.0	0.03	0.0	0,82,0	0.0	0.0	0.0	0,0,0	-1.40e-03	-1.12e-03	-1.00e-03	81,87,92
	40.0	0.0	0.03	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
1062	0.0	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0	4.41e-03	3.45e-03	3.27e-03	85,90,92
	40.1	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
1063	0.0	0.0	0.03	0.0	0,85,0	0.0	0.0	0.0	0,0,0	8.42e-04	7.19e-04	6.85e-04	82,87,92
	40.1	0.0	0.05	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
1064	0.0	0.0	0.50	0.0	0,85,0	0.15	0.13	0.12	85,90,92	6.73e-03	4.29e-03	1.78e-03	85,90,92
	40.1	0.0	0.63	0.0	0,85,0	0.20	0.18	0.0	85,90,0				
1065	0.0	0.0	0.57	0.0	0,85,0	0.18	0.0	0.0	85,0,0	0.03	1.62e-03	1.51e-03	85,90,92
	40.1	0.0	0.55	0.0	0,85,0	0.18	0.0	0.0	85,0,0				
1066	0.0	2.61e-03	1.45e-03	1.79e-03	83,83,92	0.0	0.0	0.0	0,0,0	-1.85e-03	-1.52e-03	-1.39e-03	81,87,92
	40.0	1.71e-03	9.97e-04	1.25e-03	85,85,92	0.0	0.0	0.0	0,0,0				
1067	0.0	0.0	0.04	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-1.51e-03	-8.18e-04	-6.56e-04	85,90,92
	40.1	0.0	0.04	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
1068	0.0	6.06e-04	3.64e-04	5.55e-04	85,85,92	0.0	0.0	0.0	0,0,0	-1.88e-03	-1.59e-03	-1.48e-03	81,87,92
	41.5	6.81e-04	3.93e-04	6.47e-04	82,85,92	0.0	0.0	0.0	0,0,0				
1069	0.0	0.0	0.03	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.21e-03	-1.11e-03	-1.07e-03	81,87,92
	40.1	0.0	0.04	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
1070	0.0	0.01	6.83e-03	0.01	85,85,92	0.0	0.0	0.0	0,0,0	-3.71e-03	-2.73e-03	-2.55e-03	85,90,92
	40.1	0.01	5.93e-03	0.01	85,85,92	0.0	0.0	0.0	0,0,0				
1071	0.0	1.39e-03	8.55e-04	1.22e-03	83,83,92	0.0	0.0	0.0	0,0,0	-1.65e-03	-1.35e-03	-1.23e-03	81,87,92
	41.5	1.58e-03	9.56e-04	1.43e-03	85,85,92	0.0	0.0	0.0	0,0,0				
1072	0.0	0.0	0.03	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-1.59e-03	-1.30e-03	-1.19e-03	81,87,92
	40.0	0.0	0.02	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
1073	0.0	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0	4.46e-03	3.50e-03	3.31e-03	85,90,92
	40.1	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
1074	0.0	0.01	0.06	0.01	83,85,91	0.0	0.0	0.0	0,0,0	9.05e-04	7.68e-04	7.33e-04	82,87,92
	40.1	0.0	0.03	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
1075	0.0	0.0	0.60	0.0	0,85,0	0.17	0.15	0.14	85,90,92	-0.01	-0.01	-0.01	85,90,92
	40.1	0.0	0.56	0.0	0,85,0	0.17	0.15	0.14	85,90,92				
1076	0.0	3.75e-03	4.17e-03	3.20e-03	85,79,92	0.0	0.0	0.0	0,0,0	-1.90e-03	-1.56e-03	-1.43e-03	81,87,92
	40.0	5.07e-03	8.00e-03	5.28e-03	81,81,92	0.0	0.0	0.0	0,0,0				
1077	0.0	0.0	0.05	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-1.02e-03	-4.32e-04	-2.97e-04	85,90,92
	40.1	0.0	0.05	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
1078	0.0	5.59e-04	3.41e-04	4.69e-04	85,85,92	0.0	0.0	0.0	0,0,0	-1.84e-03	-1.56e-03	-1.45e-03	81,87,92
	41.5	5.98e-04	3.60e-04	5.43e-04	85,85,92	0.0	0.0	0.0	0,0,0				
1079	0.0	1.51e-03	0.02	0.0	83,81,0	0.0	0.0	0.0	0,0,0	-1.43e-03	-1.29e-03	-1.23e-03	81,87,92
	40.1	0.0	0.02	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
1080	0.0	9.50e-03	5.25e-03	9.72e-03	85,85,92	0.0	0.0	0.0	0,0,0	-3.39e-03	-2.46e-03	-2.29e-03	85,90,92
	40.1	7.97e-03	4.50e-03	7.48e-03	85,85,92	0.0	0.0	0.0	0,0,0				
1081	0.0	1.26e-03	7.75e-04	1.04e-03	83,83,91	0.0	0.0	0.0	0,0,0	-1.61e-03	-1.32e-03	-1.21e-03	81,87,92
	41.5	1.35e-03	8.22e-04	1.20e-03	85,85,92	0.0	0.0	0.0	0,0,0				
1082	0.0	0.0	0.03	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-1.66e-03	-1.37e-03	-1.26e-03	81,87,92
	40.0	0.0	0.02	0.0	0,82,0	0.0	0.0	0.0	0,0,0				
1083	0.0	0.03	0.02	0.03	85,85,92	0.0	0.0	0.0	0,0,0	4.53e-03	3.55e-03	3.36e-03	85,90,92
	40.1	0.02	0.01	0.03	85,85,92	0.0	0.0	0.0	0,0,0				
1084	0.0	0.0	0.04	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-1.00e-04	-1.02e-04	-1.02e-04	83,88,91
	40.1	0.0	0.04	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
1085	0.0	0.0	0.53	0.0	0,85,0	0.15	0.13	0.12	85,90,92	-0.02	-0.01	-0.01	85,90,92
	40.1	0.0	0.61	0.0	0,85,0	0.19	0.16	0.15	85,90,92				
1086	0.0	0.0	0.55	0.0	0,85,0	0.16	0.14	0.13	85,90,92	-2.75e-03	-2.98e-03	-2.98e-03	79,86,91
	40.1	0.0	0.52	0.0	0,85,0	0.15	0.13	0.13	85,90,92				
1087	0.0	6.52e-03	6.16e-03	7.43e-03	82,83,92	0.0	0.0	0.0	0,0,0	-2.25e-03	-1.88e-03	-1.72e-03	81,87,92
	40.0	5.20e-03	3.49e-03	5.29e-03	81,81,92	0.0	0.0	0.0	0,0,0				
1088	0.0	0.0	0.05	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-5.17e-04	-7.13e-05	6.05e-05	85,90,91
	40.1	0.0	0.05	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
1089	0.0	5.11e-04	3.14e-04	3.80e-04	85,85,92	0.0	0.0	0.0	0,0,0	-1.80e-03	-1.53e-03	-1.42e-03	81,87,92
	41.5	5.50e-04	3.33e-04	4.56e-04	85,85,92	0.0	0.0	0.0	0,0,0				
1090	0.0	3.74e-03	0.01	3.67e-03	83,81,91	0.0	0.0	0.0	0,0,0	-1.84e-03	-1.65e-03	-1.57e-03	81,87,92
	40.1	7.28e-04	9.84e-03	0.0	83,81,0	0.0	0.0	0.0	0,0,0				
1091	0.0	7.98e-03	5.20e-03	8.94e-03	85,81,92	0.0	0.0	0.0	0,0,0	-3.15e-03	-2.25e-03	-2.09e-03	85,90,92
	40.1	5.81e-03	3.19e-03	6.06e-03	85,85,92	0.0	0.0	0.0	0,0,0				
1092	0.0	1.13e-03	6.91e-04	9.17e-04	83,83,91	0.0	0.0	0.0	0,0,0	-1.58e-03	-1.30e-03	-1.18e-03	81,87,92
	41.5	1.16e-03	7.04e-04	1.00e-03									

1096	0.0	8.49e-03	4.25e-03	9.50e-03	81,81,92	0.0	0.0	0.0	0,0,0	-2.74e-03	-2.30e-03	-2.12e-03	81,87,92
	40.0	2.36e-03	1.42e-03	2.10e-03	81,81,92	0.0	0.0	0.0	0,0,0				
1097	0.0	0.0	0.06	0.0	0,85,0	0.0	0.0	0.0	0,0,0	2.19e-04	2.19e-04	2.19e-04	79,86,91
	40.1	0.0	0.06	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
1098	0.0	4.71e-04	2.88e-04	2.81e-04	83,83,92	0.0	0.0	0.0	0,0,0	-1.77e-03	-1.50e-03	-1.39e-03	81,87,92
	41.5	4.99e-04	3.02e-04	3.67e-04	85,85,92	0.0	0.0	0.0	0,0,0				
1099	0.0	1.23e-03	1.67e-03	6.23e-04	83,81,91	0.0	0.0	0.0	0,0,0	-2.20e-03	-1.97e-03	-1.88e-03	81,87,92
	40.1	2.53e-03	5.47e-03	3.02e-03	81,81,92	0.0	0.0	0.0	0,0,0				
1100	0.0	7.68e-03	9.16e-03	8.25e-03	85,81,92	0.0	0.0	0.0	0,0,0	-2.96e-03	-2.08e-03	-1.93e-03	85,90,92
	40.1	4.68e-03	5.18e-03	5.00e-03	82,81,92	0.0	0.0	0.0	0,0,0				
1101	0.0	9.97e-04	6.07e-04	7.86e-04	83,83,91	0.0	0.0	0.0	0,0,0	-1.55e-03	-1.27e-03	-1.16e-03	81,87,92
	41.5	9.79e-04	5.96e-04	8.16e-04	85,85,92	0.0	0.0	0.0	0,0,0				
1102	0.0	2.53e-04	0.02	3.38e-04	79,81,91	0.0	0.0	0.0	0,0,0	-2.40e-03	-2.11e-03	-1.99e-03	81,87,92
	40.0	9.58e-03	0.03	0.01	79,81,91	0.0	0.0	0.0	0,0,0				
1103	0.0	0.04	0.02	0.04	83,83,91	0.0	0.0	0.0	0,0,0	4.69e-03	3.70e-03	3.50e-03	85,90,92
	40.1	0.03	0.02	0.03	85,85,92	0.0	0.0	0.0	0,0,0				
1104	0.0	0.0	0.01	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-1.60e-04	-1.23e-04	-1.23e-04	82,86,91
	40.1	0.0	0.01	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1105	0.0	5.71e-03	3.14e-03	6.10e-03	81,81,92	0.0	0.0	0.0	0,0,0	-3.00e-03	-2.51e-03	-2.31e-03	81,87,92
	40.0	5.04e-03	2.80e-03	6.05e-03	82,82,92	0.0	0.0	0.0	0,0,0				
1106	0.0	0.0	0.07	0.0	0,85,0	0.0	0.0	0.0	0,0,0	2.71e-04	2.71e-04	2.71e-04	79,86,91
	40.1	0.0	0.07	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
1107	0.0	4.33e-04	2.63e-04	1.71e-04	83,83,92	0.0	0.0	0.0	0,0,0	-1.73e-03	-1.47e-03	-1.37e-03	81,87,92
	41.5	4.35e-04	2.62e-04	2.68e-04	85,85,92	0.0	0.0	0.0	0,0,0				
1108	0.0	4.42e-03	7.18e-03	4.12e-03	81,81,92	0.0	0.0	0.0	0,0,0	-2.28e-03	-2.06e-03	-1.97e-03	81,87,92
	40.1	7.93e-04	1.41e-03	3.78e-04	82,79,92	0.0	0.0	0.0	0,0,0				
1109	0.0	7.86e-03	0.01	8.01e-03	85,81,92	0.0	0.0	0.0	0,0,0	-2.79e-03	-1.93e-03	-1.78e-03	85,90,92
	40.1	4.02e-03	6.86e-03	3.88e-03	85,81,92	0.0	0.0	0.0	0,0,0				
1110	0.0	8.65e-04	5.24e-04	6.52e-04	83,83,91	0.0	0.0	0.0	0,0,0	-1.53e-03	-1.25e-03	-1.14e-03	81,87,92
	41.5	8.12e-04	4.93e-04	6.37e-04	85,85,92	0.0	0.0	0.0	0,0,0				
1111	0.0	0.03	0.02	0.04	85,85,92	0.0	0.0	0.0	0,0,0	4.87e-03	3.87e-03	3.66e-03	85,90,92
	40.1	0.04	0.02	0.04	85,85,92	0.0	0.0	0.0	0,0,0				
1112	0.0	0.0	5.99e-03	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-1.23e-04	-1.23e-04	-1.23e-04	79,86,91
	40.1	0.0	8.81e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1113	0.0	0.0	0.08	0.0	0,85,0	0.0	0.0	0.0	0,0,0	4.36e-04	4.36e-04	4.36e-04	79,86,91
	40.1	0.0	0.08	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
1114	0.0	3.73e-04	2.40e-04	7.51e-05	83,81,91	0.0	0.0	0.0	0,0,0	-1.70e-03	-1.45e-03	-1.34e-03	81,87,92
	41.5	3.53e-04	4.78e-04	2.03e-04	85,81,92	0.0	0.0	0.0	0,0,0				
1115	0.0	4.28e-03	0.01	3.74e-03	81,81,92	0.0	0.0	0.0	0,0,0	-2.00e-03	-1.82e-03	-1.75e-03	81,87,92
	40.1	6.17e-03	0.02	6.38e-03	82,81,92	0.0	0.0	0.0	0,0,0				
1116	0.0	7.25e-03	0.01	7.18e-03	85,81,92	0.0	0.0	0.0	0,0,0	-2.63e-03	-1.79e-03	-1.64e-03	85,90,92
	40.1	3.34e-03	5.09e-03	3.12e-03	82,81,92	0.0	0.0	0.0	0,0,0				
1117	0.0	7.32e-04	4.41e-04	5.16e-04	83,83,91	0.0	0.0	0.0	0,0,0	-1.50e-03	-1.23e-03	-1.13e-03	81,87,92
	41.5	6.48e-04	3.92e-04	4.63e-04	85,83,92	0.0	0.0	0.0	0,0,0				
1118	0.0	0.06	0.04	0.07	85,85,92	0.0	0.0	0.0	0,0,0	3.66e-03	2.77e-03	2.59e-03	85,90,92
	40.1	0.05	0.03	0.05	85,85,92	0.0	0.0	0.0	0,0,0				
1119	0.0	1.70e-03	8.26e-03	2.16e-03	81,82,92	0.0	0.0	0.0	0,0,0	-1.44e-04	-1.44e-04	-1.44e-04	79,86,91
	40.1	7.85e-04	7.68e-03	2.86e-04	83,83,91	0.0	0.0	0.0	0,0,0				
1120	0.0	0.0	0.09	0.0	0,85,0	0.0	0.0	0.0	0,0,0	1.01e-03	8.97e-04	8.69e-04	83,88,91
	40.1	0.0	0.08	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
1121	0.0	2.93e-04	7.83e-04	0.0	83,81,0	0.0	0.0	0.0	0,0,0	-1.67e-03	-1.42e-03	-1.32e-03	81,87,92
	41.5	2.54e-04	1.03e-03	0.0	85,81,0	0.0	0.0	0.0	0,0,0				
1122	0.0	0.0	0.01	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.67e-03	-1.53e-03	-1.47e-03	81,87,92
	40.1	7.67e-03	0.02	8.10e-03	82,81,92	0.0	0.0	0.0	0,0,0				
1123	0.0	6.64e-03	9.38e-03	6.18e-03	85,81,92	0.0	0.0	0.0	0,0,0	-2.45e-03	-1.63e-03	-1.50e-03	85,90,92
	40.1	3.67e-03	6.12e-03	3.26e-03	82,79,92	0.0	0.0	0.0	0,0,0				
1124	0.0	5.97e-04	3.56e-04	3.80e-04	83,83,91	0.0	0.0	0.0	0,0,0	-1.48e-03	-1.21e-03	-1.11e-03	81,87,92
	41.5	4.90e-04	3.03e-04	2.97e-04	83,83,91	0.0	0.0	0.0	0,0,0				
1125	0.0	0.12	0.07	0.13	85,85,92	0.0	0.0	0.0	0,0,0	4.07e-03	3.15e-03	2.96e-03	85,90,92
	40.1	0.07	0.04	0.07	85,85,92	0.0	0.0	0.0	0,0,0				
1126	0.0	1.09e-03	1.22e-03	1.45e-03	79,81,91	0.0	0.0	0.0	0,0,0	-5.33e-04	-5.33e-04	-5.32e-04	83,88,91
	40.1	3.92e-03	5.32e-03	4.31e-03	83,83,91	0.0	0.0	0.0	0,0,0				
1127	0.0	0.0	0.07	0.0	0,85,0	0.0	0.0	0.0	0,0,0	1.44e-03	1.20e-03	1.14e-03	83,88,91
	40.1	0.0	0.07	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
1128	0.0	2.00e-04	1.34e-03	0.0	83,81,0	0.0	0.0	0.0	0,0,0	-1.65e-03	-1.40e-03	-1.30e-03	81,87,92
	41.5	1.54e-04	1.59e-03	0.0	85,81,0	0.0	0.0	0.0	0,0,0				
1129	0.0	0.0	0.02	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.48e-03	-1.36e-03	-1.32e-03	81,87,92
	40.1	5.71e-03	0.02	6.05e-03	81,82,92	0.0	0.0	0.0	0,0,0				
1130	0.0	4.46e-03	8.96e-03	2.93e-03	85,79,92	0.0	0.0	0.0	0,0,0	-2.28e-03	-1.50e-03	-1.37e-03	85,90,92
	40.1	2.71e-03	7.31e-03	1.04e-03	82,79,92	0.0	0.0	0.0	0,0,0				
1131	0.0	4.59e-04	3.00e-04	2.45e-04	83,81,91	0.0	0.0	0.0	0,0,0	-1.45e-03	-1.20e-03	-1.09e-03	81,87,92
	41.5	3.44e-04	5.95e-04	1.43e-04	83,81,91	0.0	0.0	0.0	0,0,0				
1132	0.0	0.23	0.13	0.24	85,85,92	0.0	0.0	0.0	0,0,0	6.38e-03	5.13e-03	4.86e-03	85,90,92
	40.1	0.12	0.07	0.12	85,85,92	0.0	0.0	0.0	0,0,0				
1133	0.0	0.02	0.01	0.02	82,82,92	0.0	0.0	0.0	0,0,0	-1.24e-03	-1.19e-03	-1.18e-03	85,90,92
	40.1	0.02	0.02	0.03	85,85,92	0.0	0.0	0.0	0,0,0				
1134	0.0	0.0	0.03	0.0	0,85,0	0.0	0.0	0.0	0,0,0	9.90e-04	8.42e-04	8.05e-04	83,88,91
	40.1	0.0	0.04	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
1135	0.0	1.15e-04	1.88e-03	0.0	83,81,0	0.0	0.0	0.0	0,0,0	-1.62e-03	-1.37e-03	-1.28e-03	81,87,92
	41.5	4.92e-05	2.13e-03	0.0	83,81,0	0.0	0.0	0.0	0,0,0				
1136	0.0	3.23e-04	9.65e-04	1.81e-04	83,81,91	0.0	0.0	0.0	0,0,0	-1.43e-03	-1.18e-03	-1.08e-03	81,87,92
	41.5	2.00e-04	1.22e-03	0.0	83,81,0	0.0	0.0	0.0	0,0,0				
1137	0.0	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0	9.49e-03	7.79e-03	7.42e-03	85,90,92
	40.1	0.03	0.02	0.03	85,85,92	0.0	0.0	0.0	0,0,0				
1138	0.0	0.01	7.27e-03	0.02	82,82,92	0.0	0.0	0.0	0,0,0	-4.73e-04	-4.57e-04	-4.52e-04	83,88,91
	40.1	6.82e-03	3.99e-03	8.25e-03	81,81,92	0.0	0.0	0.0	0,0,0				
1139	0.0	0.0	0.04	0.0	0,85,0	0.0	0.0	0.0	0,0,0	4.73e-04	4.38e-04	4.29e-04	83,88,91
	40.1	0.0	0.04	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
1140	0.0	0.0	2.40e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.59e-03	-1.35e-03	-1.26e-03	81,87,92
	41.5	0.0	2.62e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
1141	0.0	2.07e-04	1.57e-03	0.0	83,81,0	0.0	0.0	0.0	0,0,0	-1.41e-03	-1.16e-03	-1.06e-03	81,87,92
	41.5	7.81e-05	1.79e-03	0.0	83,81,0	0.0	0.0	0.0	0,0,0				

	41.5	0.0	3.07e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
1147	0.0	1.18e-04	2.10e-03	0.0	83,81,0	0.0	0.0	0.0	0,0,0	-1.39e-03	-1.15e-03	-1.05e-03	81,87,92
	41.5	0.0	2.29e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
1148	0.0	0.01	7.37e-03	0.01	85,85,92	0.0	0.0	0.0	0,0,0	0.01	8.98e-03	8.54e-03	85,90,92
	40.1	8.73e-03	5.39e-03	8.14e-03	83,83,91	0.0	0.0	0.0	0,0,0				
1149	0.0	0.01	7.28e-03	0.02	81,81,92	0.0	0.0	0.0	0,0,0	8.89e-04	7.89e-04	7.49e-04	81,87,92
	40.1	0.01	6.22e-03	0.01	81,81,92	0.0	0.0	0.0	0,0,0				
1150	0.0	0.03	0.02	0.03	85,85,92	0.0	0.0	0.0	0,0,0	0.01	8.73e-03	8.32e-03	85,90,92
	40.1	0.05	0.03	0.05	85,85,92	0.0	0.0	0.0	0,0,0				
1151	0.0	0.02	0.01	0.02	83,83,91	0.0	0.0	0.0	0,0,0	9.47e-03	7.77e-03	7.40e-03	85,90,92
	40.1	0.03	0.02	0.03	85,85,92	0.0	0.0	0.0	0,0,0				
1152	0.0	0.0	0.04	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.96e-04	-7.18e-05	-4.65e-05	85,90,92
	40.1	0.0	0.04	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1153	0.0	0.0	3.28e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.54e-03	-1.31e-03	-1.22e-03	81,87,92
	41.5	0.0	3.46e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
1154	0.0	0.0	2.54e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.37e-03	-1.13e-03	-1.04e-03	81,87,92
	41.5	0.0	2.71e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
1155	0.0	9.30e-03	0.02	8.94e-03	85,81,92	0.0	0.0	0.0	0,0,0	0.01	8.96e-03	8.52e-03	85,90,92
	40.1	1.10e-03	4.92e-03	0.0	83,81,0	0.0	0.0	0.0	0,0,0				
1156	0.0	4.93e-04	1.21e-03	0.0	85,81,0	0.0	0.0	0.0	0,0,0	4.03e-04	3.41e-04	3.16e-04	81,87,92
	40.1	2.16e-03	3.71e-03	2.08e-03	85,81,92	0.0	0.0	0.0	0,0,0				
1157	0.0	0.02	0.01	0.03	85,85,92	0.0	0.0	0.0	0,0,0	9.99e-03	8.23e-03	7.84e-03	85,90,92
	40.1	0.04	0.02	0.04	85,85,92	0.0	0.0	0.0	0,0,0				
1158	0.0	0.02	0.01	0.02	83,83,91	0.0	0.0	0.0	0,0,0	9.67e-03	7.93e-03	7.56e-03	85,90,92
	40.1	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0				
1159	0.0	0.04	0.02	0.04	85,85,92	0.0	0.0	0.0	0,0,0	0.01	9.61e-03	9.16e-03	85,90,92
	40.1	0.06	0.03	0.06	85,85,92	0.0	0.0	0.0	0,0,0				
1160	0.0	0.0	0.04	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-3.88e-04	-2.23e-04	-1.88e-04	85,90,92
	40.1	0.0	0.04	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1161	0.0	0.0	3.64e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.51e-03	-1.29e-03	-1.20e-03	81,87,92
	41.5	0.0	3.79e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
1162	0.0	0.0	2.91e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.35e-03	-1.12e-03	-1.02e-03	81,87,92
	41.5	0.0	3.06e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
1163	0.0	1.20e-03	6.40e-04	9.32e-04	85,85,92	0.0	0.0	0.0	0,0,0	-1.26e-04	-1.27e-04	-1.27e-04	83,88,91
	40.1	3.86e-03	4.67e-03	4.67e-03	85,81,92	0.0	0.0	0.0	0,0,0				
1164	0.0	0.02	0.01	0.02	85,85,92	0.0	0.0	0.0	0,0,0	9.65e-03	7.94e-03	7.56e-03	85,90,92
	40.1	0.03	0.02	0.03	85,85,92	0.0	0.0	0.0	0,0,0				
1165	0.0	0.0	0.04	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-5.40e-04	-3.44e-04	-3.00e-04	85,90,92
	40.1	0.0	0.04	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1166	0.0	0.0	3.96e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.49e-03	-1.26e-03	-1.18e-03	81,87,92
	41.5	0.0	4.09e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
1167	0.0	0.0	3.21e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.33e-03	-1.10e-03	-1.01e-03	81,87,92
	41.5	0.0	3.34e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
1168	0.0	1.68e-03	9.16e-04	1.53e-03	85,85,92	0.0	0.0	0.0	0,0,0	-1.32e-04	-1.29e-04	-1.28e-04	83,88,91
	40.1	1.73e-03	9.36e-04	2.01e-03	83,83,91	0.0	0.0	0.0	0,0,0				
1169	0.0	0.0	0.04	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-6.74e-04	-4.50e-04	-3.99e-04	85,90,92
	40.1	0.0	0.04	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1170	0.0	0.0	4.23e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.46e-03	-1.24e-03	-1.16e-03	81,87,92
	41.5	0.0	4.34e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
1171	0.0	0.0	3.47e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.31e-03	-1.09e-03	-9.99e-04	81,87,92
	41.5	0.0	3.58e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
1172	0.0	2.15e-03	1.20e-03	2.10e-03	85,85,92	0.0	0.0	0.0	0,0,0	-1.92e-04	-1.90e-04	-1.89e-04	83,88,91
	40.1	1.42e-03	8.31e-04	1.39e-03	83,83,91	0.0	0.0	0.0	0,0,0				
1173	0.0	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-8.08e-04	-5.55e-04	-4.97e-04	85,90,92
	40.1	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1174	0.0	0.0	4.46e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.43e-03	-1.22e-03	-1.14e-03	81,87,92
	41.5	0.0	4.56e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
1175	0.0	0.0	3.70e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.29e-03	-1.07e-03	-9.87e-04	81,87,92
	41.5	0.0	3.78e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
1176	0.0	2.58e-03	1.49e-03	2.59e-03	85,85,92	0.0	0.0	0.0	0,0,0	-2.33e-04	-2.30e-04	-2.29e-04	83,88,91
	40.1	1.78e-03	1.08e-03	1.90e-03	82,82,92	0.0	0.0	0.0	0,0,0				
1177	0.0	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-9.59e-04	-6.73e-04	-6.05e-04	85,90,92
	40.1	0.0	0.03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1178	0.0	0.0	4.66e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.41e-03	-1.20e-03	-1.12e-03	81,87,92
	41.5	0.0	4.75e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
1179	0.0	0.0	3.89e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.28e-03	-1.06e-03	-9.75e-04	81,87,92
	41.5	0.0	3.94e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
1180	0.0	2.48e-03	1.54e-03	2.88e-03	85,85,92	0.0	0.0	0.0	0,0,0	-2.67e-04	-2.64e-04	-2.64e-04	83,88,91
	40.1	2.72e-03	1.64e-03	3.00e-03	82,82,92	0.0	0.0	0.0	0,0,0				
1181	0.0	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0	-1.15e-03	-8.20e-04	-7.41e-04	85,90,92
	40.1	0.0	0.02	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1182	0.0	0.0	4.81e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.38e-03	-1.18e-03	-1.10e-03	81,87,92
	41.5	0.0	4.88e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
1183	0.0	0.0	4.04e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.26e-03	-1.05e-03	-9.64e-04	81,87,92
	41.5	0.0	4.07e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
1184	0.0	5.71e-03	3.23e-03	6.94e-03	85,85,92	0.0	0.0	0.0	0,0,0	-3.31e-04	-3.29e-04	-3.29e-04	83,88,91
	40.1	3.41e-03	2.08e-03	3.76e-03	82,82,92	0.0	0.0	0.0	0,0,0				
1185	0.0	1.03e-03	9.18e-03	0.0	85,83,0	0.0	0.0	0.0	0,0,0	-1.41e-03	-1.02e-03	-9.24e-04	85,90,92
	40.1	5.70e-03	0.02	3.70e-03	85,83,92	0.0	0.0	0.0	0,0,0				
1186	0.0	0.0	4.91e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.36e-03	-1.16e-03	-1.08e-03	81,87,92
	41.5	0.0	4.96e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
1187	0.0	0.0	4.16e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.24e-03	-1.04e-03	-9.53e-04	81,87,92
	41.5	0.0	4.17e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
1188	0.0	9.48e-03	5.21e-03	0.01	85,85,92	0.0	0.0	0.0	0,0,0	-6.18e-04	-6.16e-04	-6.15e-04	83,88,91
	40.1	4.41e-03	2.70e-03	4.94e-03	85,85,92	0.0	0.0	0.0	0,0,0				
1189	0.0	3.81e-03	2.07e-03	3.32e-03	85,85,91	0.0	0.0	0.0	0,0,0	-1.79e-03	-1.30e-03	-1.18e-03	85,90,92
	40.1	5.62e-03	3.45e-03	4.89e-03	83,79,91	0.0	0.0	0.0	0,0,0				
1190	0.0	0.0	4.96e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.34e-03	-1.14e-03	-1.06e-03	81,87,92
	41.5	0.0	4.98e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
1191	0.0	0.0	4.24e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0	-1.23e-03	-1.02e-03	-9.42e-04	81,87,92
	41.5	0.0	4.21e-03	0.0	0,81,0	0.0	0.0	0.0	0,0,0				
1192	0.0	8.96e-03	5.20e-03	0.01	85,85,92	0.0	0.0	0.0	0,0,0	-1.44e-03	-1.39e-03	-1.37e-03	85,87,92
	40.1	0.02	0.01	0.03	85,85,92	0.0	0.0	0.0	0,0,0				
1193	0.0	5.39e-03	3.08e-03	4.07e-03	85,85,92	0.0	0.0	0.0	0,0,0	-2.33e-03	-1.70e-03	-1.55e-03	85,90,92
	40.1	8.92e-03	4.77e-03	7.84e-03	85,85,92	0.0	0.0	0.0	0,0,0				
1194													

1298	0.0	3.69e-03	2.27e-03	2.90e-03	85,85,92	0.0	0.0	0.0	0,0,0	5.40e-04	2.45e-04	1.77e-04	85,90,92
	40.1	4.00e-03	2.43e-03	3.13e-03	85,85,92	0.0	0.0	0.0	0,0,0				
1299	0.0	0.0	0.01	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-1.03e-03	-8.86e-04	-8.29e-04	81,87,92
	41.5	0.0	0.01	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
1300	0.0	0.0	0.01	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-9.70e-04	-8.49e-04	-8.00e-04	81,87,92
	41.5	0.0	0.01	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
1301	0.0	3.25e-03	2.00e-03	2.56e-03	85,85,92	0.0	0.0	0.0	0,0,0	5.50e-04	2.52e-04	1.83e-04	85,90,92
	40.1	3.71e-03	2.24e-03	2.90e-03	85,85,92	0.0	0.0	0.0	0,0,0				
1302	0.0	0.0	0.01	0.0	0,85,0	0.0	0.0	0.0	0,0,0	-1.13e-03	-9.97e-04	-9.44e-04	81,87,92
	41.5	0.0	0.01	0.0	0,85,0	0.0	0.0	0.0	0,0,0				
1303	0.0	2.73e-03	1.68e-03	2.18e-03	85,85,92	0.0	0.0	0.0	0,0,0	5.66e-04	2.61e-04	1.91e-04	85,90,92
	40.1	3.29e-03	1.96e-03	2.58e-03	85,85,92	0.0	0.0	0.0	0,0,0				
1304	0.0	2.17e-03	1.33e-03	1.76e-03	85,85,92	0.0	0.0	0.0	0,0,0	5.90e-04	2.76e-04	2.04e-04	85,90,92
	40.1	2.78e-03	1.63e-03	2.20e-03	85,85,92	0.0	0.0	0.0	0,0,0				
1305	0.0	1.63e-03	9.89e-04	1.36e-03	85,85,92	0.0	0.0	0.0	0,0,0	6.23e-04	2.96e-04	2.20e-04	85,90,92
	40.1	2.21e-03	1.27e-03	1.78e-03	85,85,92	0.0	0.0	0.0	0,0,0				
1306	0.0	1.14e-03	6.77e-04	9.90e-04	85,85,92	0.0	0.0	0.0	0,0,0	6.65e-04	3.21e-04	2.41e-04	85,90,92
	40.1	1.63e-03	9.20e-04	1.36e-03	85,85,92	0.0	0.0	0.0	0,0,0				
1307	0.0	7.51e-04	4.21e-04	6.78e-04	85,85,92	0.0	0.0	0.0	0,0,0	7.12e-04	3.50e-04	2.65e-04	85,90,92
	40.1	1.23e-03	6.43e-04	1.05e-03	85,85,92	0.0	0.0	0.0	0,0,0				
1308	0.0	7.05e-04	1.24e-03	6.21e-04	85,83,92	0.0	0.0	0.0	0,0,0	7.63e-04	3.80e-04	2.91e-04	85,90,92
	40.1	1.04e-03	1.76e-03	9.36e-04	85,83,92	0.0	0.0	0.0	0,0,0				
1309	0.0	4.78e-04	2.57e-03	3.73e-04	82,83,92	0.0	0.0	0.0	0,0,0	8.13e-04	4.10e-04	3.16e-04	85,90,92
	40.1	6.18e-04	2.76e-03	5.87e-04	82,83,92	0.0	0.0	0.0	0,0,0				
1310	0.0	2.10e-04	3.16e-03	0.0	81,83,0	0.0	0.0	0.0	0,0,0	8.58e-04	4.38e-04	3.40e-04	85,90,92
	40.1	2.92e-04	3.08e-03	0.0	81,83,0	0.0	0.0	0.0	0,0,0				
1311	0.0	0.0	3.16e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0	8.96e-04	4.61e-04	3.60e-04	85,90,92
	40.1	0.0	2.92e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1312	0.0	9.10e-05	2.80e-03	0.0	85,83,0	0.0	0.0	0.0	0,0,0	9.26e-04	4.81e-04	3.77e-04	85,90,92
	40.1	0.0	2.50e-03	0.0	0,83,0	0.0	0.0	0.0	0,0,0				
1313	0.0	2.37e-04	2.50e-03	0.0	85,79,0	0.0	0.0	0.0	0,0,0	9.48e-04	4.96e-04	3.91e-04	85,90,92
	40.1	0.0	2.47e-03	0.0	0,79,0	0.0	0.0	0.0	0,0,0				
1314	0.0	2.79e-04	2.52e-03	0.0	85,79,0	0.0	0.0	0.0	0,0,0	9.63e-04	5.07e-04	4.02e-04	85,90,92
	40.1	8.13e-05	2.52e-03	0.0	85,79,0	0.0	0.0	0.0	0,0,0				
1315	0.0	2.31e-04	2.59e-03	0.0	85,79,0	0.0	0.0	0.0	0,0,0	9.73e-04	5.16e-04	4.10e-04	85,90,92
	40.1	1.38e-04	2.62e-03	0.0	85,79,0	0.0	0.0	0.0	0,0,0				
1316	0.0	7.88e-05	2.72e-03	0.0	85,79,0	0.0	0.0	0.0	0,0,0	9.78e-04	5.22e-04	4.16e-04	85,90,92
	40.1	7.01e-05	2.79e-03	0.0	85,79,0	0.0	0.0	0.0	0,0,0				
1317	0.0	0.0	2.93e-03	0.0	0,79,0	0.0	0.0	0.0	0,0,0	9.81e-04	5.26e-04	4.22e-04	85,90,92
	40.1	0.0	3.02e-03	0.0	0,79,0	0.0	0.0	0.0	0,0,0				
1318	0.0	0.0	3.18e-03	0.0	0,79,0	0.0	0.0	0.0	0,0,0	9.82e-04	5.31e-04	4.27e-04	85,90,92
	40.1	0.0	3.29e-03	0.0	0,79,0	0.0	0.0	0.0	0,0,0				
1319	0.0	0.0	3.45e-03	0.0	0,79,0	0.0	0.0	0.0	0,0,0	9.83e-04	5.35e-04	4.32e-04	85,90,92
	40.1	0.0	3.57e-03	0.0	0,79,0	0.0	0.0	0.0	0,0,0				
1320	0.0	0.0	3.73e-03	0.0	0,79,0	0.0	0.0	0.0	0,0,0	9.83e-04	5.40e-04	4.38e-04	85,90,92
	40.1	0.0	3.82e-03	0.0	0,79,0	0.0	0.0	0.0	0,0,0				
1321	0.0	0.0	3.95e-03	0.0	0,79,0	0.0	0.0	0.0	0,0,0	9.84e-04	5.45e-04	4.45e-04	85,90,92
	40.1	0.0	3.93e-03	0.0	0,79,0	0.0	0.0	0.0	0,0,0				
1322	0.0	0.0	3.99e-03	0.0	0,79,0	0.0	0.0	0.0	0,0,0	9.84e-04	5.51e-04	4.52e-04	85,90,92
	40.1	0.0	3.66e-03	0.0	0,79,0	0.0	0.0	0.0	0,0,0				
1323	0.0	0.0	3.56e-03	0.0	0,79,0	0.0	0.0	0.0	0,0,0	5.20e-04	5.52e-04	4.55e-04	85,90,92
	40.1	1.53e-04	4.25e-03	0.0	85,79,0	0.0	0.0	0.0	0,0,0				
1324	0.0	3.85e-04	2.53e-03	0.0	85,79,0	0.0	0.0	0.0	0,0,0	9.36e-04	5.23e-04	4.29e-04	85,90,92
	40.1	4.24e-03	7.60e-03	2.65e-03	85,85,92	0.0	0.0	0.0	0,0,0				
Trave		rRfck	rRfyk	rPfck		wR	wF	wP		dR	dF	dP	
		0.41	0.63	0.44		0.42	0.18	0.17		0.05	0.05	0.05	

VERIFICHE ELEMENTI PARETE E/O GUSCIO IN C.A.

Per le pareti in c.a., in ottemperanza al cap. 7 del DM 17-01-18, viene effettuata una doppia progettazione: sia come *Singolo Elemento* sia come *Parete Sismica* o *Parete Debolmente Armata*.

Per la progettazione come *Singolo Elemento* di ogni elemento vengono riportati il codice dello stato di verifica con le sigle **Ok e NV**, il rapporto x/d , la verifica per sollecitazioni ultime (verifica a compressione media gli sforzi membranali, verifica a presso-flessionale e verifica a sollecitazioni taglianti), gli sforzi membranali e flessionali, il quantitativo di armatura nella direzione principale e secondaria sia inferiore che superiore e il quantitativo di armatura a taglio.

Per la progettazione come *Parete Sismica* o *Parete Debolmente Armata* vengono riportate invece le caratteristiche geometriche della parete e delle zone dissipative (quest'ultime solo nel caso di parete sismica), i coefficienti di verifica a compressione assiale, pressoflessione e sollecitazioni taglianti.

Inoltre vengono riportate per ogni quota significativa l'armatura principale e secondaria, l'armatura in zona confinata (solo per parete sismica) e non confinata, l'armatura concentrata all'estremità (per pareti debolmente armate), lo sforzo assiale aggiuntivo per q superiore a 2 e i valori di inviluppo di taglio e momento. Per le pareti debolmente armate viene riportato anche lo stato di verifica relativo alla snellezza.

Le azioni derivate dall'analisi, in ogni combinazione di calcolo, sono elaborate come previsto al punto 7.4.4.5.1: traslazione del momento, incremento e variazione diagramma taglio, incremento e decremento sforzo assiale

La progettazione nel caso dei gusci viene effettuata una progettazione come *Singolo Elemento*, riportando in tabella il rapporto x/d , la verifica per sollecitazioni ultime, (verifica a compressione media gli sforzi membranali, verifica a presso-flessionale e verifica a sollecitazioni taglianti) di ogni elemento.

Per ogni elemento, viene riportata inoltre la maglia di armatura necessaria in relazione alle risultanze della progettazione dei nodi dell'elemento stesso. Le quantità di armature necessarie sono armature (disposte rispettivamente in direzione principale e secondaria, inferiore e superiore) distribuite nell'elemento ed espresse in centimetri quadri per sviluppo lineare pari ad un metro.

Nel caso dei gusci viene effettuata, inoltre, la verifica a punzonamento, riportando in tabella il codice dello stato di verifica, il coefficiente di verifica per piastre prive di armature a taglio lungo il perimetro resistente e lungo il perimetro del pilastro, coefficiente di incremento dovuto ai momenti flettenti, fattore di amplificazione per le fondazioni, il fattore di amplificazione dell'altezza utile per individuare il perimetro di verifica lungo il quale l'armatura a taglio non è richiesta, il quantitativo di armatura a punzonamento, il numero di serie di armature, il numero di braccia di armatura ed il riferimento alla combinazione più gravosa.

Simbologia adottata nelle tabelle di verifica

Per gli elementi con progettazione "*Singolo Elemento ...*" è presente una tabella con i simboli di seguito descritti:

Macro Guscio	Numero del macroelemento di tipo guscio (elementi non verticali contigui ed analoghi per proprietà)
Macro Setto	Numero del macroelemento di tipo setto (elementi verticali contigui ed analoghi per proprietà)
Spessore	Spessore della parete
Id Materiale	Codice del materiale assegnato all'elemento
Id Criterio	Codice del criterio di progetto assegnato all'elemento
Progettazione	Sigla tipo di Elemento: - Singolo Elemento; - Singolo Elemento FONDAZIONE; - Singolo Elemento NON DISSIPATIVO

Per gli elementi con progettazione "*Parete Sismica o Parete Debolmente Armata*" è presente una tabella con i simboli di seguito descritti:

Parete	Numero della PARETE SISMICA
Parete PDA	Numero della PARETE DEBOLMENTE ARMATA

H totale	Altezza complessiva della parete
Spessore	Spessore della parete
H critica	Altezza come da punto 7.4.4.5.1 per traslazione momento (solo in Parete Sismica)
H critica V	Altezza della zona dissipativa (solo in Parete Sismica)
L totale	Larghezza di base della parete
L confinata	Lunghezza della zona dissipativa (solo in Parete Sismica)
Verif. N	Verifica di cui al punto 7.4.4.5.1 compressione semplice
Verif. N-M	Verifica di cui al punto 7.4.4.5.1 pressoflessione
Fattore V	Fattore di amplificazione del taglio di cui al punto 7.4.4.5.1
Diagramma V	Diagramma elaborato per effetto modi superiori come da fig. 7.4.4
Verif. V	Verifica di cui al punto 7.4.4.5.1 taglio (compressione cls, trazione acciaio, scorrimento in zona critica) (solo in Parete Sismica)
Verifica Snellezza	Verifica di cui al punto 7.4.4.5.1 limitazione compressione per prevenire l'instabilità (solo in Parete Debolmente Armata)
Prog. composta	Sigla per la progettazione composta

Per le verifiche degli elementi con progettazione “Singolo Elemento ...” e Progettazione Composta è presente una tabella con i simboli di seguito descritti:

Nodo	numero del nodo
Stato	codice di verifica dell'elemento ok o NV
x/d	rapporto tra posizione dell'asse neutro e altezza utile alla rottura della sezione (per sola flessione)
V N/M	Verifica delle sollecitazioni Normali (momento e sforzo normale)
Ver. rid	Rapporto Nd/Nu (Nu ottenuto con riduzione del 25% di fcd)
Af pr+	quantità di armatura richiesta in direzione principale relativa alla faccia positiva (estradosso piastre) (valore derivante da calcolo o minimo normativo)
Af pr-	quantità di armatura richiesta in direzione principale relativa alla faccia negativa (intradosso piastre) (valore derivante da calcolo o minimo normativo)
Af sec+	quantità di armatura richiesta in direzione secondaria relativa alla faccia positiva (estradosso piastre) (valore derivante da calcolo o minimo normativo)
Af sec-	quantità di armatura richiesta in direzione secondaria relativa alla faccia negativa (intradosso piastre) (valore derivante da calcolo o minimo normativo)
Nz No Nzo	Sforzi membranali per pareti e/o setti verticali
Mz Mo Mzo	Sforzi flessionali per pareti e/o setti verticali
Nx Ny Nxy	Sforzi membranali per gusci orizzontali
Mx My Mxy	Sforzi flessionali per gusci orizzontali

Nodo	numero del nodo
Stato	codice di verifica dell'elemento ok o NV
Max tau	Tensione tangenziale Massima
Ver V pr	Verifica a taglio nella direzione principale lato calcestruzzo
Ver V sec	Verifica a taglio nella direzione secondaria lato calcestruzzo
Af V pr	Armatura nella direzione principale
V pr-	Verifica dell'armatura nella direzione principale
Af V sec	Armatura nella direzione secondaria
V sec-	Verifica dell'armatura nella direzione secondaria

Per le verifiche degli elementi con progettazione “Parete Sismica o Parete Debolmente Armata”, oltre alla tabella con le verifiche per gli elementi con progettazione “Singolo Elemento ...”, è presente una tabella con i simboli di seguito descritti:

Quota	Ascissa verticale di riferimento
Af conf.	Numero e diametro armatura presente in una zona confinata
Af std	Diametro e passo armatura in zona non confinata (doppia maglia)

Af estremi	Diametro dei ferri di estremità del pannello; se posto uguale 0, viene utilizzato il diametro standard
Af V (ori)	Diametro e passo armatura orizzontale (doppia maglia)
Ver. N	Rapporto tra azione di calcolo e resistenza a compressione (normalizzato a 1 in quanto da confrontare con 40% in CDB e 35 % in CDA)
Ver. N/M	Rapporto tra azione di calcolo e resistenza a pressoflessione
Ver. V acc(7)	Rapporto tra azione di calcolo e resistenza a taglio-trazione secondo paragrafo 7.4.4.5.1
Ver. V cls	Rapporto tra azione di calcolo e resistenza a taglio-compressione
Ver. V acc	Rapporto tra azione di calcolo e resistenza a taglio-trazione
Ver. V scorr.	Rapporto tra azione di calcolo e resistenza a taglio scorrimento
N add	Sforzo assiale di cui al punto 7.4.4.5.1 da sommare e sottrarre nelle verifiche quando q supera 2
N invil M invil	Inviluppo del Momento e Sforzo Normale come al punto 7.4.4.5.1 (informativo) (solo in Parete Sismica)

Quota	Ascissa verticale di riferimento
N v.N	Valore dello sforzo assiale per cui Ver. N attinge il massimo valore
N v.M/N, M v.M/N	Valore dello sforzo assiale e momento per cui Ver. N/M attinge il massimo valore
N v.M/N, M v.M/N Mo v.M/N	Valore dello sforzo assiale e dei momenti per cui Ver. N/M attinge il massimo valore (per le pareti estese debolmente armate)
N v.Vcls, V v.Vcls,	Valore dello sforzo assiale e taglio per cui Ver. V. cls attinge il massimo valore
N v.Vacc, M v.Vacc, V v.Vacc,	Valore dello sforzo assiale, momento e taglio per cui Ver. V. acc attinge il massimo valore
N v.Vscorr, M v.Vscorr, V v.Vscorr,	Valore dello sforzo assiale, momento e taglio per cui Ver. V. scorr.e attinge il massimo valore
N v.N	Valore dello sforzo assiale per cui Ver. N attinge il massimo valore
N v.M/N, M v.M/N	Valore dello sforzo assiale e momento per cui Ver. N/M attinge il massimo valore
N v.M/N, M v.M/N Mo v.M/N	Valore dello sforzo assiale e dei momenti per cui Ver. N/M attinge il massimo valore (per le pareti estese debolmente armate)
N v.Vcls, V v.Vcls,	Valore dello sforzo assiale e taglio per cui Ver. V. cls attinge il massimo valore

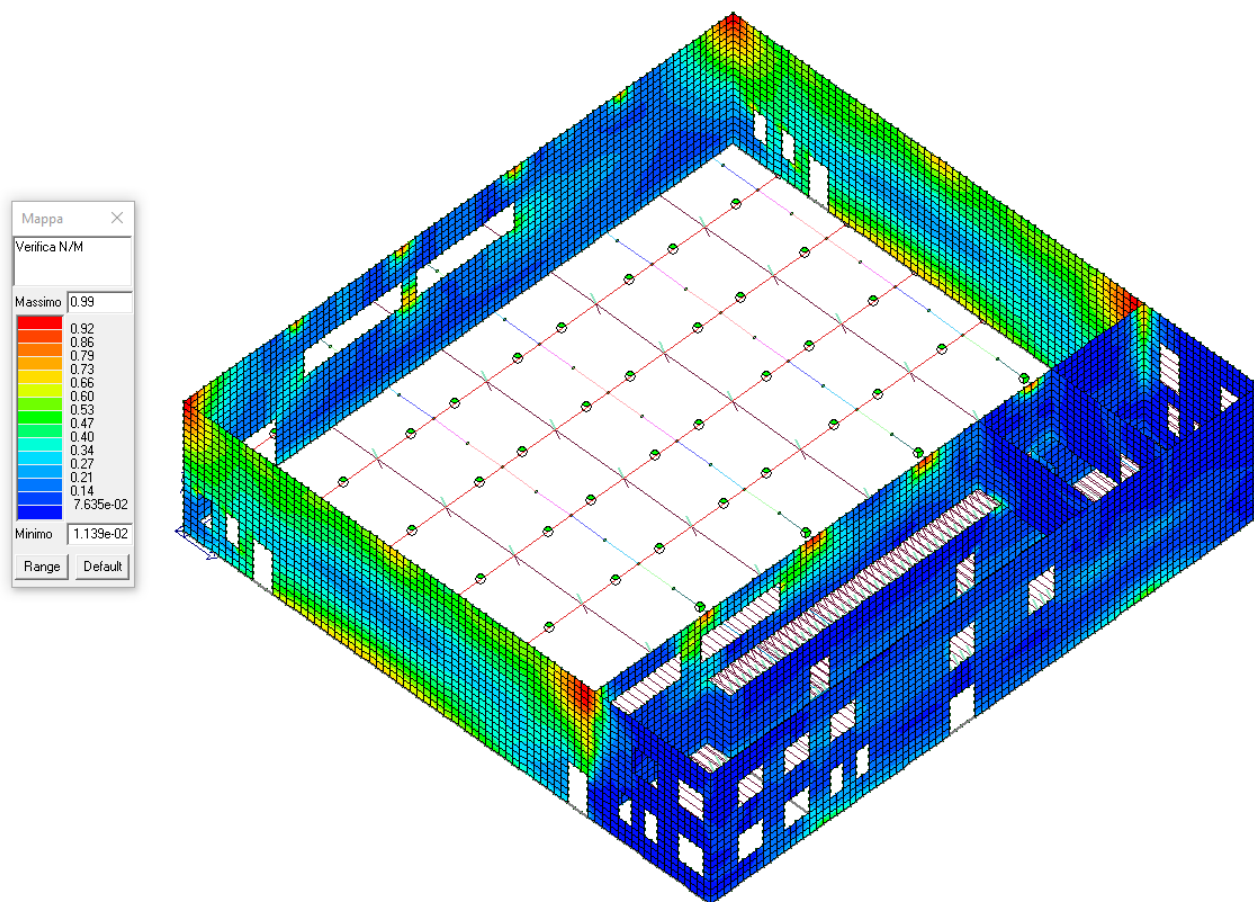
Quota	Ascissa verticale di riferimento
CtgT Vcls	Valore di ctg(teta) adottato nella verifica V compressione cls
Vrsd Vcls	Valore della resistenza a taglio trazione (armatura di calcolo)
Vrcd Vcls	Valore della resistenza a taglio compressione
CtgT Vacc	Valore di ctg(teta) adottato nella verifica V trazione armatura
Vrsd Vacc	Valore della resistenza a taglio trazione (armatura presente)
Vrcd Vacc	Valore della resistenza a taglio compressione
Vdd	Valore del contributo alla resistenza allo scorrimento come da [7.4.20]
Vid	Valore del contributo alla resistenza allo scorrimento come da [7.4.21]
A s.i.	Somma delle aree di armature
Incli.	Angolo di inclinazione delle armature
Dist.	Distanza alla base tra le armature inclinate

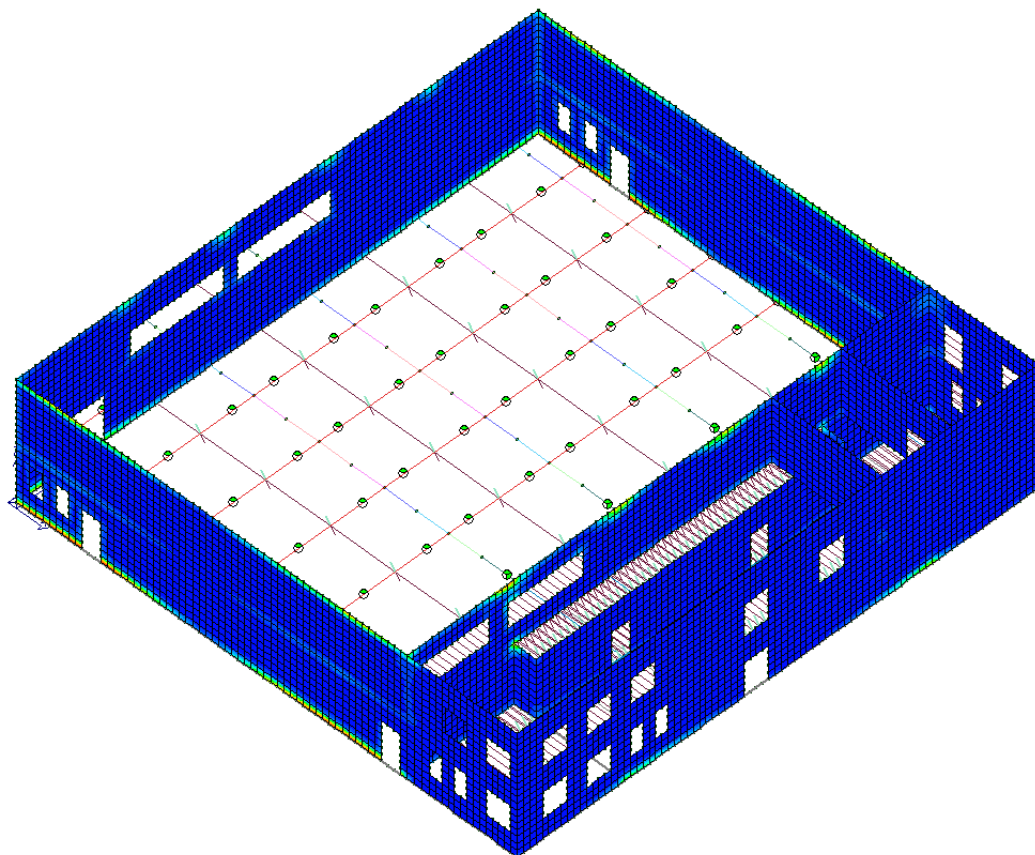
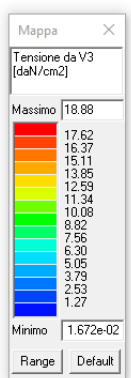
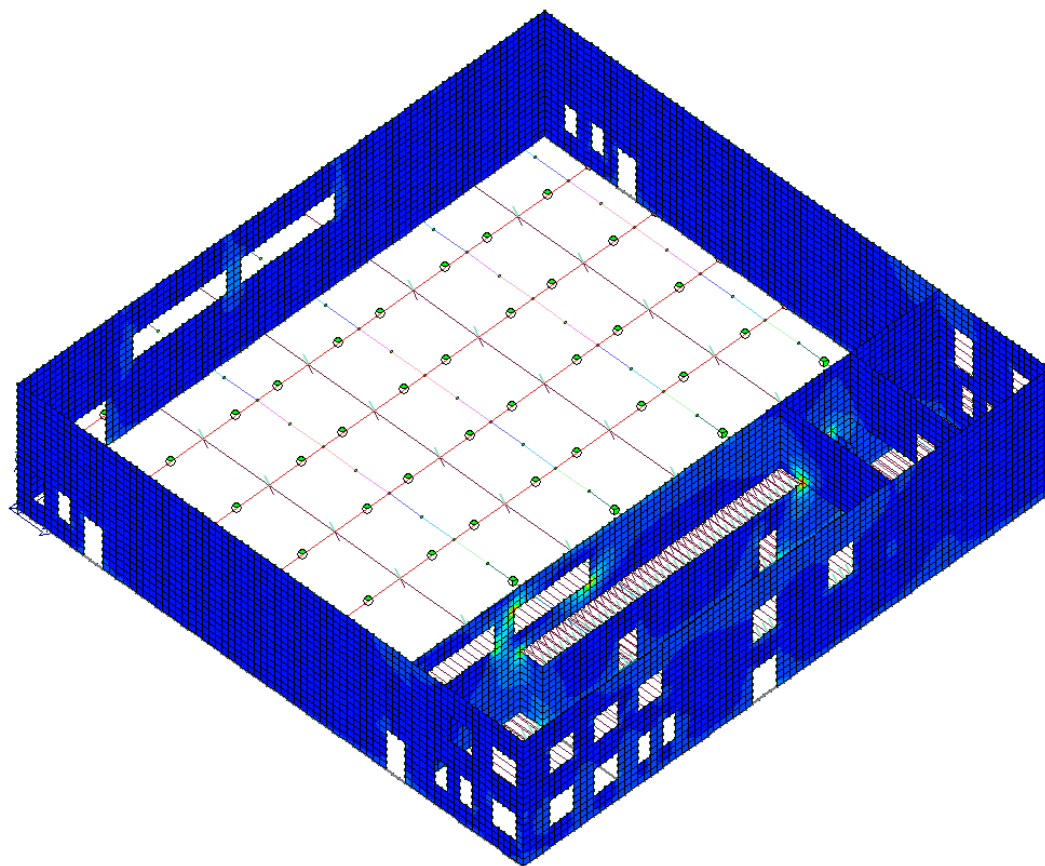
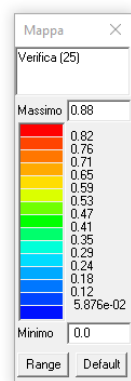
Quota	Ascissa verticale di riferimento
V[7.4.16]	Verifica a taglio-trazione dell'armatura dell'anima (7.4.16)
N M V	Sollecitazioni di calcolo della condizione più gravosa
Alfas	Rapporto di Taglio
Vrd,c	Resistenza a taglio degli elementi non armati
VRd,s	Resistenza a taglio nei confronti dello scorrimento
V[7.4.17]	Verifica a taglio-trazione dell'armatura dell'anima (7.4.17)

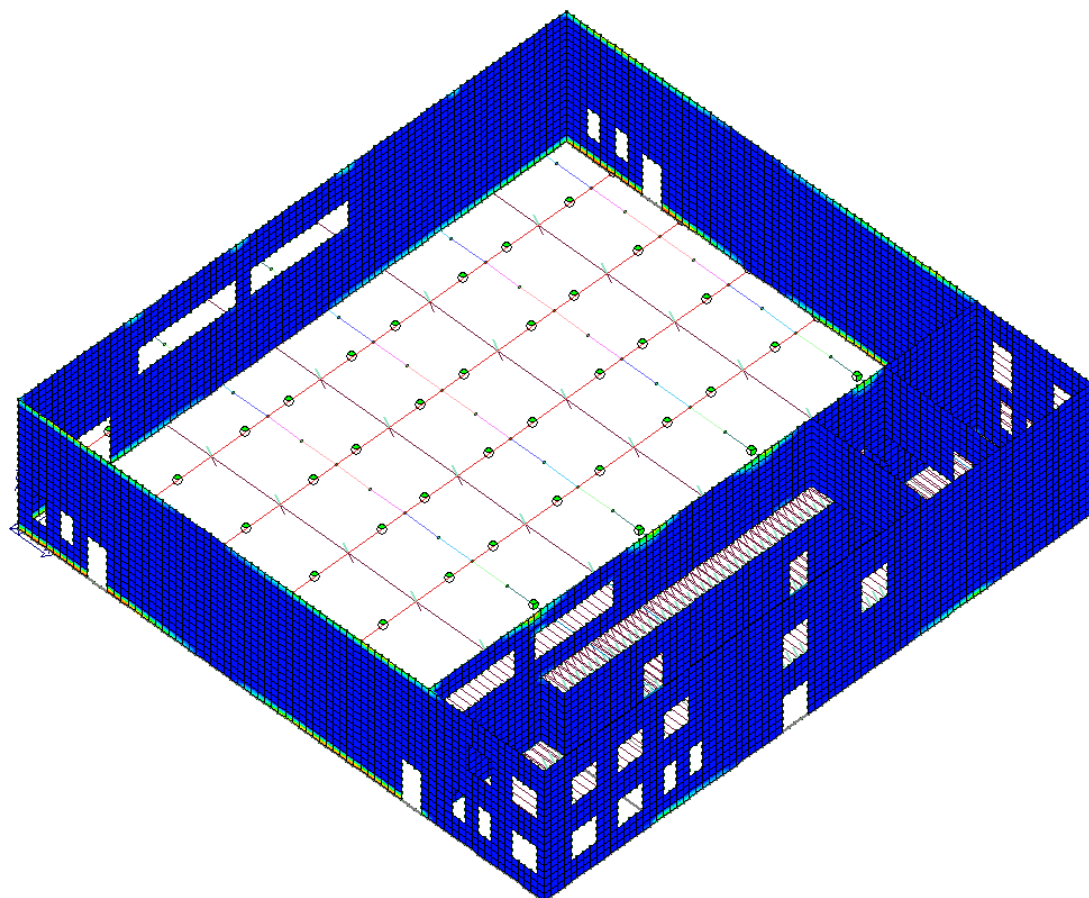
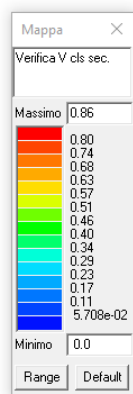
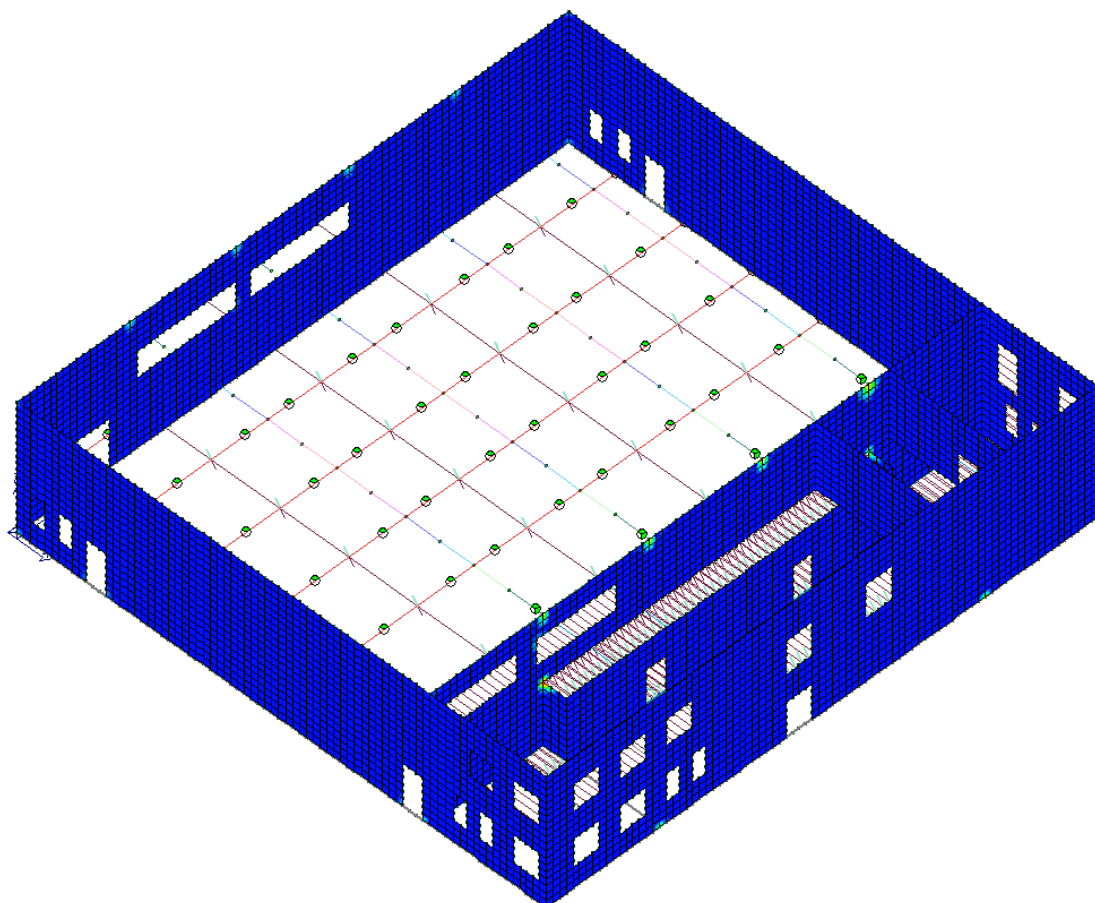
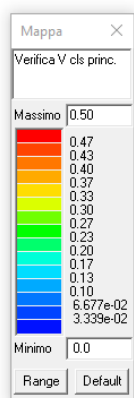
roH	Rapporto tra l'armatura orizzontale e l'area della sezione relativa di calcestruzzo
roV	Rapporto tra l'armatura verticale e l'area della sezione relativa di calcestruzzo
roN	Sforzo normale adimensionalizzato $N_{ed}/(b_w f_{yd})$

Per la verifica a **Punzonamento** è presente una tabella con i simboli di seguito descritti:

Nodo	numero del nodo
Stato	codice di verifica dell'elemento ok o NV
V. 6.47	Fattore di sicurezza per la verifica per piastre prive di armature a taglio lungo il perimetro resistente U1
V. 6.53	Fattore di sicurezza per la verifica per piastre prive di armature a taglio lungo il perimetro del pilastro U0
Beta	Fattore di incremento dovuto ai momenti flettenti
f. a fon	fattore di amplificazione per le fondazioni (solo per gusci di fondazione)
f. Uout	fattore di amplificazione dell'altezza utile per individuare il perimetro di verifica lungo il quale l'armatura a taglio non è richiesta
Aw tot	Quantitativo di armatura per la verifica di piastre munite di armatura (formula 6.52 dell'EC2)
Asw,min	Quantitativo minimo di armatura previsto dai dettagli costruttivi (formula 9.11 dell'EC2)
n. x serie	Numero di serie di armature
n.ser 0(R)	Numero di braccia delle armature in direzione 0 (o numero di braccia radiale)
n.ser 90	Numero di braccia delle armature in direzione 90 (solo se armatura cruciforme)
Rif. cmb	Riferimento combinazioni da cui si generano le verifiche più gravose







VERIFICHE S.L. ELEMENTI IN LEGNO

legenda tabella verifiche s.l. elementi in legno

Il programma consente la verifica dei seguenti tipi di elementi:

1. Aste
2. Travi
3. Pilastri

L'esito delle verifiche è espresso con un codice come di seguito indicato:

ok: verifica con esito positivo

NV: verifica con esito negativo

Simbologia adottata nelle tabelle di verifica

Le verifiche effettuate ai sensi delle NTC 2018 sono dettagliatamente riportate come da tabella seguente:

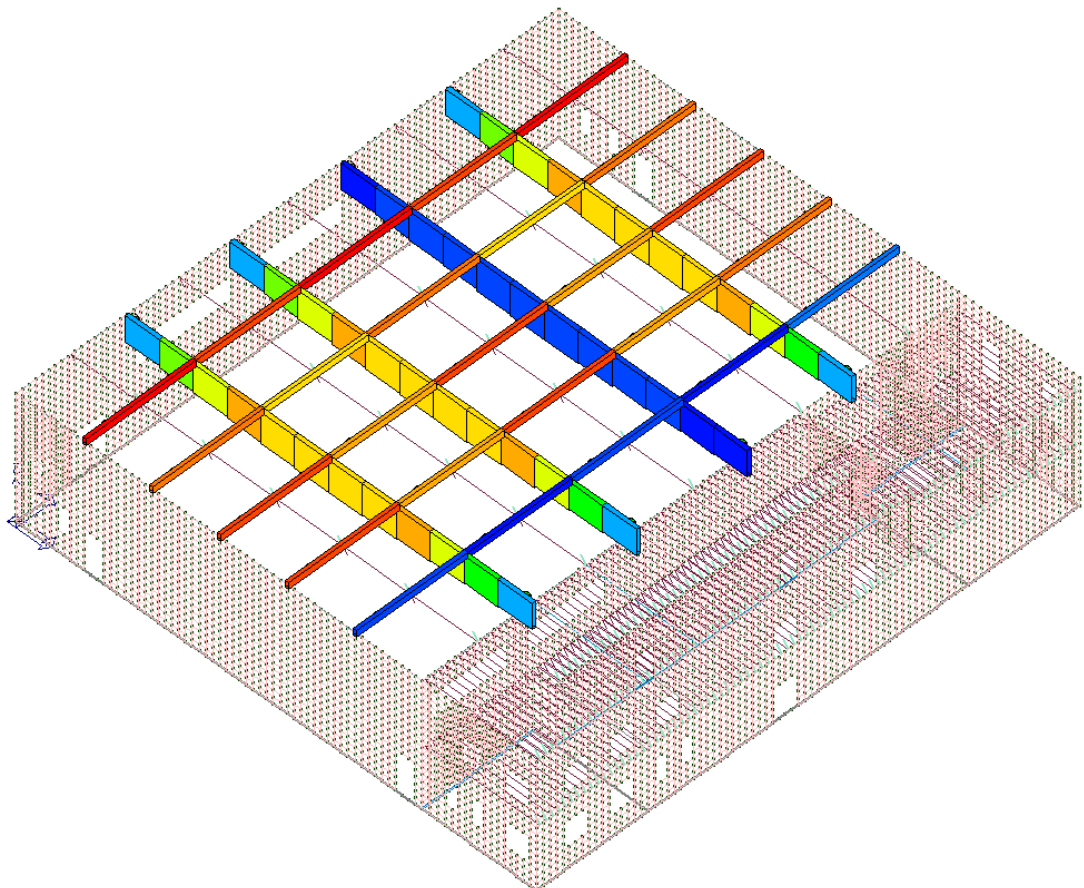
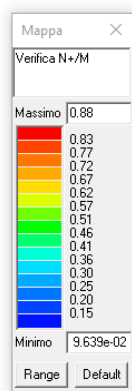
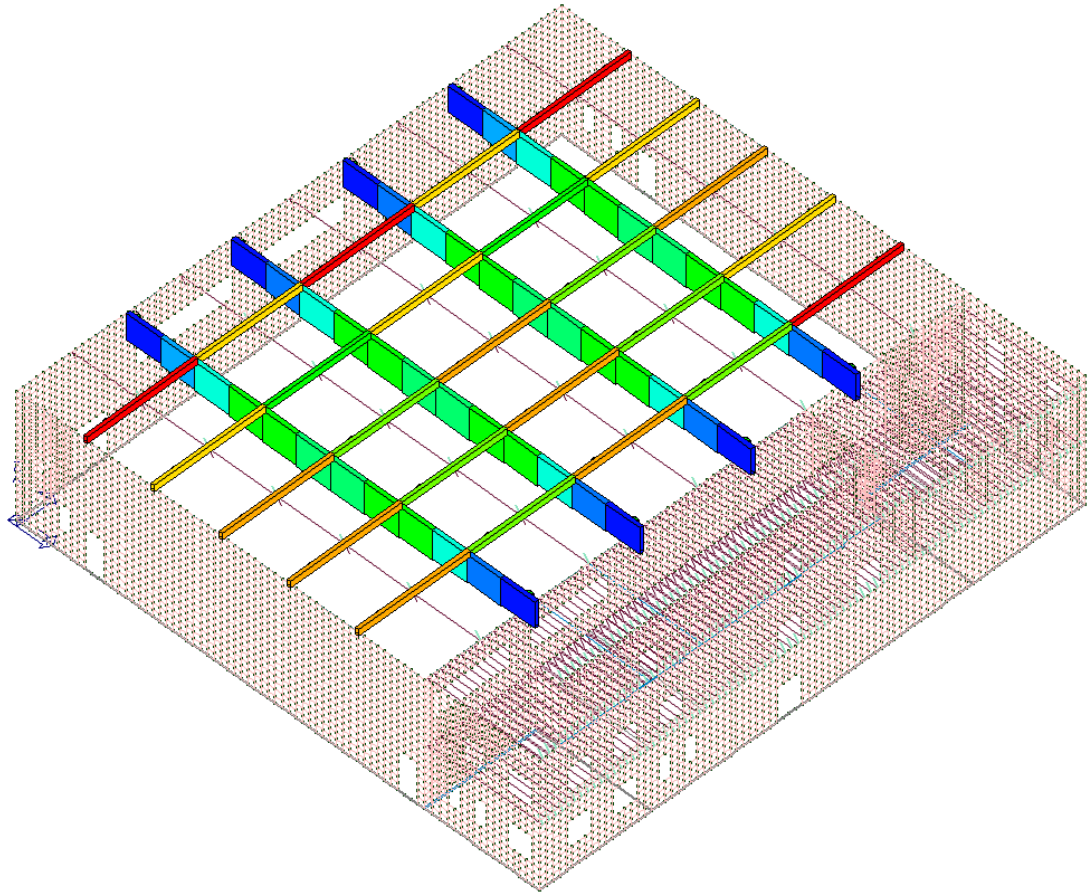
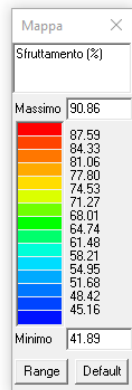
Elem.	Numero dell'elemento
Tipo	Codice di individuazione del tipo di elemento: Trave (T) , Pilastro (P) , Asta (A)
Stato	Codice della verifica: ok verificato, NV non verificato
Note	Numero della sezione (s) e del materiale (m) dell'archivio
Ver N+/M	Verifica come da formule 4.4.6a e 4.4.6b per tensoflessione, con i valori di km definiti nel par. 4.4.8.1.6
Ver N-/M	Verifica come da formule 4.4.7a e 4.4.7b per pressoflessione, con i valori di km definiti nel par. 4.4.8.1.6
Ver V/T	Verifica come da formula 4.4.10 (taglio torsione) con interazione ottenuta per quadratura del termine di taglio
Ver N(s)	Verifica instabilità a compressione come da par. 4.4.8.2.2
Kcy(z)	Fattore di instabilità Kcrit,c utilizzato nella formula 4.4.13, in funzione della snellezza relativa
Ver M(s)	Verifica instabilità laterale come da par. 4.4.8.2.1, effettuata in entrambi i piani principali y e z
Kcrit (y)/(z)	Fattore di instabilità laterale utilizzato nella formula 4.4.11 rispettivamente per la flessione y e z
w _{net R}	Massima deformazione in combinazione rara (F frequente, P quasi permanente)
w _{net Ri}	Massima deformazione in combinazione rara (F frequente, P quasi permanente) valutata a tempo infinito
kdef	Fattore di deformazione dell' elemento
Rif. cmb	Numero della combinazione in cui si è attinto il valore riportato per le verifiche

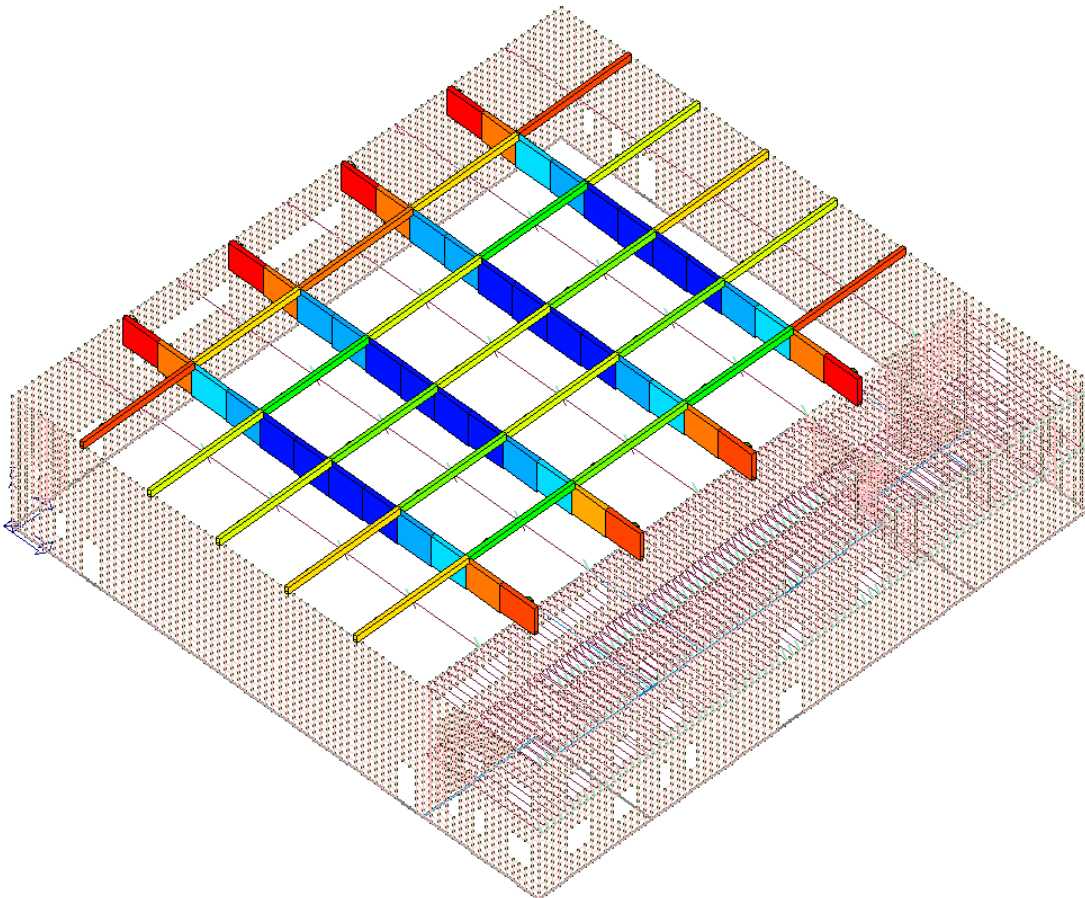
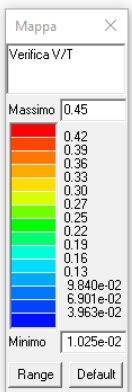
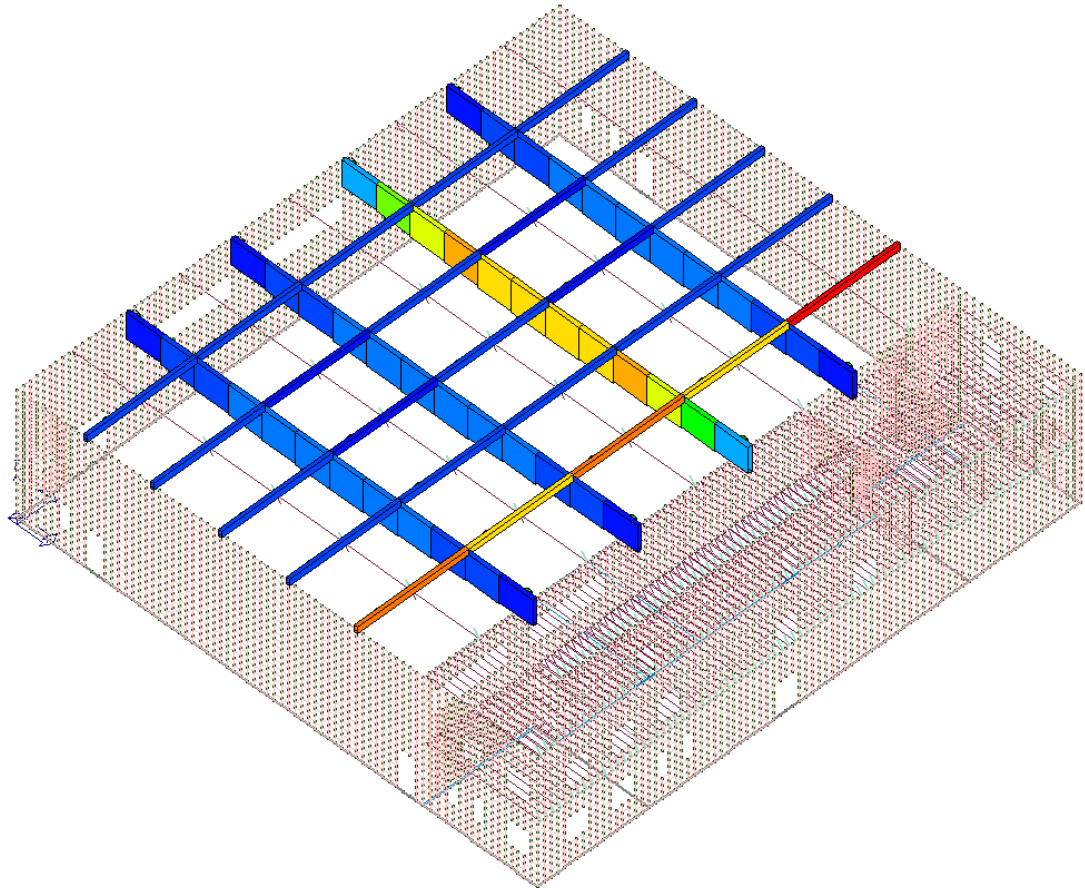
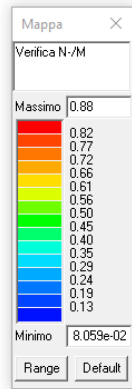
Le verifiche effettuate ai sensi dell'EC5 sono dettagliatamente riportate come da tabella seguente:

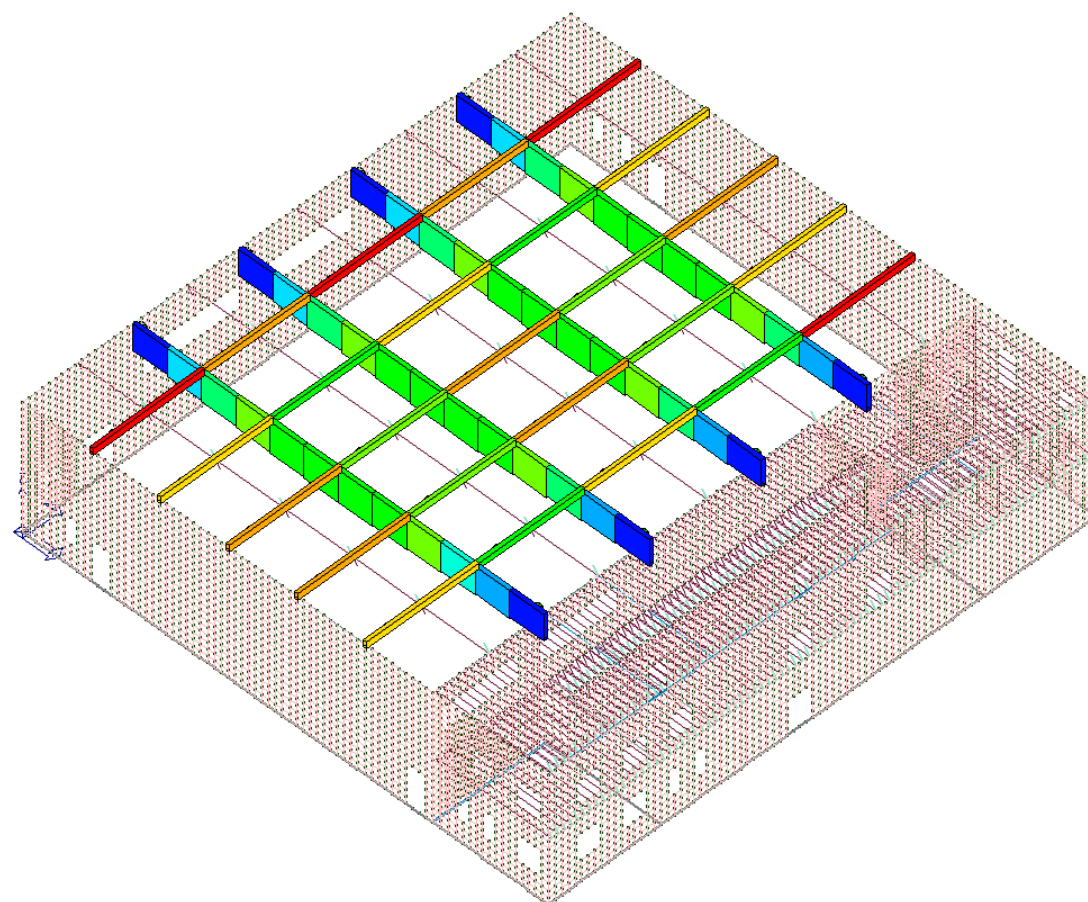
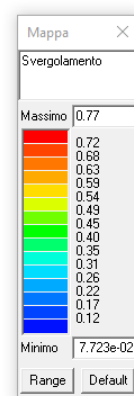
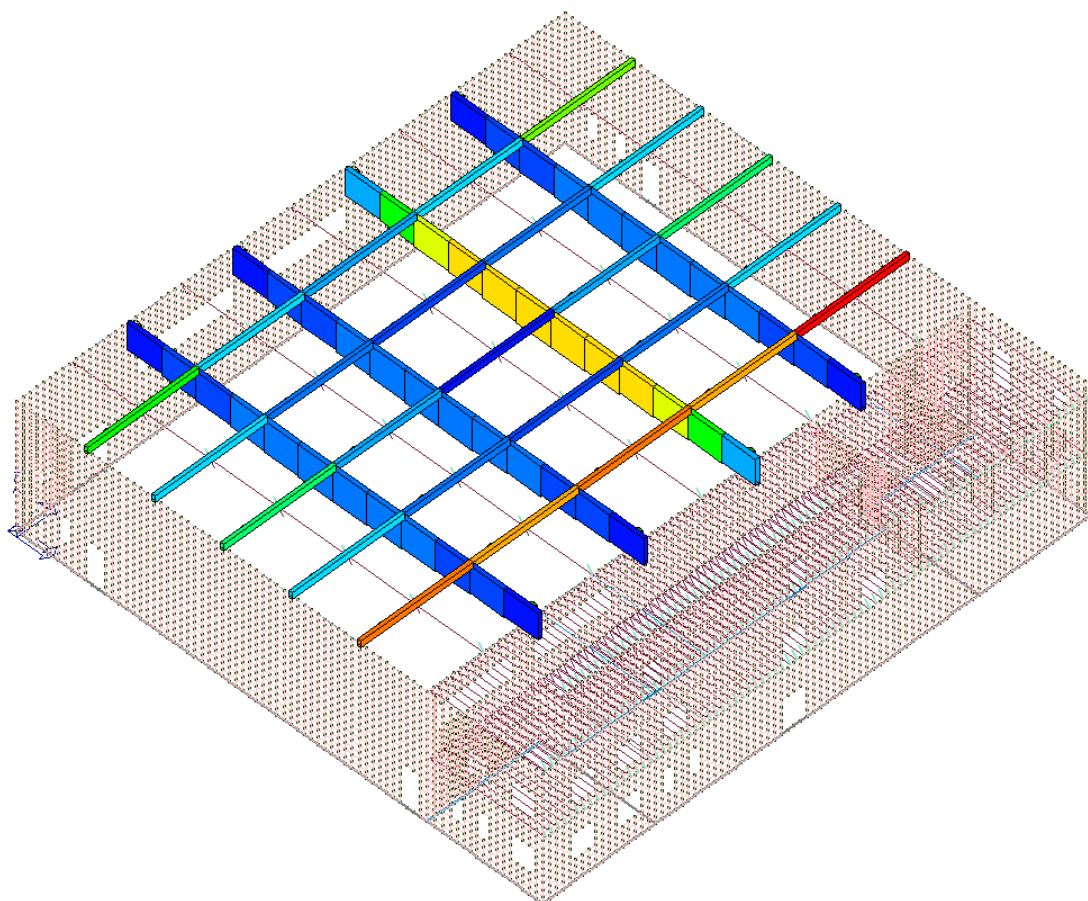
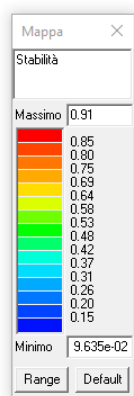
Elem.	Numero dell'elemento
Tipo	Codice di individuazione del tipo di elemento: Trave (T) , Pilastro (P) , Asta (A)
Stato	Codice della verifica ok verificato, NV non verificato
Note	Numero della sezione (s) e del materiale (m) dell'archivio
Ver N+/M	Verifica come da formula 6.17 e 6.18 per tensoflessione
Ver N-/M	Verifica come da formula 6.19 e 6.20 per pressoflessione
Ver V/T	Verifica come da formula 6.13 e 6.14 (taglio torsione) con interazione ottenuta per quadratura del termine di taglio
Ver N(s)	Verifica come da formula 6.23 e 6.24 per pressoflessione di elementi con snellezza relativa in un piano maggiore di 0.3
Kcy (z)	Fattore di instabilità utilizzato nella formula 6.23 (6.24)
Ver M(s)	Verifica come da formula 6.35 (effettuata in entrambi i piani principali) per instabilità laterale
Kcrit (y) (z)	Fattore di instabilità laterale utilizzato nella formula 6.35 rispettivamente per la flessione y e z
w _{net R}	Massima deformazione in combinazione rara (F frequente, P quasi permanente)
w _{net Ri}	Massima deformazione in combinazione rara (F frequente, P quasi permanente) valutata a tempo infinito
kdef	Fattore di deformazione dell' elemento
Rif. cmb	Numero della combinazione in cui si è attinto il valore riportato per le verifiche

Elem.	Note	Pos.	Ver N+/M	Ver N-/M	Ver V/T	Rif. cmb	Ver N(s)	Kcy	Kcz	Ver M(s)	Kcrit(y)	Kcrit(z)	Rif. cmb
412 ok	T,s=8,m=58	0.0	0.6	0.2	1.49e-02	11,36,41	0.2	0.9	0.8	0.4	1.0	1.0	36,9
		207.5	0.6	0.2	1.53e-02	11,36,41	0.2	0.9	0.8	0.4	1.0	1.0	36,9
413 ok	T,s=3,m=58	0.0	1.44e-02	1.14e-04	0.5	30,27,9	1.37e-02	0.9	0.8	1.37e-02	1.0	1.0	27,27

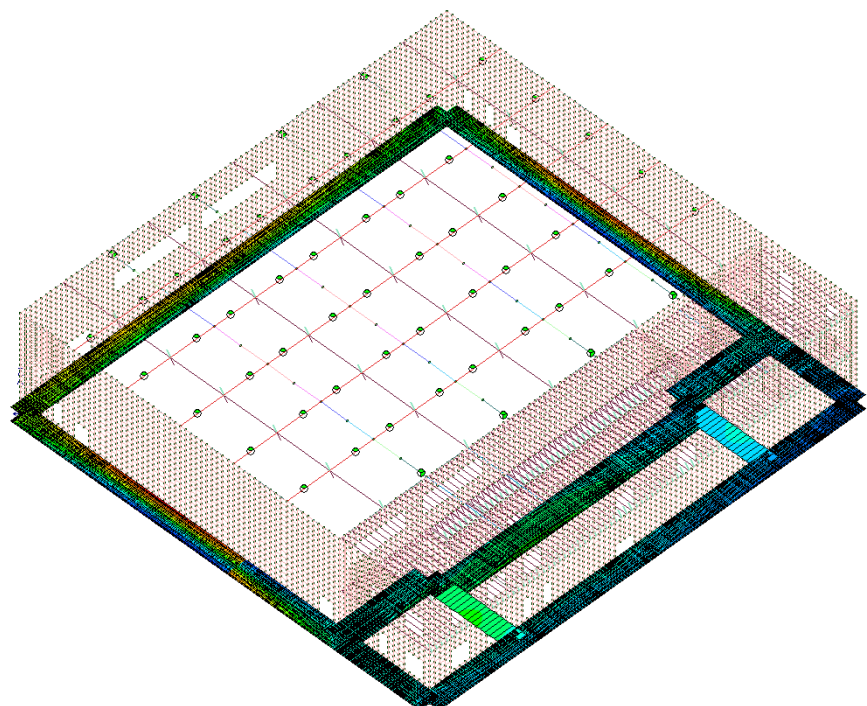
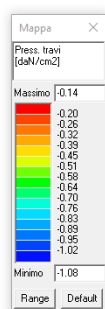
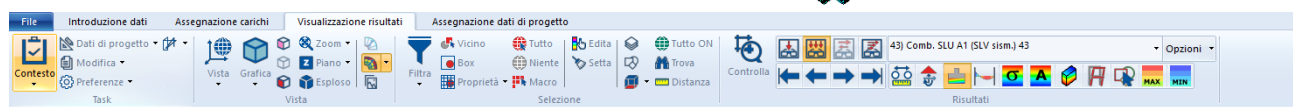
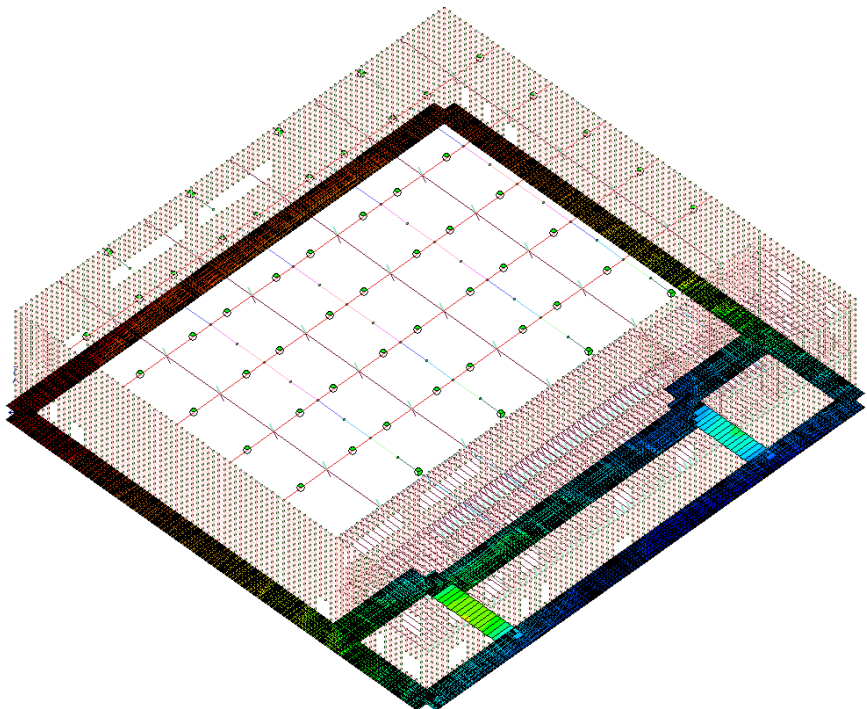
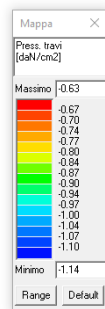
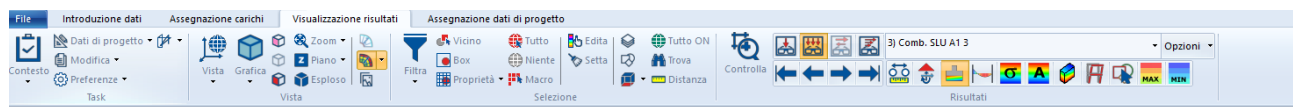
414	5.5	3.0	2.3	83,88,91	0.6	8.8	6.3	3.7	83,88,91
415	6.1	3.3	2.6	83,88,91	0.6	9.7	7.0	4.2	83,88,91
416	5.6	3.1	2.4	85,90,92	0.6	9.0	6.4	3.9	85,90,92
417	1.8	1.0	0.8	83,88,91	0.6	2.9	2.0	1.2	83,88,91
418	3.2	1.7	1.3	83,88,91	0.6	5.1	3.6	2.2	83,88,91
419	4.3	2.3	1.8	83,88,91	0.6	6.9	4.9	3.0	83,88,91
420	4.4	2.4	1.9	85,90,92	0.6	7.0	5.0	3.0	85,90,92
421	3.2	1.8	1.4	85,90,92	0.6	5.2	3.7	2.2	85,90,92
422	1.8	1.0	0.8	85,90,92	0.6	2.9	2.1	1.3	85,90,92
423	0.7	0.4	0.3	85,90,92	0.6	1.1	0.8	0.5	85,90,92
424	0.6	0.3	0.3	83,88,91	0.6	1.0	0.7	0.4	83,88,91
425	5.5	3.0	2.4	83,88,91	0.6	8.9	6.3	3.8	83,88,91
426	6.2	3.3	2.6	83,88,91	0.6	9.8	7.0	4.2	83,88,91
427	6.2	3.4	2.7	85,90,92	0.6	10.0	7.2	4.3	85,90,92
428	5.6	3.1	2.4	85,90,92	0.6	9.0	6.5	3.9	85,90,92
429	1.8	0.9	0.7	83,88,91	0.6	2.8	2.0	1.2	83,88,91
430	3.2	1.7	1.3	83,88,91	0.6	5.1	3.6	2.1	83,88,91
431	4.3	2.3	1.8	83,88,91	0.6	6.9	4.9	2.9	83,88,91
432	4.4	2.4	1.9	85,90,92	0.6	7.0	5.0	3.1	85,90,92
433	3.2	1.8	1.4	85,90,92	0.6	5.2	3.7	2.3	85,90,92
434	1.8	1.0	0.8	85,90,92	0.6	2.9	2.1	1.3	85,90,92
435	0.7	0.4	0.3	85,90,92	0.6	1.1	0.8	0.5	85,90,92
436	0.6	0.3	0.2	83,88,91	0.6	1.0	0.7	0.4	83,88,91
437	5.5	2.9	2.3	83,88,91	0.6	8.8	6.2	3.7	83,88,91
438	6.1	3.3	2.6	83,88,91	0.6	9.7	6.9	4.1	83,88,91
439	6.3	3.4	2.7	85,90,92	0.6	10.0	7.2	4.4	85,90,92
440	5.6	3.1	2.4	85,90,92	0.6	9.0	6.5	3.9	85,90,92
441	1.7	0.9	0.7	83,88,91	0.6	2.8	2.0	1.2	83,88,91
442	3.1	1.7	1.3	83,88,91	0.6	5.0	3.6	2.1	83,88,91
443	4.3	2.3	1.8	83,88,91	0.6	6.8	4.9	2.9	83,88,91
444	4.4	2.4	1.9	85,90,92	0.6	7.0	5.1	3.1	85,90,92
445	3.3	1.8	1.4	85,90,92	0.6	5.2	3.7	2.3	85,90,92
446	1.9	1.0	0.8	85,90,92	0.6	3.0	2.2	1.3	85,90,92
447	0.7	0.4	0.3	85,90,92	0.6	1.1	0.8	0.5	85,90,92
448	0.6	0.3	0.2	83,88,91	0.6	1.0	0.7	0.4	83,88,91
449	5.5	2.9	2.3	83,88,91	0.6	8.7	6.2	3.7	83,88,91
450	6.1	3.3	2.6	83,88,91	0.6	9.7	6.9	4.1	83,88,91
451	6.2	3.4	2.7	85,90,92	0.6	9.9	7.1	4.3	85,90,92
452	5.6	3.0	2.4	85,90,92	0.6	8.9	6.4	3.9	85,90,92
453	1.8	1.0	0.8	83,88,91	0.6	2.9	2.0	1.2	83,88,91
454	3.2	1.7	1.3	83,88,91	0.6	5.1	3.6	2.2	83,88,91
455	4.3	2.3	1.8	83,88,91	0.6	6.9	4.9	2.9	83,88,91
456	4.3	2.4	1.9	85,90,92	0.6	7.0	5.0	3.0	85,90,92
457	3.2	1.8	1.4	85,90,92	0.6	5.1	3.7	2.2	85,90,92
458	1.8	1.0	0.8	85,90,92	0.6	2.9	2.1	1.3	85,90,92
459	0.7	0.4	0.3	85,90,92	0.6	1.1	0.8	0.5	85,90,92
460	2.0	0.9	0.7	83,88,91	0.6	3.3	2.2	1.1	83,88,91
461	2.4	1.1	0.8	83,88,91	0.6	3.9	2.6	1.3	83,88,91
462	2.0	0.9	0.7	83,88,91	0.6	3.3	2.2	1.1	83,88,91
463	6.7	3.6	2.9	85,90,92	0.6	10.7	7.6	4.6	85,90,92
464	6.7	3.6	2.9	85,90,92	0.6	10.7	7.7	4.6	85,90,92
465	2.0	0.9	0.6	83,88,91	0.6	3.1	2.1	1.0	83,88,91
466	2.3	1.1	0.8	83,88,91	0.6	3.7	2.5	1.2	83,88,91
467	2.0	0.9	0.6	83,88,91	0.6	3.1	2.1	1.0	83,88,91
468	5.9	3.2	2.6	85,90,92	0.6	9.5	6.8	4.1	85,90,92
469	5.9	3.2	2.6	85,90,92	0.6	9.5	6.8	4.1	85,90,92
470	2.3	1.0	0.7	83,88,91	0.6	3.6	2.4	1.2	83,88,91
471	2.7	1.2	0.9	83,88,91	0.6	4.3	2.9	1.4	83,88,91
472	2.3	1.0	0.7	83,88,91	0.6	3.6	2.4	1.2	83,88,91
473	3.6	2.0	1.6	85,90,92	0.6	5.8	4.1	2.5	85,90,92
474	3.6	2.0	1.6	85,90,92	0.6	5.8	4.1	2.5	85,90,92
475	2.0	0.9	0.7	83,88,91	0.6	3.3	2.2	1.1	83,88,91
476	2.4	1.1	0.8	83,88,91	0.6	3.9	2.6	1.3	83,88,91
477	2.0	0.9	0.7	83,88,91	0.6	3.3	2.2	1.1	83,88,91
478	5.9	3.2	2.6	85,90,92	0.6	9.5	6.8	4.1	85,90,92
479	5.9	3.2	2.6	85,90,92	0.6	9.5	6.8	4.1	85,90,92
480	1.9	0.9	0.6	83,88,91	0.6	3.1	2.1	1.0	83,88,91
481	2.3	1.1	0.8	83,88,91	0.6	3.7	2.5	1.2	83,88,91
482	1.9	0.9	0.6	83,88,91	0.6	3.1	2.1	1.0	83,88,91
483	3.6	2.0	1.6	85,90,92	0.6	5.8	4.2	2.5	85,90,92
484	3.6	2.0	1.6	85,90,92	0.6	5.8	4.2	2.5	85,90,92
Elem.	w,net R 6.69	w,net F 3.64	w,net P 2.88			w,net Ri 10.70	w,net Fi 7.66	w,net Pi 4.61	







RELAZIONE SULLE FONDAZIONI



La tensione massima sul terreno, 0.114 Mpa è comunque inferiore a quella di riferimento 0.25 MPa

8 VALIDAZIONE DEI RISULTATI

Il programma di calcolo utilizzato PRO-SAP (*licenza dsi 2278*) è idoneo a riprodurre nel modello matematico il comportamento della struttura e gli elementi finiti disponibili e utilizzati sono rappresentativi della realtà costruttiva. Le funzioni di controllo disponibili, innanzitutto quelle grafiche, che consentono di verificare la riproduzione della realtà costruttiva ed accertare la corrispondenza del modello con la geometria strutturale e con le condizioni di carico ipotizzate. Si evidenzia che il modello viene generato direttamente dal disegno architettonico riproducendone così fedelmente le proporzioni geometriche. In ogni caso sono stati effettuati alcuni controlli dimensionali con gli strumenti software a disposizione dell'utente. Tutte le proprietà di rilevanza strutturale (materiali, sezioni, carichi, sconnessioni, etc.) sono state controllate attraverso le funzioni di indagine specificatamente previste.

Sono state sfruttate le funzioni di autodiagnostica presenti nel software che hanno accertato che non sussistono difetti formali di impostazione.

E' stato accertato che le risultanti delle azioni verticali sono in equilibrio con i carichi applicati.

Sono state controllate le azioni taglianti di piano ed accertata la loro congruenza con quella ricavabile da semplici ed agevoli elaborazioni. Le sollecitazioni prodotte da alcune combinazioni di carico di prova hanno prodotto valori prossimi a quelli ricavabili adottando consolidate formulazioni ricavate dalla Scienza delle Costruzioni. Anche le deformazioni risultano prossime ai valori attesi. Il dimensionamento e le verifiche di sicurezza hanno determinato risultati che sono in linea con casi di comprovata validità, confortati anche dalla propria esperienza.